



APPENDIX A

Site Selection Criteria



**APPENDIX A
SITE SELECTION CRITERIA**

**USACE Baltimore District and Maryland Department of the Environment
July 2019**

Mitigation Site Name **Eccleston Mitigation Project**

**Principal
Criteria (check
all that apply)**

- Site activities will result in at least 80% of wetland credits obtained through wetland restoration/establishment/re-establishment.**
- Site activities will result in at least 50% of stream credits obtained through stream restoration/enhancement/re-establishment/rehabilitation.**
- Site is contiguous or connected to other aquatic resources.**
- Site contains minimal or no invasive/undesirable/nuisance species.**
Due to site impairments, invasive species have established dominance. These species are to be controlled through site activities and mitigation of the impairments.
- Site has not been logged in the past 5 years.**
- Site abuts and/or adjoins an existing preservation/conservation area, etc.**
- Site has no known encumbrances (ie easements, liens, rights of way, reserved timber, severed surface or subsurface mineral or natural gas rights, etc.) on the site, on adjacent properties or within the watershed of the site that will negatively affect the compensation goals.**
- Immediately adjacent land is less than 10% impervious cover.**
- Site does not contain any impoundments that are not proposed for removal.**
- Site is able to be protected long-term through the recordation of an appropriate site protection instrument or other mechanism that will support the long-term protection of the site.**
- Site is expected to provide in-kind compensation (similar hydrologic regime).**



Watershed Scale Features (check all that apply)

****Explanation Required**

- Site activities will contribute to habitat diversity.****
The upper Jones Falls is considered a blue-ribbon trout stream by Maryland Department of Natural Resources. Improving this section of the Jones Falls will further improve trout habitat in the tributary and increase the habitat for prey species that trout feed upon.
- Site activities will contribute to habitat connectivity.****
A significant flow diversion and dam occurs in the property, which causes drastic changes to the habitat and segregates the upper Jones Falls from the lower for small fish and younger trout. Removing these flow and obstruction barriers restores connectivity between the upper and lower Jones Falls and tributaries.
- Site activities will remove pollutants from downstream waters.****
The site is in one of the most impaired tributaries in the state, as the Jones Falls watershed is impacted by multiple Total Maximum Daily Loads (TMDLs). Improving this tributary will have downstream benefits for the residents of Baltimore County and Baltimore City.
- Site activities will remediate inputs of substantial amounts of sediments to downstream waters.****
Channelization has disrupted the natural sediment transport processes. Ongoing loss of sediment from erosion causes various impairments within the project reach and downstream. Restoration activities will address these impacts.
- Site is in the same HUC-8 as the impact.**
- Site is in an adjoining HUC-8 as the impact.**
- Site is in the same physiographic province as the impact.**

Development Trends in the Watershed Where Site is Located (check all that apply)

****Explanation Required**

- Site will address watershed needs for habitat protection as identified in the state wildlife action plan, compensation planning framework, Habitat Conservation Plan, etc.****
The Eccleston property represents a threshold in the quality and function of the Jones Falls. The upper reaches of the project are reference areas which hold natural trout reproduction areas worthy of protection under easement. Downstream of the project location, the character of the Jones Falls changes considerably and more closely resembles a warm water fishery in the mainstem, though some high-quality tributaries are assumed to be present as well (they are potentially not studied well downstream).
- Site will address watershed needs for flood management as identified in the state wildlife action plan, compensation planning framework, Habitat Conservation Plan, etc. ****
- Site will address watershed needs for water quality improvement as identified through the 303(d) list.****



The restoration of the Jones Falls through this project will reduce sediment and nutrient sources, in support of TMDL goals for the watershed and in support of 303(d) watershed goals. This, however, is not the primary goal of the project, but rather an incidentally achieved goal.

- Site will address watershed needs for reduction of sediment loads as identified through the 303(d) list.****

The restoration of the Jones Falls through this project will reduce sediment and nutrient sources, in support of TMDL goals for the watershed and in support of 303(d) watershed goals. This, however, is not the primary goal of the project, but rather an incidentally achieved goal.

- Less than 50% of land use within the watershed is residential/commercial/industrial.**
- Less than 50% of land use within the watershed is agricultural.**
- Future land use plans (i.e. local comprehensive plans, conservation plans) show minimal or no change.**
- No water withdrawal permits issued within the vicinity of the site.**
- No point source permits within the vicinity of the site.**

Watershed vs. Site Specific Water Quality Goals (check all that apply)

- Site is likely to contribute to improved water quality within the watershed and not solely within the site boundaries.****

The site is in one of the most impaired tributaries in the state, as the Jones Falls watershed is impacted by multiple Total Maximum Daily Loads (TMDLs). Improving this tributary will have downstream benefits for the residents of Baltimore County and Baltimore City.

****Explanation Required**

- Site will include preservation/establishment/rehabilitation of the entire watershed upstream of the project to the drainage divide.**
- No downstream impoundments (excluding drinking water) that would limit the watershed benefits derived from site activities.**



Positive Effects Site will have on Ecological/Cultural Resources (check all that apply)

****Explanation Required**

- Site activities will conserve/restore habitat for species identified as rare by MD DNR.****
MD DNR, both internally and through comments on the project, have identified trout as a special species of concern here. In conjunction with local NGO groups and the MD DNR, restoration is proposed to restore habitats with the long-term goal of preserving the system as a trout stream into the future, correcting the principle impairments to the site and working against watershed impairments.
- Site activities will conserve/restore natural communities identified by MDDNR as imperiled.****
- Site activities are within areas that have been identified by MD DNR as meriting improvement.****
MD DNR, both internally and through comments on the project, have identified trout as a special species of concern here. In conjunction with local NGO groups and the MD DNR, restoration is proposed to restore habitats with the long-term goal of preserving the system as a trout stream into the future, correcting the principle impairments to the site and working against watershed impairments.
- Site activities will conserve/restore areas designated by MD DNR as wild trout streams.****
The upper Jones Falls is considered a blue-ribbon trout stream by Maryland Department of Natural Resources. Improving this section of the Jones Falls will further improve trout habitat in the tributary and increase the habitat for prey species that trout feed upon.
- Site activities will conserve/restore areas designated by MD DNR as anadromous fish use areas.****
- Site activities will protect state or federal threatened and/or endangered species.****
- Site contains historical cultural resources that will be preserved.****
- Site activities will establish new or expand existing wildlife corridors.****
A significant flow diversion and dam occurs in the property, which limits use of areas of the existing corridor for aquatic wildlife. Removing these flow and obstruction barriers expands the existing wildlife corridor by restoring connectivity between the upper and lower Jones Falls and tributaries.
- Site activities will result in removal of barriers to fish passage.****
A significant flow diversion and dam occurs in the property, which causes drastic changes to the habitat and segregates the upper Jones Falls from the lower for small fish and younger trout. Removing these flow and obstruction barriers restores connectivity between the upper and lower Jones Falls and tributaries.



**Hydrologic Sources/
Ecological Features
(check all that apply)**

- Site activities do not consist of wetland creation in the uplands.**
- Site activities do not consist of stream creation.**
Length to be added.
- Site activities do not entail impounding or diverting water from other areas to the project site.**
- Site activities do not entail excavation to reach groundwater.**
Excavation will be included due to buried hydric soil.

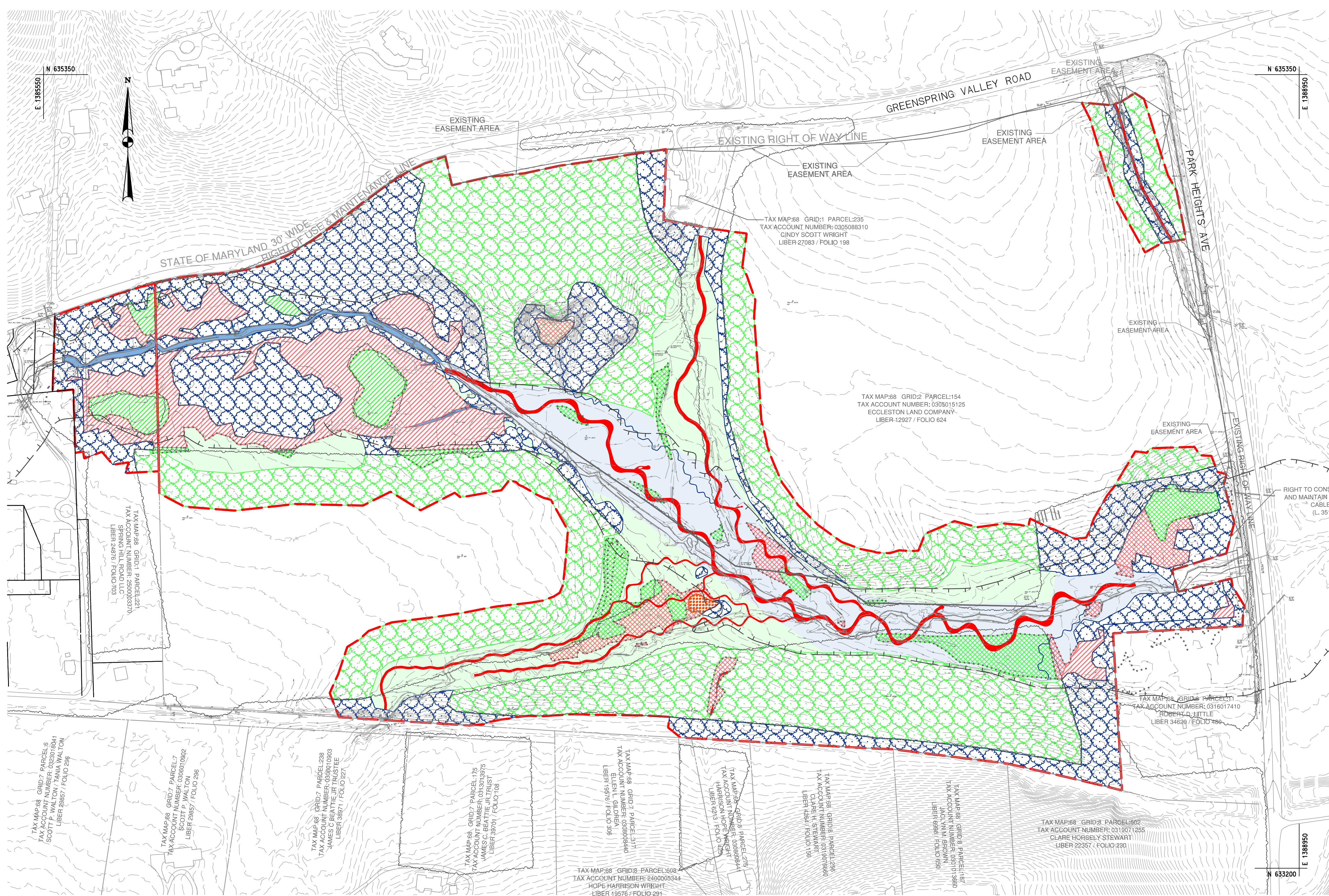
**Physical/
Chemical Characteristics
(check all that apply)**

****Explanation Required**

- Sites receiving waters are 303(d) listed.**
Yes
- Site qualifies for preservation only, as 1) the resources provide important physical, chemical, or biological functions to the watershed; 2) the resources contribute significantly to the ecological sustainability of the watershed; 3) the IRT has determined that preservation is appropriate and practicable; 4) the resources are under threat of destruction or adverse modification; and 5) the site will be permanently protected through an appropriate real estate instrument.****
- Site activities will not result in the construction of artificial or unnatural wetlands that will have limited opportunity to provide the desired functions.**
- Past land use was PC crop or ditched wetlands.**
- Past land use was agriculture/silviculture.****
The proposed site is in a large farm field; thus, the restoration, enhancement and preservation will improve environmental resources and define clear monitored boundaries for farming practices.
- Past land use was commercial or industrial.****
- No impoundments exist upstream of the site that will cause thermal increases in water temperature, decreases in dissolved oxygen, erosion and degradation of the channel downstream from the impoundment, or dam failure from a storm event.****
- Site activities will result in all onsite impoundments being removed and streams re-established/rehabilitated.**



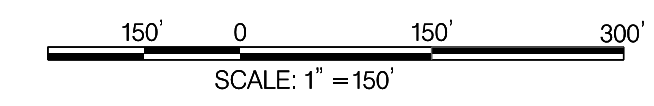
APPENDIX B Mitigation Credit Map



| LEGEND | |
|--------|---|
| | PROPOSED EASEMENT |
| | FORESTED BUFFER PRESERVATION 15.59 ac. |
| | BUFFER ENHANCEMENT 22.82 ac. |
| | WETLAND REMOVAL AREA 0.06 ac. |
| | PERENNIAL STREAM RESTORATION 8.46194 LF |
| | PERENNIAL STREAM PRESERVATION 1.46895 LF |
| | PFO RESTORATION 7.29 ac. |
| | PFO ENHANCEMENT 1.45 ac. |
| | PFO PRESERVATION 4.50 ac. |
| | PEM RESTORATION 6.96 ac. |
| | PEM ENHANCEMENT 1.87 ac. |
| | PEM PRESERVATION 1.21 ac. |

RIGHT TO CONSTRUCT, OPERATE AND MAINTAIN YORK-BALTIMORE CABLE SYSTEM (L. 3511/F. 509)

| |
|---|
| OWNER / DEVELOPER INFORMATION |
| JOHNSON MIRMIRAN AND THOMPSON 40 WIGHT AVE. COCKEYSVILLE, MD 21030 |
| CONTACT |
| JEREMY KOSER 40 WIGHT AVE. HUNT VALLEY, MD 21030 TEL: 410-329-3100 |



MARYLAND COORDINATE SYSTEM - HOR. NAD 83/91 MD STATE PLANE VERT. NAVD 88

GREENSPRING VALLEY ROAD
SW CORNER PARK HEIGHTS AVE
OWINGS MILLS, MD 21117

BALTIMORE COUNTY ELECTION DISTRICT: 3 COUNCILMANIC DISTRICT 2

MITIGATION CREDIT MAP

| | | |
|----------------------------|-------------------------|--------------------------|
| SCALE AS SHOWN | DATE JULY 2019 | PROJECT NO. 17-10977-001 |
| DESIGNED BY JM | COUNTY BALTIMORE COUNTY | |
| DRAWN BY KNH | LOGMILE | |
| CHECKED BY JJ CD G | HORIZONTAL SCALE N/A | |
| F.A.P. NO. SEE TITLE SHEET | VERTICAL SCALE N/A | |
| DRAWING NO. | OF | SHEET NO. xx OF xx |

REVISIONS

CONCEPT SUBMISSION

NOT FOR CONSTRUCTION

ECCLESTON MITIGATION SITE

DESIGN PROFESSIONAL

JEREMY KOSER

JOHNSON MIRMIRAN & THOMPSON INC.
40 WIGHT AVENUE, HUNT VALLEY, MD 21030

TEL: 410-329-3100
EMAIL: JKoser@jmt.com

PROFESSIONAL CERTIFICATION

I HEREBY CERTIFY THAT THESE DOCUMENTS WERE PREPARED OR APPROVED BY ME AND THAT I AM A DULY LICENSED PROFESSIONAL ENGINEER UNDER THE LAWS OF THE STATE OF MARYLAND, LICENSE NO. 31183, EXPIRATION DATE: 1/13/2021.



BY: K. Higgins

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APPENDIX C

Hydrologic Analysis Data

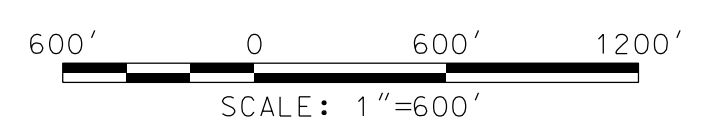


| DRAINAGE AREA SUMMARY TABLE | | | |
|-----------------------------|----------------|--------|-----|
| POI | D.A. (SQ. MI.) | TcPATH | RCN |
| 1 | 2.783 | 1.505 | 71 |
| 2 | 1.323 | 1.377 | 72 |
| 3 | 0.920 | 1.241 | 67 |
| 4 | 0.450 | 1.130 | 75 |
| 5 | 0.139 | 0.609 | 73 |

| DISCHARGE SUMMARY TABLE | | | |
|-------------------------|----------------|-----------------|------------------|
| POI | Q ₂ | Q ₁₀ | Q ₁₀₀ |
| 1 | 593.4 | 1438.7 | 3050.4 |
| 2 | 317.9 | 736.5 | 1526.6 |
| 3 | 161.4 | 439.0 | 998.8 |
| 4 | 151.7 | 322.2 | 622.1 |
| 5 | 62.2 | 133.9 | 256.2 |

LEGEND

- 360 — EXISTING CONTOUR
- SOIL BOUNDARY
- ⊙ SOIL TYPE
- * POINT OF INVESTIGATION (POI)
- TcPATH (TIME OF CONCENTRATION)
- DRAINAGE AREA BOUNDARY
- · — · — LAND USE BOUNDARY
- RES 1/4 AC RESIDENTIAL 1/4 ACRE
- RES 1/8 AC RESIDENTIAL 1/8 ACRE
- RES 1 AC RESIDENTIAL 1 ACRE
- RES 2 AC RESIDENTIAL 2 ACRE
- AGRI AGRICULTURAL
- COMM COMMERCIAL
- CROP CROP
- OS OPEN SPACE
- WD WOODS



**ECCLESTON MITIGATION SITE
DRAINAGE AREA MAP
EXISTING CONDITIONS**

| REVISIONS | SCALE AS SHOWN | DATE | CONTRACT NO. |
|----------------------------|----------------------|------------------|--------------|
| DESIGNED BY MRG | APRIL, 2018 | BALTIMORE COUNTY | |
| DRAWN BY MRG | LOGMILE | | |
| CHECKED BY FAB | HORIZONTAL SCALE N/A | | |
| F.A.P. NO. SEE TITLE SHEET | VERTICAL SCALE N/A | | |
| DRAWING NO. OF | SHEET NO. OF XX | | |

BY: Cwagner



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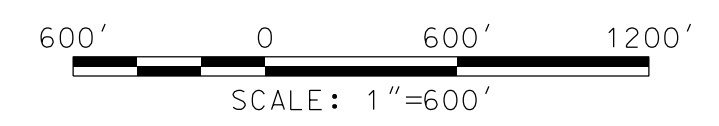


| DRAINAGE AREA SUMMARY TABLE | | | |
|-----------------------------|----------------|--------|-----|
| POI | D.A. (SQ. MI.) | TcPATH | RCN |
| 1 | 2.783 | 1.505 | 72 |
| 2 | 1.323 | 1.377 | 74 |
| 3 | 0.920 | 1.241 | 68 |
| 4 | 0.450 | 1.130 | 75 |
| 5 | 0.139 | .609 | 74 |

| DISCHARGE SUMMARY TABLE | | | |
|-------------------------|----------------|-----------------|------------------|
| POI | Q ₂ | Q ₁₀ | Q ₁₀₀ |
| 1 | 655.4 | 1520.5 | 3144.3 |
| 2 | 363.3 | 798.4 | 1593.4 |
| 3 | 175.5 | 459.7 | 1025.9 |
| 4 | 151.7 | 146.8 | 622.1 |
| 5 | 66.3 | 138.9 | 261.2 |

LEGEND

- 380 --- EXISTING CONTOUR
- SOIL BOUNDARY
- ⊙ SOIL TYPE
- * POINT OF INVESTIGATION (POI)
- TcPATH (TIME OF CONCENTRATION)
- DRAINAGE AREA BOUNDARY
- LAND USE BOUNDARY
- RES 1/4 AC RESIDENTIAL 1/4 ACRE
- RES 1/8 AC RESIDENTIAL 1/8 ACRE
- RES 1 AC RESIDENTIAL 1 ACRE
- RES 2 AC RESIDENTIAL 2 ACRE
- AGRI AGRICULTURAL
- COMM COMMERCIAL
- WATERSHED WATERSHED



ECCLESTON MITIGATION BANK
DRAINAGE AREA MAP
ULTIMATE CONDITIONS

| | | | |
|----------------------|----------------------------|-------------------------|--------------|
| REVISIONS | SCALE AS SHOWN | DATE APRIL, 2018 | CONTRACT NO. |
| CONCEPT SUBMISSION | DESIGNED BY MRG | COUNTY BALTIMORE COUNTY | |
| NOT FOR CONSTRUCTION | DRAWN BY MRG | LOGMILE | |
| | CHECKED BY FAB | HORIZONTAL SCALE N/A | |
| | F.A.P. NO. SEE TITLE SHEET | VERTICAL SCALE N/A | |
| DRAWING NO. | OF | SHEET NO. | OF XX |



BY: RBucci-

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GISHydro Release Version Date: January 8, 2011
 Hydro Extension Version Date: January 8, 2011
 Analysis Date: June 5, 2018

Landuse and Soil Distributions for: Eccelston

Distribution of Landuse by Soil Group

| Land Use | Acres on Indicated Soil Group | | | |
|----------------------------|-------------------------------|---------|--------|--------|
| | A-Soil | B-Soil | C-Soil | D-Soil |
| Low Density Residential | 0 | 668.07 | 20.02 | 21.35 |
| Medium Density Residential | 0 | 54.93 | 5.34 | 0 |
| High Density Residential | 0 | 130.1 | 6.67 | 0 |
| Commercial | 0 | 30.25 | 8.01 | 0 |
| Institutional | 0 | 24.02 | 0 | 0 |
| Open Urban Land | 0 | 102.75 | 4.89 | 0 |
| Cropland | 0 | 107.64 | 26.46 | 0 |
| Pasture | 0 | 5.78 | 2.67 | 0 |
| Deciduous Forest | 0 | 183.03 | 7.56 | 4.67 |
| Large Lot Agricultural | 0 | 110.97 | 11.12 | 4 |
| Large Lot Forest | 0 | 177.69 | 9.79 | 7.34 |
| Total Area: | 0 | 1595.23 | 102.52 | 37.36 |

Distribution of Land Use and Curve Numbers Used

| Land Use | Acres | Percent | Curve Numbers | | | |
|----------------------------|--------|---------|---------------|----|----|----|
| | | | A | B | C | D |
| Low Density Residential | 709.44 | 40.89 | 54 | 70 | 80 | 85 |
| Medium Density Residential | 60.27 | 3.47 | 61 | 75 | 83 | 87 |
| High Density Residential | 136.77 | 7.88 | 77 | 85 | 90 | 92 |
| Commercial | 38.25 | 2.2 | 89 | 92 | 94 | 95 |
| Institutional | 24.02 | 1.38 | 69 | 80 | 86 | 89 |
| Open Urban Land | 107.64 | 6.2 | 39 | 61 | 74 | 80 |
| Cropland | 134.1 | 7.73 | 67 | 78 | 85 | 89 |
| Pasture | 8.45 | 0.49 | 39 | 61 | 74 | 80 |
| Deciduous Forest | 195.26 | 11.25 | 30 | 55 | 70 | 77 |
| Large Lot Agricultural | 126.1 | 7.27 | 67 | 78 | 85 | 89 |
| Large Lot Forest | 194.82 | 11.23 | 30 | 55 | 70 | 77 |

Watershed Statistics for: Eccelston
GISHydro Release Version Date: January 8, 2011
Hydro Extension Version Date: January 8, 2011
Analysis Date: June 5, 2018

Data Selected:

Quadrangles Used: cockeysville, reisterstown, hampstead, hereford
DEM Coverage: NED DEMs
Land Use Coverage: 2010 MOP Landuse
Soil Coverage: Ragan Soils
Hydrologic Condition: (see Lookup Table)
Impose NHD stream Locations: Yes
Outlet Easting: 423369 m. (MD Stateplane, NAD 1983)
Outlet Northing: 193262 m. (MD Stateplane, NAD 1983)

Findings:

Outlet Location: Piedmont
Outlet State: Maryland
Drainage Area: 2.7 square miles
-Piedmont (100.0% of area)
Channel Slope: 77.1 feet/mile
Land Slope: 0.072 ft/ft
Urban Area: 54.4%
Impervious Area: 22.7%

URBAN DEVELOPMENT IN WATERSHED EXCEEDS 15%.
Calculated discharges from USGS Regression
Equations may not be appropriate.

Time of Concentration: 2.1 hours [W.O. Thomas, Jr. Equation]
Time of Concentration: 2.2 hours [From SCS Lag Equation * 1.67]
Longest Flow Path: 2.68 miles
Basin Relief: 146.4 feet
Average CN: 70
% Forest Cover: 22.5
% Storage: 0.0
% Limestone: 0.0
Selected Soils Data Statistics:
% A Soils: 0.0
% B Soils: 91.9
% C Soils: 5.9
% D Soils: 2.2
SSURGO Soils Data Statistics (used in Regression Equations):
% A Soils: 0.8
% B Soils: 80.7
% C Soils: 9.7
% D Soils: 8.8
2-Year,24-hour Prec.: 3.27 inches
Mean Annual Prec.: 46.07 inches

U.S.G.S. Peak Flow Estimates for: Eccelston
 GISHydro Release Version Date: January 8, 2011
 Hydro Extension Version Date: January 8, 2011
 Analysis Date: June 5, 2018

Geographic Province(s):
 -Piedmont (100.0% of area)

Q(2): 335 cfs
 Q(5): 646 cfs
 Q(10): 937 cfs
 Q(25): 1400 cfs
 Q(50): 1810 cfs
 Q(100): 2300 cfs
 Q(500): 3790 cfs

Area Weighted Prediction Intervals (from Tasker)

| Return Period | 50 PERCENT | | 67 PERCENT | | 90 PERCENT | | 95 PERCENT | |
|---------------|------------|-------|------------|-------|------------|-------|------------|-------|
| | lower | upper | lower | upper | lower | upper | lower | upper |
| 2 | 258 | 434 | 229 | 491 | 178 | 631 | 155 | 722 |
| 5 | 509 | 819 | 455 | 917 | 361 | 1160 | 319 | 1310 |
| 10 | 740 | 1190 | 662 | 1330 | 526 | 1670 | 466 | 1890 |
| 25 | 1090 | 1790 | 971 | 2010 | 763 | 2560 | 671 | 2910 |
| 50 | 1390 | 2360 | 1230 | 2670 | 952 | 3450 | 831 | 3960 |
| 100 | 1730 | 3050 | 1520 | 3490 | 1150 | 4600 | 994 | 5320 |
| 500 | 2700 | 5320 | 2300 | 6250 | 1650 | 8700 | 1380 | 10400 |

Individual Province Tasker Analyses Follow:

Flood frequency estimates for
 Eccelston
 REGION: Piedmont region
 area= 2.70: forest = 22.50 :skew= 0.53

| Return Period | Discharge (cfs) | Standard Error of Prediction (percent) | Equivalent Years of Record | Standard Error of Prediction (logs) |
|---------------|-----------------|--|----------------------------|-------------------------------------|
| 2 | 335. | 39.6 | 3.27 | 0.1659 |
| 5 | 646. | 36.2 | 7.35 | 0.1523 |
| 10 | 937. | 35.9 | 11.33 | 0.1512 |
| 25 | 1400. | 37.7 | 15.85 | 0.1585 |
| 50 | 1810. | 40.3 | 18.19 | 0.1685 |
| 100 | 2300. | 43.6 | 19.66 | 0.1812 |
| 500 | 3790. | 53.4 | 20.69 | 0.2175 |

| Return Period | P R E D I C T I O N I N T E R V A L S | | | | | | | |
|---------------|---------------------------------------|-------|------------|-------|------------|-------|------------|--------|
| | 50 PERCENT | | 67 PERCENT | | 90 PERCENT | | 95 PERCENT | |
| | lower | upper | lower | upper | lower | upper | lower | upper |
| 2 | 258. | 434. | 229. | 491. | 178. | 631. | 155. | 722. |
| 5 | 509. | 819. | 455. | 917. | 361. | 1160. | 319. | 1310. |
| 10 | 740. | 1190. | 662. | 1330. | 526. | 1670. | 466. | 1890. |
| 25 | 1090. | 1790. | 971. | 2010. | 763. | 2560. | 671. | 2910. |
| 50 | 1390. | 2360. | 1230. | 2670. | 952. | 3450. | 831. | 3960. |
| 100 | 1730. | 3050. | 1520. | 3490. | 1150. | 4600. | 994. | 5320. |
| 500 | 2700. | 5320. | 2300. | 6250. | 1650. | 8700. | 1380. | 10400. |

POI 5 basincomposition.txt

GISHydro Release Version Date: January 8, 2011
 Hydro Extension Version Date: January 8, 2011
 Analysis Date: June 5, 2018

Landuse and Soil Distributions for: Eccelston POI 6

Distribution of Landuse by Soil Group

| Land Use | Acres on Indicated Soil Group | | | |
|-------------------------|-------------------------------|--------|--------|--------|
| | A-Soil | B-Soil | C-Soil | D-Soil |
| Low Density Residential | 0 | 40.48 | 0 | 0 |
| Institutional | 0 | 4.89 | 0 | 0 |
| Cropland | 0 | 8.45 | 0 | 0 |
| Deciduous Forest | 0 | 8.67 | 0.67 | 0 |
| Large Lot Agricultural | 0 | 25.58 | 0 | 0 |
| Large Lot Forest | 0 | 9.34 | 0 | 0 |
| Total Area: | 0 | 97.41 | 0.67 | 0 |

Distribution of Land Use and Curve Numbers Used

| Land Use | Acres | Percent | Curve Numbers | | | |
|-------------------------|-------|---------|---------------|----|----|----|
| | | | A | B | C | D |
| Low Density Residential | 40.48 | 41.27 | 54 | 70 | 80 | 85 |
| Institutional | 4.89 | 4.99 | 69 | 80 | 86 | 89 |
| Cropland | 8.45 | 8.62 | 67 | 78 | 85 | 89 |
| Deciduous Forest | 9.34 | 9.52 | 30 | 55 | 70 | 77 |
| Large Lot Agricultural | 25.58 | 26.08 | 67 | 78 | 85 | 89 |
| Large Lot Forest | 9.34 | 9.52 | 30 | 55 | 70 | 77 |

Watershed Statistics for: Eccelston POI 6
GISHydro Release Version Date: January 8, 2011
Hydro Extension Version Date: January 8, 2011
Analysis Date: June 5, 2018

Data Selected:

Quadrangles Used: cockeysville, reisterstown, hereford, hampstead
DEM Coverage: NED DEMs
Land Use Coverage: 2010 MOP Landuse
Soil Coverage: Ragan Soils
Hydrologic Condition: (see Lookup Table)
Impose NHD stream Locations: Yes
Outlet Easting: 423252 m. (MD Stateplane, NAD 1983)
Outlet Northing: 193531 m. (MD Stateplane, NAD 1983)

Findings:

Outlet Location: Piedmont
Outlet State: Maryland
Drainage Area: 0.2 square miles
-Piedmont (100.0% of area)
Channel Slope: 169.2 feet/mile
Land Slope: 0.065 ft/ft
Urban Area: 41.3%
Impervious Area: 18.2%

URBAN DEVELOPMENT IN WATERSHED EXCEEDS 15%.
Calculated discharges from USGS Regression
Equations may not be appropriate.

Time of Concentration: 1.2 hours [W.O. Thomas, Jr. Equation]
Time of Concentration: 1.0 hours [From SCS Lag Equation * 1.67]
Longest Flow Path: 0.98 miles
Basin Relief: 90.6 feet
Average CN: 71
% Forest Cover: 19.0
% Storage: 0.0
% Limestone: 0.0
Selected Soils Data Statistics:
% A Soils: 0.0
% B Soils: 99.3
% C Soils: 0.7
% D Soils: 0.0
SSURGO Soils Data Statistics (used in Regression Equations):
% A Soils: 0.0
% B Soils: 82.5
% C Soils: 17.5
% D Soils: 0.0
2-Year,24-hour Prec.: 3.28 inches
Mean Annual Prec.: 46.32 inches

POI 5 discharges.txt
 U.S.G.S. Peak Flow Estimates for: Eccelston POI 6
 GISHydro Release Version Date: January 8, 2011
 Hydro Extension Version Date: January 8, 2011
 Analysis Date: June 5, 2018

Geographic Province(s):
 -Piedmont (100.0% of area)

Q(2): 66 cfs
 Q(5): 137 cfs
 Q(10): 208 cfs
 Q(25): 323 cfs
 Q(50): 429 cfs
 Q(100): 555 cfs
 Q(500): 948 cfs

Area weighted Prediction Intervals (from Tasker)

| Return Period | 50 PERCENT | | 67 PERCENT | | 90 PERCENT | | 95 PERCENT | |
|---------------|------------|-------|------------|-------|------------|-------|------------|-------|
| | lower | upper | lower | upper | lower | upper | lower | upper |
| 2 | 50 | 87 | 44 | 99 | 34 | 129 | 29 | 149 |
| 5 | 106 | 178 | 94 | 201 | 73 | 258 | 64 | 294 |
| 10 | 161 | 269 | 142 | 304 | 111 | 391 | 97 | 447 |
| 25 | 246 | 424 | 216 | 483 | 166 | 630 | 144 | 725 |
| 50 | 321 | 574 | 279 | 659 | 210 | 874 | 181 | 1020 |
| 100 | 406 | 759 | 350 | 881 | 258 | 1190 | 219 | 1400 |
| 500 | 652 | 1380 | 545 | 1650 | 378 | 2380 | 312 | 2890 |

Individual Province Tasker Analyses Follow:

Flood frequency estimates for
 Eccelston POI 6
 REGION: Piedmont region
 area= 0.20: forest = 19.00 :skew= 0.53

| Return Period | Discharge (cfs) | Standard Error of Prediction (percent) | Equivalent Years of Record | Standard Error of Prediction (logs) |
|---------------|-----------------|--|----------------------------|-------------------------------------|
| 2 | 66. | 42.2 | 3.79 | 0.1758 |
| 5 | 137. | 39.3 | 8.19 | 0.1647 |
| 10 | 208. | 39.5 | 12.36 | 0.1653 |
| 25 | 323. | 41.9 | 17.00 | 0.1747 |
| 50 | 429. | 45.0 | 19.39 | 0.1863 |
| 100 | 555. | 48.8 | 20.90 | 0.2006 |
| 500 | 948. | 59.9 | 22.04 | 0.2405 |

| Return Period | P R E D I C T I O N I N T E R V A L S | | | | | | | |
|---------------|---------------------------------------|-------|------------|-------|------------|-------|------------|-------|
| | 50 PERCENT | | 67 PERCENT | | 90 PERCENT | | 95 PERCENT | |
| | lower | upper | lower | upper | lower | upper | lower | upper |
| 2 | 50. | 87. | 44. | 99. | 34. | 129. | 29. | 149. |
| 5 | 106. | 178. | 94. | 201. | 73. | 258. | 64. | 294. |
| 10 | 161. | 269. | 142. | 304. | 111. | 391. | 97. | 447. |
| 25 | 246. | 424. | 216. | 483. | 166. | 630. | 144. | 725. |
| 50 | 321. | 574. | 279. | 659. | 210. | 874. | 181. | 1020. |
| 100 | 406. | 759. | 350. | 881. | 258. | 1190. | 219. | 1400. |
| 500 | 652. | 1380. | 545. | 1650. | 378. | 2380. | 312. | 2890. |

WARNING -- Prediction beyond observed data
 WARNING - Drainage area out of range of observed data

| | | | |
|---------------------------------------|--------|-----------|------------------|
| WinTR-20: version 3.20 | 0 | 0 | 0 |
| Eccelston Mitigation POI 1-4 Existing | | | |
| SUB-AREA: | | | |
| DA1 | OUTLET | 0.0900312 | 75. .260 YY |
| DA4 | CON-1 | 0.4501281 | 75. 1.13 YY |
| DA2 | CON-1 | 1.3229781 | 72. 1.377 YY |
| DA3 | CON-1 | 0.9202734 | 67. 1.241 YY |
| STREAM REACH: | | | |
| CON-1 | OUTLET | XS1 | 1547.3143 YY Y |
| STORM ANALYSIS: | | | |
| 1_yr_sm | | 2.7 | 1_yr_sm 2 3.27 |
| 2_yr_sm | | 3.27 | 2_yr_sm 2 3.27 |
| 5_yr_sm | | 4.21 | 5_yr_sm 2 3.27 |
| 10_yr_sm | | 5.03 | 10_yr_sm 2 3.27 |
| 25_yr_sm | | 6.29 | 25_yr_sm 2 3.27 |
| 50_yr_sm | | 7.41 | 50_yr_sm 2 3.27 |
| 100_yr_sm | | 8.68 | 100_yr_sm 2 3.27 |
| 500_yr_sm | | 12.35 | 500_yr_sm 2 3.27 |
| STREAM CROSS SECTION: | | | |
| XS1 | 361.8 | | |
| | 360.16 | 0.00 | 0.00 2. .1 |
| | 360.57 | 1.92 | 1.80 2. |
| | 360.98 | 11.84 | 6.44 2. |
| | 361.39 | 31.78 | 12.95 2. |
| | 361.80 | 63.07 | 21.08 2. |
| | 362.57 | 246.03 | 172.72 2. |
| | 363.35 | 678.76 | 348.03 2. |
| | 364.12 | 1313.55 | 539.74 2. |
| | 364.89 | 2034.29 | 766.67 2. |
| | 365.67 | 3178.49 | 1025.20 2. |
| | 366.44 | 4545.31 | 1296.17 2. |
| | 367.21 | 6128.84 | 1579.56 2. |
| | 367.99 | 7541.79 | 1894.24 2. |
| | 368.76 | 9145.25 | 2251.86 2. |
| | 369.53 | 11751.18 | 2644.71 2. |
| | 370.31 | 14631.71 | 3047.25 2. |
| | 371.08 | 17781.04 | 3459.48 2. |
| | 371.85 | 21194.89 | 3881.38 2. |
| | 372.63 | 24870.16 | 4312.97 2. |
| | 373.40 | 28804.62 | 4754.24 2. |

Eccelston POI 1-4 Existing.out

RAINFALL DISTRIBUTION:

1_yr_sm

| 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
|--------|--------|--------|--------|--------|
| 0.0000 | 0.0011 | 0.0022 | 0.0033 | 0.0044 |
| 0.0055 | 0.0067 | 0.0078 | 0.0089 | 0.0100 |
| 0.0111 | 0.0122 | 0.0133 | 0.0144 | 0.0155 |
| 0.0166 | 0.0178 | 0.0189 | 0.0200 | 0.0211 |
| 0.0222 | 0.0233 | 0.0244 | 0.0255 | 0.0266 |
| 0.0277 | 0.0289 | 0.0300 | 0.0311 | 0.0322 |
| 0.0333 | 0.0344 | 0.0355 | 0.0366 | 0.0377 |
| 0.0388 | 0.0399 | 0.0411 | 0.0422 | 0.0433 |
| 0.0444 | 0.0455 | 0.0466 | 0.0477 | 0.0488 |
| 0.0499 | 0.0510 | 0.0522 | 0.0533 | 0.0544 |
| 0.0555 | 0.0566 | 0.0577 | 0.0588 | 0.0599 |
| 0.0610 | 0.0621 | 0.0633 | 0.0644 | 0.0655 |
| 0.0666 | 0.0693 | 0.0721 | 0.0748 | 0.0776 |
| 0.0803 | 0.0830 | 0.0858 | 0.0885 | 0.0913 |
| 0.0940 | 0.0967 | 0.0995 | 0.1022 | 0.1050 |
| 0.1077 | 0.1105 | 0.1132 | 0.1159 | 0.1187 |
| 0.1214 | 0.1242 | 0.1269 | 0.1297 | 0.1324 |
| 0.1351 | 0.1379 | 0.1406 | 0.1434 | 0.1461 |
| 0.1488 | 0.1535 | 0.1581 | 0.1627 | 0.1674 |
| 0.1720 | 0.1766 | 0.1813 | 0.1859 | 0.1905 |
| 0.1951 | 0.1998 | 0.2044 | 0.2090 | 0.2137 |
| 0.2183 | 0.2224 | 0.2266 | 0.2307 | 0.2348 |
| 0.2390 | 0.2476 | 0.2562 | 0.2648 | 0.2734 |
| 0.2820 | 0.2992 | 0.3165 | 0.3440 | 0.3877 |
| 0.5000 | 0.6123 | 0.6560 | 0.6835 | 0.7008 |
| 0.7180 | 0.7266 | 0.7352 | 0.7438 | 0.7524 |
| 0.7610 | 0.7652 | 0.7693 | 0.7734 | 0.7776 |
| 0.7817 | 0.7863 | 0.7910 | 0.7956 | 0.8002 |
| 0.8049 | 0.8095 | 0.8141 | 0.8187 | 0.8234 |
| 0.8280 | 0.8326 | 0.8373 | 0.8419 | 0.8465 |
| 0.8512 | 0.8539 | 0.8566 | 0.8594 | 0.8621 |
| 0.8649 | 0.8676 | 0.8703 | 0.8731 | 0.8758 |
| 0.8786 | 0.8813 | 0.8841 | 0.8868 | 0.8895 |
| 0.8923 | 0.8950 | 0.8978 | 0.9005 | 0.9033 |
| 0.9060 | 0.9087 | 0.9115 | 0.9142 | 0.9170 |
| 0.9197 | 0.9224 | 0.9252 | 0.9279 | 0.9307 |
| 0.9334 | 0.9345 | 0.9356 | 0.9367 | 0.9379 |
| 0.9390 | 0.9401 | 0.9412 | 0.9423 | 0.9434 |
| 0.9445 | 0.9456 | 0.9467 | 0.9478 | 0.9490 |
| 0.9501 | 0.9512 | 0.9523 | 0.9534 | 0.9545 |
| 0.9556 | 0.9567 | 0.9578 | 0.9589 | 0.9601 |
| 0.9612 | 0.9623 | 0.9634 | 0.9645 | 0.9656 |
| 0.9667 | 0.9678 | 0.9689 | 0.9700 | 0.9711 |
| 0.9723 | 0.9734 | 0.9745 | 0.9756 | 0.9767 |
| 0.9778 | 0.9789 | 0.9800 | 0.9811 | 0.9822 |
| 0.9834 | 0.9845 | 0.9856 | 0.9867 | 0.9878 |
| 0.9889 | 0.9900 | 0.9911 | 0.9922 | 0.9933 |
| 0.9945 | 0.9956 | 0.9967 | 0.9978 | 0.9989 |
| 1.0000 | | | | |

2_yr_sm

| 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
|--------|--------|--------|--------|--------|
| 0.0000 | 0.0011 | 0.0022 | 0.0033 | 0.0044 |
| 0.0055 | 0.0066 | 0.0077 | 0.0088 | 0.0099 |
| 0.0110 | 0.0122 | 0.0133 | 0.0144 | 0.0155 |
| 0.0166 | 0.0177 | 0.0188 | 0.0199 | 0.0210 |
| 0.0221 | 0.0232 | 0.0243 | 0.0254 | 0.0265 |
| 0.0276 | 0.0287 | 0.0298 | 0.0309 | 0.0320 |
| 0.0331 | 0.0343 | 0.0354 | 0.0365 | 0.0376 |

Eccelston POI 1-4 Existing.out

| | | | | |
|--------|--------|--------|--------|--------|
| 0.0387 | 0.0398 | 0.0409 | 0.0420 | 0.0431 |
| 0.0442 | 0.0453 | 0.0464 | 0.0475 | 0.0486 |
| 0.0497 | 0.0508 | 0.0519 | 0.0530 | 0.0541 |
| 0.0552 | 0.0564 | 0.0575 | 0.0586 | 0.0597 |
| 0.0608 | 0.0619 | 0.0630 | 0.0641 | 0.0652 |
| 0.0663 | 0.0690 | 0.0717 | 0.0745 | 0.0772 |
| 0.0799 | 0.0826 | 0.0853 | 0.0881 | 0.0908 |
| 0.0935 | 0.0962 | 0.0989 | 0.1017 | 0.1044 |
| 0.1071 | 0.1098 | 0.1125 | 0.1153 | 0.1180 |
| 0.1207 | 0.1234 | 0.1261 | 0.1289 | 0.1316 |
| 0.1343 | 0.1370 | 0.1397 | 0.1425 | 0.1452 |
| 0.1479 | 0.1525 | 0.1571 | 0.1616 | 0.1662 |
| 0.1708 | 0.1754 | 0.1799 | 0.1845 | 0.1891 |
| 0.1937 | 0.1982 | 0.2028 | 0.2074 | 0.2120 |
| 0.2165 | 0.2207 | 0.2248 | 0.2289 | 0.2330 |
| 0.2372 | 0.2457 | 0.2543 | 0.2629 | 0.2714 |
| 0.2800 | 0.2979 | 0.3158 | 0.3440 | 0.3886 |
| 0.5000 | 0.6114 | 0.6560 | 0.6842 | 0.7021 |
| 0.7200 | 0.7286 | 0.7371 | 0.7457 | 0.7543 |
| 0.7628 | 0.7670 | 0.7711 | 0.7752 | 0.7793 |
| 0.7835 | 0.7880 | 0.7926 | 0.7972 | 0.8018 |
| 0.8063 | 0.8109 | 0.8155 | 0.8201 | 0.8246 |
| 0.8292 | 0.8338 | 0.8384 | 0.8429 | 0.8475 |
| 0.8521 | 0.8548 | 0.8575 | 0.8603 | 0.8630 |
| 0.8657 | 0.8684 | 0.8711 | 0.8739 | 0.8766 |
| 0.8793 | 0.8820 | 0.8847 | 0.8875 | 0.8902 |
| 0.8929 | 0.8956 | 0.8983 | 0.9011 | 0.9038 |
| 0.9065 | 0.9092 | 0.9119 | 0.9147 | 0.9174 |
| 0.9201 | 0.9228 | 0.9255 | 0.9283 | 0.9310 |
| 0.9337 | 0.9348 | 0.9359 | 0.9370 | 0.9381 |
| 0.9392 | 0.9403 | 0.9414 | 0.9425 | 0.9436 |
| 0.9448 | 0.9459 | 0.9470 | 0.9481 | 0.9492 |
| 0.9503 | 0.9514 | 0.9525 | 0.9536 | 0.9547 |
| 0.9558 | 0.9569 | 0.9580 | 0.9591 | 0.9602 |
| 0.9613 | 0.9624 | 0.9635 | 0.9646 | 0.9657 |
| 0.9669 | 0.9680 | 0.9691 | 0.9702 | 0.9713 |
| 0.9724 | 0.9735 | 0.9746 | 0.9757 | 0.9768 |
| 0.9779 | 0.9790 | 0.9801 | 0.9812 | 0.9823 |
| 0.9834 | 0.9845 | 0.9856 | 0.9867 | 0.9878 |
| 0.9890 | 0.9901 | 0.9912 | 0.9923 | 0.9934 |
| 0.9945 | 0.9956 | 0.9967 | 0.9978 | 0.9989 |

5_yr_sm

| | | | | |
|--------|--------|--------|--------|--------|
| 1.0000 | 0.1 | | | |
| 0.0000 | 0.0012 | 0.0024 | 0.0035 | 0.0047 |
| 0.0059 | 0.0071 | 0.0082 | 0.0094 | 0.0106 |
| 0.0118 | 0.0129 | 0.0141 | 0.0153 | 0.0165 |
| 0.0176 | 0.0188 | 0.0200 | 0.0212 | 0.0223 |
| 0.0235 | 0.0247 | 0.0259 | 0.0270 | 0.0282 |
| 0.0294 | 0.0306 | 0.0317 | 0.0329 | 0.0341 |
| 0.0353 | 0.0364 | 0.0376 | 0.0388 | 0.0400 |
| 0.0411 | 0.0423 | 0.0435 | 0.0447 | 0.0458 |
| 0.0470 | 0.0482 | 0.0494 | 0.0505 | 0.0517 |
| 0.0529 | 0.0541 | 0.0552 | 0.0564 | 0.0576 |
| 0.0588 | 0.0599 | 0.0611 | 0.0623 | 0.0635 |
| 0.0646 | 0.0658 | 0.0670 | 0.0682 | 0.0693 |
| 0.0705 | 0.0733 | 0.0761 | 0.0788 | 0.0816 |
| 0.0844 | 0.0871 | 0.0899 | 0.0927 | 0.0954 |
| 0.0982 | 0.1010 | 0.1037 | 0.1065 | 0.1093 |
| 0.1120 | 0.1148 | 0.1176 | 0.1203 | 0.1231 |
| 0.1259 | 0.1286 | 0.1314 | 0.1342 | 0.1369 |
| 0.1397 | 0.1425 | 0.1452 | 0.1480 | 0.1508 |
| 0.1535 | 0.1580 | 0.1624 | 0.1669 | 0.1713 |
| 0.1758 | 0.1802 | 0.1847 | 0.1891 | 0.1936 |

Eccelston POI 1-4 Existing.out

| | | | | |
|----------|--------|--------|--------|--------|
| 0.1981 | 0.2025 | 0.2070 | 0.2114 | 0.2159 |
| 0.2203 | 0.2245 | 0.2287 | 0.2329 | 0.2371 |
| 0.2413 | 0.2501 | 0.2588 | 0.2676 | 0.2763 |
| 0.2851 | 0.3040 | 0.3229 | 0.3522 | 0.3968 |
| 0.5000 | 0.6032 | 0.6478 | 0.6771 | 0.6960 |
| 0.7149 | 0.7237 | 0.7324 | 0.7412 | 0.7499 |
| 0.7587 | 0.7629 | 0.7671 | 0.7713 | 0.7755 |
| 0.7797 | 0.7841 | 0.7886 | 0.7930 | 0.7975 |
| 0.8019 | 0.8064 | 0.8109 | 0.8153 | 0.8198 |
| 0.8242 | 0.8287 | 0.8331 | 0.8376 | 0.8420 |
| 0.8465 | 0.8492 | 0.8520 | 0.8548 | 0.8575 |
| 0.8603 | 0.8631 | 0.8658 | 0.8686 | 0.8714 |
| 0.8741 | 0.8769 | 0.8797 | 0.8824 | 0.8852 |
| 0.8880 | 0.8907 | 0.8935 | 0.8963 | 0.8990 |
| 0.9018 | 0.9046 | 0.9073 | 0.9101 | 0.9129 |
| 0.9156 | 0.9184 | 0.9212 | 0.9239 | 0.9267 |
| 0.9295 | 0.9307 | 0.9318 | 0.9330 | 0.9342 |
| 0.9354 | 0.9365 | 0.9377 | 0.9389 | 0.9401 |
| 0.9412 | 0.9424 | 0.9436 | 0.9448 | 0.9459 |
| 0.9471 | 0.9483 | 0.9495 | 0.9506 | 0.9518 |
| 0.9530 | 0.9542 | 0.9553 | 0.9565 | 0.9577 |
| 0.9589 | 0.9600 | 0.9612 | 0.9624 | 0.9636 |
| 0.9647 | 0.9659 | 0.9671 | 0.9683 | 0.9694 |
| 0.9706 | 0.9718 | 0.9730 | 0.9741 | 0.9753 |
| 0.9765 | 0.9777 | 0.9788 | 0.9800 | 0.9812 |
| 0.9824 | 0.9835 | 0.9847 | 0.9859 | 0.9871 |
| 0.9882 | 0.9894 | 0.9906 | 0.9918 | 0.9929 |
| 0.9941 | 0.9953 | 0.9965 | 0.9976 | 0.9988 |
| 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| 10_yr_sm | 0.1 | | | |
| 0.0000 | 0.0012 | 0.0025 | 0.0037 | 0.0049 |
| 0.0061 | 0.0074 | 0.0086 | 0.0098 | 0.0110 |
| 0.0123 | 0.0135 | 0.0147 | 0.0159 | 0.0172 |
| 0.0184 | 0.0196 | 0.0209 | 0.0221 | 0.0233 |
| 0.0245 | 0.0258 | 0.0270 | 0.0282 | 0.0294 |
| 0.0307 | 0.0319 | 0.0331 | 0.0344 | 0.0356 |
| 0.0368 | 0.0380 | 0.0393 | 0.0405 | 0.0417 |
| 0.0429 | 0.0442 | 0.0454 | 0.0466 | 0.0478 |
| 0.0491 | 0.0503 | 0.0515 | 0.0528 | 0.0540 |
| 0.0552 | 0.0564 | 0.0577 | 0.0589 | 0.0601 |
| 0.0613 | 0.0626 | 0.0638 | 0.0650 | 0.0663 |
| 0.0675 | 0.0687 | 0.0699 | 0.0712 | 0.0724 |
| 0.0736 | 0.0765 | 0.0794 | 0.0822 | 0.0851 |
| 0.0880 | 0.0908 | 0.0937 | 0.0966 | 0.0995 |
| 0.1023 | 0.1052 | 0.1081 | 0.1110 | 0.1138 |
| 0.1167 | 0.1196 | 0.1224 | 0.1253 | 0.1282 |
| 0.1311 | 0.1339 | 0.1368 | 0.1397 | 0.1425 |
| 0.1454 | 0.1483 | 0.1512 | 0.1540 | 0.1569 |
| 0.1598 | 0.1642 | 0.1687 | 0.1732 | 0.1777 |
| 0.1821 | 0.1866 | 0.1911 | 0.1956 | 0.2000 |
| 0.2045 | 0.2090 | 0.2134 | 0.2179 | 0.2224 |
| 0.2269 | 0.2311 | 0.2353 | 0.2395 | 0.2438 |
| 0.2480 | 0.2570 | 0.2659 | 0.2749 | 0.2838 |
| 0.2928 | 0.3120 | 0.3312 | 0.3606 | 0.4040 |
| 0.5000 | 0.5960 | 0.6394 | 0.6688 | 0.6880 |
| 0.7072 | 0.7162 | 0.7251 | 0.7341 | 0.7430 |
| 0.7520 | 0.7562 | 0.7605 | 0.7647 | 0.7689 |
| 0.7731 | 0.7776 | 0.7821 | 0.7866 | 0.7910 |
| 0.7955 | 0.8000 | 0.8044 | 0.8089 | 0.8134 |
| 0.8179 | 0.8223 | 0.8268 | 0.8313 | 0.8358 |
| 0.8402 | 0.8431 | 0.8460 | 0.8488 | 0.8517 |
| 0.8546 | 0.8575 | 0.8603 | 0.8632 | 0.8661 |
| 0.8689 | 0.8718 | 0.8747 | 0.8776 | 0.8804 |

Eccelston POI 1-4 Existing.out

| | | | | |
|----------|--------|--------|--------|--------|
| 0.8833 | 0.8862 | 0.8890 | 0.8919 | 0.8948 |
| 0.8977 | 0.9005 | 0.9034 | 0.9063 | 0.9092 |
| 0.9120 | 0.9149 | 0.9178 | 0.9206 | 0.9235 |
| 0.9264 | 0.9276 | 0.9288 | 0.9301 | 0.9313 |
| 0.9325 | 0.9337 | 0.9350 | 0.9362 | 0.9374 |
| 0.9387 | 0.9399 | 0.9411 | 0.9423 | 0.9436 |
| 0.9448 | 0.9460 | 0.9472 | 0.9485 | 0.9497 |
| 0.9509 | 0.9522 | 0.9534 | 0.9546 | 0.9558 |
| 0.9571 | 0.9583 | 0.9595 | 0.9607 | 0.9620 |
| 0.9632 | 0.9644 | 0.9656 | 0.9669 | 0.9681 |
| 0.9693 | 0.9706 | 0.9718 | 0.9730 | 0.9742 |
| 0.9755 | 0.9767 | 0.9779 | 0.9791 | 0.9804 |
| 0.9816 | 0.9828 | 0.9841 | 0.9853 | 0.9865 |
| 0.9877 | 0.9890 | 0.9902 | 0.9914 | 0.9926 |
| 0.9939 | 0.9951 | 0.9963 | 0.9975 | 0.9988 |
| 1.0000 | | | | |
| 25_yr_sm | 0.1 | | | |
| 0.0000 | 0.0013 | 0.0026 | 0.0039 | 0.0052 |
| 0.0066 | 0.0079 | 0.0092 | 0.0105 | 0.0118 |
| 0.0131 | 0.0144 | 0.0157 | 0.0170 | 0.0184 |
| 0.0197 | 0.0210 | 0.0223 | 0.0236 | 0.0249 |
| 0.0262 | 0.0275 | 0.0289 | 0.0302 | 0.0315 |
| 0.0328 | 0.0341 | 0.0354 | 0.0367 | 0.0380 |
| 0.0393 | 0.0407 | 0.0420 | 0.0433 | 0.0446 |
| 0.0459 | 0.0472 | 0.0485 | 0.0498 | 0.0511 |
| 0.0525 | 0.0538 | 0.0551 | 0.0564 | 0.0577 |
| 0.0590 | 0.0603 | 0.0616 | 0.0630 | 0.0643 |
| 0.0656 | 0.0669 | 0.0682 | 0.0695 | 0.0708 |
| 0.0721 | 0.0734 | 0.0748 | 0.0761 | 0.0774 |
| 0.0787 | 0.0817 | 0.0847 | 0.0877 | 0.0907 |
| 0.0937 | 0.0967 | 0.0997 | 0.1028 | 0.1058 |
| 0.1088 | 0.1118 | 0.1148 | 0.1178 | 0.1208 |
| 0.1238 | 0.1268 | 0.1298 | 0.1328 | 0.1358 |
| 0.1389 | 0.1419 | 0.1449 | 0.1479 | 0.1509 |
| 0.1539 | 0.1569 | 0.1599 | 0.1629 | 0.1659 |
| 0.1689 | 0.1735 | 0.1781 | 0.1826 | 0.1872 |
| 0.1918 | 0.1963 | 0.2009 | 0.2054 | 0.2100 |
| 0.2146 | 0.2191 | 0.2237 | 0.2283 | 0.2328 |
| 0.2374 | 0.2417 | 0.2460 | 0.2503 | 0.2546 |
| 0.2589 | 0.2681 | 0.2774 | 0.2866 | 0.2958 |
| 0.3050 | 0.3245 | 0.3439 | 0.3726 | 0.4137 |
| 0.5000 | 0.5863 | 0.6274 | 0.6561 | 0.6755 |
| 0.6950 | 0.7042 | 0.7134 | 0.7226 | 0.7319 |
| 0.7411 | 0.7454 | 0.7497 | 0.7540 | 0.7583 |
| 0.7626 | 0.7672 | 0.7717 | 0.7763 | 0.7809 |
| 0.7854 | 0.7900 | 0.7946 | 0.7991 | 0.8037 |
| 0.8082 | 0.8128 | 0.8174 | 0.8219 | 0.8265 |
| 0.8311 | 0.8341 | 0.8371 | 0.8401 | 0.8431 |
| 0.8461 | 0.8491 | 0.8521 | 0.8551 | 0.8581 |
| 0.8611 | 0.8642 | 0.8672 | 0.8702 | 0.8732 |
| 0.8762 | 0.8792 | 0.8822 | 0.8852 | 0.8882 |
| 0.8912 | 0.8942 | 0.8972 | 0.9003 | 0.9033 |
| 0.9063 | 0.9093 | 0.9123 | 0.9153 | 0.9183 |
| 0.9213 | 0.9226 | 0.9239 | 0.9252 | 0.9266 |
| 0.9279 | 0.9292 | 0.9305 | 0.9318 | 0.9331 |
| 0.9344 | 0.9357 | 0.9370 | 0.9384 | 0.9397 |
| 0.9410 | 0.9423 | 0.9436 | 0.9449 | 0.9462 |
| 0.9475 | 0.9489 | 0.9502 | 0.9515 | 0.9528 |
| 0.9541 | 0.9554 | 0.9567 | 0.9580 | 0.9593 |
| 0.9607 | 0.9620 | 0.9633 | 0.9646 | 0.9659 |
| 0.9672 | 0.9685 | 0.9698 | 0.9711 | 0.9725 |
| 0.9738 | 0.9751 | 0.9764 | 0.9777 | 0.9790 |
| 0.9803 | 0.9816 | 0.9830 | 0.9843 | 0.9856 |

| | Eccelston | POI | 1-4 Existing.out | |
|-----------|-----------|--------|------------------|--------|
| | 0.9869 | 0.9882 | 0.9895 | 0.9908 |
| | 0.9934 | 0.9948 | 0.9961 | 0.9974 |
| | 1.0000 | | | 0.9921 |
| | | | | 0.9987 |
| 50_yr_sm | 0.1 | | | |
| | 0.0000 | 0.0014 | 0.0027 | 0.0041 |
| | 0.0068 | 0.0082 | 0.0096 | 0.0109 |
| | 0.0137 | 0.0150 | 0.0164 | 0.0178 |
| | 0.0205 | 0.0219 | 0.0232 | 0.0246 |
| | 0.0273 | 0.0287 | 0.0301 | 0.0314 |
| | 0.0342 | 0.0355 | 0.0369 | 0.0383 |
| | 0.0410 | 0.0424 | 0.0437 | 0.0451 |
| | 0.0478 | 0.0492 | 0.0505 | 0.0519 |
| | 0.0546 | 0.0560 | 0.0574 | 0.0587 |
| | 0.0615 | 0.0628 | 0.0642 | 0.0656 |
| | 0.0683 | 0.0697 | 0.0710 | 0.0724 |
| | 0.0751 | 0.0765 | 0.0779 | 0.0792 |
| | 0.0820 | 0.0851 | 0.0882 | 0.0914 |
| | 0.0977 | 0.1008 | 0.1039 | 0.1071 |
| | 0.1134 | 0.1165 | 0.1196 | 0.1228 |
| | 0.1290 | 0.1322 | 0.1353 | 0.1385 |
| | 0.1447 | 0.1479 | 0.1510 | 0.1541 |
| | 0.1604 | 0.1636 | 0.1667 | 0.1698 |
| | 0.1761 | 0.1808 | 0.1854 | 0.1901 |
| | 0.1994 | 0.2040 | 0.2087 | 0.2133 |
| | 0.2227 | 0.2273 | 0.2320 | 0.2366 |
| | 0.2459 | 0.2503 | 0.2546 | 0.2589 |
| | 0.2676 | 0.2771 | 0.2866 | 0.2961 |
| | 0.3151 | 0.3345 | 0.3538 | 0.3819 |
| | 0.5000 | 0.5792 | 0.6181 | 0.6462 |
| | 0.6849 | 0.6944 | 0.7039 | 0.7134 |
| | 0.7324 | 0.7367 | 0.7411 | 0.7454 |
| | 0.7541 | 0.7587 | 0.7634 | 0.7680 |
| | 0.7773 | 0.7820 | 0.7867 | 0.7913 |
| | 0.8006 | 0.8053 | 0.8099 | 0.8146 |
| | 0.8239 | 0.8270 | 0.8302 | 0.8333 |
| | 0.8396 | 0.8427 | 0.8459 | 0.8490 |
| | 0.8553 | 0.8584 | 0.8615 | 0.8647 |
| | 0.8710 | 0.8741 | 0.8772 | 0.8804 |
| | 0.8866 | 0.8898 | 0.8929 | 0.8961 |
| | 0.9023 | 0.9055 | 0.9086 | 0.9118 |
| | 0.9180 | 0.9194 | 0.9208 | 0.9221 |
| | 0.9249 | 0.9262 | 0.9276 | 0.9290 |
| | 0.9317 | 0.9331 | 0.9344 | 0.9358 |
| | 0.9385 | 0.9399 | 0.9413 | 0.9426 |
| | 0.9454 | 0.9467 | 0.9481 | 0.9495 |
| | 0.9522 | 0.9535 | 0.9549 | 0.9563 |
| | 0.9590 | 0.9604 | 0.9617 | 0.9631 |
| | 0.9658 | 0.9672 | 0.9686 | 0.9699 |
| | 0.9727 | 0.9740 | 0.9754 | 0.9768 |
| | 0.9795 | 0.9809 | 0.9822 | 0.9836 |
| | 0.9863 | 0.9877 | 0.9891 | 0.9904 |
| | 0.9932 | 0.9945 | 0.9959 | 0.9973 |
| | 1.0000 | | | 0.9986 |
| 100_yr_sm | 0.1 | | | |
| | 0.0000 | 0.0014 | 0.0029 | 0.0043 |
| | 0.0071 | 0.0086 | 0.0100 | 0.0114 |
| | 0.0143 | 0.0157 | 0.0171 | 0.0186 |
| | 0.0214 | 0.0229 | 0.0243 | 0.0257 |
| | 0.0286 | 0.0300 | 0.0314 | 0.0329 |
| | 0.0357 | 0.0372 | 0.0386 | 0.0400 |
| | 0.0429 | 0.0443 | 0.0457 | 0.0472 |
| | 0.0500 | 0.0514 | 0.0529 | 0.0543 |
| | 0.0572 | 0.0586 | 0.0600 | 0.0614 |

Eccelston POI 1-4 Existing.out

| | | | | |
|-----------|--------|--------|--------|--------|
| 0.0643 | 0.0657 | 0.0672 | 0.0686 | 0.0700 |
| 0.0714 | 0.0729 | 0.0743 | 0.0757 | 0.0772 |
| 0.0786 | 0.0800 | 0.0814 | 0.0829 | 0.0843 |
| 0.0857 | 0.0890 | 0.0923 | 0.0955 | 0.0988 |
| 0.1021 | 0.1054 | 0.1086 | 0.1119 | 0.1152 |
| 0.1185 | 0.1217 | 0.1250 | 0.1283 | 0.1315 |
| 0.1348 | 0.1381 | 0.1414 | 0.1446 | 0.1479 |
| 0.1512 | 0.1544 | 0.1577 | 0.1610 | 0.1643 |
| 0.1675 | 0.1708 | 0.1741 | 0.1773 | 0.1806 |
| 0.1839 | 0.1886 | 0.1934 | 0.1981 | 0.2029 |
| 0.2076 | 0.2123 | 0.2171 | 0.2218 | 0.2266 |
| 0.2313 | 0.2361 | 0.2408 | 0.2455 | 0.2503 |
| 0.2550 | 0.2594 | 0.2637 | 0.2680 | 0.2723 |
| 0.2767 | 0.2864 | 0.2961 | 0.3058 | 0.3155 |
| 0.3252 | 0.3444 | 0.3635 | 0.3907 | 0.4275 |
| 0.5000 | 0.5725 | 0.6093 | 0.6365 | 0.6556 |
| 0.6748 | 0.6845 | 0.6942 | 0.7039 | 0.7136 |
| 0.7233 | 0.7277 | 0.7320 | 0.7363 | 0.7406 |
| 0.7450 | 0.7497 | 0.7545 | 0.7592 | 0.7639 |
| 0.7687 | 0.7734 | 0.7782 | 0.7829 | 0.7877 |
| 0.7924 | 0.7971 | 0.8019 | 0.8066 | 0.8114 |
| 0.8161 | 0.8194 | 0.8227 | 0.8259 | 0.8292 |
| 0.8325 | 0.8357 | 0.8390 | 0.8423 | 0.8456 |
| 0.8488 | 0.8521 | 0.8554 | 0.8586 | 0.8619 |
| 0.8652 | 0.8685 | 0.8717 | 0.8750 | 0.8783 |
| 0.8815 | 0.8848 | 0.8881 | 0.8914 | 0.8946 |
| 0.8979 | 0.9012 | 0.9045 | 0.9077 | 0.9110 |
| 0.9143 | 0.9157 | 0.9171 | 0.9186 | 0.9200 |
| 0.9214 | 0.9228 | 0.9243 | 0.9257 | 0.9271 |
| 0.9286 | 0.9300 | 0.9314 | 0.9328 | 0.9343 |
| 0.9357 | 0.9371 | 0.9386 | 0.9400 | 0.9414 |
| 0.9428 | 0.9443 | 0.9457 | 0.9471 | 0.9486 |
| 0.9500 | 0.9514 | 0.9528 | 0.9543 | 0.9557 |
| 0.9571 | 0.9586 | 0.9600 | 0.9614 | 0.9628 |
| 0.9643 | 0.9657 | 0.9671 | 0.9686 | 0.9700 |
| 0.9714 | 0.9729 | 0.9743 | 0.9757 | 0.9771 |
| 0.9786 | 0.9800 | 0.9814 | 0.9829 | 0.9843 |
| 0.9857 | 0.9871 | 0.9886 | 0.9900 | 0.9914 |
| 0.9929 | 0.9943 | 0.9957 | 0.9971 | 0.9986 |
| 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| 500_yr_sm | 0.1 | | | |
| 0.0000 | 0.0016 | 0.0031 | 0.0047 | 0.0063 |
| 0.0079 | 0.0094 | 0.0110 | 0.0126 | 0.0141 |
| 0.0157 | 0.0173 | 0.0189 | 0.0204 | 0.0220 |
| 0.0236 | 0.0252 | 0.0267 | 0.0283 | 0.0299 |
| 0.0314 | 0.0330 | 0.0346 | 0.0362 | 0.0377 |
| 0.0393 | 0.0409 | 0.0424 | 0.0440 | 0.0456 |
| 0.0472 | 0.0487 | 0.0503 | 0.0519 | 0.0535 |
| 0.0550 | 0.0566 | 0.0582 | 0.0597 | 0.0613 |
| 0.0629 | 0.0645 | 0.0660 | 0.0676 | 0.0692 |
| 0.0707 | 0.0723 | 0.0739 | 0.0755 | 0.0770 |
| 0.0786 | 0.0802 | 0.0817 | 0.0833 | 0.0849 |
| 0.0865 | 0.0880 | 0.0896 | 0.0912 | 0.0928 |
| 0.0943 | 0.0979 | 0.1015 | 0.1051 | 0.1087 |
| 0.1123 | 0.1159 | 0.1195 | 0.1231 | 0.1267 |
| 0.1303 | 0.1340 | 0.1376 | 0.1412 | 0.1448 |
| 0.1484 | 0.1520 | 0.1556 | 0.1592 | 0.1628 |
| 0.1664 | 0.1700 | 0.1736 | 0.1772 | 0.1808 |
| 0.1844 | 0.1880 | 0.1916 | 0.1952 | 0.1988 |
| 0.2024 | 0.2073 | 0.2122 | 0.2172 | 0.2221 |
| 0.2270 | 0.2319 | 0.2368 | 0.2418 | 0.2467 |
| 0.2516 | 0.2565 | 0.2615 | 0.2664 | 0.2713 |
| 0.2762 | 0.2806 | 0.2849 | 0.2893 | 0.2936 |

Eccelston POI 1-4 Existing.out

| | | | | |
|--------|--------|--------|--------|--------|
| 0.2979 | 0.3081 | 0.3182 | 0.3283 | 0.3384 |
| 0.3486 | 0.3669 | 0.3853 | 0.4101 | 0.4419 |
| 0.5000 | 0.5581 | 0.5899 | 0.6147 | 0.6331 |
| 0.6514 | 0.6616 | 0.6717 | 0.6818 | 0.6919 |
| 0.7021 | 0.7064 | 0.7107 | 0.7151 | 0.7194 |
| 0.7238 | 0.7287 | 0.7336 | 0.7385 | 0.7435 |
| 0.7484 | 0.7533 | 0.7582 | 0.7632 | 0.7681 |
| 0.7730 | 0.7779 | 0.7828 | 0.7878 | 0.7927 |
| 0.7976 | 0.8012 | 0.8048 | 0.8084 | 0.8120 |
| 0.8156 | 0.8192 | 0.8228 | 0.8264 | 0.8300 |
| 0.8336 | 0.8372 | 0.8408 | 0.8444 | 0.8480 |
| 0.8516 | 0.8552 | 0.8588 | 0.8624 | 0.8660 |
| 0.8697 | 0.8733 | 0.8769 | 0.8805 | 0.8841 |
| 0.8877 | 0.8913 | 0.8949 | 0.8985 | 0.9021 |
| 0.9057 | 0.9072 | 0.9088 | 0.9104 | 0.9120 |
| 0.9135 | 0.9151 | 0.9167 | 0.9183 | 0.9198 |
| 0.9214 | 0.9230 | 0.9245 | 0.9261 | 0.9277 |
| 0.9293 | 0.9308 | 0.9324 | 0.9340 | 0.9355 |
| 0.9371 | 0.9387 | 0.9403 | 0.9418 | 0.9434 |
| 0.9450 | 0.9465 | 0.9481 | 0.9497 | 0.9513 |
| 0.9528 | 0.9544 | 0.9560 | 0.9576 | 0.9591 |
| 0.9607 | 0.9623 | 0.9638 | 0.9654 | 0.9670 |
| 0.9686 | 0.9701 | 0.9717 | 0.9733 | 0.9748 |
| 0.9764 | 0.9780 | 0.9796 | 0.9811 | 0.9827 |
| 0.9843 | 0.9859 | 0.9874 | 0.9890 | 0.9906 |
| 0.9921 | 0.9937 | 0.9953 | 0.9969 | 0.9984 |
| 1.0000 | | | | |

GLOBAL OUTPUT:

.2 NN N NN N

winTR-20 Printed Page File End of Input Data List

Eccelston Mitigation POI 1-4 Existing

Name of printed page file:
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STORM 1_yr_sm

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Flow Time (hr) | Rate (cfs) | Rate (csm) |
|--------------------------|--|--------------------------|--------------------|----------------|---------------------|------------|------------|
| DA4 | 0.450 | | 0.770 | | 12.80 | 97.0 | 215.53 |
| Line | | | | | | | |
| Start Time (hr) | Flow values @ time increment of 0.200 hr | | | | | | |
| | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) |
| 11.600 | 0.0 | 1.2 | 5.2 | 21.7 | 54.2 | 85.6 | 96.9 |
| 13.000 | 89.4 | 72.1 | 56.5 | 44.3 | 35.1 | 28.8 | 24.9 |
| 14.400 | 22.7 | 21.4 | 20.6 | 20.2 | 19.8 | 19.0 | 17.4 |

| Eccelston POI 1-4 Existing.out | | | | | | | |
|--------------------------------|------|------|------|------|------|------|------|
| 15.800 | 15.8 | 14.4 | 13.5 | 13.0 | 12.6 | 12.5 | 12.4 |
| 17.200 | 12.3 | 12.3 | 12.3 | 12.4 | 12.4 | 12.3 | 11.6 |
| 18.600 | 10.3 | 8.8 | 7.5 | 6.6 | 6.1 | 5.7 | 5.5 |
| 20.000 | 5.4 | 5.3 | 5.3 | 5.2 | 5.2 | 5.2 | 5.2 |
| 21.400 | 5.2 | 5.2 | 5.2 | 5.2 | 5.3 | 5.2 | 5.2 |
| 22.800 | 5.3 | 5.3 | 5.3 | 5.3 | 5.3 | 5.3 | 5.3 |
| 24.200 | 5.2 | 4.7 | 3.8 | 2.7 | 1.7 | 1.1 | 0.7 |
| 25.600 | 0.0 | | | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| DA2 | 1.323 | | 0.636 | | 13.01 | 192.4 | 145.41 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|------------|------------|------------|------------|------------|
| 11.800 | 0.336E-01 | 4.1 | 24.5 | 69.7 | 131.5 | 176.2 | 192.0 |
| 13.200 | 182.4 | 155.8 | 127.4 | 104.4 | 87.1 | 74.4 | 65.8 |
| 14.600 | 60.4 | 57.0 | 54.8 | 53.2 | 51.2 | 48.3 | 44.7 |
| 16.000 | 41.0 | 37.9 | 35.6 | 34.2 | 33.3 | 32.8 | 32.5 |
| 17.400 | 32.4 | 32.3 | 32.3 | 32.4 | 32.2 | 31.2 | 29.0 |
| 18.800 | 25.9 | 22.7 | 19.9 | 17.8 | 16.4 | 15.5 | 14.9 |
| 20.200 | 14.5 | 14.2 | 14.0 | 13.9 | 13.8 | 13.8 | 13.8 |
| 21.600 | 13.7 | 13.7 | 13.8 | 13.8 | 13.8 | 13.8 | 13.8 |
| 23.000 | 13.9 | 13.9 | 13.9 | 13.9 | 14.0 | 14.0 | 13.8 |
| 24.400 | 13.1 | 11.4 | 9.1 | 6.7 | 4.7 | 3.2 | 2.2 |
| 25.800 | 1.5 | 1.0 | 0.7 | 0.0 | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| DA3 | 0.920 | | 0.443 | | 12.94 | 86.3 | 93.76 |

Eccelston Mitigation POI 1-4 Existing

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|------------|------------|------------|------------|------------|
| 11.800 | 0.0 | 0.6 | 8.7 | 30.1 | 60.3 | 80.9 | 86.2 |
| 13.200 | 79.4 | 66.5 | 54.8 | 45.3 | 38.3 | 33.5 | 30.7 |
| 14.600 | 29.1 | 28.3 | 27.8 | 27.4 | 26.6 | 25.0 | 22.9 |
| 16.000 | 21.0 | 19.5 | 18.7 | 18.2 | 17.9 | 17.7 | 17.7 |
| 17.400 | 17.7 | 17.7 | 17.8 | 17.9 | 17.8 | 17.1 | 15.5 |
| 18.800 | 13.6 | 11.7 | 10.3 | 9.3 | 8.7 | 8.3 | 8.1 |
| 20.200 | 7.9 | 7.8 | 7.7 | 7.7 | 7.7 | 7.7 | 7.7 |
| 21.600 | 7.7 | 7.7 | 7.7 | 7.8 | 7.8 | 7.8 | 7.8 |
| 23.000 | 7.8 | 7.9 | 7.9 | 7.9 | 7.9 | 7.9 | 7.8 |
| 24.400 | 7.3 | 6.1 | 4.6 | 3.1 | 2.0 | 1.3 | 0.9 |
| 25.800 | 0.6 | 0.0 | | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|

Eccelston POI 1-4 Existing.out

CON-1 2.693 Upstream 0.592 362.79 12.95 369.8 137.30

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | values @ time (cfs) | increment (cfs) | of 0.200 (cfs) | hr (cfs) | (cfs) |
|----------------------|------------|------------|---------------------|-----------------|----------------|----------|-------|
| 11.600 | 0.0 | 1.3 | 10.3 | 55.0 | 154.8 | 277.3 | 353.8 |
| 13.000 | 367.4 | 333.2 | 278.9 | 226.6 | 184.9 | 154.2 | 132.9 |
| 14.400 | 119.3 | 110.9 | 105.9 | 102.8 | 100.4 | 96.8 | 90.7 |
| 15.800 | 83.4 | 76.4 | 70.9 | 67.2 | 65.0 | 63.7 | 62.9 |
| 17.200 | 62.5 | 62.4 | 62.4 | 62.5 | 62.6 | 62.2 | 59.9 |
| 18.600 | 54.9 | 48.3 | 41.9 | 36.8 | 33.2 | 30.9 | 29.4 |
| 20.000 | 28.4 | 27.7 | 27.3 | 27.0 | 26.8 | 26.8 | 26.7 |
| 21.400 | 26.6 | 26.6 | 26.7 | 26.7 | 26.8 | 26.8 | 26.8 |
| 22.800 | 26.9 | 27.0 | 27.1 | 27.1 | 27.1 | 27.2 | 27.2 |
| 24.200 | 26.8 | 25.0 | 21.2 | 16.3 | 11.6 | 7.8 | 5.2 |
| 25.600 | 3.4 | 2.1 | 1.0 | 0.7 | 0.0 | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| CON-1 | 2.693 | Downstream | 0.592 | 362.74 | 13.23 | 339.2 | 125.93 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | values @ time (cfs) | increment (cfs) | of 0.200 (cfs) | hr (cfs) | (cfs) |
|----------------------|------------|------------|---------------------|-----------------|----------------|----------|-------|
| 11.800 | 0.0 | 2.2 | 16.3 | 60.3 | 142.5 | 238.7 | 310.3 |
| 13.200 | 338.2 | 325.2 | 287.6 | 242.7 | 201.6 | 168.3 | 143.8 |
| 14.600 | 126.9 | 116.0 | 109.1 | 104.7 | 101.3 | 97.3 | 91.8 |
| 16.000 | 85.3 | 78.8 | 73.3 | 69.1 | 66.3 | 64.5 | 63.5 |
| 17.400 | 62.9 | 62.6 | 62.5 | 62.5 | 62.5 | 61.9 | 59.6 |
| 18.800 | 55.4 | 49.8 | 44.0 | 38.9 | 34.9 | 32.1 | 30.2 |
| 20.200 | 29.0 | 28.1 | 27.5 | 27.2 | 26.9 | 26.8 | 26.7 |
| 21.600 | 26.7 | 26.6 | 26.7 | 26.7 | 26.8 | 26.8 | 26.8 |

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Eccelston Mitigation POI 1-4 Existing

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | values @ time (cfs) | increment (cfs) | of 0.200 (cfs) | hr (cfs) | (cfs) |
|----------------------|------------|------------|---------------------|-----------------|----------------|----------|-------|
| 23.000 | 26.9 | 27.0 | 27.0 | 27.1 | 27.1 | 27.2 | 27.1 |
| 24.400 | 26.6 | 24.9 | 21.7 | 17.5 | 13.2 | 9.4 | 6.5 |
| 25.800 | 4.3 | 2.7 | 1.6 | 0.8 | 0.0 | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| DA1 | 0.090 | | 0.768 | | 12.21 | 45.3 | 503.39 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | values @ time (cfs) | increment (cfs) | of 0.200 (cfs) | hr (cfs) | (cfs) |
|----------------------|------------|------------|---------------------|-----------------|----------------|----------|-------|
| 11.400 | 0.0 | 0.7 | 2.4 | 12.4 | 45.2 | 26.3 | 13.9 |
| 12.800 | 7.8 | 6.8 | 4.8 | 3.5 | 3.4 | 3.7 | 3.8 |
| 14.200 | 3.8 | 3.8 | 3.9 | 3.9 | 4.0 | 3.1 | 2.5 |
| 15.600 | 2.4 | 2.4 | 2.4 | 2.4 | 2.4 | 2.4 | 2.5 |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| 17.000 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 | 1.7 |
| 18.400 | 1.1 | 1.1 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| 19.800 | 1.0 | 1.0 | 1.0 | 1.0 | 1.1 | 1.0 | 1.0 |
| 21.200 | 1.0 | 1.0 | 1.1 | 1.1 | 1.0 | 1.0 | 1.0 |
| 22.600 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 |
| 24.000 | 1.1 | 0.0 | | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| OUTLET | 2.783 | | 0.597 | | 13.23 | 343.4 | 123.38 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow (cfs) | Rate (cfs) |
|----------------------|------------|------------|---------------------|-----------------|-------------------|------------|------------|
| 11.400 | 0.0 | 0.7 | 2.4 | 14.6 | 61.5 | 86.7 | 156.5 |
| 12.800 | 246.4 | 317.1 | 343.0 | 328.7 | 291.0 | 246.4 | 205.3 |
| 14.200 | 172.1 | 147.6 | 130.8 | 119.9 | 113.0 | 107.7 | 103.7 |
| 15.600 | 99.7 | 94.2 | 87.7 | 81.2 | 75.7 | 71.6 | 68.8 |
| 17.000 | 67.0 | 65.9 | 65.3 | 65.0 | 65.0 | 65.0 | 64.2 |
| 18.400 | 63.0 | 60.7 | 56.4 | 50.9 | 45.0 | 39.9 | 36.0 |
| 19.800 | 33.2 | 31.3 | 30.0 | 29.1 | 28.6 | 28.2 | 28.0 |
| 21.200 | 27.9 | 27.8 | 27.8 | 27.7 | 27.7 | 27.8 | 27.8 |
| 22.600 | 27.9 | 27.9 | 28.0 | 28.0 | 28.1 | 28.2 | 28.2 |
| 24.000 | 28.2 | 27.5 | 26.6 | 24.9 | 21.7 | 17.5 | 13.2 |
| 25.400 | 9.4 | 6.5 | 4.3 | 2.7 | 1.6 | 0.8 | 0.0 |

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Eccelston Mitigation POI 1-4 Existing

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| DA4 | 0.450 | | 1.141 | | 12.79 | 151.7 | 337.08 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow (cfs) | Rate (cfs) |
|----------------------|------------|------------|---------------------|-----------------|-------------------|------------|------------|
| 11.000 | 0.0 | 0.9 | 1.7 | 3.1 | 5.7 | 13.6 | 40.8 |
| 12.400 | 91.0 | 136.9 | 151.5 | 137.6 | 109.3 | 84.6 | 65.5 |
| 13.800 | 51.3 | 41.6 | 35.6 | 32.1 | 30.0 | 28.7 | 28.0 |
| 15.200 | 27.4 | 26.1 | 23.9 | 21.6 | 19.7 | 18.5 | 17.7 |
| 16.600 | 17.3 | 17.0 | 16.9 | 16.8 | 16.8 | 16.8 | 16.8 |
| 18.000 | 16.8 | 16.7 | 15.8 | 14.0 | 11.9 | 10.1 | 9.0 |
| 19.400 | 8.3 | 7.8 | 7.5 | 7.3 | 7.2 | 7.1 | 7.1 |
| 20.800 | 7.0 | 7.0 | 7.0 | 7.1 | 7.1 | 7.1 | 7.1 |
| 22.200 | 7.1 | 7.1 | 7.1 | 7.1 | 7.1 | 7.1 | 7.1 |
| 23.600 | 7.2 | 7.2 | 7.2 | 7.0 | 6.3 | 5.1 | 3.6 |
| 25.000 | 2.3 | 1.4 | 0.9 | 0.6 | 0.0 | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|

| Identifier | (sq mi) | Location | Eccelston POI 1-4 (in) | Existing.out (ft) | (hr) | (cfs) | (csm) |
|------------|---------|----------|------------------------|-------------------|-------|-------|--------|
| DA2 | 1.323 | | 0.973 | | 13.01 | 317.9 | 240.29 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Values @ time (cfs) | increment (cfs) | of 0.200 (cfs) | hr (cfs) | (cfs) |
|----------------------|------------|------------|---------------------|-----------------|----------------|----------|-------|
| 11.400 | 0.0 | 1.1 | 3.9 | 15.0 | 54.5 | 132.9 | 232.2 |
| 12.800 | 299.2 | 317.8 | 295.2 | 247.8 | 199.8 | 161.7 | 133.1 |
| 14.200 | 112.3 | 97.9 | 88.9 | 82.9 | 79.0 | 76.1 | 73.0 |
| 15.600 | 68.6 | 63.3 | 57.9 | 53.3 | 49.9 | 47.9 | 46.7 |
| 17.000 | 45.9 | 45.4 | 45.1 | 45.0 | 45.0 | 45.0 | 44.7 |
| 18.400 | 43.4 | 40.2 | 35.8 | 31.4 | 27.5 | 24.7 | 22.9 |
| 19.800 | 21.6 | 20.7 | 20.1 | 19.6 | 19.4 | 19.2 | 19.1 |
| 21.200 | 19.0 | 19.0 | 19.1 | 19.1 | 19.0 | 19.0 | 19.0 |
| 22.600 | 19.0 | 19.0 | 19.1 | 19.1 | 19.2 | 19.3 | 19.3 |
| 24.000 | 19.3 | 19.0 | 18.0 | 15.6 | 12.5 | 9.2 | 6.4 |
| 25.400 | 4.4 | 3.0 | 2.1 | 1.4 | 1.0 | 0.7 | 0.0 |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| DA3 | 0.920 | | 0.724 | | 12.95 | 161.4 | 175.39 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Values @ time (cfs) | increment (cfs) | of 0.200 (cfs) | hr (cfs) | (cfs) |
|----------------------|------------|------------|---------------------|-----------------|----------------|----------|-------|
| 11.800 | 0.0 | 3.0 | 22.7 | 67.5 | 122.8 | 156.0 | 159.6 |
| 13.200 | 141.7 | 115.5 | 93.1 | 75.4 | 62.5 | 53.7 | 48.4 |

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Eccelston Mitigation POI 1-4 Existing

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Values @ time (cfs) | increment (cfs) | of 0.200 (cfs) | hr (cfs) | (cfs) |
|----------------------|------------|------------|---------------------|-----------------|----------------|----------|-------|
| 14.600 | 45.2 | 43.3 | 42.2 | 41.3 | 39.9 | 37.3 | 34.0 |
| 16.000 | 31.1 | 28.9 | 27.6 | 26.8 | 26.3 | 26.0 | 25.9 |
| 17.400 | 25.9 | 25.9 | 26.0 | 26.0 | 25.9 | 24.8 | 22.6 |
| 18.800 | 19.7 | 16.9 | 14.8 | 13.5 | 12.7 | 12.1 | 11.7 |
| 20.200 | 11.4 | 11.3 | 11.2 | 11.1 | 11.1 | 11.1 | 11.1 |
| 21.600 | 11.2 | 11.2 | 11.2 | 11.2 | 11.2 | 11.2 | 11.2 |
| 23.000 | 11.2 | 11.2 | 11.3 | 11.4 | 11.4 | 11.4 | 11.2 |
| 24.400 | 10.4 | 8.7 | 6.5 | 4.5 | 2.9 | 1.9 | 1.3 |
| 25.800 | 0.8 | 0.5 | 0.0 | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| CON-1 | 2.693 | Upstream | 0.916 | 363.25 | 12.94 | 622.8 | 231.23 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Values @ time (cfs) | increment (cfs) | of 0.200 (cfs) | hr (cfs) | (cfs) |
|----------------------|------------|------------|---------------------|-----------------|----------------|----------|-------|
| 11.000 | 0.0 | 0.9 | 1.7 | 4.3 | 9.6 | 31.8 | 118.3 |
| 12.400 | 292.8 | 491.7 | 606.3 | 614.9 | 545.4 | 447.9 | 358.6 |

Eccelston POI 1-4 Existing.out

| | | | | | | | |
|--------|-------|-------|-------|-------|-------|-------|-------|
| 13.800 | 288.5 | 237.3 | 201.6 | 178.6 | 164.1 | 155.0 | 149.2 |
| 15.200 | 144.8 | 138.9 | 129.7 | 118.9 | 108.7 | 100.6 | 95.3 |
| 16.600 | 92.0 | 90.0 | 88.8 | 88.1 | 87.8 | 87.7 | 87.8 |
| 18.000 | 87.9 | 87.2 | 83.9 | 76.7 | 67.4 | 58.4 | 51.3 |
| 19.400 | 46.5 | 43.4 | 41.2 | 39.7 | 38.7 | 38.0 | 37.6 |
| 20.800 | 37.3 | 37.2 | 37.1 | 37.2 | 37.3 | 37.3 | 37.3 |
| 22.200 | 37.3 | 37.3 | 37.3 | 37.3 | 37.4 | 37.5 | 37.6 |
| 23.600 | 37.8 | 37.8 | 37.8 | 37.2 | 34.6 | 29.3 | 22.6 |
| 25.000 | 16.0 | 10.8 | 7.2 | 4.8 | 2.9 | 1.9 | 1.0 |
| 26.400 | 0.7 | 0.0 | | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| CON-1 | 2.693 | Downstream | 0.916 | 363.18 | 13.15 | 584.9 | 217.16 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|------------|------------|------------|------------|------------|
| 11.400 | 0.0 | 1.9 | 5.2 | 14.7 | 54.0 | 155.7 | 318.1 |
| 12.800 | 478.3 | 571.2 | 578.7 | 523.5 | 441.5 | 360.5 | 293.3 |
| 14.200 | 242.4 | 206.2 | 182.1 | 166.4 | 156.5 | 150.0 | 144.4 |
| 15.600 | 137.5 | 128.5 | 118.4 | 109.0 | 101.4 | 96.0 | 92.5 |
| 17.000 | 90.3 | 89.0 | 88.3 | 87.9 | 87.8 | 87.8 | 87.7 |
| 18.400 | 86.3 | 82.3 | 75.4 | 66.9 | 58.6 | 51.9 | 47.1 |
| 19.800 | 43.7 | 41.5 | 39.9 | 38.8 | 38.1 | 37.7 | 37.4 |
| 21.200 | 37.2 | 37.2 | 37.2 | 37.3 | 37.3 | 37.3 | 37.3 |
| 22.600 | 37.3 | 37.3 | 37.3 | 37.4 | 37.5 | 37.6 | 37.8 |

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Eccelston Mitigation POI 1-4 Existing

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|------------|------------|------------|------------|------------|
| 24.000 | 37.8 | 37.6 | 36.5 | 33.5 | 28.4 | 22.2 | 16.2 |
| 25.400 | 11.2 | 7.6 | 5.1 | 3.2 | 1.9 | 1.1 | 0.0 |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| DA1 | 0.090 | | 1.138 | | 12.19 | 69.5 | 772.01 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|------------|------------|------------|------------|------------|
| 11.000 | 0.0 | 0.9 | 1.5 | 2.3 | 5.7 | 22.6 | 69.5 |
| 12.400 | 39.3 | 20.6 | 11.1 | 9.6 | 6.7 | 4.9 | 4.8 |
| 13.800 | 5.1 | 5.2 | 5.3 | 5.3 | 5.3 | 5.4 | 5.4 |
| 15.200 | 4.2 | 3.4 | 3.3 | 3.3 | 3.3 | 3.3 | 3.3 |
| 16.600 | 3.3 | 3.3 | 3.4 | 3.3 | 3.4 | 3.4 | 3.4 |
| 18.000 | 3.4 | 2.3 | 1.5 | 1.4 | 1.4 | 1.4 | 1.4 |
| 19.400 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 |
| 20.800 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 |
| 22.200 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.5 | 1.4 |
| 23.600 | 1.4 | 1.4 | 1.4 | 0.6 | 0.0 | | |

Eccelston POI 1-4 Existing.out

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| OUTLET | 2.783 | | 0.923 | | 13.08 | 593.4 | 213.21 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | values @ time (cfs) | increment (cfs) | of 0.200 (cfs) | hr (cfs) | (cfs) |
|----------------------|------------|------------|---------------------|-----------------|----------------|----------|-------|
| 11.000 | 0.0 | 0.9 | 1.5 | 4.2 | 10.9 | 37.4 | 123.5 |
| 12.400 | 195.0 | 338.7 | 489.3 | 580.6 | 585.4 | 528.4 | 446.2 |
| 13.800 | 365.7 | 298.5 | 247.6 | 211.5 | 187.4 | 171.8 | 161.9 |
| 15.200 | 154.2 | 147.8 | 140.8 | 131.8 | 121.7 | 112.3 | 104.7 |
| 16.600 | 99.3 | 95.8 | 93.7 | 92.3 | 91.7 | 91.3 | 91.1 |
| 18.000 | 91.2 | 89.9 | 87.8 | 83.7 | 76.8 | 68.3 | 60.1 |
| 19.400 | 53.3 | 48.5 | 45.1 | 42.9 | 41.3 | 40.2 | 39.5 |
| 20.800 | 39.1 | 38.8 | 38.6 | 38.6 | 38.6 | 38.7 | 38.7 |
| 22.200 | 38.7 | 38.7 | 38.7 | 38.7 | 38.7 | 38.8 | 38.9 |
| 23.600 | 39.1 | 39.2 | 39.2 | 38.3 | 36.5 | 33.5 | 28.4 |
| 25.000 | 22.2 | 16.2 | 11.2 | 7.6 | 5.1 | 3.3 | 1.9 |
| 26.400 | 1.2 | 0.0 | | | | | |

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Eccelston Mitigation POI 1-4 Existing

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| DA4 | 0.450 | | 1.825 | | 12.75 | 243.7 | 541.36 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | values @ time (cfs) | increment (cfs) | of 0.200 (cfs) | hr (cfs) | (cfs) |
|----------------------|------------|------------|---------------------|-----------------|----------------|----------|-------|
| 9.800 | 0.4 | 1.1 | 1.8 | 2.7 | 3.7 | 4.7 | 5.6 |
| 11.200 | 6.7 | 8.6 | 11.9 | 18.0 | 33.7 | 78.9 | 157.1 |
| 12.600 | 225.3 | 243.0 | 218.2 | 172.7 | 133.1 | 102.4 | 79.8 |
| 14.000 | 64.1 | 54.0 | 48.0 | 44.4 | 42.1 | 40.7 | 39.6 |
| 15.400 | 37.6 | 34.6 | 31.5 | 28.9 | 27.2 | 26.2 | 25.6 |
| 16.800 | 25.2 | 25.0 | 24.9 | 24.8 | 24.8 | 24.9 | 24.9 |
| 18.200 | 24.6 | 23.4 | 20.8 | 17.9 | 15.3 | 13.6 | 12.5 |
| 19.600 | 11.9 | 11.5 | 11.2 | 11.0 | 10.9 | 10.9 | 10.8 |
| 21.000 | 10.8 | 10.8 | 10.8 | 10.8 | 10.8 | 10.8 | 10.9 |
| 22.400 | 10.9 | 10.9 | 10.9 | 10.9 | 10.9 | 10.9 | 10.9 |
| 23.800 | 10.9 | 10.9 | 10.7 | 9.7 | 7.8 | 5.5 | 3.5 |
| 25.200 | 2.2 | 1.4 | 0.9 | 0.6 | 0.0 | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| DA2 | 1.323 | | 1.609 | | 12.92 | 541.1 | 409.03 |

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| Start Time (hr) | Eccelston POI 1-4 Existing.out Flow Values @ time increment of 0.200 hr | | | | | | |
|-----------------|--|-------|-------|-------|-------|-------|-------|
| (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) |
| 10.200 | 0.0 | 0.8 | 1.9 | 3.4 | 5.2 | 7.6 | 11.0 |
| 11.600 | 16.6 | 26.7 | 53.1 | 126.6 | 259.7 | 417.7 | 518.5 |
| 13.000 | 539.2 | 493.5 | 410.6 | 329.0 | 264.3 | 215.4 | 179.5 |
| 14.400 | 154.4 | 138.2 | 127.3 | 120.0 | 114.6 | 109.2 | 102.4 |
| 15.800 | 94.6 | 86.9 | 80.2 | 75.4 | 72.6 | 70.8 | 69.6 |
| 17.200 | 68.9 | 68.5 | 68.3 | 68.2 | 68.2 | 67.7 | 65.7 |
| 18.600 | 61.1 | 54.7 | 48.1 | 42.4 | 38.3 | 35.5 | 33.6 |
| 20.000 | 32.3 | 31.4 | 30.9 | 30.5 | 30.2 | 30.0 | 29.9 |
| 21.400 | 29.9 | 29.8 | 29.8 | 29.8 | 29.8 | 29.9 | 29.9 |
| 22.800 | 29.9 | 30.0 | 30.0 | 30.0 | 30.1 | 30.1 | 30.1 |
| 24.200 | 29.7 | 28.1 | 24.5 | 19.6 | 14.5 | 10.1 | 6.9 |
| 25.600 | 4.7 | 3.2 | 2.2 | 1.5 | 1.0 | 0.7 | 0.0 |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| DA3 | 0.920 | | 1.276 | | 12.86 | 306.1 | 332.62 |

Eccelston Mitigation POI 1-4 Existing

| Line Start Time (hr) | Flow values @ time increment of 0.200 hr | | | | | | |
|----------------------|--|-------|-------|-------|-------|-------|-------|
| (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) |
| 11.200 | 0.0 | 0.7 | 2.2 | 6.3 | 19.3 | 65.7 | 153.1 |
| 12.600 | 249.6 | 300.9 | 298.5 | 258.8 | 207.9 | 165.5 | 132.1 |
| 14.000 | 107.9 | 91.0 | 80.4 | 73.8 | 69.7 | 67.1 | 65.1 |
| 15.400 | 62.5 | 58.3 | 53.4 | 48.9 | 45.7 | 43.7 | 42.6 |
| 16.800 | 41.8 | 41.4 | 41.2 | 41.1 | 41.1 | 41.2 | 41.3 |
| 18.200 | 41.0 | 39.4 | 35.9 | 31.5 | 27.3 | 24.0 | 21.9 |
| 19.600 | 20.6 | 19.7 | 19.1 | 18.7 | 18.5 | 18.4 | 18.3 |
| 21.000 | 18.2 | 18.2 | 18.2 | 18.2 | 18.2 | 18.2 | 18.3 |
| 22.400 | 18.3 | 18.3 | 18.4 | 18.4 | 18.4 | 18.4 | 18.5 |
| 23.800 | 18.5 | 18.5 | 18.2 | 16.9 | 14.2 | 10.7 | 7.4 |
| 25.200 | 4.8 | 3.1 | 2.1 | 1.4 | 0.9 | 0.6 | 0.0 |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| CON-1 | 2.693 | Upstream | 1.531 | 363.84 | 12.89 | 1079.0 | 400.62 |

| Line Start Time (hr) | Flow values @ time increment of 0.200 hr | | | | | | |
|----------------------|--|--------|--------|-------|-------|-------|-------|
| (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) |
| 9.800 | 0.4 | 1.1 | 1.9 | 3.6 | 5.6 | 8.0 | 10.8 |
| 11.200 | 14.3 | 20.3 | 30.7 | 51.2 | 107.3 | 272.6 | 570.4 |
| 12.600 | 892.2 | 1061.3 | 1053.4 | 924.7 | 751.8 | 596.9 | 476.8 |
| 14.000 | 387.4 | 324.8 | 283.1 | 256.4 | 239.1 | 227.9 | 219.2 |
| 15.400 | 209.3 | 195.3 | 179.5 | 164.8 | 153.2 | 145.3 | 140.7 |
| 16.800 | 137.8 | 136.0 | 135.0 | 134.5 | 134.3 | 134.3 | 134.4 |

Eccelston POI 1-4 Existing.out

| | | | | | | | |
|--------|-------|-------|-------|-------|------|------|------|
| 18.200 | 133.3 | 128.4 | 117.8 | 104.1 | 90.8 | 80.1 | 72.7 |
| 19.600 | 67.9 | 64.8 | 62.6 | 61.2 | 60.3 | 59.7 | 59.3 |
| 21.000 | 59.1 | 59.0 | 58.9 | 58.9 | 58.9 | 58.9 | 59.0 |
| 22.400 | 59.0 | 59.1 | 59.2 | 59.3 | 59.3 | 59.4 | 59.5 |
| 23.800 | 59.5 | 59.6 | 58.6 | 54.7 | 46.4 | 35.8 | 25.5 |
| 25.200 | 17.2 | 11.4 | 7.7 | 5.2 | 3.1 | 2.1 | 1.0 |
| 26.600 | 0.7 | 0.0 | | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| CON-1 | 2.693 | Downstream | 1.531 | 363.78 | 13.03 | 1032.3 | 383.28 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|------------|------------|------------|------------|------------|
| 10.000 | 0.0 | 0.8 | 2.4 | 4.2 | 6.4 | 8.9 | 11.9 |
| 11.400 | 16.3 | 23.9 | 38.0 | 71.5 | 170.5 | 380.8 | 675.6 |
| 12.800 | 921.7 | 1027.2 | 990.4 | 861.5 | 706.6 | 567.8 | 457.2 |
| 14.200 | 375.0 | 317.2 | 278.8 | 253.7 | 237.4 | 226.2 | 216.4 |
| 15.600 | 204.7 | 190.3 | 175.3 | 161.9 | 151.6 | 144.6 | 140.3 |
| 17.000 | 137.6 | 135.9 | 135.0 | 134.5 | 134.3 | 134.3 | 133.9 |

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Eccelston Mitigation POI 1-4 Existing

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|------------|------------|------------|------------|------------|
| 18.400 | 131.4 | 124.4 | 113.1 | 100.1 | 88.1 | 78.6 | 71.9 |
| 19.800 | 67.4 | 64.4 | 62.4 | 61.1 | 60.2 | 59.6 | 59.3 |
| 21.200 | 59.1 | 58.9 | 58.9 | 58.9 | 58.9 | 58.9 | 59.0 |
| 22.600 | 59.1 | 59.1 | 59.2 | 59.3 | 59.4 | 59.4 | 59.5 |
| 24.000 | 59.6 | 59.2 | 57.1 | 51.6 | 42.8 | 32.7 | 23.3 |
| 25.400 | 16.0 | 10.8 | 7.2 | 4.7 | 3.0 | 1.9 | 1.1 |
| 26.800 | 0.7 | 0.0 | | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| DA1 | 0.090 | | 1.823 | | 12.20 | 107.0 | 1188.49 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|------------|------------|------------|------------|------------|
| 9.600 | 0.0 | 0.6 | 0.8 | 1.0 | 1.2 | 1.4 | 1.5 |
| 11.000 | 1.7 | 3.1 | 4.4 | 6.1 | 13.5 | 41.9 | 106.8 |
| 12.400 | 60.8 | 32.6 | 17.2 | 14.7 | 10.2 | 7.4 | 7.1 |
| 13.800 | 7.4 | 7.5 | 7.6 | 7.6 | 7.6 | 7.7 | 7.7 |
| 15.200 | 6.1 | 5.0 | 4.9 | 4.8 | 4.9 | 4.9 | 4.9 |
| 16.600 | 4.9 | 4.9 | 4.9 | 5.0 | 5.0 | 5.0 | 5.0 |
| 18.000 | 5.0 | 3.4 | 2.3 | 2.2 | 2.1 | 2.2 | 2.1 |
| 19.400 | 2.2 | 2.1 | 2.2 | 2.2 | 2.2 | 2.2 | 2.2 |
| 20.800 | 2.2 | 2.2 | 2.2 | 2.2 | 2.2 | 2.2 | 2.2 |
| 22.200 | 2.2 | 2.2 | 2.2 | 2.2 | 2.2 | 2.2 | 2.2 |
| 23.600 | 2.2 | 2.2 | 2.2 | 1.0 | 0.0 | | |

Eccelston POI 1-4 Existing.out

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| OUTLET | 2.783 | | 1.540 | | 13.03 | 1046.7 | 376.06 |

Line

| Start Time (hr) | Flow (cfs) | Flow (cfs) | values @ time (cfs) | increment (cfs) | of 0.200 (cfs) | hr (cfs) | Rate (cfs) |
|-----------------|------------|------------|---------------------|-----------------|----------------|----------|------------|
| 9.600 | 0.0 | 0.6 | 0.8 | 1.8 | 3.7 | 5.6 | 7.9 |
| 11.000 | 10.6 | 15.0 | 20.7 | 30.0 | 51.5 | 113.4 | 277.3 |
| 12.400 | 441.7 | 708.2 | 939.0 | 1041.9 | 1000.6 | 868.9 | 713.7 |
| 13.800 | 575.2 | 464.7 | 382.6 | 324.8 | 286.5 | 261.4 | 245.1 |
| 15.200 | 232.3 | 221.5 | 209.6 | 195.2 | 180.2 | 166.8 | 156.5 |
| 16.600 | 149.6 | 145.2 | 142.5 | 140.9 | 139.9 | 139.4 | 139.3 |
| 18.000 | 139.3 | 137.3 | 133.7 | 126.6 | 115.2 | 102.3 | 90.2 |
| 19.400 | 80.7 | 74.0 | 69.6 | 66.6 | 64.6 | 63.2 | 62.4 |
| 20.800 | 61.8 | 61.5 | 61.2 | 61.1 | 61.1 | 61.1 | 61.1 |
| 22.200 | 61.1 | 61.2 | 61.3 | 61.3 | 61.4 | 61.5 | 61.6 |
| 23.600 | 61.6 | 61.7 | 61.7 | 60.2 | 57.1 | 51.6 | 42.8 |
| 25.000 | 32.7 | 23.4 | 16.0 | 10.8 | 7.2 | 4.7 | 3.0 |

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Eccelston Mitigation POI 1-4 Existing

Line

| Start Time (hr) | Flow (cfs) | Flow (cfs) | values @ time (cfs) | increment (cfs) | of 0.200 (cfs) | hr (cfs) | Rate (cfs) |
|-----------------|------------|------------|---------------------|-----------------|----------------|----------|------------|
| 26.400 | 1.9 | 1.1 | 0.7 | 0.0 | | | |

STORM 10_yr_sm

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| DA4 | 0.450 | | 2.473 | | 12.76 | 322.2 | 715.80 |

Line

| Start Time (hr) | Flow (cfs) | Flow (cfs) | values @ time (cfs) | increment (cfs) | of 0.200 (cfs) | hr (cfs) | Rate (cfs) |
|-----------------|------------|------------|---------------------|-----------------|----------------|----------|------------|
| 8.800 | 0.0 | 0.8 | 1.3 | 2.1 | 3.2 | 4.5 | 5.9 |
| 10.200 | 7.4 | 8.8 | 10.1 | 11.4 | 12.6 | 14.1 | 17.0 |
| 11.600 | 22.3 | 31.8 | 54.7 | 115.0 | 215.5 | 299.8 | 320.3 |
| 13.000 | 286.8 | 227.2 | 175.3 | 135.0 | 105.0 | 84.1 | 70.6 |
| 14.400 | 62.6 | 57.7 | 54.6 | 52.8 | 51.2 | 48.7 | 45.0 |
| 15.800 | 41.1 | 38.0 | 35.8 | 34.6 | 33.8 | 33.4 | 33.1 |
| 17.200 | 33.0 | 33.0 | 33.0 | 33.0 | 33.0 | 32.6 | 31.0 |
| 18.600 | 27.6 | 23.7 | 20.3 | 18.0 | 16.7 | 15.8 | 15.2 |
| 20.000 | 14.9 | 14.7 | 14.5 | 14.5 | 14.4 | 14.4 | 14.4 |
| 21.400 | 14.4 | 14.4 | 14.4 | 14.4 | 14.4 | 14.4 | 14.4 |
| 22.800 | 14.4 | 14.5 | 14.5 | 14.5 | 14.5 | 14.5 | 14.5 |
| 24.200 | 14.2 | 12.9 | 10.3 | 7.3 | 4.7 | 2.9 | 1.9 |
| 25.600 | 1.2 | 0.7 | 0.0 | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|

| Eccelston POI 1-4 Existing.out | | | | | | | |
|--------------------------------|-------|-------|-------|-------|-------|-------|-------|
| 15.800 | 238.7 | 220.1 | 205.4 | 195.5 | 189.7 | 186.0 | 183.7 |
| 17.200 | 182.3 | 181.7 | 181.4 | 181.4 | 181.5 | 179.9 | 173.2 |
| 18.600 | 158.8 | 140.4 | 122.5 | 108.2 | 98.4 | 92.0 | 87.7 |
| 20.000 | 84.8 | 82.9 | 81.6 | 80.9 | 80.3 | 80.0 | 79.7 |
| 21.400 | 79.6 | 79.5 | 79.6 | 79.7 | 79.7 | 79.8 | 79.8 |
| 22.800 | 79.9 | 80.1 | 80.2 | 80.2 | 80.3 | 80.3 | 80.3 |
| 24.200 | 79.0 | 73.8 | 62.6 | 48.2 | 34.3 | 23.1 | 15.4 |
| 25.600 | 10.3 | 6.9 | 4.4 | 2.8 | 1.8 | 0.9 | 0.6 |
| 27.000 | 0.0 | | | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| CON-1 | 2.693 | Downstream | 2.127 | 364.23 | 12.98 | 1419.2 | 526.91 |

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Eccelston Mitigation POI 1-4 Existing

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|------------|------------|------------|------------|------------|
| 9.200 | 0.563E-01 | 1.5 | 3.3 | 5.6 | 8.8 | 12.7 | 17.1 |
| 10.600 | | 22.3 | 27.9 | 33.8 | 40.3 | 49.5 | 64.8 |
| 12.000 | | 151.0 | 304.7 | 608.4 | 1002.9 | 1307.5 | 1418.7 |
| 13.400 | | 1155.6 | 943.5 | 756.4 | 608.2 | 498.0 | 421.1 |
| 14.800 | | 336.3 | 314.1 | 298.9 | 285.7 | 269.9 | 251.1 |
| 16.200 | | 215.2 | 202.5 | 194.1 | 188.8 | 185.4 | 183.4 |
| 17.600 | | 181.7 | 181.5 | 181.5 | 180.8 | 176.9 | 166.8 |
| 19.000 | | 133.7 | 117.7 | 105.3 | 96.7 | 90.9 | 86.9 |
| 20.400 | | 82.6 | 81.4 | 80.7 | 80.2 | 79.9 | 79.7 |
| 21.800 | | 79.6 | 79.6 | 79.7 | 79.8 | 79.9 | 79.9 |
| 23.200 | | 80.1 | 80.2 | 80.2 | 80.3 | 80.3 | 79.7 |
| 24.600 | | 68.8 | 56.6 | 43.0 | 30.5 | 20.8 | 14.0 |
| 26.000 | | 6.3 | 4.0 | 2.6 | 1.5 | 0.9 | 0.0 |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| DA1 | 0.090 | | 2.470 | | 12.19 | 136.8 | 1519.45 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|------------|------------|------------|------------|------------|
| 8.800 | 0.0 | 0.5 | 0.9 | 1.3 | 1.6 | 1.9 | 2.2 |
| 10.200 | 2.4 | 2.7 | 2.9 | 3.0 | 3.2 | 5.7 | 7.8 |
| 11.600 | 10.3 | 21.6 | 59.5 | 136.4 | 78.5 | 42.9 | 22.8 |
| 13.000 | 19.4 | 13.5 | 9.7 | 9.2 | 9.7 | 9.7 | 9.8 |
| 14.400 | 9.8 | 9.9 | 9.9 | 10.0 | 8.0 | 6.6 | 6.5 |
| 15.800 | 6.4 | 6.5 | 6.5 | 6.5 | 6.5 | 6.5 | 6.6 |
| 17.200 | 6.5 | 6.6 | 6.6 | 6.6 | 6.6 | 4.5 | 3.1 |
| 18.600 | 2.8 | 2.9 | 2.8 | 2.9 | 2.8 | 2.9 | 2.8 |
| 20.000 | 2.9 | 2.9 | 2.8 | 2.9 | 2.8 | 2.9 | 2.8 |
| 21.400 | 2.9 | 2.9 | 2.9 | 2.9 | 2.9 | 2.9 | 2.9 |
| 22.800 | 2.9 | 2.9 | 2.9 | 2.9 | 2.9 | 2.9 | 3.0 |
| 24.200 | 1.3 | 0.0 | | | | | |

Eccelston POI 1-4 Existing.out

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| OUTLET | 2.783 | | 2.138 | | 12.98 | 1438.7 | 516.88 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow Rate (cfs) | Rate (cfs) |
|----------------------|------------|------------|---------------------|-----------------|-------------------|-----------------|------------|
| 8.800 | 0.0 | 0.5 | 0.9 | 2.8 | 4.9 | 7.5 | 11.0 |
| 10.200 | 15.1 | 19.8 | 25.2 | 30.9 | 37.0 | 46.0 | 57.3 |
| 11.600 | 75.1 | 113.3 | 210.5 | 441.3 | 686.9 | 1045.9 | 1330.5 |
| 13.000 | 1438.2 | 1356.7 | 1165.2 | 952.6 | 766.0 | 617.9 | 507.8 |
| 14.400 | 431.0 | 379.9 | 346.2 | 324.1 | 306.9 | 292.2 | 276.4 |

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Eccelston Mitigation POI 1-4 Existing

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow Rate (cfs) | Rate (cfs) |
|----------------------|------------|------------|---------------------|-----------------|-------------------|-----------------|------------|
| 15.800 | 257.6 | 238.5 | 221.7 | 209.1 | 200.7 | 195.3 | 192.0 |
| 17.200 | 189.9 | 188.9 | 188.3 | 188.1 | 188.1 | 185.2 | 180.0 |
| 18.600 | 169.6 | 154.1 | 136.5 | 120.6 | 108.2 | 99.6 | 93.7 |
| 20.000 | 89.8 | 87.2 | 85.4 | 84.4 | 83.5 | 83.1 | 82.7 |
| 21.400 | 82.6 | 82.5 | 82.5 | 82.5 | 82.6 | 82.6 | 82.7 |
| 22.800 | 82.8 | 82.9 | 83.0 | 83.0 | 83.2 | 83.2 | 83.3 |
| 24.200 | 81.0 | 76.7 | 68.8 | 56.6 | 43.0 | 30.5 | 20.8 |
| 25.600 | 14.0 | 9.5 | 6.3 | 4.0 | 2.6 | 1.5 | 0.9 |
| 27.000 | 0.0 | | | | | | |

STORM 25_yr_sm

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| DA4 | 0.450 | | 3.530 | | 12.76 | 434.7 | 965.82 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow Rate (cfs) | Rate (cfs) |
|----------------------|------------|------------|---------------------|-----------------|-------------------|-----------------|------------|
| 7.600 | 0.4 | 1.1 | 1.9 | 2.8 | 3.8 | 4.8 | 5.8 |
| 9.000 | 6.8 | 7.9 | 9.4 | 11.7 | 14.2 | 16.7 | 19.0 |
| 10.400 | 21.1 | 23.0 | 24.8 | 26.2 | 28.3 | 32.9 | 41.8 |
| 11.800 | 57.2 | 91.6 | 173.6 | 303.5 | 408.9 | 431.7 | 385.6 |
| 13.200 | 307.1 | 238.3 | 184.1 | 143.6 | 115.1 | 96.8 | 85.9 |
| 14.600 | 79.2 | 75.0 | 72.4 | 70.2 | 67.0 | 62.0 | 56.9 |
| 16.000 | 52.7 | 49.9 | 48.3 | 47.4 | 46.8 | 46.4 | 46.2 |
| 17.400 | 46.1 | 46.1 | 46.1 | 46.2 | 45.6 | 43.3 | 38.6 |
| 18.800 | 33.3 | 28.7 | 25.5 | 23.6 | 22.4 | 21.6 | 21.2 |
| 20.200 | 20.8 | 20.7 | 20.6 | 20.5 | 20.4 | 20.4 | 20.4 |
| 21.600 | 20.5 | 20.4 | 20.4 | 20.5 | 20.5 | 20.5 | 20.5 |
| 23.000 | 20.5 | 20.6 | 20.6 | 20.5 | 20.5 | 20.6 | 20.2 |
| 24.400 | 18.3 | 14.6 | 10.3 | 6.6 | 4.1 | 2.6 | 1.6 |
| 25.800 | 1.0 | 0.6 | 0.0 | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|

Eccelston POI 1-4 Existing.out

| Reach Identifier | Area (sq mi) | ID or Location | Amount (in) | Elevation (ft) | Time (hr) | Rate (cfs) | Rate (csm) |
|------------------|--------------|----------------|-------------|----------------|-----------|------------|------------|
| DA2 | 1.323 | | 3.232 | | 12.89 | 1024.4 | 774.30 |

Line

| Start Time (hr) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|-----------------|------------|------------|------------|------------|------------|------------|------------|
| 8.000 | 0.0 | 0.9 | 2.0 | 3.5 | 5.5 | 7.8 | 10.3 |
| 9.400 | 13.5 | 17.8 | 22.9 | 28.6 | 34.5 | 40.2 | 45.7 |
| 10.800 | 50.8 | 55.5 | 60.9 | 69.8 | 86.1 | 115.7 | 179.2 |
| 12.200 | 328.2 | 573.1 | 840.3 | 1001.0 | 1014.6 | 920.3 | 765.4 |
| 13.600 | 616.1 | 495.6 | 402.9 | 334.8 | 287.7 | 256.2 | 235.0 |

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Eccelston Mitigation POI 1-4 Existing

Line

| Start Time (hr) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|-----------------|------------|------------|------------|------------|------------|------------|------------|
| 15.000 | 220.9 | 210.4 | 200.5 | 188.5 | 175.0 | 161.8 | 150.5 |
| 16.400 | 142.5 | 137.7 | 134.6 | 132.6 | 131.3 | 130.5 | 130.1 |
| 17.800 | 130.0 | 130.0 | 129.0 | 124.9 | 116.3 | 104.4 | 92.1 |
| 19.200 | 81.5 | 73.6 | 68.4 | 65.0 | 62.6 | 60.9 | 59.8 |
| 20.600 | 59.1 | 58.6 | 58.2 | 58.0 | 57.8 | 57.8 | 57.7 |
| 22.000 | 57.7 | 57.7 | 57.8 | 57.8 | 57.9 | 57.9 | 58.0 |
| 23.400 | 58.1 | 58.0 | 58.1 | 58.1 | 57.4 | 54.2 | 47.3 |
| 24.800 | 37.7 | 27.9 | 19.4 | 13.1 | 9.0 | 6.2 | 4.2 |
| 26.200 | 2.9 | 2.0 | 1.3 | 0.9 | 0.6 | 0.0 | 0.0 |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Time (hr) | Peak Flow Rate (cfs) | Peak Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|-----------|----------------------|----------------------|
| DA3 | 0.920 | | 2.750 | | 12.82 | 640.5 | 696.00 |

Line

| Start Time (hr) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|-----------------|------------|------------|------------|------------|------------|------------|------------|
| 9.200 | 0.0 | 1.2 | 2.7 | 4.9 | 7.5 | 10.5 | 13.6 |
| 10.600 | 16.7 | 19.8 | 22.7 | 26.1 | 31.9 | 42.3 | 60.5 |
| 12.000 | 103.0 | 206.5 | 382.2 | 557.2 | 636.6 | 616.1 | 527.6 |
| 13.400 | 423.4 | 335.9 | 267.5 | 216.7 | 181.9 | 159.5 | 145.5 |
| 14.800 | 136.5 | 130.7 | 126.3 | 121.3 | 113.6 | 104.6 | 96.7 |
| 16.200 | 90.9 | 87.5 | 85.4 | 84.0 | 83.2 | 82.7 | 82.5 |
| 17.600 | 82.5 | 82.6 | 82.7 | 82.0 | 78.8 | 71.8 | 63.2 |
| 19.000 | 55.0 | 48.5 | 44.4 | 41.8 | 40.1 | 38.9 | 38.2 |
| 20.400 | 37.7 | 37.4 | 37.2 | 37.1 | 37.0 | 37.0 | 37.0 |
| 21.800 | 37.0 | 37.0 | 37.1 | 37.2 | 37.2 | 37.2 | 37.3 |
| 23.200 | 37.3 | 37.4 | 37.4 | 37.4 | 37.4 | 36.8 | 34.2 |
| 24.600 | 28.6 | 21.5 | 14.9 | 9.7 | 6.4 | 4.2 | 2.8 |
| 26.000 | 1.8 | 1.2 | 0.8 | 0.0 | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Time (hr) | Peak Flow Rate (cfs) | Peak Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|-----------|----------------------|----------------------|
| CON-1 | 2.693 | Upstream | 3.117 | 364.92 | 12.83 | 2078.9 | 771.87 |

Eccelston POI 1-4 Existing.out

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|------------|------------|------------|------------|------------|
| 7.600 | 0.4 | 1.1 | 1.9 | 3.7 | 5.7 | 8.3 | 11.3 |
| 9.000 | 14.5 | 18.3 | 24.2 | 32.1 | 42.0 | 52.9 | 64.0 |
| 10.400 | 74.9 | 85.4 | 95.3 | 104.4 | 115.4 | 134.6 | 170.5 |
| 11.800 | 234.0 | 376.3 | 709.9 | 1258.9 | 1804.4 | 2063.1 | 2015.4 |
| 13.200 | 1754.3 | 1427.1 | 1136.9 | 906.8 | 735.7 | 613.9 | 533.1 |
| 14.600 | 480.9 | 446.8 | 424.0 | 407.0 | 388.7 | 364.0 | 336.6 |
| 16.000 | 311.3 | 291.4 | 278.3 | 270.5 | 265.5 | 262.2 | 260.2 |
| 17.400 | 259.1 | 258.7 | 258.8 | 258.8 | 256.5 | 247.0 | 226.7 |

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Eccelston Mitigation POI 1-4 Existing

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|------------|------------|------------|------------|------------|
| 18.800 | 200.8 | 175.8 | 155.5 | 141.5 | 132.6 | 126.7 | 122.7 |
| 20.200 | 119.9 | 118.2 | 117.1 | 116.3 | 115.7 | 115.4 | 115.3 |
| 21.600 | 115.3 | 115.2 | 115.2 | 115.3 | 115.5 | 115.6 | 115.6 |
| 23.000 | 115.7 | 115.9 | 116.0 | 116.0 | 116.0 | 116.1 | 114.3 |
| 24.400 | 106.6 | 90.4 | 69.5 | 49.4 | 33.3 | 22.2 | 14.9 |
| 25.800 | 10.0 | 6.7 | 4.4 | 2.7 | 1.8 | 0.9 | 0.6 |
| 27.200 | 0.0 | | | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| CON-1 | 2.693 | Downstream | 3.117 | 364.84 | 12.97 | 1987.9 | 738.07 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|------------|------------|------------|------------|------------|
| 7.800 | 0.0 | 1.1 | 2.7 | 4.6 | 6.9 | 9.6 | 12.6 |
| 9.200 | 16.1 | 21.0 | 27.8 | 36.5 | 46.6 | 57.4 | 68.3 |
| 10.600 | 79.0 | 89.2 | 98.7 | 108.8 | 124.1 | 151.6 | 200.4 |
| 12.000 | 302.0 | 539.4 | 971.2 | 1494.0 | 1868.7 | 1983.6 | 1857.6 |
| 13.400 | 1596.1 | 1308.7 | 1054.4 | 851.5 | 699.2 | 592.2 | 520.6 |
| 14.800 | 473.0 | 441.4 | 419.4 | 400.4 | 378.1 | 352.4 | 326.6 |
| 16.200 | 304.2 | 287.5 | 276.5 | 269.4 | 264.8 | 261.8 | 260.0 |
| 17.600 | 259.1 | 258.9 | 258.9 | 257.7 | 251.7 | 236.9 | 214.8 |
| 19.000 | 190.5 | 168.4 | 151.2 | 139.2 | 131.2 | 125.7 | 122.0 |
| 20.400 | 119.5 | 118.0 | 116.9 | 116.1 | 115.6 | 115.4 | 115.3 |
| 21.800 | 115.3 | 115.2 | 115.2 | 115.4 | 115.5 | 115.6 | 115.7 |
| 23.200 | 115.8 | 115.9 | 116.0 | 116.0 | 116.1 | 115.2 | 110.4 |
| 24.600 | 98.6 | 80.8 | 61.2 | 43.6 | 29.8 | 20.2 | 13.7 |
| 26.000 | 9.2 | 6.1 | 3.9 | 2.5 | 1.4 | 0.9 | 0.0 |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| DA1 | 0.090 | | 3.528 | | 12.19 | 177.5 | 1971.10 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|------------|------------|------------|------------|------------|
|----------------------|------------|------------|------------|------------|------------|------------|------------|

Eccelston POI 1-4 Existing.out

| | | | | | | | |
|--------|------|------|------|-------|-------|------|------|
| 7.400 | 0.0 | 0.6 | 0.8 | 1.0 | 1.2 | 1.4 | 1.6 |
| 8.800 | 1.8 | 2.0 | 2.9 | 3.7 | 4.1 | 4.5 | 4.9 |
| 10.200 | 5.2 | 5.5 | 5.8 | 5.8 | 6.0 | 10.5 | 14.0 |
| 11.600 | 17.9 | 35.2 | 85.4 | 176.8 | 103.1 | 58.4 | 31.7 |
| 13.000 | 27.2 | 18.7 | 13.3 | 12.8 | 13.2 | 13.4 | 13.5 |
| 14.400 | 13.5 | 13.5 | 13.6 | 13.7 | 11.1 | 9.3 | 9.1 |
| 15.800 | 9.1 | 9.1 | 9.2 | 9.1 | 9.1 | 9.2 | 9.2 |
| 17.200 | 9.2 | 9.3 | 9.2 | 9.2 | 9.2 | 6.3 | 4.4 |
| 18.600 | 4.1 | 4.0 | 4.0 | 4.0 | 4.2 | 4.1 | 4.0 |

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Eccelston Mitigation POI 1-4 Existing

Line

| Start Time (hr) | Flow values @ time increment of 0.200 hr | | | | | | |
|-----------------|--|-------|-------|-------|-------|-------|-------|
| | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) |
| 20.000 | 4.0 | 4.2 | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 |
| 21.400 | 4.1 | 4.1 | 4.1 | 4.2 | 4.1 | 4.1 | 4.1 |
| 22.800 | 4.2 | 4.1 | 4.1 | 4.1 | 4.1 | 4.2 | 4.1 |
| 24.200 | 1.8 | 0.0 | | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| OUTLET | 2.783 | | 3.130 | | 12.98 | 2013.7 | 723.47 |

Line

| Start Time (hr) | Flow values @ time increment of 0.200 hr | | | | | | |
|-----------------|--|--------|--------|--------|--------|--------|--------|
| | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) |
| 7.400 | 0.0 | 0.6 | 0.8 | 2.2 | 3.9 | 6.0 | 8.5 |
| 8.800 | 11.4 | 14.7 | 19.0 | 24.7 | 31.9 | 40.9 | 51.4 |
| 10.200 | 62.5 | 73.8 | 84.7 | 95.0 | 104.7 | 119.3 | 138.2 |
| 11.600 | 169.5 | 235.6 | 387.4 | 716.3 | 1075.0 | 1552.5 | 1900.5 |
| 13.000 | 2010.8 | 1876.2 | 1609.2 | 1321.4 | 1067.5 | 864.9 | 712.7 |
| 14.400 | 605.9 | 534.1 | 486.7 | 455.1 | 430.5 | 409.7 | 387.2 |
| 15.800 | 361.5 | 335.7 | 313.5 | 296.7 | 285.6 | 278.5 | 273.9 |
| 17.200 | 271.0 | 269.3 | 268.4 | 268.1 | 268.1 | 264.0 | 256.0 |
| 18.600 | 241.0 | 218.8 | 194.5 | 172.4 | 155.3 | 143.3 | 135.2 |
| 20.000 | 129.7 | 126.2 | 123.6 | 122.0 | 121.0 | 120.2 | 119.8 |
| 21.400 | 119.5 | 119.4 | 119.3 | 119.4 | 119.3 | 119.4 | 119.6 |
| 22.800 | 119.8 | 119.8 | 119.9 | 120.0 | 120.1 | 120.1 | 120.2 |
| 24.200 | 117.0 | 110.4 | 98.6 | 80.8 | 61.2 | 43.6 | 29.8 |
| 25.600 | 20.2 | 13.7 | 9.2 | 6.1 | 3.9 | 2.5 | 1.4 |
| 27.000 | 0.9 | 0.0 | | | | | |

STORM 50_yr_sm

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| DA4 | 0.450 | | 4.512 | | 12.75 | 526.7 | 1170.14 |

Line

| Start Time (hr) | Flow values @ time increment of 0.200 hr | | | | | | |
|-----------------|--|-------|-------|-------|-------|-------|-------|
| | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) |
| 6.800 | 0.0 | 1.0 | 1.9 | 3.2 | 4.5 | 6.0 | 7.5 |

| Eccelston POI 1-4 Existing.out | | | | | | | |
|--------------------------------|-------|-------|-------|-------|-------|-------|-------|
| 8.200 | 8.9 | 10.4 | 11.8 | 13.2 | 14.5 | 16.0 | 18.2 |
| 9.600 | 21.4 | 25.0 | 28.6 | 31.7 | 34.4 | 36.8 | 38.8 |
| 11.000 | 40.4 | 42.9 | 49.1 | 61.6 | 82.8 | 127.3 | 226.8 |
| 12.400 | 378.3 | 499.3 | 522.8 | 466.8 | 374.3 | 292.6 | 226.9 |
| 13.800 | 177.5 | 142.6 | 120.3 | 107.0 | 98.9 | 93.8 | 90.5 |
| 15.200 | 87.9 | 83.9 | 78.0 | 71.9 | 66.9 | 63.6 | 61.6 |
| 16.600 | 60.3 | 59.6 | 59.2 | 59.0 | 58.8 | 58.8 | 58.8 |
| 18.000 | 58.9 | 58.2 | 55.2 | 49.2 | 42.4 | 36.5 | 32.5 |

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Eccelston Mitigation POI 1-4 Existing

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|------------|------------|------------|------------|------------|
| 19.400 | 30.1 | 28.5 | 27.5 | 26.9 | 26.5 | 26.3 | 26.1 |
| 20.800 | 26.0 | 25.9 | 25.9 | 25.9 | 25.9 | 26.0 | 26.0 |
| 22.200 | 26.0 | 26.0 | 26.0 | 26.1 | 26.1 | 26.1 | 26.1 |
| 23.600 | 26.1 | 26.1 | 26.1 | 25.6 | 23.2 | 18.5 | 13.1 |
| 25.000 | 8.4 | 5.3 | 3.3 | 2.1 | 1.3 | 0.8 | 0.5 |
| 26.400 | 0.0 | | | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| DA2 | 1.323 | | 4.181 | | 12.91 | 1269.6 | 959.64 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|------------|------------|------------|------------|------------|
| 7.200 | 0.0 | 1.1 | 2.6 | 4.8 | 7.6 | 10.9 | 14.4 |
| 8.600 | 18.1 | 21.7 | 25.4 | 29.4 | 34.3 | 40.8 | 48.7 |
| 10.000 | 57.2 | 65.7 | 73.6 | 80.8 | 87.2 | 92.9 | 99.6 |
| 11.400 | 111.6 | 134.5 | 176.2 | 261.8 | 446.1 | 740.1 | 1054.6 |
| 12.800 | 1239.4 | 1255.6 | 1137.3 | 950.2 | 767.2 | 618.8 | 504.2 |
| 14.200 | 419.4 | 360.7 | 322.1 | 296.1 | 278.5 | 265.5 | 253.2 |
| 15.600 | 238.5 | 222.0 | 206.1 | 192.4 | 182.6 | 176.7 | 172.9 |
| 17.000 | 170.4 | 168.9 | 168.0 | 167.5 | 167.2 | 167.1 | 165.8 |
| 18.400 | 160.7 | 149.5 | 134.2 | 118.3 | 104.7 | 94.6 | 87.9 |
| 19.800 | 83.4 | 80.3 | 78.1 | 76.7 | 75.7 | 75.0 | 74.5 |
| 21.200 | 74.2 | 74.0 | 73.9 | 73.9 | 73.9 | 73.9 | 74.0 |
| 22.600 | 74.0 | 74.1 | 74.1 | 74.2 | 74.2 | 74.3 | 74.3 |
| 24.000 | 74.4 | 73.3 | 69.3 | 60.4 | 48.3 | 35.7 | 24.9 |
| 25.400 | 16.9 | 11.6 | 8.0 | 5.4 | 3.7 | 2.5 | 1.7 |
| 26.800 | 1.1 | 0.8 | 0.0 | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| DA3 | 0.920 | | 3.637 | | 12.88 | 812.6 | 883.04 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|------------|------------|------------|------------|------------|
| 8.200 | 0.2 | 1.3 | 2.5 | 4.1 | 6.0 | 8.2 | 11.0 |
| 9.600 | 14.7 | 19.1 | 23.9 | 28.7 | 33.2 | 37.5 | 41.6 |
| 11.000 | 45.1 | 49.5 | 57.8 | 73.6 | 101.1 | 159.2 | 294.9 |

| Eccelston POI 1-4 Existing.out | | | | | | | |
|--------------------------------|-------|-------|-------|-------|-------|-------|-------|
| 12.400 | 509.9 | 717.3 | 811.1 | 778.8 | 668.2 | 538.9 | 429.1 |
| 13.800 | 341.9 | 277.7 | 232.8 | 204.6 | 186.8 | 175.4 | 167.9 |
| 15.200 | 162.4 | 155.9 | 146.3 | 135.3 | 125.6 | 118.5 | 114.1 |
| 16.600 | 111.4 | 109.7 | 108.8 | 108.2 | 108.0 | 107.9 | 107.9 |
| 18.000 | 108.0 | 107.2 | 102.8 | 93.9 | 82.4 | 71.7 | 63.3 |
| 19.400 | 57.9 | 54.5 | 52.2 | 50.7 | 49.7 | 49.1 | 48.7 |

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Eccelston Mitigation POI 1-4 Existing

| Line Start Time (hr) | Flow values @ time increment of 0.200 hr | | | | | | |
|----------------------|--|-------|-------|-------|-------|-------|-------|
| (hr) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) |
| 20.800 | 48.4 | 48.2 | 48.1 | 48.0 | 48.1 | 48.1 | 48.2 |
| 22.200 | 48.2 | 48.3 | 48.3 | 48.4 | 48.4 | 48.5 | 48.5 |
| 23.600 | 48.5 | 48.6 | 48.6 | 47.8 | 44.4 | 37.1 | 27.9 |
| 25.000 | 19.3 | 12.5 | 8.2 | 5.4 | 3.6 | 2.3 | 1.5 |
| 26.400 | 1.0 | 0.6 | 0.0 | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| CON-1 | 2.693 | Upstream | 4.050 | 365.26 | 12.82 | 2584.3 | 959.50 |

| Line Start Time (hr) | Flow values @ time increment of 0.200 hr | | | | | | |
|----------------------|--|--------|--------|--------|--------|--------|--------|
| (hr) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) |
| 6.800 | 0.0 | 1.0 | 1.9 | 4.3 | 7.1 | 10.8 | 15.1 |
| 8.200 | 20.1 | 26.1 | 32.3 | 39.0 | 46.0 | 53.6 | 63.5 |
| 9.600 | 76.9 | 92.9 | 109.7 | 126.0 | 141.2 | 155.1 | 167.6 |
| 11.000 | 178.5 | 192.0 | 218.6 | 269.8 | 361.1 | 550.2 | 970.5 |
| 12.400 | 1628.2 | 2269.9 | 2569.8 | 2496.6 | 2179.5 | 1782.0 | 1423.6 |
| 13.800 | 1139.0 | 924.7 | 773.6 | 672.4 | 607.9 | 565.3 | 537.2 |
| 15.200 | 515.7 | 492.9 | 462.8 | 429.3 | 398.6 | 374.5 | 358.2 |
| 16.600 | 348.5 | 342.3 | 338.5 | 336.1 | 334.8 | 334.1 | 334.0 |
| 18.000 | 334.0 | 331.0 | 318.8 | 292.6 | 259.0 | 226.6 | 200.6 |
| 19.400 | 182.6 | 170.9 | 163.1 | 157.9 | 154.4 | 152.0 | 150.5 |
| 20.800 | 149.4 | 148.6 | 148.2 | 148.0 | 147.9 | 148.0 | 148.0 |
| 22.200 | 148.1 | 148.3 | 148.4 | 148.5 | 148.6 | 148.7 | 148.8 |
| 23.600 | 148.9 | 149.0 | 149.1 | 146.6 | 136.8 | 116.0 | 89.3 |
| 25.000 | 63.5 | 42.8 | 28.5 | 19.1 | 12.8 | 8.6 | 5.8 |
| 26.400 | 3.5 | 2.3 | 1.2 | 0.8 | 0.0 | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| CON-1 | 2.693 | Downstream | 4.050 | 365.20 | 12.96 | 2482.1 | 921.56 |

| Line Start Time (hr) | Flow values @ time increment of 0.200 hr | | | | | | |
|----------------------|--|--------|--------|--------|--------|--------|--------|
| (hr) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) |
| 7.000 | 0.0 | 1.2 | 3.1 | 5.7 | 8.9 | 12.9 | 17.5 |
| 8.400 | 23.0 | 29.0 | 35.5 | 42.2 | 49.5 | 58.4 | 70.2 |
| 9.800 | 84.7 | 100.8 | 117.1 | 132.8 | 147.3 | 160.5 | 172.2 |
| 11.200 | 184.7 | 205.7 | 245.5 | 317.4 | 460.0 | 774.5 | 1312.4 |
| 12.600 | 1938.3 | 2367.1 | 2472.9 | 2298.3 | 1969.4 | 1614.5 | 1302.8 |
| 14.000 | 1053.7 | 868.2 | 738.0 | 651.4 | 594.2 | 556.3 | 529.6 |

| Eccelston POI 1-4 Existing.out | | | | | | | |
|--------------------------------|-------|-------|-------|-------|-------|-------|-------|
| 15.400 | 506.0 | 478.4 | 446.7 | 415.4 | 388.5 | 368.4 | 355.1 |
| 16.800 | 346.6 | 341.2 | 337.8 | 335.8 | 334.7 | 334.2 | 334.1 |
| 18.200 | 332.3 | 324.2 | 304.7 | 275.5 | 243.8 | 215.4 | 193.7 |
| 19.600 | 178.5 | 168.3 | 161.4 | 156.7 | 153.6 | 151.5 | 150.1 |

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Eccelston Mitigation POI 1-4 Existing

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | values @ time (cfs) | increment (cfs) | of (cfs) | 0.200 hr (cfs) | (cfs) |
|----------------------|------------|------------|---------------------|-----------------|----------|----------------|-------|
| 21.000 | 149.1 | 148.5 | 148.1 | 148.0 | 148.0 | 148.0 | 148.1 |
| 22.400 | 148.2 | 148.3 | 148.5 | 148.6 | 148.7 | 148.8 | 148.9 |
| 23.800 | 149.0 | 149.0 | 147.7 | 141.2 | 125.6 | 102.4 | 77.1 |
| 25.200 | 54.6 | 37.3 | 25.2 | 17.0 | 11.4 | 7.7 | 4.9 |
| 26.600 | 3.2 | 1.9 | 1.1 | 0.7 | 0.0 | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| DA1 | 0.090 | | 4.511 | | 12.18 | 209.2 | 2323.11 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | values @ time (cfs) | increment (cfs) | of (cfs) | 0.200 hr (cfs) | (cfs) |
|----------------------|------------|------------|---------------------|-----------------|----------|----------------|-------|
| 6.600 | 0.0 | 0.6 | 1.0 | 1.3 | 1.6 | 1.9 | 2.2 |
| 8.000 | 2.5 | 2.8 | 3.0 | 3.3 | 3.5 | 3.8 | 5.1 |
| 9.400 | 6.3 | 6.8 | 7.3 | 7.7 | 8.1 | 8.4 | 8.7 |
| 10.800 | 8.6 | 8.8 | 15.4 | 20.5 | 25.5 | 47.9 | 106.9 |
| 12.200 | 208.2 | 123.0 | 71.5 | 40.0 | 34.5 | 23.5 | 16.6 |
| 13.600 | 15.9 | 16.6 | 16.8 | 16.9 | 16.9 | 17.0 | 17.0 |
| 15.000 | 17.1 | 14.0 | 11.9 | 11.7 | 11.7 | 11.6 | 11.6 |
| 16.400 | 11.7 | 11.8 | 11.7 | 11.7 | 11.8 | 11.8 | 11.7 |
| 17.800 | 11.8 | 11.8 | 8.1 | 5.5 | 5.2 | 5.2 | 5.1 |
| 19.200 | 5.2 | 5.2 | 5.1 | 5.2 | 5.2 | 5.1 | 5.2 |
| 20.600 | 5.2 | 5.2 | 5.1 | 5.2 | 5.2 | 5.2 | 5.2 |
| 22.000 | 5.2 | 5.2 | 5.3 | 5.2 | 5.2 | 5.3 | 5.2 |
| 23.400 | 5.2 | 5.3 | 5.3 | 5.2 | 2.3 | 0.0 | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| OUTLET | 2.783 | | 4.065 | | 12.97 | 2514.9 | 903.53 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | values @ time (cfs) | increment (cfs) | of (cfs) | 0.200 hr (cfs) | (cfs) |
|----------------------|------------|------------|---------------------|-----------------|----------|----------------|--------|
| 6.600 | 0.0 | 0.6 | 1.0 | 2.4 | 4.7 | 7.6 | 11.1 |
| 8.000 | 15.4 | 20.2 | 26.0 | 32.3 | 39.0 | 46.0 | 54.7 |
| 9.400 | 64.7 | 77.0 | 92.0 | 108.5 | 125.2 | 141.2 | 156.0 |
| 10.800 | 169.1 | 181.1 | 200.1 | 226.1 | 271.0 | 365.3 | 566.9 |
| 12.200 | 982.9 | 1435.5 | 2009.5 | 2407.1 | 2507.3 | 2321.7 | 1985.8 |
| 13.600 | 1630.4 | 1319.3 | 1070.5 | 885.1 | 754.9 | 668.4 | 611.2 |
| 15.000 | 573.4 | 543.6 | 517.9 | 490.1 | 458.4 | 427.0 | 400.1 |
| 16.400 | 380.1 | 366.9 | 358.2 | 352.9 | 349.5 | 347.6 | 346.4 |
| 17.800 | 346.0 | 345.9 | 340.4 | 329.7 | 309.9 | 280.7 | 248.9 |
| 19.200 | 220.6 | 198.9 | 183.7 | 173.5 | 166.6 | 161.9 | 158.8 |

| Eccelston POI 1-4 Existing.out | | | | | | | |
|--------------------------------|-------|-------|-------|-------|-------|-------|-------|
| 20.600 | 156.7 | 155.3 | 154.3 | 153.7 | 153.3 | 153.1 | 153.2 |
| 22.000 | 153.2 | 153.3 | 153.5 | 153.6 | 153.6 | 153.8 | 153.9 |

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Eccelston Mitigation POI 1-4 Existing

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|---------------------|-----------------|-------------------|------------|------------|
| 23.400 | 154.0 | 154.1 | 154.2 | 154.2 | 150.0 | 141.2 | 125.6 |
| 24.800 | 102.4 | 77.2 | 54.6 | 37.3 | 25.2 | 17.0 | 11.4 |
| 26.200 | 7.7 | 4.9 | 3.2 | 1.9 | 1.1 | 0.7 | 0.0 |

STORM 100_yr_sm

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| DA4 | 0.450 | | 5.658 | | 12.72 | 622.1 | 1382.12 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|---------------------|-----------------|-------------------|------------|------------|
| 6.200 | 0.3 | 1.1 | 2.2 | 3.9 | 5.9 | 8.0 | 10.1 |
| 7.600 | 12.2 | 14.3 | 16.3 | 18.3 | 20.1 | 21.9 | 23.7 |
| 9.000 | 25.3 | 27.2 | 30.2 | 34.5 | 39.4 | 44.1 | 48.1 |
| 10.400 | 51.4 | 54.3 | 56.6 | 58.2 | 60.9 | 69.0 | 85.6 |
| 11.800 | 113.1 | 168.3 | 285.8 | 457.6 | 592.4 | 618.7 | 552.5 |
| 13.200 | 446.0 | 351.2 | 273.6 | 214.3 | 172.6 | 146.3 | 130.7 |
| 14.600 | 121.1 | 115.1 | 111.3 | 108.2 | 103.5 | 96.6 | 89.4 |
| 16.000 | 83.5 | 79.6 | 77.2 | 75.8 | 75.0 | 74.5 | 74.2 |
| 17.400 | 74.0 | 74.0 | 74.0 | 74.0 | 73.2 | 69.4 | 61.9 |
| 18.800 | 53.3 | 45.9 | 40.9 | 37.8 | 35.8 | 34.6 | 33.9 |
| 20.200 | 33.4 | 33.1 | 32.9 | 32.8 | 32.7 | 32.7 | 32.7 |
| 21.600 | 32.7 | 32.7 | 32.7 | 32.8 | 32.8 | 32.8 | 32.8 |
| 23.000 | 32.8 | 32.8 | 32.8 | 32.8 | 32.8 | 32.9 | 32.2 |
| 24.400 | 29.2 | 23.2 | 16.4 | 10.5 | 6.6 | 4.2 | 2.6 |
| 25.800 | 1.7 | 1.0 | 0.6 | 0.0 | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| DA2 | 1.323 | | 5.296 | | 12.90 | 1526.6 | 1153.92 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|---------------------|-----------------|-------------------|------------|------------|
| 6.600 | 0.4 | 1.7 | 4.0 | 7.4 | 11.6 | 16.4 | 21.5 |
| 8.000 | 26.8 | 32.1 | 37.4 | 42.5 | 47.6 | 52.5 | 57.7 |
| 9.400 | 64.4 | 73.4 | 84.6 | 96.3 | 107.7 | 118.0 | 127.0 |
| 10.800 | 134.8 | 141.2 | 148.9 | 164.3 | 194.9 | 250.7 | 359.5 |
| 12.200 | 581.9 | 926.8 | 1287.1 | 1495.7 | 1507.4 | 1366.7 | 1146.7 |
| 13.600 | 930.5 | 753.1 | 614.9 | 512.7 | 442.3 | 396.1 | 365.2 |
| 15.000 | 344.2 | 328.7 | 314.0 | 296.5 | 276.9 | 257.9 | 241.7 |
| 16.400 | 230.1 | 223.1 | 218.6 | 215.7 | 213.8 | 212.7 | 212.0 |
| 17.800 | 211.7 | 211.6 | 210.0 | 203.5 | 189.3 | 169.9 | 149.8 |
| 19.200 | 132.6 | 119.8 | 111.3 | 105.7 | 101.7 | 99.0 | 97.1 |

Eccelston POI 1-4 Existing.out

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Eccelston Mitigation POI 1-4 Existing

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | values @ time (cfs) | increment (cfs) | of (cfs) | 0.200 hr (cfs) | Flow (cfs) |
|----------------------|------------|------------|---------------------|-----------------|----------|----------------|------------|
| 20.600 | 95.9 | 95.1 | 94.5 | 94.1 | 93.9 | 93.8 | 93.6 |
| 22.000 | 93.6 | 93.7 | 93.8 | 93.8 | 93.8 | 93.9 | 93.9 |
| 23.400 | 93.9 | 94.0 | 94.0 | 94.1 | 92.8 | 87.6 | 76.4 |
| 24.800 | 61.0 | 45.2 | 31.5 | 21.3 | 14.6 | 10.1 | 6.9 |
| 26.200 | 4.7 | 3.2 | 2.2 | 1.4 | 1.0 | 0.6 | 0.0 |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| DA3 | 0.920 | | 4.691 | | 12.80 | 998.8 | 1085.30 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | values @ time (cfs) | increment (cfs) | of (cfs) | 0.200 hr (cfs) | Flow (cfs) |
|----------------------|------------|------------|---------------------|-----------------|----------|----------------|------------|
| 7.200 | 0.0 | 0.6 | 1.7 | 3.4 | 5.8 | 8.5 | 11.5 |
| 8.600 | 14.5 | 17.6 | 20.7 | 24.0 | 28.3 | 34.1 | 40.8 |
| 10.000 | 47.8 | 54.5 | 60.6 | 66.1 | 71.1 | 75.1 | 80.3 |
| 11.400 | 91.3 | 113.8 | 152.0 | 229.1 | 395.9 | 652.3 | 893.3 |
| 12.800 | 997.5 | 954.7 | 820.5 | 665.0 | 531.5 | 424.6 | 345.2 |
| 14.200 | 290.1 | 255.6 | 234.0 | 220.1 | 211.0 | 204.2 | 196.4 |
| 15.600 | 184.8 | 171.5 | 159.8 | 151.2 | 146.0 | 142.7 | 140.7 |
| 17.000 | 139.5 | 138.8 | 138.5 | 138.4 | 138.4 | 138.6 | 137.4 |
| 18.400 | 131.9 | 120.3 | 105.7 | 91.9 | 81.2 | 74.3 | 69.9 |
| 19.800 | 66.9 | 65.0 | 63.7 | 62.9 | 62.4 | 62.1 | 61.9 |
| 21.200 | 61.8 | 61.7 | 61.7 | 61.7 | 61.7 | 61.8 | 61.9 |
| 22.600 | 62.0 | 62.0 | 62.0 | 62.0 | 62.1 | 62.1 | 62.2 |
| 24.000 | 62.2 | 61.1 | 56.8 | 47.4 | 35.7 | 24.7 | 16.0 |
| 25.400 | 10.6 | 7.0 | 4.6 | 3.0 | 1.9 | 1.3 | 0.8 |
| 26.800 | 0.5 | 0.0 | | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| CON-1 | 2.693 | Upstream | 5.150 | 365.63 | 12.87 | 3120.0 | 1158.38 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | values @ time (cfs) | increment (cfs) | of (cfs) | 0.200 hr (cfs) | Flow (cfs) |
|----------------------|------------|------------|---------------------|-----------------|----------|----------------|------------|
| 6.200 | 0.3 | 1.1 | 2.6 | 5.6 | 9.9 | 15.3 | 22.3 |
| 7.600 | 30.3 | 39.3 | 48.9 | 58.9 | 69.0 | 79.0 | 88.9 |
| 9.000 | 98.5 | 109.1 | 122.9 | 142.1 | 164.8 | 188.2 | 210.2 |
| 10.400 | 230.0 | 247.4 | 262.5 | 274.5 | 290.2 | 325.2 | 395.0 |
| 11.800 | 515.8 | 757.1 | 1268.5 | 2036.9 | 2771.2 | 3109.6 | 3011.6 |
| 13.200 | 2632.0 | 2163.5 | 1736.9 | 1392.1 | 1133.1 | 950.0 | 829.2 |
| 14.600 | 751.5 | 700.5 | 666.6 | 641.1 | 613.8 | 577.8 | 537.8 |
| 16.000 | 501.2 | 472.6 | 453.5 | 441.7 | 434.2 | 429.7 | 426.8 |
| 17.400 | 425.2 | 424.4 | 424.2 | 424.2 | 420.4 | 404.6 | 371.4 |
| 18.800 | 328.8 | 287.5 | 254.7 | 232.0 | 217.1 | 207.2 | 200.5 |

Eccelston POI 1-4 Existing.out

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Eccelston Mitigation POI 1-4 Existing

| Line Start Time (hr) | Flow (cfs) | values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow (cfs) | Rate (csm) |
|----------------------|------------|---------------------|-----------------|-------------------|------------|------------|
| 20.200 | 196.1 | 193.1 | 191.2 | 190.0 | 189.1 | 188.6 |
| 21.600 | 188.1 | 188.0 | 188.1 | 188.3 | 188.4 | 188.6 |
| 23.000 | 188.7 | 188.8 | 188.8 | 188.9 | 189.1 | 189.1 |
| 24.400 | 173.3 | 147.0 | 113.1 | 80.4 | 54.2 | 36.1 |
| 25.800 | 16.3 | 10.9 | 7.3 | 4.6 | 3.0 | 1.9 |
| 27.200 | 0.6 | 0.0 | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| CON-1 | 2.693 | Downstream | 5.150 | 365.55 | 12.94 | 3008.1 | 1116.84 |

| Line Start Time (hr) | Flow (cfs) | values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow (cfs) | Rate (csm) |
|----------------------|------------|---------------------|-----------------|-------------------|------------|------------|
| 6.400 | 0.0 | 1.5 | 4.2 | 7.9 | 12.8 | 19.0 |
| 7.800 | 35.0 | 44.2 | 54.0 | 64.0 | 74.0 | 83.9 |
| 9.200 | 103.8 | 116.4 | 133.2 | 154.1 | 176.8 | 199.2 |
| 10.600 | 238.3 | 254.6 | 268.0 | 282.4 | 309.7 | 364.5 |
| 12.000 | 650.2 | 1048.5 | 1696.0 | 2419.9 | 2902.3 | 2994.8 |
| 13.400 | 2367.8 | 1945.1 | 1572.4 | 1275.2 | 1054.7 | 901.0 |
| 14.800 | 731.8 | 687.4 | 656.2 | 628.1 | 595.0 | 557.0 |
| 16.200 | 487.9 | 464.4 | 448.9 | 438.9 | 432.6 | 428.6 |
| 17.600 | 425.0 | 424.4 | 424.3 | 422.0 | 411.1 | 385.5 |
| 19.000 | 307.6 | 271.9 | 244.8 | 226.0 | 213.2 | 204.6 |
| 20.400 | 194.9 | 192.4 | 190.7 | 189.6 | 188.9 | 188.5 |
| 21.800 | 188.1 | 188.1 | 188.2 | 188.4 | 188.5 | 188.5 |
| 23.200 | 188.7 | 188.8 | 188.9 | 189.0 | 189.1 | 187.2 |
| 24.600 | 158.2 | 128.5 | 96.3 | 67.9 | 46.3 | 31.3 |
| 26.000 | 14.1 | 9.5 | 6.2 | 4.0 | 2.5 | 1.4 |
| 27.400 | 0.0 | | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| DA1 | 0.090 | | 5.657 | | 12.19 | 240.2 | 2667.58 |

| Line Start Time (hr) | Flow (cfs) | values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow (cfs) | Rate (csm) |
|----------------------|------------|---------------------|-----------------|-------------------|------------|------------|
| 6.000 | 0.0 | 0.6 | 1.2 | 1.7 | 2.2 | 2.7 |
| 7.400 | 3.5 | 3.8 | 4.2 | 4.6 | 4.9 | 5.3 |
| 8.800 | 5.9 | 6.1 | 8.1 | 9.7 | 10.3 | 10.8 |
| 10.200 | 11.8 | 12.1 | 12.4 | 12.0 | 12.1 | 21.4 |
| 11.600 | 34.4 | 62.2 | 129.6 | 238.7 | 143.5 | 85.7 |
| 13.000 | 42.7 | 29.0 | 20.1 | 19.4 | 20.5 | 20.7 |
| 14.400 | 20.9 | 20.9 | 21.0 | 21.1 | 17.4 | 14.9 |
| 15.800 | 14.6 | 14.7 | 14.7 | 14.6 | 14.8 | 14.7 |

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Eccelston POI 1-4 Existing.out

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|---------------------|-----------------|-------------------|------------|------------|
| 17.200 | 14.8 | 14.8 | 14.8 | 14.9 | 14.9 | 10.1 | 7.1 |
| 18.600 | 6.5 | 6.6 | 6.5 | 6.5 | 6.5 | 6.5 | 6.6 |
| 20.000 | 6.4 | 6.6 | 6.5 | 6.5 | 6.5 | 6.5 | 6.6 |
| 21.400 | 6.5 | 6.6 | 6.5 | 6.6 | 6.6 | 6.5 | 6.6 |
| 22.800 | 6.5 | 6.6 | 6.5 | 6.6 | 6.7 | 6.5 | 6.6 |
| 24.200 | 2.8 | 0.0 | | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| OUTLET | 2.783 | | 5.166 | | 12.94 | 3050.4 | 1095.92 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|---------------------|-----------------|-------------------|------------|------------|
| 6.000 | 0.0 | 0.6 | 1.2 | 3.3 | 6.4 | 10.6 | 15.9 |
| 7.400 | 22.5 | 30.3 | 39.2 | 48.8 | 58.9 | 69.2 | 79.5 |
| 8.800 | 89.8 | 99.8 | 111.9 | 126.0 | 143.5 | 165.0 | 188.2 |
| 10.200 | 211.0 | 231.9 | 250.7 | 266.5 | 280.1 | 303.7 | 337.9 |
| 11.600 | 398.9 | 524.7 | 779.9 | 1287.4 | 1839.7 | 2505.8 | 2951.4 |
| 13.000 | 3037.6 | 2794.5 | 2387.8 | 1964.4 | 1592.8 | 1295.9 | 1075.5 |
| 14.400 | 921.9 | 820.0 | 752.8 | 708.5 | 673.6 | 643.0 | 609.6 |
| 15.800 | 571.6 | 534.2 | 502.5 | 479.0 | 463.7 | 453.5 | 447.4 |
| 17.200 | 443.4 | 441.1 | 439.8 | 439.3 | 439.1 | 432.0 | 418.2 |
| 18.600 | 392.0 | 354.7 | 314.1 | 278.4 | 251.3 | 232.5 | 219.8 |
| 20.000 | 211.0 | 205.4 | 201.5 | 198.9 | 197.2 | 196.1 | 195.5 |
| 21.400 | 194.9 | 194.9 | 194.6 | 194.6 | 194.8 | 194.8 | 195.1 |
| 22.800 | 195.1 | 195.2 | 195.2 | 195.4 | 195.5 | 195.5 | 195.7 |
| 24.200 | 190.1 | 178.7 | 158.2 | 128.5 | 96.4 | 68.0 | 46.3 |
| 25.600 | 31.3 | 21.1 | 14.1 | 9.5 | 6.2 | 4.0 | 2.6 |
| 27.000 | 1.4 | 0.9 | 0.0 | | | | |

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| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| DA4 | 0.450 | | 9.089 | | 12.71 | 853.7 | 1896.50 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|---------------------|-----------------|-------------------|------------|------------|
| 4.000 | 0.0 | 0.7 | 1.4 | 2.3 | 3.3 | 4.4 | 5.4 |
| 5.400 | 6.5 | 7.5 | 8.5 | 9.5 | 10.9 | 13.7 | 18.5 |
| 6.800 | 24.3 | 30.3 | 35.6 | 40.3 | 44.5 | 48.3 | 51.7 |
| 8.200 | 54.9 | 57.9 | 60.6 | 63.3 | 65.7 | 68.6 | 73.4 |
| 9.600 | 80.8 | 89.1 | 96.7 | 102.8 | 107.6 | 111.5 | 114.2 |
| 11.000 | 115.1 | 117.8 | 131.2 | 160.4 | 206.9 | 288.7 | 444.1 |

| Start Time (hr) | Eccelston POI 1-4 Existing.out | | | | | | Flow Values @ time increment of 0.200 hr | |
|--------------------|--------------------------------|-------|-------|-------|-------|-------|--|-------|
| | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) |
| 12.400 | 658.1 | 819.9 | 848.0 | 764.7 | 629.7 | 506.1 | 399.9 | |
| 13.800 | 316.4 | 256.8 | 219.9 | 198.7 | 185.6 | 177.3 | 172.1 | |
| 15.200 | 167.8 | 161.4 | 152.0 | 142.4 | 134.3 | 129.0 | 125.8 | |
| 16.600 | 123.9 | 122.7 | 122.1 | 121.7 | 121.7 | 121.7 | 121.6 | |
| 18.000 | 121.5 | 120.0 | 113.7 | 101.3 | 87.2 | 75.1 | 66.9 | |
| 19.400 | 61.9 | 58.7 | 56.7 | 55.4 | 54.6 | 54.1 | 53.8 | |
| 20.800 | 53.6 | 53.4 | 53.4 | 53.4 | 53.4 | 53.4 | 53.4 | |
| 22.200 | 53.4 | 53.4 | 53.4 | 53.4 | 53.5 | 53.5 | 53.6 | |
| 23.600 | 53.5 | 53.5 | 53.5 | 52.4 | 47.5 | 37.9 | 26.8 | |
| 25.000 | 17.2 | 10.7 | 6.8 | 4.3 | 2.7 | 1.7 | 1.0 | |
| 26.400 | 0.6 | 0.0 | | | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| DA2 | 1.323 | | 8.661 | | 12.88 | 2165.1 | 1636.52 |

| Line Start Time (hr) | Flow values @ time increment of 0.200 hr | | | | | | Flow Values @ time increment of 0.200 hr | |
|-------------------------|--|--------|--------|--------|--------|--------|--|-------|
| | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) |
| 4.600 | 0.5 | 1.4 | 2.7 | 4.6 | 6.8 | 9.2 | 11.8 | |
| 6.000 | 14.5 | 17.7 | 22.7 | 30.9 | 42.2 | 55.1 | 68.5 | |
| 7.400 | 81.5 | 93.5 | 104.8 | 115.3 | 125.2 | 134.5 | 143.3 | |
| 8.800 | 151.7 | 159.6 | 168.2 | 179.4 | 195.4 | 215.0 | 235.2 | |
| 10.200 | 254.2 | 270.5 | 284.0 | 294.6 | 301.8 | 311.1 | 335.1 | |
| 11.600 | 390.0 | 486.0 | 653.8 | 970.6 | 1421.9 | 1878.6 | 2132.8 | |
| 13.000 | 2135.7 | 1950.5 | 1658.5 | 1366.9 | 1117.0 | 918.8 | 773.5 | |
| 14.400 | 673.1 | 607.6 | 564.4 | 535.0 | 512.9 | 492.3 | 467.9 | |
| 15.800 | 440.9 | 414.8 | 392.7 | 376.9 | 367.1 | 360.8 | 356.7 | |
| 17.200 | 354.2 | 353.0 | 352.3 | 351.8 | 351.5 | 348.4 | 337.3 | |
| 18.600 | 313.7 | 281.3 | 248.0 | 219.4 | 198.0 | 184.2 | 174.7 | |
| 20.000 | 168.1 | 163.6 | 160.5 | 158.5 | 157.0 | 156.0 | 155.4 | |
| 21.400 | 155.1 | 154.8 | 154.7 | 154.6 | 154.5 | 154.5 | 154.5 | |
| 22.800 | 154.6 | 154.7 | 154.8 | 154.9 | 155.0 | 155.0 | 154.9 | |
| 24.200 | 152.8 | 144.3 | 126.0 | 100.5 | 74.3 | 51.7 | 34.9 | |
| 25.600 | 24.0 | 16.5 | 11.3 | 7.7 | 5.2 | 3.5 | 2.4 | |
| 27.000 | 1.6 | 1.0 | 0.6 | 0.0 | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| DA3 | 0.920 | | 7.928 | | 12.83 | 1471.9 | 1599.37 |

| Line Start Time (hr) | Flow values @ time increment of 0.200 hr | | | | | | Flow Values @ time increment of 0.200 hr | |
|-------------------------|--|-------|-------|-------|-------|-------|--|-------|
| | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) |
| 5.600 | 0.0 | 0.7 | 1.5 | 2.8 | 5.1 | 9.2 | 14.7 | |
| 7.000 | 21.4 | 28.5 | 35.7 | 42.8 | 49.7 | 56.3 | 62.7 | |

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Eccelston Mitigation POI 1-4 Existing

| Line Start Time (hr) | Flow values @ time increment of 0.200 hr | | | | | | Flow Values @ time increment of 0.200 hr | |
|-------------------------|--|-------|-------|-------|-------|-------|--|-------|
| | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) |

Eccelston POI 1-4 Existing.out

| | | | | | | | |
|--------|--------|--------|--------|--------|--------|-------|--------|
| 8.400 | 68.8 | 74.7 | 80.3 | 85.7 | 91.6 | 99.6 | 111.0 |
| 9.800 | 124.2 | 137.4 | 149.3 | 159.4 | 168.0 | 174.8 | 179.3 |
| 11.200 | 185.8 | 205.4 | 247.7 | 318.3 | 445.5 | 684.0 | 1029.0 |
| 12.600 | 1344.5 | 1467.2 | 1406.1 | 1220.0 | 1005.4 | 813.7 | 655.2 |
| 14.000 | 535.8 | 453.9 | 402.9 | 371.9 | 351.5 | 338.1 | 328.1 |
| 15.400 | 316.6 | 300.2 | 281.5 | 265.2 | 253.0 | 245.7 | 241.0 |
| 16.800 | 238.1 | 236.5 | 235.6 | 235.4 | 235.3 | 235.3 | 235.2 |
| 18.200 | 232.8 | 223.6 | 203.5 | 178.7 | 155.4 | 137.3 | 125.6 |
| 19.600 | 118.0 | 113.0 | 109.7 | 107.5 | 106.1 | 105.3 | 104.7 |
| 21.000 | 104.3 | 104.1 | 104.0 | 104.0 | 104.0 | 104.0 | 104.0 |
| 22.400 | 104.1 | 104.1 | 104.1 | 104.2 | 104.3 | 104.4 | 104.5 |
| 23.800 | 104.5 | 104.4 | 102.7 | 95.1 | 79.6 | 59.9 | 41.4 |
| 25.200 | 27.0 | 17.7 | 11.7 | 7.7 | 5.0 | 3.3 | 2.1 |
| 26.600 | 1.4 | 0.8 | 0.5 | 0.0 | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| CON-1 | 2.693 | Upstream | 8.482 | 366.39 | 12.85 | 4458.7 | 1655.42 |

Line Start Time (hr) ----- Flow values @ time increment of 0.200 hr -----

| Start Time (hr) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|-----------------|------------|------------|------------|------------|------------|------------|------------|
| 4.000 | 0.0 | 0.7 | 1.4 | 2.8 | 4.7 | 7.1 | 10.0 |
| 5.400 | 13.3 | 16.7 | 21.1 | 25.5 | 31.5 | 41.6 | 58.6 |
| 6.800 | 81.3 | 106.8 | 132.7 | 157.5 | 180.8 | 202.7 | 223.4 |
| 8.200 | 242.8 | 261.2 | 278.6 | 295.2 | 311.1 | 328.4 | 352.7 |
| 9.600 | 387.2 | 428.3 | 469.4 | 506.3 | 537.5 | 563.4 | 583.5 |
| 11.000 | 596.1 | 614.9 | 672.8 | 798.6 | 1013.1 | 1389.4 | 2101.5 |
| 12.400 | 3109.1 | 4030.9 | 4443.1 | 4306.2 | 3800.2 | 3171.1 | 2581.4 |
| 13.800 | 2089.2 | 1712.3 | 1448.1 | 1275.3 | 1165.6 | 1093.5 | 1045.2 |
| 15.200 | 1008.8 | 970.2 | 920.1 | 864.9 | 814.3 | 774.8 | 748.4 |
| 16.600 | 732.1 | 721.7 | 715.2 | 711.6 | 710.0 | 709.3 | 708.7 |
| 18.000 | 708.1 | 701.2 | 674.3 | 618.4 | 547.3 | 478.6 | 423.5 |
| 19.400 | 385.7 | 361.0 | 344.5 | 333.2 | 325.7 | 320.7 | 317.5 |
| 20.800 | 315.2 | 313.7 | 312.9 | 312.4 | 312.3 | 312.1 | 311.9 |
| 22.200 | 311.9 | 312.1 | 312.1 | 312.2 | 312.4 | 312.6 | 312.9 |
| 23.600 | 313.0 | 313.0 | 312.9 | 308.0 | 286.9 | 243.2 | 187.2 |
| 25.000 | 133.0 | 89.5 | 59.6 | 40.1 | 26.9 | 18.0 | 12.0 |
| 26.400 | 8.0 | 5.1 | 3.2 | 2.0 | 1.0 | 0.6 | 0.0 |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| CON-1 | 2.693 | Downstream | 8.482 | 366.32 | 12.92 | 4326.3 | 1606.27 |

Eccelston Mitigation POI 1-4 Existing

Line Start Time (hr) ----- Flow values @ time increment of 0.200 hr -----

| Start Time (hr) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|-----------------|------------|------------|------------|------------|------------|------------|------------|
| 4.200 | 0.0 | 0.8 | 2.1 | 3.9 | 6.1 | 8.8 | 11.9 |

Eccelston POI 1-4 Existing.out

| | | | | | | | |
|--------|--------|--------|--------|--------|--------|--------|--------|
| 5.600 | 15.3 | 19.3 | 23.6 | 29.0 | 37.6 | 52.1 | 72.4 |
| 7.000 | 96.4 | 121.8 | 146.8 | 170.6 | 193.1 | 214.3 | 234.3 |
| 8.400 | 253.1 | 271.0 | 288.0 | 304.2 | 321.0 | 342.9 | 373.6 |
| 9.800 | 411.8 | 452.1 | 490.1 | 523.4 | 551.5 | 574.1 | 589.7 |
| 11.200 | 606.7 | 651.4 | 752.1 | 931.7 | 1244.3 | 1834.3 | 2720.6 |
| 12.600 | 3646.6 | 4220.7 | 4295.2 | 3956.2 | 3407.5 | 2827.8 | 2308.2 |
| 14.000 | 1887.7 | 1577.4 | 1363.9 | 1223.8 | 1131.7 | 1070.6 | 1027.2 |
| 15.400 | 987.6 | 940.6 | 887.7 | 836.1 | 792.9 | 761.5 | 740.7 |
| 16.800 | 727.3 | 718.7 | 713.7 | 711.1 | 709.8 | 709.0 | 708.4 |
| 18.200 | 703.7 | 683.8 | 638.8 | 575.0 | 507.3 | 448.3 | 404.1 |
| 19.600 | 373.6 | 353.0 | 339.0 | 329.6 | 323.3 | 319.2 | 316.4 |
| 21.000 | 314.5 | 313.4 | 312.7 | 312.4 | 312.2 | 312.0 | 311.9 |
| 22.400 | 312.0 | 312.1 | 312.1 | 312.3 | 312.5 | 312.8 | 312.9 |
| 23.800 | 313.0 | 312.9 | 309.7 | 294.4 | 259.1 | 209.0 | 155.6 |
| 25.200 | 109.0 | 74.1 | 50.1 | 33.7 | 22.6 | 15.1 | 10.1 |
| 26.600 | 6.6 | 4.2 | 2.7 | 1.5 | 0.9 | 0.0 | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| DA1 | 0.090 | | 9.087 | | 12.18 | 308.6 | 3427.49 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|------------|------------|------------|------------|------------|
| 4.000 | 0.0 | 0.7 | 0.9 | 1.1 | 1.4 | 1.6 | 1.8 |
| 5.400 | 2.0 | 2.2 | 2.4 | 2.6 | 4.9 | 6.9 | 7.9 |
| 6.800 | 8.7 | 9.4 | 10.2 | 10.8 | 11.4 | 11.9 | 12.4 |
| 8.200 | 12.9 | 13.4 | 13.9 | 14.3 | 14.7 | 18.2 | 21.0 |
| 9.600 | 21.8 | 22.4 | 23.0 | 23.5 | 24.0 | 24.0 | 22.4 |
| 11.000 | 22.3 | 39.9 | 52.3 | 61.7 | 101.6 | 184.0 | 306.4 |
| 12.400 | 192.8 | 123.0 | 75.6 | 67.2 | 44.9 | 30.7 | 29.4 |
| 13.800 | 31.7 | 32.6 | 32.5 | 32.8 | 32.6 | 32.7 | 32.8 |
| 15.200 | 27.8 | 24.5 | 24.1 | 24.1 | 24.1 | 24.1 | 24.1 |
| 16.600 | 24.2 | 24.2 | 24.3 | 24.4 | 24.3 | 24.3 | 24.3 |
| 18.000 | 24.3 | 16.4 | 11.5 | 10.6 | 10.8 | 10.5 | 10.7 |
| 19.400 | 10.6 | 10.7 | 10.7 | 10.5 | 10.8 | 10.6 | 10.7 |
| 20.800 | 10.7 | 10.7 | 10.7 | 10.8 | 10.7 | 10.6 | 10.8 |
| 22.200 | 10.6 | 10.7 | 10.7 | 10.8 | 10.7 | 10.8 | 10.7 |
| 23.600 | 10.6 | 10.8 | 10.6 | 4.7 | 0.6 | 0.0 | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| OUTLET | 2.783 | | 8.502 | | 12.92 | 4394.6 | 1578.84 |

Eccelston Mitigation POI 1-4 Existing

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|------------|------------|------------|------------|------------|
| 4.000 | 0.0 | 0.7 | 1.7 | 3.3 | 5.3 | 7.7 | 10.6 |
| 5.400 | 13.9 | 17.5 | 21.7 | 26.2 | 33.9 | 44.6 | 60.0 |
| 6.800 | 81.1 | 105.8 | 132.0 | 157.5 | 182.0 | 205.0 | 226.7 |

| Eccelston POI 1-4 Existing.out | | | | | | | |
|--------------------------------|--------|--------|--------|--------|--------|--------|--------|
| 8.200 | 247.2 | 266.5 | 284.8 | 302.3 | 318.8 | 339.2 | 364.0 |
| 9.600 | 395.4 | 434.2 | 475.2 | 513.6 | 547.4 | 575.6 | 596.5 |
| 11.000 | 612.0 | 646.6 | 703.7 | 813.8 | 1033.3 | 1429.4 | 2140.8 |
| 12.400 | 2913.4 | 3769.7 | 4296.3 | 4360.7 | 4001.0 | 3438.2 | 2857.1 |
| 13.800 | 2339.8 | 1920.6 | 1609.8 | 1396.6 | 1256.4 | 1164.4 | 1103.4 |
| 15.200 | 1055.0 | 1012.1 | 964.7 | 911.7 | 860.2 | 817.0 | 785.6 |
| 16.600 | 764.9 | 751.5 | 743.0 | 738.1 | 735.4 | 734.1 | 733.3 |
| 18.000 | 732.7 | 720.0 | 695.4 | 649.4 | 585.8 | 517.9 | 459.0 |
| 19.400 | 414.7 | 384.4 | 363.7 | 349.6 | 340.4 | 333.9 | 329.9 |
| 20.800 | 327.0 | 325.3 | 324.0 | 323.5 | 323.1 | 322.7 | 322.8 |
| 22.200 | 322.5 | 322.7 | 322.8 | 322.9 | 323.0 | 323.3 | 323.5 |
| 23.600 | 323.5 | 323.8 | 323.5 | 314.4 | 295.0 | 259.2 | 209.0 |
| 25.000 | 155.7 | 109.1 | 74.2 | 50.2 | 33.8 | 22.6 | 15.1 |
| 26.400 | 10.1 | 6.6 | 4.2 | 2.7 | 1.5 | 0.9 | 0.0 |

Eccelston Mitigation POI 1-4 Existing

| Area or Reach Identifier | Drainage Area (sq mi) | ----- Peak Flow by Storm ----- | | | | |
|--------------------------|-----------------------|--------------------------------|---------------|---------------|----------------|----------------|
| | | 1_yr_sm (cfs) | 2_yr_sm (cfs) | 5_yr_sm (cfs) | 10_yr_sm (cfs) | 25_yr_sm (cfs) |
| DA1 | 0.090 | 45.3 | 69.5 | 107.0 | 136.8 | 177.5 |
| DA4 | 0.450 | 97.0 | 151.7 | 243.7 | 322.2 | 434.7 |
| DA2 | 1.323 | 192.4 | 317.9 | 541.1 | 736.5 | 1024.4 |
| DA3 | 0.920 | 86.3 | 161.4 | 306.1 | 439.0 | 640.5 |
| CON-1 | 2.693 | 369.8 | 622.8 | 1079.0 | 1480.9 | 2078.9 |

| | | Eccelston POI 1-4 Existing.out | | | | |
|--------------------------------|-----------------------------|--------------------------------|--------------------|--------------------|--------|--------|
| | | 339.2 | 584.9 | 1032.3 | 1419.2 | 1987.9 |
| DOWNSTREAM OUTLET | | 2.783 | 343.4 | 593.4 | 1046.7 | 1438.7 |
| Area or Reach Identifier | Drainage Area (sq mi) | ----- Peak Flow by Storm ----- | | | | |
| | | 50_yr_sm (cfs) | 100_yr_sm (cfs) | 500_yr_sm (cfs) | (cfs) | (cfs) |
| DA1 | 0.090 | 209.2 | 240.2 | 308.6 | | |
| DA4 | 0.450 | 526.7 | 622.1 | 853.7 | | |
| DA2 | 1.323 | 1269.6 | 1526.6 | 2165.1 | | |
| DA3 | 0.920 | 812.6 | 998.8 | 1471.9 | | |
| CON-1 | 2.693 | 2584.3 | 3120.0 | 4458.7 | | |
| DOWNSTREAM OUTLET | 2.783 | 2482.1 | 3008.1 | 4326.3 | | |
| | | 2514.9 | 3050.4 | 4394.6 | | |

Eccelston POI 5 Existing.out

| | | | | |
|---------|--------|--------|--------|--------|
| 0.2824 | 0.2996 | 0.3169 | 0.3444 | 0.3880 |
| 0.5000 | 0.6120 | 0.6556 | 0.6831 | 0.7004 |
| 0.7176 | 0.7262 | 0.7348 | 0.7434 | 0.7520 |
| 0.7606 | 0.7647 | 0.7688 | 0.7729 | 0.7770 |
| 0.7812 | 0.7858 | 0.7905 | 0.7951 | 0.7998 |
| 0.8044 | 0.8091 | 0.8137 | 0.8184 | 0.8230 |
| 0.8277 | 0.8323 | 0.8370 | 0.8416 | 0.8463 |
| 0.8509 | 0.8536 | 0.8564 | 0.8591 | 0.8619 |
| 0.8646 | 0.8674 | 0.8701 | 0.8729 | 0.8756 |
| 0.8784 | 0.8811 | 0.8839 | 0.8866 | 0.8894 |
| 0.8921 | 0.8949 | 0.8976 | 0.9004 | 0.9031 |
| 0.9059 | 0.9086 | 0.9114 | 0.9141 | 0.9169 |
| 0.9196 | 0.9224 | 0.9251 | 0.9279 | 0.9306 |
| 0.9334 | 0.9345 | 0.9356 | 0.9367 | 0.9378 |
| 0.9389 | 0.9400 | 0.9411 | 0.9422 | 0.9434 |
| 0.9445 | 0.9456 | 0.9467 | 0.9478 | 0.9489 |
| 0.9500 | 0.9511 | 0.9522 | 0.9534 | 0.9545 |
| 0.9556 | 0.9567 | 0.9578 | 0.9589 | 0.9600 |
| 0.9611 | 0.9622 | 0.9634 | 0.9645 | 0.9656 |
| 0.9667 | 0.9678 | 0.9689 | 0.9700 | 0.9711 |
| 0.9722 | 0.9733 | 0.9745 | 0.9756 | 0.9767 |
| 0.9778 | 0.9789 | 0.9800 | 0.9811 | 0.9822 |
| 0.9833 | 0.9845 | 0.9856 | 0.9867 | 0.9878 |
| 0.9889 | 0.9900 | 0.9911 | 0.9922 | 0.9933 |
| 0.9944 | 0.9956 | 0.9967 | 0.9978 | 0.9989 |
| 1.0000 | | | | |
| 2_yr_sm | 0.1 | | | |
| 0.0000 | 0.0011 | 0.0022 | 0.0033 | 0.0044 |
| 0.0055 | 0.0066 | 0.0077 | 0.0088 | 0.0099 |
| 0.0110 | 0.0121 | 0.0132 | 0.0143 | 0.0154 |
| 0.0166 | 0.0177 | 0.0188 | 0.0199 | 0.0210 |
| 0.0221 | 0.0232 | 0.0243 | 0.0254 | 0.0265 |
| 0.0276 | 0.0287 | 0.0298 | 0.0309 | 0.0320 |
| 0.0331 | 0.0342 | 0.0353 | 0.0364 | 0.0375 |
| 0.0386 | 0.0397 | 0.0408 | 0.0419 | 0.0430 |
| 0.0441 | 0.0452 | 0.0463 | 0.0474 | 0.0486 |
| 0.0497 | 0.0508 | 0.0519 | 0.0530 | 0.0541 |
| 0.0552 | 0.0563 | 0.0574 | 0.0585 | 0.0596 |
| 0.0607 | 0.0618 | 0.0629 | 0.0640 | 0.0651 |
| 0.0662 | 0.0689 | 0.0717 | 0.0744 | 0.0771 |
| 0.0799 | 0.0826 | 0.0853 | 0.0880 | 0.0908 |
| 0.0935 | 0.0962 | 0.0990 | 0.1017 | 0.1044 |
| 0.1072 | 0.1099 | 0.1126 | 0.1153 | 0.1181 |
| 0.1208 | 0.1235 | 0.1263 | 0.1290 | 0.1317 |
| 0.1344 | 0.1372 | 0.1399 | 0.1426 | 0.1454 |
| 0.1481 | 0.1527 | 0.1573 | 0.1619 | 0.1665 |
| 0.1711 | 0.1757 | 0.1802 | 0.1848 | 0.1894 |
| 0.1940 | 0.1986 | 0.2032 | 0.2078 | 0.2124 |
| 0.2170 | 0.2211 | 0.2252 | 0.2293 | 0.2334 |
| 0.2375 | 0.2461 | 0.2547 | 0.2632 | 0.2718 |
| 0.2803 | 0.2982 | 0.3160 | 0.3443 | 0.3888 |
| 0.5000 | 0.6112 | 0.6557 | 0.6840 | 0.7018 |
| 0.7197 | 0.7282 | 0.7368 | 0.7453 | 0.7539 |
| 0.7625 | 0.7666 | 0.7707 | 0.7748 | 0.7789 |
| 0.7830 | 0.7876 | 0.7922 | 0.7968 | 0.8014 |
| 0.8060 | 0.8106 | 0.8152 | 0.8198 | 0.8243 |
| 0.8289 | 0.8335 | 0.8381 | 0.8427 | 0.8473 |
| 0.8519 | 0.8546 | 0.8574 | 0.8601 | 0.8628 |
| 0.8656 | 0.8683 | 0.8710 | 0.8737 | 0.8765 |
| 0.8792 | 0.8819 | 0.8847 | 0.8874 | 0.8901 |
| 0.8928 | 0.8956 | 0.8983 | 0.9010 | 0.9038 |
| 0.9065 | 0.9092 | 0.9120 | 0.9147 | 0.9174 |
| 0.9201 | 0.9229 | 0.9256 | 0.9283 | 0.9311 |

| | Eccelston | POI | 5 Existing | .out | |
|---------|-----------|--------|------------|--------|--------|
| | 0.9338 | 0.9349 | 0.9360 | 0.9371 | 0.9382 |
| | 0.9393 | 0.9404 | 0.9415 | 0.9426 | 0.9437 |
| | 0.9448 | 0.9459 | 0.9470 | 0.9481 | 0.9492 |
| | 0.9503 | 0.9514 | 0.9526 | 0.9537 | 0.9548 |
| | 0.9559 | 0.9570 | 0.9581 | 0.9592 | 0.9603 |
| | 0.9614 | 0.9625 | 0.9636 | 0.9647 | 0.9658 |
| | 0.9669 | 0.9680 | 0.9691 | 0.9702 | 0.9713 |
| | 0.9724 | 0.9735 | 0.9746 | 0.9757 | 0.9768 |
| | 0.9779 | 0.9790 | 0.9801 | 0.9812 | 0.9823 |
| | 0.9834 | 0.9846 | 0.9857 | 0.9868 | 0.9879 |
| | 0.9890 | 0.9901 | 0.9912 | 0.9923 | 0.9934 |
| | 0.9945 | 0.9956 | 0.9967 | 0.9978 | 0.9989 |
| | 1.0000 | | | | |
| 5_yr_sm | 0.1 | | | | |
| | 0.0000 | 0.0012 | 0.0023 | 0.0035 | 0.0047 |
| | 0.0059 | 0.0070 | 0.0082 | 0.0094 | 0.0106 |
| | 0.0117 | 0.0129 | 0.0141 | 0.0153 | 0.0164 |
| | 0.0176 | 0.0188 | 0.0200 | 0.0211 | 0.0223 |
| | 0.0235 | 0.0246 | 0.0258 | 0.0270 | 0.0282 |
| | 0.0293 | 0.0305 | 0.0317 | 0.0329 | 0.0340 |
| | 0.0352 | 0.0364 | 0.0376 | 0.0387 | 0.0399 |
| | 0.0411 | 0.0422 | 0.0434 | 0.0446 | 0.0458 |
| | 0.0469 | 0.0481 | 0.0493 | 0.0505 | 0.0516 |
| | 0.0528 | 0.0540 | 0.0552 | 0.0563 | 0.0575 |
| | 0.0587 | 0.0599 | 0.0610 | 0.0622 | 0.0634 |
| | 0.0645 | 0.0657 | 0.0669 | 0.0681 | 0.0692 |
| | 0.0704 | 0.0732 | 0.0760 | 0.0787 | 0.0815 |
| | 0.0843 | 0.0871 | 0.0898 | 0.0926 | 0.0954 |
| | 0.0982 | 0.1009 | 0.1037 | 0.1065 | 0.1093 |
| | 0.1120 | 0.1148 | 0.1176 | 0.1204 | 0.1232 |
| | 0.1259 | 0.1287 | 0.1315 | 0.1343 | 0.1370 |
| | 0.1398 | 0.1426 | 0.1454 | 0.1481 | 0.1509 |
| | 0.1537 | 0.1582 | 0.1626 | 0.1671 | 0.1716 |
| | 0.1760 | 0.1805 | 0.1850 | 0.1894 | 0.1939 |
| | 0.1984 | 0.2029 | 0.2073 | 0.2118 | 0.2163 |
| | 0.2207 | 0.2249 | 0.2291 | 0.2333 | 0.2375 |
| | 0.2416 | 0.2504 | 0.2592 | 0.2679 | 0.2767 |
| | 0.2854 | 0.3043 | 0.3232 | 0.3524 | 0.3970 |
| | 0.5000 | 0.6030 | 0.6476 | 0.6768 | 0.6957 |
| | 0.7146 | 0.7233 | 0.7321 | 0.7408 | 0.7496 |
| | 0.7584 | 0.7625 | 0.7667 | 0.7709 | 0.7751 |
| | 0.7793 | 0.7837 | 0.7882 | 0.7927 | 0.7971 |
| | 0.8016 | 0.8061 | 0.8106 | 0.8150 | 0.8195 |
| | 0.8240 | 0.8284 | 0.8329 | 0.8374 | 0.8418 |
| | 0.8463 | 0.8491 | 0.8519 | 0.8546 | 0.8574 |
| | 0.8602 | 0.8630 | 0.8657 | 0.8685 | 0.8713 |
| | 0.8741 | 0.8768 | 0.8796 | 0.8824 | 0.8852 |
| | 0.8880 | 0.8907 | 0.8935 | 0.8963 | 0.8991 |
| | 0.9018 | 0.9046 | 0.9074 | 0.9102 | 0.9129 |
| | 0.9157 | 0.9185 | 0.9213 | 0.9240 | 0.9268 |
| | 0.9296 | 0.9308 | 0.9319 | 0.9331 | 0.9343 |
| | 0.9355 | 0.9366 | 0.9378 | 0.9390 | 0.9401 |
| | 0.9413 | 0.9425 | 0.9437 | 0.9448 | 0.9460 |
| | 0.9472 | 0.9484 | 0.9495 | 0.9507 | 0.9519 |
| | 0.9531 | 0.9542 | 0.9554 | 0.9566 | 0.9578 |
| | 0.9589 | 0.9601 | 0.9613 | 0.9624 | 0.9636 |
| | 0.9648 | 0.9660 | 0.9671 | 0.9683 | 0.9695 |
| | 0.9707 | 0.9718 | 0.9730 | 0.9742 | 0.9754 |
| | 0.9765 | 0.9777 | 0.9789 | 0.9800 | 0.9812 |
| | 0.9824 | 0.9836 | 0.9847 | 0.9859 | 0.9871 |
| | 0.9883 | 0.9894 | 0.9906 | 0.9918 | 0.9930 |
| | 0.9941 | 0.9953 | 0.9965 | 0.9977 | 0.9988 |
| | 1.0000 | | | | |

| | Eccelston POI 5 Existing.out | | | | |
|----------|------------------------------|--------|--------|--------|--------|
| 10_yr_sm | 0.0000 | 0.0012 | 0.0025 | 0.0037 | 0.0049 |
| | 0.0061 | 0.0074 | 0.0086 | 0.0098 | 0.0110 |
| | 0.0123 | 0.0135 | 0.0147 | 0.0159 | 0.0172 |
| | 0.0184 | 0.0196 | 0.0208 | 0.0221 | 0.0233 |
| | 0.0245 | 0.0257 | 0.0270 | 0.0282 | 0.0294 |
| | 0.0306 | 0.0319 | 0.0331 | 0.0343 | 0.0355 |
| | 0.0368 | 0.0380 | 0.0392 | 0.0404 | 0.0417 |
| | 0.0429 | 0.0441 | 0.0453 | 0.0466 | 0.0478 |
| | 0.0490 | 0.0502 | 0.0515 | 0.0527 | 0.0539 |
| | 0.0552 | 0.0564 | 0.0576 | 0.0588 | 0.0601 |
| | 0.0613 | 0.0625 | 0.0637 | 0.0650 | 0.0662 |
| | 0.0674 | 0.0686 | 0.0699 | 0.0711 | 0.0723 |
| | 0.0735 | 0.0764 | 0.0793 | 0.0822 | 0.0851 |
| | 0.0879 | 0.0908 | 0.0937 | 0.0966 | 0.0995 |
| | 0.1023 | 0.1052 | 0.1081 | 0.1110 | 0.1139 |
| | 0.1167 | 0.1196 | 0.1225 | 0.1254 | 0.1283 |
| | 0.1311 | 0.1340 | 0.1369 | 0.1398 | 0.1427 |
| | 0.1455 | 0.1484 | 0.1513 | 0.1542 | 0.1570 |
| | 0.1599 | 0.1644 | 0.1689 | 0.1734 | 0.1779 |
| | 0.1824 | 0.1869 | 0.1914 | 0.1958 | 0.2003 |
| | 0.2048 | 0.2093 | 0.2138 | 0.2183 | 0.2228 |
| | 0.2273 | 0.2315 | 0.2357 | 0.2399 | 0.2441 |
| | 0.2483 | 0.2573 | 0.2663 | 0.2752 | 0.2842 |
| | 0.2931 | 0.3123 | 0.3315 | 0.3608 | 0.4041 |
| | 0.5000 | 0.5959 | 0.6392 | 0.6685 | 0.6877 |
| | 0.7069 | 0.7158 | 0.7248 | 0.7337 | 0.7427 |
| | 0.7517 | 0.7559 | 0.7601 | 0.7643 | 0.7685 |
| | 0.7727 | 0.7772 | 0.7817 | 0.7862 | 0.7907 |
| | 0.7952 | 0.7997 | 0.8042 | 0.8086 | 0.8131 |
| | 0.8176 | 0.8221 | 0.8266 | 0.8311 | 0.8356 |
| | 0.8401 | 0.8430 | 0.8458 | 0.8487 | 0.8516 |
| | 0.8545 | 0.8573 | 0.8602 | 0.8631 | 0.8660 |
| | 0.8689 | 0.8717 | 0.8746 | 0.8775 | 0.8804 |
| | 0.8833 | 0.8861 | 0.8890 | 0.8919 | 0.8948 |
| | 0.8977 | 0.9005 | 0.9034 | 0.9063 | 0.9092 |
| | 0.9121 | 0.9149 | 0.9178 | 0.9207 | 0.9236 |
| | 0.9265 | 0.9277 | 0.9289 | 0.9301 | 0.9314 |
| | 0.9326 | 0.9338 | 0.9350 | 0.9363 | 0.9375 |
| | 0.9387 | 0.9399 | 0.9412 | 0.9424 | 0.9436 |
| | 0.9448 | 0.9461 | 0.9473 | 0.9485 | 0.9498 |
| | 0.9510 | 0.9522 | 0.9534 | 0.9547 | 0.9559 |
| | 0.9571 | 0.9583 | 0.9596 | 0.9608 | 0.9620 |
| | 0.9632 | 0.9645 | 0.9657 | 0.9669 | 0.9681 |
| | 0.9694 | 0.9706 | 0.9718 | 0.9730 | 0.9743 |
| | 0.9755 | 0.9767 | 0.9779 | 0.9792 | 0.9804 |
| | 0.9816 | 0.9828 | 0.9841 | 0.9853 | 0.9865 |
| | 0.9877 | 0.9890 | 0.9902 | 0.9914 | 0.9926 |
| | 0.9939 | 0.9951 | 0.9963 | 0.9975 | 0.9988 |
| | 1.0000 | | | | |
| 25_yr_sm | | 0.1 | | | |
| | 0.0000 | 0.0013 | 0.0026 | 0.0039 | 0.0052 |
| | 0.0065 | 0.0079 | 0.0092 | 0.0105 | 0.0118 |
| | 0.0131 | 0.0144 | 0.0157 | 0.0170 | 0.0183 |
| | 0.0196 | 0.0210 | 0.0223 | 0.0236 | 0.0249 |
| | 0.0262 | 0.0275 | 0.0288 | 0.0301 | 0.0314 |
| | 0.0327 | 0.0340 | 0.0354 | 0.0367 | 0.0380 |
| | 0.0393 | 0.0406 | 0.0419 | 0.0432 | 0.0445 |
| | 0.0458 | 0.0471 | 0.0485 | 0.0498 | 0.0511 |
| | 0.0524 | 0.0537 | 0.0550 | 0.0563 | 0.0576 |
| | 0.0589 | 0.0602 | 0.0616 | 0.0629 | 0.0642 |
| | 0.0655 | 0.0668 | 0.0681 | 0.0694 | 0.0707 |
| | 0.0720 | 0.0733 | 0.0746 | 0.0760 | 0.0773 |

Eccelston POI 5 Existing.out

| | | | | |
|----------|--------|--------|--------|--------|
| 0.0786 | 0.0816 | 0.0846 | 0.0876 | 0.0906 |
| 0.0937 | 0.0967 | 0.0997 | 0.1027 | 0.1057 |
| 0.1087 | 0.1118 | 0.1148 | 0.1178 | 0.1208 |
| 0.1238 | 0.1268 | 0.1299 | 0.1329 | 0.1359 |
| 0.1389 | 0.1419 | 0.1449 | 0.1480 | 0.1510 |
| 0.1540 | 0.1570 | 0.1600 | 0.1630 | 0.1661 |
| 0.1691 | 0.1737 | 0.1782 | 0.1828 | 0.1874 |
| 0.1920 | 0.1966 | 0.2011 | 0.2057 | 0.2103 |
| 0.2149 | 0.2195 | 0.2241 | 0.2286 | 0.2332 |
| 0.2378 | 0.2421 | 0.2464 | 0.2507 | 0.2549 |
| 0.2592 | 0.2685 | 0.2777 | 0.2869 | 0.2961 |
| 0.3054 | 0.3248 | 0.3441 | 0.3728 | 0.4138 |
| 0.5000 | 0.5862 | 0.6272 | 0.6559 | 0.6752 |
| 0.6946 | 0.7039 | 0.7131 | 0.7223 | 0.7315 |
| 0.7408 | 0.7451 | 0.7493 | 0.7536 | 0.7579 |
| 0.7622 | 0.7668 | 0.7714 | 0.7759 | 0.7805 |
| 0.7851 | 0.7897 | 0.7943 | 0.7989 | 0.8034 |
| 0.8080 | 0.8126 | 0.8172 | 0.8218 | 0.8263 |
| 0.8309 | 0.8339 | 0.8370 | 0.8400 | 0.8430 |
| 0.8460 | 0.8490 | 0.8520 | 0.8551 | 0.8581 |
| 0.8611 | 0.8641 | 0.8671 | 0.8701 | 0.8732 |
| 0.8762 | 0.8792 | 0.8822 | 0.8852 | 0.8882 |
| 0.8913 | 0.8943 | 0.8973 | 0.9003 | 0.9033 |
| 0.9063 | 0.9094 | 0.9124 | 0.9154 | 0.9184 |
| 0.9214 | 0.9227 | 0.9240 | 0.9254 | 0.9267 |
| 0.9280 | 0.9293 | 0.9306 | 0.9319 | 0.9332 |
| 0.9345 | 0.9358 | 0.9371 | 0.9384 | 0.9398 |
| 0.9411 | 0.9424 | 0.9437 | 0.9450 | 0.9463 |
| 0.9476 | 0.9489 | 0.9502 | 0.9515 | 0.9529 |
| 0.9542 | 0.9555 | 0.9568 | 0.9581 | 0.9594 |
| 0.9607 | 0.9620 | 0.9633 | 0.9646 | 0.9660 |
| 0.9673 | 0.9686 | 0.9699 | 0.9712 | 0.9725 |
| 0.9738 | 0.9751 | 0.9764 | 0.9777 | 0.9790 |
| 0.9804 | 0.9817 | 0.9830 | 0.9843 | 0.9856 |
| 0.9869 | 0.9882 | 0.9895 | 0.9908 | 0.9921 |
| 0.9935 | 0.9948 | 0.9961 | 0.9974 | 0.9987 |
| 1.0000 | | | | |
| 50_yr_sm | 0.1 | | | |
| 0.0000 | 0.0014 | 0.0027 | 0.0041 | 0.0055 |
| 0.0068 | 0.0082 | 0.0095 | 0.0109 | 0.0123 |
| 0.0136 | 0.0150 | 0.0164 | 0.0177 | 0.0191 |
| 0.0205 | 0.0218 | 0.0232 | 0.0246 | 0.0259 |
| 0.0273 | 0.0286 | 0.0300 | 0.0314 | 0.0327 |
| 0.0341 | 0.0355 | 0.0368 | 0.0382 | 0.0396 |
| 0.0409 | 0.0423 | 0.0436 | 0.0450 | 0.0464 |
| 0.0477 | 0.0491 | 0.0505 | 0.0518 | 0.0532 |
| 0.0546 | 0.0559 | 0.0573 | 0.0587 | 0.0600 |
| 0.0614 | 0.0627 | 0.0641 | 0.0655 | 0.0668 |
| 0.0682 | 0.0696 | 0.0709 | 0.0723 | 0.0737 |
| 0.0750 | 0.0764 | 0.0777 | 0.0791 | 0.0805 |
| 0.0818 | 0.0850 | 0.0881 | 0.0913 | 0.0944 |
| 0.0976 | 0.1007 | 0.1039 | 0.1070 | 0.1102 |
| 0.1133 | 0.1165 | 0.1196 | 0.1227 | 0.1259 |
| 0.1290 | 0.1322 | 0.1353 | 0.1385 | 0.1416 |
| 0.1448 | 0.1479 | 0.1511 | 0.1542 | 0.1574 |
| 0.1605 | 0.1636 | 0.1668 | 0.1699 | 0.1731 |
| 0.1762 | 0.1809 | 0.1856 | 0.1903 | 0.1949 |
| 0.1996 | 0.2043 | 0.2089 | 0.2136 | 0.2183 |
| 0.2230 | 0.2276 | 0.2323 | 0.2370 | 0.2417 |
| 0.2463 | 0.2507 | 0.2550 | 0.2593 | 0.2636 |
| 0.2679 | 0.2774 | 0.2869 | 0.2964 | 0.3059 |
| 0.3154 | 0.3348 | 0.3541 | 0.3821 | 0.4210 |
| 0.5000 | 0.5790 | 0.6179 | 0.6459 | 0.6652 |

Eccelston POI 5 Existing.out

| | | | | |
|--------|--------|--------|--------|--------|
| 0.6846 | 0.6941 | 0.7036 | 0.7131 | 0.7226 |
| 0.7321 | 0.7364 | 0.7407 | 0.7450 | 0.7493 |
| 0.7537 | 0.7583 | 0.7630 | 0.7677 | 0.7724 |
| 0.7770 | 0.7817 | 0.7864 | 0.7911 | 0.7957 |
| 0.8004 | 0.8051 | 0.8097 | 0.8144 | 0.8191 |
| 0.8238 | 0.8269 | 0.8301 | 0.8332 | 0.8364 |
| 0.8395 | 0.8426 | 0.8458 | 0.8489 | 0.8521 |
| 0.8552 | 0.8584 | 0.8615 | 0.8647 | 0.8678 |
| 0.8710 | 0.8741 | 0.8773 | 0.8804 | 0.8835 |
| 0.8867 | 0.8898 | 0.8930 | 0.8961 | 0.8993 |
| 0.9024 | 0.9056 | 0.9087 | 0.9119 | 0.9150 |
| 0.9182 | 0.9195 | 0.9209 | 0.9223 | 0.9236 |
| 0.9250 | 0.9263 | 0.9277 | 0.9291 | 0.9304 |
| 0.9318 | 0.9332 | 0.9345 | 0.9359 | 0.9373 |
| 0.9386 | 0.9400 | 0.9413 | 0.9427 | 0.9441 |
| 0.9454 | 0.9468 | 0.9482 | 0.9495 | 0.9509 |
| 0.9523 | 0.9536 | 0.9550 | 0.9564 | 0.9577 |
| 0.9591 | 0.9604 | 0.9618 | 0.9632 | 0.9645 |
| 0.9659 | 0.9673 | 0.9686 | 0.9700 | 0.9714 |
| 0.9727 | 0.9741 | 0.9754 | 0.9768 | 0.9782 |
| 0.9795 | 0.9809 | 0.9823 | 0.9836 | 0.9850 |
| 0.9864 | 0.9877 | 0.9891 | 0.9905 | 0.9918 |
| 0.9932 | 0.9945 | 0.9959 | 0.9973 | 0.9986 |
| 1.0000 | | | | |

100_yr_sm

| | | | | |
|--------|--------|--------|--------|--------|
| | 0.1 | | | |
| 0.0000 | 0.0014 | 0.0029 | 0.0043 | 0.0057 |
| 0.0071 | 0.0086 | 0.0100 | 0.0114 | 0.0128 |
| 0.0143 | 0.0157 | 0.0171 | 0.0185 | 0.0200 |
| 0.0214 | 0.0228 | 0.0243 | 0.0257 | 0.0271 |
| 0.0285 | 0.0300 | 0.0314 | 0.0328 | 0.0342 |
| 0.0357 | 0.0371 | 0.0385 | 0.0399 | 0.0414 |
| 0.0428 | 0.0442 | 0.0457 | 0.0471 | 0.0485 |
| 0.0499 | 0.0514 | 0.0528 | 0.0542 | 0.0556 |
| 0.0571 | 0.0585 | 0.0599 | 0.0613 | 0.0628 |
| 0.0642 | 0.0656 | 0.0671 | 0.0685 | 0.0699 |
| 0.0713 | 0.0728 | 0.0742 | 0.0756 | 0.0770 |
| 0.0785 | 0.0799 | 0.0813 | 0.0827 | 0.0842 |
| 0.0856 | 0.0889 | 0.0922 | 0.0954 | 0.0987 |
| 0.1020 | 0.1053 | 0.1086 | 0.1118 | 0.1151 |
| 0.1184 | 0.1217 | 0.1250 | 0.1282 | 0.1315 |
| 0.1348 | 0.1381 | 0.1414 | 0.1447 | 0.1479 |
| 0.1512 | 0.1545 | 0.1578 | 0.1611 | 0.1643 |
| 0.1676 | 0.1709 | 0.1742 | 0.1775 | 0.1807 |
| 0.1840 | 0.1888 | 0.1935 | 0.1983 | 0.2031 |
| 0.2078 | 0.2126 | 0.2174 | 0.2221 | 0.2269 |
| 0.2317 | 0.2364 | 0.2412 | 0.2459 | 0.2507 |
| 0.2555 | 0.2598 | 0.2641 | 0.2684 | 0.2727 |
| 0.2770 | 0.2867 | 0.2964 | 0.3062 | 0.3159 |
| 0.3256 | 0.3447 | 0.3638 | 0.3910 | 0.4277 |
| 0.5000 | 0.5723 | 0.6090 | 0.6362 | 0.6553 |
| 0.6744 | 0.6841 | 0.6938 | 0.7036 | 0.7133 |
| 0.7230 | 0.7273 | 0.7316 | 0.7359 | 0.7402 |
| 0.7445 | 0.7493 | 0.7541 | 0.7588 | 0.7636 |
| 0.7683 | 0.7731 | 0.7779 | 0.7826 | 0.7874 |
| 0.7922 | 0.7969 | 0.8017 | 0.8065 | 0.8112 |
| 0.8160 | 0.8193 | 0.8225 | 0.8258 | 0.8291 |
| 0.8324 | 0.8357 | 0.8389 | 0.8422 | 0.8455 |
| 0.8488 | 0.8521 | 0.8553 | 0.8586 | 0.8619 |
| 0.8652 | 0.8685 | 0.8718 | 0.8750 | 0.8783 |
| 0.8816 | 0.8849 | 0.8882 | 0.8914 | 0.8947 |
| 0.8980 | 0.9013 | 0.9046 | 0.9078 | 0.9111 |
| 0.9144 | 0.9158 | 0.9173 | 0.9187 | 0.9201 |
| 0.9215 | 0.9230 | 0.9244 | 0.9258 | 0.9272 |

| | Eccelston POI 5 Existing.out | | | | |
|-----------|------------------------------|--------|--------|--------|--|
| 0.9287 | 0.9301 | 0.9315 | 0.9329 | 0.9344 | |
| 0.9358 | 0.9372 | 0.9387 | 0.9401 | 0.9415 | |
| 0.9429 | 0.9444 | 0.9458 | 0.9472 | 0.9486 | |
| 0.9501 | 0.9515 | 0.9529 | 0.9543 | 0.9558 | |
| 0.9572 | 0.9586 | 0.9601 | 0.9615 | 0.9629 | |
| 0.9643 | 0.9658 | 0.9672 | 0.9686 | 0.9700 | |
| 0.9715 | 0.9729 | 0.9743 | 0.9757 | 0.9772 | |
| 0.9786 | 0.9800 | 0.9815 | 0.9829 | 0.9843 | |
| 0.9857 | 0.9872 | 0.9886 | 0.9900 | 0.9914 | |
| 0.9929 | 0.9943 | 0.9957 | 0.9971 | 0.9986 | |
| 1.0000 | | | | | |
| 500_yr_sm | 0.1 | | | | |
| 0.0000 | 0.0016 | 0.0031 | 0.0047 | 0.0063 | |
| 0.0078 | 0.0094 | 0.0110 | 0.0126 | 0.0141 | |
| 0.0157 | 0.0173 | 0.0188 | 0.0204 | 0.0220 | |
| 0.0235 | 0.0251 | 0.0267 | 0.0283 | 0.0298 | |
| 0.0314 | 0.0330 | 0.0345 | 0.0361 | 0.0377 | |
| 0.0392 | 0.0408 | 0.0424 | 0.0439 | 0.0455 | |
| 0.0471 | 0.0487 | 0.0502 | 0.0518 | 0.0534 | |
| 0.0549 | 0.0565 | 0.0581 | 0.0596 | 0.0612 | |
| 0.0628 | 0.0643 | 0.0659 | 0.0675 | 0.0691 | |
| 0.0706 | 0.0722 | 0.0738 | 0.0753 | 0.0769 | |
| 0.0785 | 0.0800 | 0.0816 | 0.0832 | 0.0848 | |
| 0.0863 | 0.0879 | 0.0895 | 0.0910 | 0.0926 | |
| 0.0942 | 0.0978 | 0.1014 | 0.1050 | 0.1086 | |
| 0.1122 | 0.1158 | 0.1195 | 0.1231 | 0.1267 | |
| 0.1303 | 0.1339 | 0.1375 | 0.1411 | 0.1447 | |
| 0.1483 | 0.1520 | 0.1556 | 0.1592 | 0.1628 | |
| 0.1664 | 0.1700 | 0.1736 | 0.1772 | 0.1809 | |
| 0.1845 | 0.1881 | 0.1917 | 0.1953 | 0.1989 | |
| 0.2025 | 0.2075 | 0.2124 | 0.2174 | 0.2223 | |
| 0.2272 | 0.2322 | 0.2371 | 0.2421 | 0.2470 | |
| 0.2520 | 0.2569 | 0.2618 | 0.2668 | 0.2717 | |
| 0.2767 | 0.2810 | 0.2853 | 0.2896 | 0.2940 | |
| 0.2983 | 0.3084 | 0.3185 | 0.3287 | 0.3388 | |
| 0.3489 | 0.3673 | 0.3856 | 0.4104 | 0.4420 | |
| 0.5000 | 0.5580 | 0.5896 | 0.6144 | 0.6327 | |
| 0.6511 | 0.6612 | 0.6713 | 0.6815 | 0.6916 | |
| 0.7017 | 0.7060 | 0.7104 | 0.7147 | 0.7190 | |
| 0.7233 | 0.7283 | 0.7332 | 0.7382 | 0.7431 | |
| 0.7480 | 0.7530 | 0.7579 | 0.7629 | 0.7678 | |
| 0.7728 | 0.7777 | 0.7826 | 0.7876 | 0.7925 | |
| 0.7975 | 0.8011 | 0.8047 | 0.8083 | 0.8119 | |
| 0.8155 | 0.8191 | 0.8228 | 0.8264 | 0.8300 | |
| 0.8336 | 0.8372 | 0.8408 | 0.8444 | 0.8480 | |
| 0.8517 | 0.8553 | 0.8589 | 0.8625 | 0.8661 | |
| 0.8697 | 0.8733 | 0.8769 | 0.8805 | 0.8842 | |
| 0.8878 | 0.8914 | 0.8950 | 0.8986 | 0.9022 | |
| 0.9058 | 0.9074 | 0.9090 | 0.9105 | 0.9121 | |
| 0.9137 | 0.9152 | 0.9168 | 0.9184 | 0.9200 | |
| 0.9215 | 0.9231 | 0.9247 | 0.9262 | 0.9278 | |
| 0.9294 | 0.9309 | 0.9325 | 0.9341 | 0.9357 | |
| 0.9372 | 0.9388 | 0.9404 | 0.9419 | 0.9435 | |
| 0.9451 | 0.9466 | 0.9482 | 0.9498 | 0.9513 | |
| 0.9529 | 0.9545 | 0.9561 | 0.9576 | 0.9592 | |
| 0.9608 | 0.9623 | 0.9639 | 0.9655 | 0.9670 | |
| 0.9686 | 0.9702 | 0.9717 | 0.9733 | 0.9749 | |
| 0.9765 | 0.9780 | 0.9796 | 0.9812 | 0.9827 | |
| 0.9843 | 0.9859 | 0.9874 | 0.9890 | 0.9906 | |
| 0.9922 | 0.9937 | 0.9953 | 0.9969 | 0.9984 | |
| 1.0000 | | | | | |

Eccelston POI 5 Existing.out

GLOBAL OUTPUT:

.2 NN N NN N

winTR-20 Printed Page File End of Input Data List

Eccelston Mitigation POI 5 Existing

Name of printed page file:
C:\Users\cwagner\Desktop\Eccelston POI 5 Existing.out

STORM 1_yr_sm

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| OUTLET | 0.139 | | 0.683 | | 12.47 | 38.6 | 277.15 |

STORM 2_yr_sm

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| OUTLET | 0.139 | | 1.032 | | 12.44 | 62.2 | 446.25 |

STORM 5_yr_sm

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| OUTLET | 0.139 | | 1.685 | | 12.45 | 101.1 | 725.51 |

STORM 10_yr_sm

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| OUTLET | 0.139 | | 2.310 | | 12.43 | 133.9 | 960.95 |

STORM 25_yr_sm

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| OUTLET | 0.139 | | 3.345 | | 12.44 | 180.4 | 1295.19 |

STORM 50_yr_sm

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| OUTLET | 0.139 | | | | | | |

| Identifier | (sq mi) | Location | Eccelston POI 5 Existing.out (in) | (ft) | (hr) | (cfs) | (csm) |
|-----------------|---------|----------|--------------------------------------|------|-------|-------|---------|
| OUTLET | 0.139 | | 4.306 | | 12.41 | 217.8 | 1563.43 |
| STORM 100_yr_sm | | | | | | | |

WinTR-20 Version 3.20
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Eccelston Mitigation POI 5 Existing

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | ----- Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | ----- Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|-------------------------|----------------|-----------------|---------------------|
| OUTLET | 0.139 | | 5.442 | | 12.41 | 256.2 | 1839.31 |
| STORM 500_yr_sm | | | | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | ----- Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | ----- Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|-------------------------|----------------|-----------------|---------------------|
| OUTLET | 0.139 | | 8.841 | | 12.42 | 344.5 | 2473.35 |

Eccelston POI 5 Existing.out

WinTR-20 Version 3.20

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Eccelston Mitigation POI 5 Existing

| Area or Reach Identifier | Drainage Area (sq mi) | ----- Peak Flow by Storm ----- | | | | |
|--------------------------|-----------------------|--------------------------------|---------------|---------------|----------------|----------------|
| | | 1_yr_sm (cfs) | 2_yr_sm (cfs) | 5_yr_sm (cfs) | 10_yr_sm (cfs) | 25_yr_sm (cfs) |
| DA5 | 0.139 | 38.6 | 62.2 | 101.1 | 133.9 | 180.4 |
| OUTLET | 0.139 | 38.6 | 62.2 | 101.1 | 133.9 | 180.4 |

| Area or Reach Identifier | Drainage Area (sq mi) | ----- Peak Flow by Storm ----- | | | | |
|--------------------------|-----------------------|--------------------------------|-----------------|-----------------|-------|-------|
| | | 50_yr_sm (cfs) | 100_yr_sm (cfs) | 500_yr_sm (cfs) | (cfs) | (cfs) |
| DA5 | 0.139 | 217.8 | 256.2 | 344.5 | | |
| OUTLET | 0.139 | 217.8 | 256.2 | 344.5 | | |


```

WinTR-20: version 3.20          0          0          0
Eccelston Mitigation POI 1-4 Ultimate

SUB-AREA:
  DA1      OUTLET      0.0900312  77.      .260      YY
  DA4      CON-1       0.4501281  75.      1.13      YY
  DA2      CON-1       1.3229781  74.      1.377      YY
  DA3      CON-1       0.9202734  68.      1.241      YY

STREAM REACH:
  CON-1    OUTLET    XS1          1547.3143    YY  Y

STORM ANALYSIS:
  1_yr_sm  2.7      1_yr_sm  2      3.27
  2_yr_sm  3.27     2_yr_sm  2      3.27
  5_yr_sm  4.21     5_yr_sm  2      3.27
  10_yr_sm 5.03     10_yr_sm 2      3.27
  25_yr_sm 6.29     25_yr_sm 2      3.27
  50_yr_sm 7.41     50_yr_sm 2      3.27
  100_yr_sm 8.68     100_yr_sm 2     3.27
  500_yr_sm 12.35    500_yr_sm 2     3.27

STREAM CROSS SECTION:
  XS1      361.8
           360.16  0.00  0.00  2.      .1
           360.57  1.92  1.80  2.
           360.98  11.84  6.44  2.
           361.39  31.78  12.95  2.
           361.80  63.07  21.08  2.
           362.57  246.03  172.72  2.
           363.35  678.76  348.03  2.
           364.12  1313.55  539.74  2.
           364.89  2034.29  766.67  2.
           365.67  3178.49  1025.20  2.
           366.44  4545.31  1296.17  2.
           367.21  6128.84  1579.56  2.
           367.99  7541.79  1894.24  2.
           368.76  9145.25  2251.86  2.
           369.53  11751.18  2644.71  2.
           370.31  14631.71  3047.25  2.
           371.08  17781.04  3459.48  2.
           371.85  21194.89  3881.38  2.
           372.63  24870.16  4312.97  2.
           373.40  28804.62  4754.24  2.
  
```

Eccelston POI 1-4 Ultimate.out

RAINFALL DISTRIBUTION:

1_yr_sm

0.1

| | | | | |
|--------|--------|--------|--------|--------|
| 0.0000 | 0.0011 | 0.0022 | 0.0033 | 0.0044 |
| 0.0055 | 0.0067 | 0.0078 | 0.0089 | 0.0100 |
| 0.0111 | 0.0122 | 0.0133 | 0.0144 | 0.0155 |
| 0.0166 | 0.0178 | 0.0189 | 0.0200 | 0.0211 |
| 0.0222 | 0.0233 | 0.0244 | 0.0255 | 0.0266 |
| 0.0277 | 0.0289 | 0.0300 | 0.0311 | 0.0322 |
| 0.0333 | 0.0344 | 0.0355 | 0.0366 | 0.0377 |
| 0.0388 | 0.0399 | 0.0411 | 0.0422 | 0.0433 |
| 0.0444 | 0.0455 | 0.0466 | 0.0477 | 0.0488 |
| 0.0499 | 0.0510 | 0.0522 | 0.0533 | 0.0544 |
| 0.0555 | 0.0566 | 0.0577 | 0.0588 | 0.0599 |
| 0.0610 | 0.0621 | 0.0633 | 0.0644 | 0.0655 |
| 0.0666 | 0.0693 | 0.0721 | 0.0748 | 0.0776 |
| 0.0803 | 0.0830 | 0.0858 | 0.0885 | 0.0913 |
| 0.0940 | 0.0967 | 0.0995 | 0.1022 | 0.1050 |
| 0.1077 | 0.1105 | 0.1132 | 0.1159 | 0.1187 |
| 0.1214 | 0.1242 | 0.1269 | 0.1297 | 0.1324 |
| 0.1351 | 0.1379 | 0.1406 | 0.1434 | 0.1461 |
| 0.1488 | 0.1535 | 0.1581 | 0.1627 | 0.1674 |
| 0.1720 | 0.1766 | 0.1813 | 0.1859 | 0.1905 |
| 0.1951 | 0.1998 | 0.2044 | 0.2090 | 0.2137 |
| 0.2183 | 0.2224 | 0.2266 | 0.2307 | 0.2348 |
| 0.2390 | 0.2476 | 0.2562 | 0.2648 | 0.2734 |
| 0.2820 | 0.2992 | 0.3165 | 0.3440 | 0.3877 |
| 0.5000 | 0.6123 | 0.6560 | 0.6835 | 0.7008 |
| 0.7180 | 0.7266 | 0.7352 | 0.7438 | 0.7524 |
| 0.7610 | 0.7652 | 0.7693 | 0.7734 | 0.7776 |
| 0.7817 | 0.7863 | 0.7910 | 0.7956 | 0.8002 |
| 0.8049 | 0.8095 | 0.8141 | 0.8187 | 0.8234 |
| 0.8280 | 0.8326 | 0.8373 | 0.8419 | 0.8465 |
| 0.8512 | 0.8539 | 0.8566 | 0.8594 | 0.8621 |
| 0.8649 | 0.8676 | 0.8703 | 0.8731 | 0.8758 |
| 0.8786 | 0.8813 | 0.8841 | 0.8868 | 0.8895 |
| 0.8923 | 0.8950 | 0.8978 | 0.9005 | 0.9033 |
| 0.9060 | 0.9087 | 0.9115 | 0.9142 | 0.9170 |
| 0.9197 | 0.9224 | 0.9252 | 0.9279 | 0.9307 |
| 0.9334 | 0.9345 | 0.9356 | 0.9367 | 0.9379 |
| 0.9390 | 0.9401 | 0.9412 | 0.9423 | 0.9434 |
| 0.9445 | 0.9456 | 0.9467 | 0.9478 | 0.9490 |
| 0.9501 | 0.9512 | 0.9523 | 0.9534 | 0.9545 |
| 0.9556 | 0.9567 | 0.9578 | 0.9589 | 0.9601 |
| 0.9612 | 0.9623 | 0.9634 | 0.9645 | 0.9656 |
| 0.9667 | 0.9678 | 0.9689 | 0.9700 | 0.9711 |
| 0.9723 | 0.9734 | 0.9745 | 0.9756 | 0.9767 |
| 0.9778 | 0.9789 | 0.9800 | 0.9811 | 0.9822 |
| 0.9834 | 0.9845 | 0.9856 | 0.9867 | 0.9878 |
| 0.9889 | 0.9900 | 0.9911 | 0.9922 | 0.9933 |
| 0.9945 | 0.9956 | 0.9967 | 0.9978 | 0.9989 |
| 1.0000 | | | | |

2_yr_sm

0.1

| | | | | |
|--------|--------|--------|--------|--------|
| 0.0000 | 0.0011 | 0.0022 | 0.0033 | 0.0044 |
| 0.0055 | 0.0066 | 0.0077 | 0.0088 | 0.0099 |
| 0.0110 | 0.0122 | 0.0133 | 0.0144 | 0.0155 |
| 0.0166 | 0.0177 | 0.0188 | 0.0199 | 0.0210 |
| 0.0221 | 0.0232 | 0.0243 | 0.0254 | 0.0265 |
| 0.0276 | 0.0287 | 0.0298 | 0.0309 | 0.0320 |
| 0.0331 | 0.0343 | 0.0354 | 0.0365 | 0.0376 |

Eccelston POI 1-4 Ultimate.out

| | | | | |
|--------|--------|--------|--------|--------|
| 0.0387 | 0.0398 | 0.0409 | 0.0420 | 0.0431 |
| 0.0442 | 0.0453 | 0.0464 | 0.0475 | 0.0486 |
| 0.0497 | 0.0508 | 0.0519 | 0.0530 | 0.0541 |
| 0.0552 | 0.0564 | 0.0575 | 0.0586 | 0.0597 |
| 0.0608 | 0.0619 | 0.0630 | 0.0641 | 0.0652 |
| 0.0663 | 0.0690 | 0.0717 | 0.0745 | 0.0772 |
| 0.0799 | 0.0826 | 0.0853 | 0.0881 | 0.0908 |
| 0.0935 | 0.0962 | 0.0989 | 0.1017 | 0.1044 |
| 0.1071 | 0.1098 | 0.1125 | 0.1153 | 0.1180 |
| 0.1207 | 0.1234 | 0.1261 | 0.1289 | 0.1316 |
| 0.1343 | 0.1370 | 0.1397 | 0.1425 | 0.1452 |
| 0.1479 | 0.1525 | 0.1571 | 0.1616 | 0.1662 |
| 0.1708 | 0.1754 | 0.1799 | 0.1845 | 0.1891 |
| 0.1937 | 0.1982 | 0.2028 | 0.2074 | 0.2120 |
| 0.2165 | 0.2207 | 0.2248 | 0.2289 | 0.2330 |
| 0.2372 | 0.2457 | 0.2543 | 0.2629 | 0.2714 |
| 0.2800 | 0.2979 | 0.3158 | 0.3440 | 0.3886 |
| 0.5000 | 0.6114 | 0.6560 | 0.6842 | 0.7021 |
| 0.7200 | 0.7286 | 0.7371 | 0.7457 | 0.7543 |
| 0.7628 | 0.7670 | 0.7711 | 0.7752 | 0.7793 |
| 0.7835 | 0.7880 | 0.7926 | 0.7972 | 0.8018 |
| 0.8063 | 0.8109 | 0.8155 | 0.8201 | 0.8246 |
| 0.8292 | 0.8338 | 0.8384 | 0.8429 | 0.8475 |
| 0.8521 | 0.8548 | 0.8575 | 0.8603 | 0.8630 |
| 0.8657 | 0.8684 | 0.8711 | 0.8739 | 0.8766 |
| 0.8793 | 0.8820 | 0.8847 | 0.8875 | 0.8902 |
| 0.8929 | 0.8956 | 0.8983 | 0.9011 | 0.9038 |
| 0.9065 | 0.9092 | 0.9119 | 0.9147 | 0.9174 |
| 0.9201 | 0.9228 | 0.9255 | 0.9283 | 0.9310 |
| 0.9337 | 0.9348 | 0.9359 | 0.9370 | 0.9381 |
| 0.9392 | 0.9403 | 0.9414 | 0.9425 | 0.9436 |
| 0.9448 | 0.9459 | 0.9470 | 0.9481 | 0.9492 |
| 0.9503 | 0.9514 | 0.9525 | 0.9536 | 0.9547 |
| 0.9558 | 0.9569 | 0.9580 | 0.9591 | 0.9602 |
| 0.9613 | 0.9624 | 0.9635 | 0.9646 | 0.9657 |
| 0.9669 | 0.9680 | 0.9691 | 0.9702 | 0.9713 |
| 0.9724 | 0.9735 | 0.9746 | 0.9757 | 0.9768 |
| 0.9779 | 0.9790 | 0.9801 | 0.9812 | 0.9823 |
| 0.9834 | 0.9845 | 0.9856 | 0.9867 | 0.9878 |
| 0.9890 | 0.9901 | 0.9912 | 0.9923 | 0.9934 |
| 0.9945 | 0.9956 | 0.9967 | 0.9978 | 0.9989 |

5_yr_sm

| | | | | |
|--------|--------|--------|--------|--------|
| | 0.1 | | | |
| 0.0000 | 0.0012 | 0.0024 | 0.0035 | 0.0047 |
| 0.0059 | 0.0071 | 0.0082 | 0.0094 | 0.0106 |
| 0.0118 | 0.0129 | 0.0141 | 0.0153 | 0.0165 |
| 0.0176 | 0.0188 | 0.0200 | 0.0212 | 0.0223 |
| 0.0235 | 0.0247 | 0.0259 | 0.0270 | 0.0282 |
| 0.0294 | 0.0306 | 0.0317 | 0.0329 | 0.0341 |
| 0.0353 | 0.0364 | 0.0376 | 0.0388 | 0.0400 |
| 0.0411 | 0.0423 | 0.0435 | 0.0447 | 0.0458 |
| 0.0470 | 0.0482 | 0.0494 | 0.0505 | 0.0517 |
| 0.0529 | 0.0541 | 0.0552 | 0.0564 | 0.0576 |
| 0.0588 | 0.0599 | 0.0611 | 0.0623 | 0.0635 |
| 0.0646 | 0.0658 | 0.0670 | 0.0682 | 0.0693 |
| 0.0705 | 0.0733 | 0.0761 | 0.0788 | 0.0816 |
| 0.0844 | 0.0871 | 0.0899 | 0.0927 | 0.0954 |
| 0.0982 | 0.1010 | 0.1037 | 0.1065 | 0.1093 |
| 0.1120 | 0.1148 | 0.1176 | 0.1203 | 0.1231 |
| 0.1259 | 0.1286 | 0.1314 | 0.1342 | 0.1369 |
| 0.1397 | 0.1425 | 0.1452 | 0.1480 | 0.1508 |
| 0.1535 | 0.1580 | 0.1624 | 0.1669 | 0.1713 |
| 0.1758 | 0.1802 | 0.1847 | 0.1891 | 0.1936 |

Eccelston POI 1-4 Ultimate.out

| | | | | |
|----------|--------|--------|--------|--------|
| 0.1981 | 0.2025 | 0.2070 | 0.2114 | 0.2159 |
| 0.2203 | 0.2245 | 0.2287 | 0.2329 | 0.2371 |
| 0.2413 | 0.2501 | 0.2588 | 0.2676 | 0.2763 |
| 0.2851 | 0.3040 | 0.3229 | 0.3522 | 0.3968 |
| 0.5000 | 0.6032 | 0.6478 | 0.6771 | 0.6960 |
| 0.7149 | 0.7237 | 0.7324 | 0.7412 | 0.7499 |
| 0.7587 | 0.7629 | 0.7671 | 0.7713 | 0.7755 |
| 0.7797 | 0.7841 | 0.7886 | 0.7930 | 0.7975 |
| 0.8019 | 0.8064 | 0.8109 | 0.8153 | 0.8198 |
| 0.8242 | 0.8287 | 0.8331 | 0.8376 | 0.8420 |
| 0.8465 | 0.8492 | 0.8520 | 0.8548 | 0.8575 |
| 0.8603 | 0.8631 | 0.8658 | 0.8686 | 0.8714 |
| 0.8741 | 0.8769 | 0.8797 | 0.8824 | 0.8852 |
| 0.8880 | 0.8907 | 0.8935 | 0.8963 | 0.8990 |
| 0.9018 | 0.9046 | 0.9073 | 0.9101 | 0.9129 |
| 0.9156 | 0.9184 | 0.9212 | 0.9239 | 0.9267 |
| 0.9295 | 0.9307 | 0.9318 | 0.9330 | 0.9342 |
| 0.9354 | 0.9365 | 0.9377 | 0.9389 | 0.9401 |
| 0.9412 | 0.9424 | 0.9436 | 0.9448 | 0.9459 |
| 0.9471 | 0.9483 | 0.9495 | 0.9506 | 0.9518 |
| 0.9530 | 0.9542 | 0.9553 | 0.9565 | 0.9577 |
| 0.9589 | 0.9600 | 0.9612 | 0.9624 | 0.9636 |
| 0.9647 | 0.9659 | 0.9671 | 0.9683 | 0.9694 |
| 0.9706 | 0.9718 | 0.9730 | 0.9741 | 0.9753 |
| 0.9765 | 0.9777 | 0.9788 | 0.9800 | 0.9812 |
| 0.9824 | 0.9835 | 0.9847 | 0.9859 | 0.9871 |
| 0.9882 | 0.9894 | 0.9906 | 0.9918 | 0.9929 |
| 0.9941 | 0.9953 | 0.9965 | 0.9976 | 0.9988 |
| 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| 10_yr_sm | 0.1 | | | |
| 0.0000 | 0.0012 | 0.0025 | 0.0037 | 0.0049 |
| 0.0061 | 0.0074 | 0.0086 | 0.0098 | 0.0110 |
| 0.0123 | 0.0135 | 0.0147 | 0.0159 | 0.0172 |
| 0.0184 | 0.0196 | 0.0209 | 0.0221 | 0.0233 |
| 0.0245 | 0.0258 | 0.0270 | 0.0282 | 0.0294 |
| 0.0307 | 0.0319 | 0.0331 | 0.0344 | 0.0356 |
| 0.0368 | 0.0380 | 0.0393 | 0.0405 | 0.0417 |
| 0.0429 | 0.0442 | 0.0454 | 0.0466 | 0.0478 |
| 0.0491 | 0.0503 | 0.0515 | 0.0528 | 0.0540 |
| 0.0552 | 0.0564 | 0.0577 | 0.0589 | 0.0601 |
| 0.0613 | 0.0626 | 0.0638 | 0.0650 | 0.0663 |
| 0.0675 | 0.0687 | 0.0699 | 0.0712 | 0.0724 |
| 0.0736 | 0.0765 | 0.0794 | 0.0822 | 0.0851 |
| 0.0880 | 0.0908 | 0.0937 | 0.0966 | 0.0995 |
| 0.1023 | 0.1052 | 0.1081 | 0.1110 | 0.1138 |
| 0.1167 | 0.1196 | 0.1224 | 0.1253 | 0.1282 |
| 0.1311 | 0.1339 | 0.1368 | 0.1397 | 0.1425 |
| 0.1454 | 0.1483 | 0.1512 | 0.1540 | 0.1569 |
| 0.1598 | 0.1642 | 0.1687 | 0.1732 | 0.1777 |
| 0.1821 | 0.1866 | 0.1911 | 0.1956 | 0.2000 |
| 0.2045 | 0.2090 | 0.2134 | 0.2179 | 0.2224 |
| 0.2269 | 0.2311 | 0.2353 | 0.2395 | 0.2438 |
| 0.2480 | 0.2570 | 0.2659 | 0.2749 | 0.2838 |
| 0.2928 | 0.3120 | 0.3312 | 0.3606 | 0.4040 |
| 0.5000 | 0.5960 | 0.6394 | 0.6688 | 0.6880 |
| 0.7072 | 0.7162 | 0.7251 | 0.7341 | 0.7430 |
| 0.7520 | 0.7562 | 0.7605 | 0.7647 | 0.7689 |
| 0.7731 | 0.7776 | 0.7821 | 0.7866 | 0.7910 |
| 0.7955 | 0.8000 | 0.8044 | 0.8089 | 0.8134 |
| 0.8179 | 0.8223 | 0.8268 | 0.8313 | 0.8358 |
| 0.8402 | 0.8431 | 0.8460 | 0.8488 | 0.8517 |
| 0.8546 | 0.8575 | 0.8603 | 0.8632 | 0.8661 |
| 0.8689 | 0.8718 | 0.8747 | 0.8776 | 0.8804 |

Eccelston POI 1-4 Ultimate.out

| | | | | |
|----------|--------|--------|--------|--------|
| 0.8833 | 0.8862 | 0.8890 | 0.8919 | 0.8948 |
| 0.8977 | 0.9005 | 0.9034 | 0.9063 | 0.9092 |
| 0.9120 | 0.9149 | 0.9178 | 0.9206 | 0.9235 |
| 0.9264 | 0.9276 | 0.9288 | 0.9301 | 0.9313 |
| 0.9325 | 0.9337 | 0.9350 | 0.9362 | 0.9374 |
| 0.9387 | 0.9399 | 0.9411 | 0.9423 | 0.9436 |
| 0.9448 | 0.9460 | 0.9472 | 0.9485 | 0.9497 |
| 0.9509 | 0.9522 | 0.9534 | 0.9546 | 0.9558 |
| 0.9571 | 0.9583 | 0.9595 | 0.9607 | 0.9620 |
| 0.9632 | 0.9644 | 0.9656 | 0.9669 | 0.9681 |
| 0.9693 | 0.9706 | 0.9718 | 0.9730 | 0.9742 |
| 0.9755 | 0.9767 | 0.9779 | 0.9791 | 0.9804 |
| 0.9816 | 0.9828 | 0.9841 | 0.9853 | 0.9865 |
| 0.9877 | 0.9890 | 0.9902 | 0.9914 | 0.9926 |
| 0.9939 | 0.9951 | 0.9963 | 0.9975 | 0.9988 |
| 1.0000 | | | | |
| 25_yr_sm | 0.1 | | | |
| 0.0000 | 0.0013 | 0.0026 | 0.0039 | 0.0052 |
| 0.0066 | 0.0079 | 0.0092 | 0.0105 | 0.0118 |
| 0.0131 | 0.0144 | 0.0157 | 0.0170 | 0.0184 |
| 0.0197 | 0.0210 | 0.0223 | 0.0236 | 0.0249 |
| 0.0262 | 0.0275 | 0.0289 | 0.0302 | 0.0315 |
| 0.0328 | 0.0341 | 0.0354 | 0.0367 | 0.0380 |
| 0.0393 | 0.0407 | 0.0420 | 0.0433 | 0.0446 |
| 0.0459 | 0.0472 | 0.0485 | 0.0498 | 0.0511 |
| 0.0525 | 0.0538 | 0.0551 | 0.0564 | 0.0577 |
| 0.0590 | 0.0603 | 0.0616 | 0.0630 | 0.0643 |
| 0.0656 | 0.0669 | 0.0682 | 0.0695 | 0.0708 |
| 0.0721 | 0.0734 | 0.0748 | 0.0761 | 0.0774 |
| 0.0787 | 0.0817 | 0.0847 | 0.0877 | 0.0907 |
| 0.0937 | 0.0967 | 0.0997 | 0.1028 | 0.1058 |
| 0.1088 | 0.1118 | 0.1148 | 0.1178 | 0.1208 |
| 0.1238 | 0.1268 | 0.1298 | 0.1328 | 0.1358 |
| 0.1389 | 0.1419 | 0.1449 | 0.1479 | 0.1509 |
| 0.1539 | 0.1569 | 0.1599 | 0.1629 | 0.1659 |
| 0.1689 | 0.1735 | 0.1781 | 0.1826 | 0.1872 |
| 0.1918 | 0.1963 | 0.2009 | 0.2054 | 0.2100 |
| 0.2146 | 0.2191 | 0.2237 | 0.2283 | 0.2328 |
| 0.2374 | 0.2417 | 0.2460 | 0.2503 | 0.2546 |
| 0.2589 | 0.2681 | 0.2774 | 0.2866 | 0.2958 |
| 0.3050 | 0.3245 | 0.3439 | 0.3726 | 0.4137 |
| 0.5000 | 0.5863 | 0.6274 | 0.6561 | 0.6755 |
| 0.6950 | 0.7042 | 0.7134 | 0.7226 | 0.7319 |
| 0.7411 | 0.7454 | 0.7497 | 0.7540 | 0.7583 |
| 0.7626 | 0.7672 | 0.7717 | 0.7763 | 0.7809 |
| 0.7854 | 0.7900 | 0.7946 | 0.7991 | 0.8037 |
| 0.8082 | 0.8128 | 0.8174 | 0.8219 | 0.8265 |
| 0.8311 | 0.8341 | 0.8371 | 0.8401 | 0.8431 |
| 0.8461 | 0.8491 | 0.8521 | 0.8551 | 0.8581 |
| 0.8611 | 0.8642 | 0.8672 | 0.8702 | 0.8732 |
| 0.8762 | 0.8792 | 0.8822 | 0.8852 | 0.8882 |
| 0.8912 | 0.8942 | 0.8972 | 0.9003 | 0.9033 |
| 0.9063 | 0.9093 | 0.9123 | 0.9153 | 0.9183 |
| 0.9213 | 0.9226 | 0.9239 | 0.9252 | 0.9266 |
| 0.9279 | 0.9292 | 0.9305 | 0.9318 | 0.9331 |
| 0.9344 | 0.9357 | 0.9370 | 0.9384 | 0.9397 |
| 0.9410 | 0.9423 | 0.9436 | 0.9449 | 0.9462 |
| 0.9475 | 0.9489 | 0.9502 | 0.9515 | 0.9528 |
| 0.9541 | 0.9554 | 0.9567 | 0.9580 | 0.9593 |
| 0.9607 | 0.9620 | 0.9633 | 0.9646 | 0.9659 |
| 0.9672 | 0.9685 | 0.9698 | 0.9711 | 0.9725 |
| 0.9738 | 0.9751 | 0.9764 | 0.9777 | 0.9790 |
| 0.9803 | 0.9816 | 0.9830 | 0.9843 | 0.9856 |

| | Eccelston | POI | 1-4 | Ultimate.out | |
|-----------|-----------|--------|--------|--------------|--------|
| | 0.9869 | 0.9882 | 0.9895 | 0.9908 | 0.9921 |
| | 0.9934 | 0.9948 | 0.9961 | 0.9974 | 0.9987 |
| | 1.0000 | | | | |
| 50_yr_sm | 0.1 | | | | |
| | 0.0000 | 0.0014 | 0.0027 | 0.0041 | 0.0055 |
| | 0.0068 | 0.0082 | 0.0096 | 0.0109 | 0.0123 |
| | 0.0137 | 0.0150 | 0.0164 | 0.0178 | 0.0191 |
| | 0.0205 | 0.0219 | 0.0232 | 0.0246 | 0.0260 |
| | 0.0273 | 0.0287 | 0.0301 | 0.0314 | 0.0328 |
| | 0.0342 | 0.0355 | 0.0369 | 0.0383 | 0.0396 |
| | 0.0410 | 0.0424 | 0.0437 | 0.0451 | 0.0465 |
| | 0.0478 | 0.0492 | 0.0505 | 0.0519 | 0.0533 |
| | 0.0546 | 0.0560 | 0.0574 | 0.0587 | 0.0601 |
| | 0.0615 | 0.0628 | 0.0642 | 0.0656 | 0.0669 |
| | 0.0683 | 0.0697 | 0.0710 | 0.0724 | 0.0738 |
| | 0.0751 | 0.0765 | 0.0779 | 0.0792 | 0.0806 |
| | 0.0820 | 0.0851 | 0.0882 | 0.0914 | 0.0945 |
| | 0.0977 | 0.1008 | 0.1039 | 0.1071 | 0.1102 |
| | 0.1134 | 0.1165 | 0.1196 | 0.1228 | 0.1259 |
| | 0.1290 | 0.1322 | 0.1353 | 0.1385 | 0.1416 |
| | 0.1447 | 0.1479 | 0.1510 | 0.1541 | 0.1573 |
| | 0.1604 | 0.1636 | 0.1667 | 0.1698 | 0.1730 |
| | 0.1761 | 0.1808 | 0.1854 | 0.1901 | 0.1947 |
| | 0.1994 | 0.2040 | 0.2087 | 0.2133 | 0.2180 |
| | 0.2227 | 0.2273 | 0.2320 | 0.2366 | 0.2413 |
| | 0.2459 | 0.2503 | 0.2546 | 0.2589 | 0.2633 |
| | 0.2676 | 0.2771 | 0.2866 | 0.2961 | 0.3056 |
| | 0.3151 | 0.3345 | 0.3538 | 0.3819 | 0.4208 |
| | 0.5000 | 0.5792 | 0.6181 | 0.6462 | 0.6655 |
| | 0.6849 | 0.6944 | 0.7039 | 0.7134 | 0.7229 |
| | 0.7324 | 0.7367 | 0.7411 | 0.7454 | 0.7497 |
| | 0.7541 | 0.7587 | 0.7634 | 0.7680 | 0.7727 |
| | 0.7773 | 0.7820 | 0.7867 | 0.7913 | 0.7960 |
| | 0.8006 | 0.8053 | 0.8099 | 0.8146 | 0.8192 |
| | 0.8239 | 0.8270 | 0.8302 | 0.8333 | 0.8364 |
| | 0.8396 | 0.8427 | 0.8459 | 0.8490 | 0.8521 |
| | 0.8553 | 0.8584 | 0.8615 | 0.8647 | 0.8678 |
| | 0.8710 | 0.8741 | 0.8772 | 0.8804 | 0.8835 |
| | 0.8866 | 0.8898 | 0.8929 | 0.8961 | 0.8992 |
| | 0.9023 | 0.9055 | 0.9086 | 0.9118 | 0.9149 |
| | 0.9180 | 0.9194 | 0.9208 | 0.9221 | 0.9235 |
| | 0.9249 | 0.9262 | 0.9276 | 0.9290 | 0.9303 |
| | 0.9317 | 0.9331 | 0.9344 | 0.9358 | 0.9372 |
| | 0.9385 | 0.9399 | 0.9413 | 0.9426 | 0.9440 |
| | 0.9454 | 0.9467 | 0.9481 | 0.9495 | 0.9508 |
| | 0.9522 | 0.9535 | 0.9549 | 0.9563 | 0.9576 |
| | 0.9590 | 0.9604 | 0.9617 | 0.9631 | 0.9645 |
| | 0.9658 | 0.9672 | 0.9686 | 0.9699 | 0.9713 |
| | 0.9727 | 0.9740 | 0.9754 | 0.9768 | 0.9781 |
| | 0.9795 | 0.9809 | 0.9822 | 0.9836 | 0.9850 |
| | 0.9863 | 0.9877 | 0.9891 | 0.9904 | 0.9918 |
| | 0.9932 | 0.9945 | 0.9959 | 0.9973 | 0.9986 |
| | 1.0000 | | | | |
| 100_yr_sm | 0.1 | | | | |
| | 0.0000 | 0.0014 | 0.0029 | 0.0043 | 0.0057 |
| | 0.0071 | 0.0086 | 0.0100 | 0.0114 | 0.0129 |
| | 0.0143 | 0.0157 | 0.0171 | 0.0186 | 0.0200 |
| | 0.0214 | 0.0229 | 0.0243 | 0.0257 | 0.0271 |
| | 0.0286 | 0.0300 | 0.0314 | 0.0329 | 0.0343 |
| | 0.0357 | 0.0372 | 0.0386 | 0.0400 | 0.0414 |
| | 0.0429 | 0.0443 | 0.0457 | 0.0472 | 0.0486 |
| | 0.0500 | 0.0514 | 0.0529 | 0.0543 | 0.0557 |
| | 0.0572 | 0.0586 | 0.0600 | 0.0614 | 0.0629 |

Eccelston POI 1-4 Ultimate.out

| | | | | |
|-----------|--------|--------|--------|--------|
| 0.0643 | 0.0657 | 0.0672 | 0.0686 | 0.0700 |
| 0.0714 | 0.0729 | 0.0743 | 0.0757 | 0.0772 |
| 0.0786 | 0.0800 | 0.0814 | 0.0829 | 0.0843 |
| 0.0857 | 0.0890 | 0.0923 | 0.0955 | 0.0988 |
| 0.1021 | 0.1054 | 0.1086 | 0.1119 | 0.1152 |
| 0.1185 | 0.1217 | 0.1250 | 0.1283 | 0.1315 |
| 0.1348 | 0.1381 | 0.1414 | 0.1446 | 0.1479 |
| 0.1512 | 0.1544 | 0.1577 | 0.1610 | 0.1643 |
| 0.1675 | 0.1708 | 0.1741 | 0.1773 | 0.1806 |
| 0.1839 | 0.1886 | 0.1934 | 0.1981 | 0.2029 |
| 0.2076 | 0.2123 | 0.2171 | 0.2218 | 0.2266 |
| 0.2313 | 0.2361 | 0.2408 | 0.2455 | 0.2503 |
| 0.2550 | 0.2594 | 0.2637 | 0.2680 | 0.2723 |
| 0.2767 | 0.2864 | 0.2961 | 0.3058 | 0.3155 |
| 0.3252 | 0.3444 | 0.3635 | 0.3907 | 0.4275 |
| 0.5000 | 0.5725 | 0.6093 | 0.6365 | 0.6556 |
| 0.6748 | 0.6845 | 0.6942 | 0.7039 | 0.7136 |
| 0.7233 | 0.7277 | 0.7320 | 0.7363 | 0.7406 |
| 0.7450 | 0.7497 | 0.7545 | 0.7592 | 0.7639 |
| 0.7687 | 0.7734 | 0.7782 | 0.7829 | 0.7877 |
| 0.7924 | 0.7971 | 0.8019 | 0.8066 | 0.8114 |
| 0.8161 | 0.8194 | 0.8227 | 0.8259 | 0.8292 |
| 0.8325 | 0.8357 | 0.8390 | 0.8423 | 0.8456 |
| 0.8488 | 0.8521 | 0.8554 | 0.8586 | 0.8619 |
| 0.8652 | 0.8685 | 0.8717 | 0.8750 | 0.8783 |
| 0.8815 | 0.8848 | 0.8881 | 0.8914 | 0.8946 |
| 0.8979 | 0.9012 | 0.9045 | 0.9077 | 0.9110 |
| 0.9143 | 0.9157 | 0.9171 | 0.9186 | 0.9200 |
| 0.9214 | 0.9228 | 0.9243 | 0.9257 | 0.9271 |
| 0.9286 | 0.9300 | 0.9314 | 0.9328 | 0.9343 |
| 0.9357 | 0.9371 | 0.9386 | 0.9400 | 0.9414 |
| 0.9428 | 0.9443 | 0.9457 | 0.9471 | 0.9486 |
| 0.9500 | 0.9514 | 0.9528 | 0.9543 | 0.9557 |
| 0.9571 | 0.9586 | 0.9600 | 0.9614 | 0.9628 |
| 0.9643 | 0.9657 | 0.9671 | 0.9686 | 0.9700 |
| 0.9714 | 0.9729 | 0.9743 | 0.9757 | 0.9771 |
| 0.9786 | 0.9800 | 0.9814 | 0.9829 | 0.9843 |
| 0.9857 | 0.9871 | 0.9886 | 0.9900 | 0.9914 |
| 0.9929 | 0.9943 | 0.9957 | 0.9971 | 0.9986 |
| 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| 500_yr_sm | 0.1 | | | |
| 0.0000 | 0.0016 | 0.0031 | 0.0047 | 0.0063 |
| 0.0079 | 0.0094 | 0.0110 | 0.0126 | 0.0141 |
| 0.0157 | 0.0173 | 0.0189 | 0.0204 | 0.0220 |
| 0.0236 | 0.0252 | 0.0267 | 0.0283 | 0.0299 |
| 0.0314 | 0.0330 | 0.0346 | 0.0362 | 0.0377 |
| 0.0393 | 0.0409 | 0.0424 | 0.0440 | 0.0456 |
| 0.0472 | 0.0487 | 0.0503 | 0.0519 | 0.0535 |
| 0.0550 | 0.0566 | 0.0582 | 0.0597 | 0.0613 |
| 0.0629 | 0.0645 | 0.0660 | 0.0676 | 0.0692 |
| 0.0707 | 0.0723 | 0.0739 | 0.0755 | 0.0770 |
| 0.0786 | 0.0802 | 0.0817 | 0.0833 | 0.0849 |
| 0.0865 | 0.0880 | 0.0896 | 0.0912 | 0.0928 |
| 0.0943 | 0.0979 | 0.1015 | 0.1051 | 0.1087 |
| 0.1123 | 0.1159 | 0.1195 | 0.1231 | 0.1267 |
| 0.1303 | 0.1340 | 0.1376 | 0.1412 | 0.1448 |
| 0.1484 | 0.1520 | 0.1556 | 0.1592 | 0.1628 |
| 0.1664 | 0.1700 | 0.1736 | 0.1772 | 0.1808 |
| 0.1844 | 0.1880 | 0.1916 | 0.1952 | 0.1988 |
| 0.2024 | 0.2073 | 0.2122 | 0.2172 | 0.2221 |
| 0.2270 | 0.2319 | 0.2368 | 0.2418 | 0.2467 |
| 0.2516 | 0.2565 | 0.2615 | 0.2664 | 0.2713 |
| 0.2762 | 0.2806 | 0.2849 | 0.2893 | 0.2936 |

Eccelston POI 1-4 Ultimate.out

| | | | | |
|--------|--------|--------|--------|--------|
| 0.2979 | 0.3081 | 0.3182 | 0.3283 | 0.3384 |
| 0.3486 | 0.3669 | 0.3853 | 0.4101 | 0.4419 |
| 0.5000 | 0.5581 | 0.5899 | 0.6147 | 0.6331 |
| 0.6514 | 0.6616 | 0.6717 | 0.6818 | 0.6919 |
| 0.7021 | 0.7064 | 0.7107 | 0.7151 | 0.7194 |
| 0.7238 | 0.7287 | 0.7336 | 0.7385 | 0.7435 |
| 0.7484 | 0.7533 | 0.7582 | 0.7632 | 0.7681 |
| 0.7730 | 0.7779 | 0.7828 | 0.7878 | 0.7927 |
| 0.7976 | 0.8012 | 0.8048 | 0.8084 | 0.8120 |
| 0.8156 | 0.8192 | 0.8228 | 0.8264 | 0.8300 |
| 0.8336 | 0.8372 | 0.8408 | 0.8444 | 0.8480 |
| 0.8516 | 0.8552 | 0.8588 | 0.8624 | 0.8660 |
| 0.8697 | 0.8733 | 0.8769 | 0.8805 | 0.8841 |
| 0.8877 | 0.8913 | 0.8949 | 0.8985 | 0.9021 |
| 0.9057 | 0.9072 | 0.9088 | 0.9104 | 0.9120 |
| 0.9135 | 0.9151 | 0.9167 | 0.9183 | 0.9198 |
| 0.9214 | 0.9230 | 0.9245 | 0.9261 | 0.9277 |
| 0.9293 | 0.9308 | 0.9324 | 0.9340 | 0.9355 |
| 0.9371 | 0.9387 | 0.9403 | 0.9418 | 0.9434 |
| 0.9450 | 0.9465 | 0.9481 | 0.9497 | 0.9513 |
| 0.9528 | 0.9544 | 0.9560 | 0.9576 | 0.9591 |
| 0.9607 | 0.9623 | 0.9638 | 0.9654 | 0.9670 |
| 0.9686 | 0.9701 | 0.9717 | 0.9733 | 0.9748 |
| 0.9764 | 0.9780 | 0.9796 | 0.9811 | 0.9827 |
| 0.9843 | 0.9859 | 0.9874 | 0.9890 | 0.9906 |
| 0.9921 | 0.9937 | 0.9953 | 0.9969 | 0.9984 |
| 1.0000 | | | | |

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Eccelston Mitigation POI 1-4 Ultimate

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STORM 1_yr_sm

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | ----- Elevation (ft) | Peak Flow Time (hr) | Rate (cfs) | Rate (csm) |
|--------------------------------|-----------------------------|--------------------------------|--------------------------|----------------------------|---------------------------|---------------|---------------|
| DA4 | 0.450 | | 0.770 | | 12.80 | 97.0 | 215.53 |

| Line Start Time (hr) | ----- (cfs) | Flow (cfs) | values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | ----- (cfs) | ----- (cfs) |
|----------------------------|----------------|---------------|------------------------|--------------------|----------------------|----------------|----------------|
| 11.600 | 0.0 | 1.2 | 5.2 | 21.7 | 54.2 | 85.6 | 96.9 |
| 13.000 | 89.4 | 72.1 | 56.5 | 44.3 | 35.1 | 28.8 | 24.9 |
| 14.400 | 22.7 | 21.4 | 20.6 | 20.2 | 19.8 | 19.0 | 17.4 |

Eccelston POI 1-4 Ultimate.out

| | | | | | | | |
|--------|------|------|------|------|------|------|------|
| 15.800 | 15.8 | 14.4 | 13.5 | 13.0 | 12.6 | 12.5 | 12.4 |
| 17.200 | 12.3 | 12.3 | 12.3 | 12.4 | 12.4 | 12.3 | 11.6 |
| 18.600 | 10.3 | 8.8 | 7.5 | 6.6 | 6.1 | 5.7 | 5.5 |
| 20.000 | 5.4 | 5.3 | 5.3 | 5.2 | 5.2 | 5.2 | 5.2 |
| 21.400 | 5.2 | 5.2 | 5.2 | 5.2 | 5.3 | 5.2 | 5.2 |
| 22.800 | 5.3 | 5.3 | 5.3 | 5.3 | 5.3 | 5.3 | 5.3 |
| 24.200 | 5.2 | 4.7 | 3.8 | 2.7 | 1.7 | 1.1 | 0.7 |
| 25.600 | 0.0 | | | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| DA2 | 1.323 | | 0.724 | | 12.99 | 228.3 | 172.56 |

Line Start Time (hr) ----- Flow values @ time increment of 0.200 hr -----

| Start Time (hr) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|-----------------|------------|------------|------------|------------|------------|------------|------------|
| 11.600 | 0.0 | 1.3 | 7.6 | 34.2 | 90.7 | 163.0 | 213.2 |
| 13.000 | 227.9 | 213.1 | 180.2 | 146.3 | 119.4 | 98.8 | 83.9 |
| 14.400 | 73.8 | 67.4 | 63.3 | 60.6 | 58.6 | 56.3 | 53.0 |
| 15.800 | 49.0 | 44.9 | 41.3 | 38.8 | 37.3 | 36.3 | 35.7 |
| 17.200 | 35.4 | 35.2 | 35.1 | 35.1 | 35.1 | 34.9 | 33.8 |
| 18.600 | 31.4 | 28.0 | 24.5 | 21.5 | 19.2 | 17.8 | 16.8 |
| 20.000 | 16.1 | 15.7 | 15.3 | 15.1 | 15.0 | 14.9 | 14.9 |
| 21.400 | 14.8 | 14.8 | 14.8 | 14.8 | 14.9 | 14.9 | 14.9 |
| 22.800 | 14.9 | 15.0 | 15.0 | 15.0 | 15.0 | 15.0 | 15.1 |
| 24.200 | 14.9 | 14.1 | 12.3 | 9.8 | 7.2 | 5.0 | 3.4 |
| 25.600 | 2.3 | 1.6 | 1.1 | 0.8 | 0.5 | 0.0 | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| DA3 | 0.920 | | 0.478 | | 12.99 | 96.7 | 105.07 |

Eccelston Mitigation POI 1-4 Ultimate

Line Start Time (hr) ----- Flow values @ time increment of 0.200 hr -----

| Start Time (hr) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|-----------------|------------|------------|------------|------------|------------|------------|------------|
| 11.800 | 0.0 | 0.8 | 10.3 | 35.6 | 69.5 | 91.3 | 96.4 |
| 13.200 | 87.7 | 72.9 | 59.8 | 49.2 | 41.3 | 36.1 | 32.9 |
| 14.600 | 31.1 | 30.1 | 29.5 | 29.1 | 28.2 | 26.4 | 24.2 |
| 16.000 | 22.1 | 20.6 | 19.7 | 19.2 | 18.8 | 18.7 | 18.6 |
| 17.400 | 18.6 | 18.6 | 18.7 | 18.8 | 18.7 | 18.0 | 16.3 |
| 18.800 | 14.3 | 12.3 | 10.7 | 9.8 | 9.1 | 8.7 | 8.5 |
| 20.200 | 8.3 | 8.2 | 8.1 | 8.1 | 8.1 | 8.1 | 8.1 |
| 21.600 | 8.0 | 8.1 | 8.1 | 8.1 | 8.1 | 8.1 | 8.2 |
| 23.000 | 8.2 | 8.2 | 8.2 | 8.2 | 8.3 | 8.3 | 8.2 |
| 24.400 | 7.6 | 6.3 | 4.8 | 3.3 | 2.1 | 1.4 | 0.9 |
| 25.800 | 0.6 | 0.0 | | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|

Eccelston POI 1-4 Ultimate.out

CON-1 2.693 Upstream 0.647 362.88 12.95 416.3 154.55

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | values @ time (cfs) | increment (cfs) | of 0.200 (cfs) | hr (cfs) | (cfs) |
|----------------------|------------|------------|---------------------|-----------------|----------------|----------|-------|
| 11.600 | 0.0 | 2.5 | 13.7 | 67.8 | 180.6 | 317.8 | 401.4 |
| 13.000 | 412.7 | 372.9 | 309.7 | 250.4 | 203.7 | 169.0 | 145.0 |
| 14.400 | 129.5 | 119.9 | 114.0 | 110.4 | 107.5 | 103.4 | 96.9 |
| 15.800 | 89.0 | 81.4 | 75.5 | 71.5 | 69.1 | 67.6 | 66.8 |
| 17.200 | 66.3 | 66.1 | 66.1 | 66.2 | 66.3 | 65.8 | 63.4 |
| 18.600 | 58.0 | 51.1 | 44.4 | 38.9 | 35.1 | 32.6 | 31.0 |
| 20.000 | 30.0 | 29.3 | 28.8 | 28.5 | 28.3 | 28.2 | 28.2 |
| 21.400 | 28.1 | 28.1 | 28.1 | 28.2 | 28.2 | 28.3 | 28.3 |
| 22.800 | 28.3 | 28.4 | 28.5 | 28.5 | 28.5 | 28.6 | 28.7 |
| 24.200 | 28.2 | 26.3 | 22.3 | 17.2 | 12.2 | 8.3 | 5.5 |
| 25.600 | 3.6 | 2.2 | 1.1 | 0.8 | 0.5 | 0.0 | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| CON-1 | 2.693 | Downstream | 0.647 | 362.81 | 13.23 | 381.8 | 141.77 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | values @ time (cfs) | increment (cfs) | of 0.200 (cfs) | hr (cfs) | (cfs) |
|----------------------|------------|------------|---------------------|-----------------|----------------|----------|-------|
| 11.800 | 0.0 | 3.7 | 22.2 | 75.9 | 172.1 | 280.0 | 356.0 |
| 13.200 | 381.6 | 362.3 | 317.2 | 266.0 | 220.0 | 183.2 | 156.1 |
| 14.600 | 137.4 | 125.2 | 117.4 | 112.4 | 108.4 | 103.8 | 97.7 |
| 16.000 | 90.6 | 83.7 | 77.7 | 73.3 | 70.4 | 68.5 | 67.3 |
| 17.400 | 66.6 | 66.3 | 66.2 | 66.2 | 66.2 | 65.4 | 62.9 |
| 18.800 | 58.4 | 52.4 | 46.2 | 40.9 | 36.8 | 33.8 | 31.9 |
| 20.200 | 30.5 | 29.6 | 29.0 | 28.6 | 28.4 | 28.3 | 28.2 |
| 21.600 | 28.1 | 28.1 | 28.1 | 28.2 | 28.2 | 28.2 | 28.3 |

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Eccelston Mitigation POI 1-4 Ultimate

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | values @ time (cfs) | increment (cfs) | of 0.200 (cfs) | hr (cfs) | (cfs) |
|----------------------|------------|------------|---------------------|-----------------|----------------|----------|-------|
| 23.000 | 28.3 | 28.4 | 28.5 | 28.5 | 28.5 | 28.6 | 28.5 |
| 24.400 | 27.9 | 26.0 | 22.6 | 18.2 | 13.6 | 9.7 | 6.7 |
| 25.800 | 4.4 | 2.8 | 1.7 | 1.0 | 0.0 | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| DA1 | 0.090 | | 0.866 | | 12.20 | 52.5 | 582.75 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | values @ time (cfs) | increment (cfs) | of 0.200 (cfs) | hr (cfs) | (cfs) |
|----------------------|------------|------------|---------------------|-----------------|----------------|----------|-------|
| 11.200 | 0.0 | 0.8 | 1.4 | 3.7 | 15.8 | 52.4 | 29.6 |
| 12.600 | 15.4 | 8.5 | 7.4 | 5.2 | 3.8 | 3.7 | 4.0 |
| 14.000 | 4.1 | 4.1 | 4.2 | 4.2 | 4.3 | 4.3 | 3.3 |
| 15.400 | 2.7 | 2.6 | 2.6 | 2.6 | 2.6 | 2.6 | 2.6 |

Eccelston POI 1-4 Ultimate.out

| | | | | | | | |
|--------|-----|-----|-----|-----|-----|-----|-----|
| 16.800 | 2.7 | 2.7 | 2.6 | 2.7 | 2.7 | 2.7 | 2.7 |
| 18.200 | 1.8 | 1.2 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 |
| 19.600 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 |
| 21.000 | 1.1 | 1.1 | 1.1 | 1.2 | 1.1 | 1.1 | 1.1 |
| 22.400 | 1.1 | 1.2 | 1.1 | 1.1 | 1.1 | 1.1 | 1.2 |
| 23.800 | 1.1 | 1.1 | 0.0 | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| OUTLET | 2.783 | | 0.654 | | 13.17 | 387.2 | 139.11 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow Rate (cfs) | Rate (cfs) |
|----------------------|------------|------------|---------------------|-----------------|-------------------|-----------------|------------|
| 11.200 | 0.0 | 0.8 | 1.4 | 3.7 | 19.5 | 74.6 | 105.5 |
| 12.600 | 187.5 | 288.6 | 363.4 | 386.9 | 366.1 | 320.9 | 270.0 |
| 14.000 | 224.1 | 187.3 | 160.2 | 141.6 | 129.5 | 121.7 | 115.7 |
| 15.400 | 111.1 | 106.4 | 100.3 | 93.2 | 86.3 | 80.3 | 76.0 |
| 16.800 | 73.0 | 71.1 | 70.0 | 69.3 | 69.0 | 68.9 | 68.9 |
| 18.200 | 67.9 | 66.6 | 64.1 | 59.5 | 53.5 | 47.3 | 42.0 |
| 19.600 | 37.9 | 34.9 | 33.0 | 31.6 | 30.8 | 30.2 | 29.7 |
| 21.000 | 29.5 | 29.4 | 29.3 | 29.3 | 29.2 | 29.2 | 29.3 |
| 22.400 | 29.3 | 29.4 | 29.4 | 29.5 | 29.5 | 29.6 | 29.7 |
| 23.800 | 29.7 | 29.7 | 29.0 | 27.9 | 26.0 | 22.6 | 18.2 |
| 25.200 | 13.6 | 9.7 | 6.7 | 4.4 | 2.8 | 1.7 | 1.0 |
| 26.600 | 0.0 | | | | | | |

STORM 2_yr_sm

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Eccelston Mitigation POI 1-4 Ultimate

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| DA4 | 0.450 | | 1.141 | | 12.79 | 151.7 | 337.08 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow Rate (cfs) | Rate (cfs) |
|----------------------|------------|------------|---------------------|-----------------|-------------------|-----------------|------------|
| 11.000 | 0.0 | 0.9 | 1.7 | 3.1 | 5.7 | 13.6 | 40.8 |
| 12.400 | 91.0 | 136.9 | 151.5 | 137.6 | 109.3 | 84.6 | 65.5 |
| 13.800 | 51.3 | 41.6 | 35.6 | 32.1 | 30.0 | 28.7 | 28.0 |
| 15.200 | 27.4 | 26.1 | 23.9 | 21.6 | 19.7 | 18.5 | 17.7 |
| 16.600 | 17.3 | 17.0 | 16.9 | 16.8 | 16.8 | 16.8 | 16.8 |
| 18.000 | 16.8 | 16.7 | 15.8 | 14.0 | 11.9 | 10.1 | 9.0 |
| 19.400 | 8.3 | 7.8 | 7.5 | 7.3 | 7.2 | 7.1 | 7.1 |
| 20.800 | 7.0 | 7.0 | 7.0 | 7.1 | 7.1 | 7.1 | 7.1 |
| 22.200 | 7.1 | 7.1 | 7.1 | 7.1 | 7.1 | 7.1 | 7.1 |
| 23.600 | 7.2 | 7.2 | 7.2 | 7.0 | 6.3 | 5.1 | 3.6 |
| 25.000 | 2.3 | 1.4 | 0.9 | 0.6 | 0.0 | | |

| Area or Reach | Drainage Area | Rain Gage ID or | Runoff Amount | Elevation | Peak Time | Flow Rate | Rate |
|---------------|---------------|-----------------|---------------|-----------|-----------|-----------|------|
|---------------|---------------|-----------------|---------------|-----------|-----------|-----------|------|

| Identifier | (sq mi) | Location | Eccelston POI 1-4 (in) | Ultimate.out (ft) | (hr) | (cfs) | (csm) |
|------------|---------|----------|------------------------|-------------------|-------|-------|--------|
| DA2 | 1.323 | | 1.084 | | 12.99 | 363.3 | 274.58 |

| Line Start Time (hr) | Flow (cfs) | values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow (cfs) | (cfs) |
|----------------------|------------|---------------------|-----------------|-------------------|------------|-------|
| 11.000 | 0.0 | 0.7 | 1.8 | 4.1 | 9.0 | 23.8 |
| 12.400 | 162.3 | 273.3 | 346.0 | 362.1 | 333.0 | 277.5 |
| 13.800 | 179.7 | 147.1 | 123.4 | 107.4 | 97.0 | 90.2 |
| 15.200 | 82.3 | 78.7 | 73.9 | 68.0 | 62.2 | 57.2 |
| 16.600 | 51.4 | 50.0 | 49.1 | 48.6 | 48.3 | 48.1 |
| 18.000 | 48.1 | 47.7 | 46.2 | 42.9 | 38.2 | 33.4 |
| 19.400 | 26.3 | 24.3 | 23.0 | 22.0 | 21.4 | 20.9 |
| 20.800 | 20.4 | 20.3 | 20.2 | 20.2 | 20.2 | 20.2 |
| 22.200 | 20.2 | 20.2 | 20.2 | 20.2 | 20.2 | 20.3 |
| 23.600 | 20.4 | 20.5 | 20.5 | 20.2 | 19.0 | 16.6 |
| 25.000 | 9.8 | 6.8 | 4.6 | 3.2 | 2.2 | 1.5 |
| 26.400 | 0.7 | 0.0 | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|--------|
| DA3 | 0.920 | | 0.771 | | 12.88 | 175.5 | 190.74 |

Eccelston Mitigation POI 1-4 Ultimate

| Line Start Time (hr) | Flow (cfs) | values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow (cfs) | (cfs) |
|----------------------|------------|---------------------|-----------------|-------------------|------------|-------|
| 11.800 | 0.2 | 4.1 | 26.8 | 76.4 | 136.0 | 170.9 |
| 13.200 | 152.7 | 123.8 | 99.4 | 80.3 | 66.4 | 56.9 |
| 14.600 | 47.6 | 45.5 | 44.2 | 43.2 | 41.7 | 38.9 |
| 16.000 | 32.4 | 30.1 | 28.7 | 27.9 | 27.4 | 27.1 |
| 17.400 | 26.9 | 26.9 | 27.0 | 27.1 | 26.9 | 25.8 |
| 18.800 | 20.4 | 17.6 | 15.4 | 14.0 | 13.2 | 12.6 |
| 20.200 | 11.9 | 11.7 | 11.6 | 11.5 | 11.5 | 11.5 |
| 21.600 | 11.6 | 11.6 | 11.6 | 11.6 | 11.6 | 11.6 |
| 23.000 | 11.6 | 11.7 | 11.7 | 11.8 | 11.8 | 11.8 |
| 24.400 | 10.7 | 9.0 | 6.7 | 4.7 | 3.0 | 2.0 |
| 25.800 | 0.9 | 0.6 | 0.0 | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|--------|
| CON-1 | 2.693 | Upstream | 0.986 | 363.35 | 12.94 | 682.1 | 253.25 |

| Line Start Time (hr) | Flow (cfs) | values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow (cfs) | (cfs) |
|----------------------|------------|---------------------|-----------------|-------------------|------------|-------|
|----------------------|------------|---------------------|-----------------|-------------------|------------|-------|

Eccelston POI 1-4 Ultimate.out

| | | | | | | | |
|--------|-------|-------|-------|-------|-------|-------|-------|
| 11.000 | 0.0 | 1.5 | 3.5 | 7.2 | 14.9 | 41.5 | 139.9 |
| 12.400 | 330.6 | 545.7 | 667.5 | 672.3 | 594.6 | 486.1 | 387.8 |
| 13.800 | 311.4 | 255.1 | 216.1 | 190.7 | 174.7 | 164.5 | 158.0 |
| 15.200 | 152.9 | 146.4 | 136.7 | 125.2 | 114.4 | 105.8 | 100.0 |
| 16.600 | 96.5 | 94.4 | 93.1 | 92.3 | 92.0 | 91.8 | 91.9 |
| 18.000 | 92.0 | 91.2 | 87.8 | 80.3 | 70.6 | 61.2 | 53.7 |
| 19.400 | 48.6 | 45.3 | 43.1 | 41.5 | 40.4 | 39.7 | 39.2 |
| 20.800 | 38.9 | 38.8 | 38.7 | 38.8 | 38.9 | 38.9 | 38.9 |
| 22.200 | 38.9 | 38.8 | 38.9 | 38.9 | 38.9 | 39.0 | 39.2 |
| 23.600 | 39.4 | 39.4 | 39.4 | 38.7 | 36.1 | 30.6 | 23.6 |
| 25.000 | 16.8 | 11.3 | 7.5 | 5.1 | 3.0 | 2.1 | 1.0 |
| 26.400 | 0.7 | 0.0 | | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| CON-1 | 2.693 | Downstream | 0.986 | 363.29 | 13.08 | 645.7 | 239.72 |

| Line Start Time (hr) | Flow (cfs) | Flow values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow Rate (cfs) | Rate (cfs) | |
|----------------------|------------|--------------------------|-----------------|-------------------|-----------------|------------|-------|
| 11.200 | 0.0 | 1.7 | 4.3 | 8.9 | 21.5 | 69.1 | 186.0 |
| 12.600 | 367.3 | 540.6 | 634.6 | 634.6 | 567.7 | 474.3 | 385.1 |
| 14.000 | 312.1 | 257.3 | 218.5 | 192.8 | 176.0 | 165.4 | 158.3 |
| 15.400 | 152.2 | 144.7 | 134.9 | 124.1 | 114.1 | 106.1 | 100.5 |
| 16.800 | 96.9 | 94.6 | 93.2 | 92.4 | 92.0 | 91.9 | 91.9 |
| 18.200 | 91.7 | 90.2 | 85.9 | 78.4 | 69.5 | 60.8 | 53.9 |
| 19.600 | 48.9 | 45.5 | 43.2 | 41.6 | 40.5 | 39.8 | 39.3 |

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Eccelston Mitigation POI 1-4 Ultimate

| Line Start Time (hr) | Flow (cfs) | Flow values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow Rate (cfs) | Rate (cfs) | |
|----------------------|------------|--------------------------|-----------------|-------------------|-----------------|------------|------|
| 21.000 | 39.0 | 38.8 | 38.8 | 38.8 | 38.9 | 38.9 | 38.9 |
| 22.400 | 38.9 | 38.9 | 38.9 | 38.9 | 39.0 | 39.1 | 39.2 |
| 23.800 | 39.3 | 39.4 | 39.2 | 38.0 | 34.7 | 29.3 | 22.8 |
| 25.200 | 16.5 | 11.4 | 7.8 | 5.1 | 3.3 | 2.0 | 1.2 |
| 26.600 | 0.0 | | | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| DA1 | 0.090 | | 1.259 | | 12.19 | 77.9 | 865.40 |

| Line Start Time (hr) | Flow (cfs) | Flow values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow Rate (cfs) | Rate (cfs) | |
|----------------------|------------|--------------------------|-----------------|-------------------|-----------------|------------|------|
| 10.400 | 0.0 | 0.5 | 0.6 | 0.7 | 1.5 | 2.2 | 3.2 |
| 11.800 | 7.4 | 26.9 | 77.9 | 43.1 | 22.4 | 12.0 | 10.3 |
| 13.200 | 7.2 | 5.2 | 5.1 | 5.5 | 5.6 | 5.6 | 5.7 |
| 14.600 | 5.7 | 5.7 | 5.8 | 4.5 | 3.6 | 3.5 | 3.5 |
| 16.000 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.6 | 3.5 |
| 17.400 | 3.6 | 3.6 | 3.6 | 3.6 | 2.4 | 1.6 | 1.5 |
| 18.800 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 |
| 20.200 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 |

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| | | | | | | | |
|--------|-----|-----|-----|-----|-----|-----|-----|
| 21.600 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 |
| 23.000 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 0.7 |
| 24.400 | 0.0 | | | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| OUTLET | 2.783 | | 0.995 | | 13.08 | 655.4 | 235.47 |

| Line Start Time (hr) | Flow (cfs) | Values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow Rate (cfs) | Rate (cfs) | |
|----------------------|------------|---------------------|-----------------|-------------------|-----------------|------------|-------|
| 10.400 | 0.0 | 0.5 | 0.6 | 0.7 | 1.5 | 4.0 | 7.5 |
| 11.800 | 16.4 | 48.5 | 147.0 | 229.2 | 389.7 | 552.6 | 644.6 |
| 13.200 | 641.8 | 572.9 | 479.4 | 390.5 | 317.7 | 262.9 | 224.2 |
| 14.600 | 198.4 | 181.8 | 171.1 | 162.7 | 155.8 | 148.1 | 138.4 |
| 16.000 | 127.6 | 117.5 | 109.6 | 104.0 | 100.4 | 98.2 | 96.8 |
| 17.400 | 96.0 | 95.6 | 95.5 | 95.5 | 94.1 | 91.8 | 87.3 |
| 18.800 | 79.9 | 70.9 | 62.3 | 55.4 | 50.4 | 47.0 | 44.7 |
| 20.200 | 43.1 | 42.0 | 41.2 | 40.8 | 40.5 | 40.3 | 40.3 |
| 21.600 | 40.3 | 40.4 | 40.4 | 40.4 | 40.4 | 40.3 | 40.4 |
| 23.000 | 40.4 | 40.5 | 40.6 | 40.7 | 40.9 | 40.9 | 39.8 |
| 24.400 | 38.0 | 34.7 | 29.3 | 22.8 | 16.5 | 11.4 | 7.8 |
| 25.800 | 5.1 | 3.3 | 2.0 | 1.2 | 0.0 | | |

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Eccelston Mitigation POI 1-4 Ultimate

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| DA4 | 0.450 | | 1.825 | | 12.75 | 243.7 | 541.36 |

| Line Start Time (hr) | Flow (cfs) | Values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow Rate (cfs) | Rate (cfs) | |
|----------------------|------------|---------------------|-----------------|-------------------|-----------------|------------|-------|
| 9.800 | 0.4 | 1.1 | 1.8 | 2.7 | 3.7 | 4.7 | 5.6 |
| 11.200 | 6.7 | 8.6 | 11.9 | 18.0 | 33.7 | 78.9 | 157.1 |
| 12.600 | 225.3 | 243.0 | 218.2 | 172.7 | 133.1 | 102.4 | 79.8 |
| 14.000 | 64.1 | 54.0 | 48.0 | 44.4 | 42.1 | 40.7 | 39.6 |
| 15.400 | 37.6 | 34.6 | 31.5 | 28.9 | 27.2 | 26.2 | 25.6 |
| 16.800 | 25.2 | 25.0 | 24.9 | 24.8 | 24.8 | 24.9 | 24.9 |
| 18.200 | 24.6 | 23.4 | 20.8 | 17.9 | 15.3 | 13.6 | 12.5 |
| 19.600 | 11.9 | 11.5 | 11.2 | 11.0 | 10.9 | 10.9 | 10.8 |
| 21.000 | 10.8 | 10.8 | 10.8 | 10.8 | 10.8 | 10.8 | 10.9 |
| 22.400 | 10.9 | 10.9 | 10.9 | 10.9 | 10.9 | 10.9 | 10.9 |
| 23.800 | 10.9 | 10.9 | 10.7 | 9.7 | 7.8 | 5.5 | 3.5 |
| 25.200 | 2.2 | 1.4 | 0.9 | 0.6 | 0.0 | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| DA2 | 1.323 | | 1.752 | | 12.95 | 597.5 | 451.60 |

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| Start Time (hr) | Eccelston POI 1-4 Ultimate.out Flow Values @ time increment of 0.200 hr | | | | | | |
|-----------------|--|-------|-------|-------|-------|-------|-------|
| (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) |
| 9.800 | 0.0 | 0.9 | 2.1 | 3.8 | 5.9 | 8.3 | 10.7 |
| 11.200 | 13.6 | 17.7 | 24.5 | 36.7 | 66.0 | 150.0 | 297.3 |
| 12.600 | 469.5 | 575.1 | 592.2 | 540.3 | 446.9 | 357.3 | 286.2 |
| 14.000 | 232.1 | 193.1 | 165.8 | 147.6 | 135.6 | 127.6 | 121.6 |
| 15.400 | 115.7 | 108.3 | 100.0 | 91.7 | 84.6 | 79.5 | 76.4 |
| 16.800 | 74.5 | 73.3 | 72.5 | 72.0 | 71.8 | 71.7 | 71.7 |
| 18.200 | 71.1 | 69.0 | 64.2 | 57.4 | 50.5 | 44.5 | 40.0 |
| 19.600 | 37.2 | 35.2 | 33.9 | 32.9 | 32.3 | 31.9 | 31.6 |
| 21.000 | 31.4 | 31.3 | 31.3 | 31.2 | 31.2 | 31.2 | 31.2 |
| 22.400 | 31.2 | 31.3 | 31.3 | 31.3 | 31.4 | 31.4 | 31.4 |
| 23.800 | 31.5 | 31.5 | 31.1 | 29.4 | 25.7 | 20.5 | 15.2 |
| 25.200 | 10.5 | 7.1 | 4.9 | 3.4 | 2.3 | 1.6 | 1.1 |
| 26.600 | 0.7 | 0.0 | | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| DA3 | 0.920 | | 1.339 | | 12.85 | 325.1 | 353.25 |

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Eccelston Mitigation POI 1-4 Ultimate

| Line Start Time (hr) | Flow values @ time increment of 0.200 hr | | | | | | |
|----------------------|--|-------|-------|-------|-------|-------|-------|
| (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) |
| 11.200 | 0.0 | 1.5 | 3.7 | 8.8 | 23.8 | 73.2 | 166.3 |
| 12.600 | 268.1 | 320.2 | 316.8 | 273.2 | 218.7 | 173.7 | 138.4 |
| 14.000 | 112.7 | 94.9 | 83.7 | 76.7 | 72.3 | 69.5 | 67.4 |
| 15.400 | 64.6 | 60.3 | 55.2 | 50.6 | 47.2 | 45.2 | 43.9 |
| 16.800 | 43.1 | 42.7 | 42.5 | 42.4 | 42.4 | 42.4 | 42.5 |
| 18.200 | 42.2 | 40.6 | 37.0 | 32.4 | 28.1 | 24.7 | 22.6 |
| 19.600 | 21.2 | 20.3 | 19.7 | 19.3 | 19.0 | 18.9 | 18.8 |
| 21.000 | 18.7 | 18.7 | 18.7 | 18.7 | 18.7 | 18.8 | 18.8 |
| 22.400 | 18.8 | 18.8 | 18.9 | 18.9 | 18.9 | 18.9 | 19.0 |
| 23.800 | 19.0 | 19.0 | 18.7 | 17.4 | 14.5 | 11.0 | 7.6 |
| 25.200 | 4.9 | 3.2 | 2.1 | 1.4 | 0.9 | 0.6 | 0.0 |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| CON-1 | 2.693 | Upstream | 1.623 | 363.93 | 12.89 | 1154.4 | 428.62 |

| Line Start Time (hr) | Flow values @ time increment of 0.200 hr | | | | | | |
|----------------------|--|--------|--------|-------|-------|-------|-------|
| (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) |
| 9.800 | 0.4 | 2.0 | 3.9 | 6.5 | 9.6 | 12.9 | 16.3 |
| 11.200 | 20.4 | 27.8 | 40.2 | 63.4 | 126.3 | 302.8 | 620.9 |
| 12.600 | 962.8 | 1135.9 | 1126.2 | 985.2 | 798.9 | 633.5 | 504.6 |
| 14.000 | 409.5 | 342.1 | 297.6 | 268.7 | 250.2 | 237.8 | 228.5 |
| 15.400 | 217.9 | 203.2 | 186.6 | 171.2 | 159.1 | 150.9 | 145.9 |
| 16.800 | 142.8 | 140.9 | 139.8 | 139.3 | 139.0 | 139.0 | 139.0 |

Eccelston POI 1-4 Ultimate.out

| | | | | | | | |
|--------|-------|-------|-------|-------|------|------|------|
| 18.200 | 137.9 | 132.8 | 121.9 | 107.7 | 93.9 | 82.9 | 75.2 |
| 19.600 | 70.2 | 66.9 | 64.7 | 63.3 | 62.3 | 61.7 | 61.3 |
| 21.000 | 61.0 | 60.9 | 60.8 | 60.8 | 60.8 | 60.8 | 60.9 |
| 22.400 | 60.9 | 61.0 | 61.1 | 61.1 | 61.2 | 61.3 | 61.3 |
| 23.800 | 61.4 | 61.4 | 60.5 | 56.5 | 48.0 | 36.9 | 26.3 |
| 25.200 | 17.7 | 11.8 | 7.9 | 5.3 | 3.2 | 2.2 | 1.1 |
| 26.600 | 0.7 | 0.0 | | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| CON-1 | 2.693 | Downstream | 1.623 | 363.87 | 13.03 | 1106.3 | 410.76 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|------------|------------|------------|------------|------------|
| 9.800 | 0.0 | 0.9 | 2.6 | 4.8 | 7.6 | 10.7 | 14.0 |
| 11.200 | 17.6 | 23.2 | 32.3 | 48.8 | 87.3 | 196.2 | 424.2 |
| 12.600 | 739.2 | 996.0 | 1102.0 | 1056.0 | 914.3 | 747.3 | 599.0 |
| 14.000 | 481.4 | 394.0 | 332.8 | 292.0 | 265.3 | 247.8 | 235.8 |
| 15.400 | 225.3 | 212.8 | 197.6 | 181.9 | 167.9 | 157.2 | 149.9 |
| 16.800 | 145.4 | 142.5 | 140.8 | 139.8 | 139.2 | 139.0 | 139.0 |

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| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|------------|------------|------------|------------|------------|
| 18.200 | 138.6 | 135.9 | 128.6 | 116.8 | 103.3 | 90.8 | 81.0 |
| 19.600 | 74.2 | 69.6 | 66.5 | 64.4 | 63.1 | 62.2 | 61.6 |
| 21.000 | 61.2 | 61.0 | 60.9 | 60.8 | 60.8 | 60.8 | 60.8 |
| 22.400 | 60.9 | 61.0 | 61.0 | 61.1 | 61.1 | 61.2 | 61.3 |
| 23.800 | 61.4 | 61.4 | 61.0 | 58.8 | 53.1 | 44.0 | 33.5 |
| 25.200 | 23.9 | 16.3 | 11.0 | 7.4 | 4.8 | 3.1 | 1.9 |
| 26.600 | 1.1 | 0.7 | 0.0 | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| DA1 | 0.090 | | 1.975 | | 12.19 | 116.5 | 1293.98 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|------------|------------|------------|------------|------------|
| 9.200 | 0.0 | 0.6 | 0.8 | 1.1 | 1.3 | 1.5 | 1.7 |
| 10.600 | 1.9 | 2.0 | 2.2 | 3.9 | 5.5 | 7.3 | 15.8 |
| 12.000 | 47.4 | 116.2 | 65.3 | 34.7 | 18.3 | 15.5 | 10.8 |
| 13.400 | 7.8 | 7.5 | 7.8 | 7.9 | 8.0 | 8.0 | 8.0 |
| 14.800 | 8.1 | 8.1 | 6.4 | 5.3 | 5.1 | 5.1 | 5.1 |
| 16.200 | 5.1 | 5.1 | 5.2 | 5.2 | 5.2 | 5.2 | 5.2 |
| 17.600 | 5.2 | 5.2 | 5.2 | 3.6 | 2.4 | 2.3 | 2.2 |
| 19.000 | 2.3 | 2.2 | 2.3 | 2.2 | 2.3 | 2.2 | 2.3 |
| 20.400 | 2.2 | 2.3 | 2.2 | 2.3 | 2.3 | 2.3 | 2.3 |
| 21.800 | 2.3 | 2.3 | 2.3 | 2.3 | 2.3 | 2.3 | 2.3 |
| 23.200 | 2.3 | 2.3 | 2.3 | 2.3 | 2.3 | 1.0 | 0.0 |

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| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| OUTLET | 2.783 | | 1.634 | | 13.03 | 1121.1 | 402.77 |

Line

| Start Time (hr) | Flow (cfs) | Flow (cfs) | values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow (cfs) | Rate (cfs) |
|-----------------|------------|------------|---------------------|-----------------|-------------------|------------|------------|
| 9.200 | 0.0 | 0.6 | 0.8 | 1.1 | 2.2 | 4.2 | 6.6 |
| 10.600 | 9.5 | 12.7 | 16.2 | 21.6 | 28.7 | 39.7 | 64.7 |
| 12.000 | 134.7 | 312.4 | 489.6 | 774.0 | 1014.3 | 1117.5 | 1066.8 |
| 13.400 | 922.1 | 754.8 | 606.7 | 489.3 | 402.0 | 340.8 | 300.0 |
| 14.800 | 273.4 | 255.9 | 242.1 | 230.6 | 217.9 | 202.7 | 187.0 |
| 16.200 | 173.0 | 162.3 | 155.1 | 150.6 | 147.7 | 146.0 | 145.0 |
| 17.600 | 144.4 | 144.3 | 144.3 | 142.2 | 138.3 | 130.8 | 119.0 |
| 19.000 | 105.5 | 93.1 | 83.3 | 76.4 | 71.8 | 68.7 | 66.7 |
| 20.400 | 65.3 | 64.4 | 63.8 | 63.5 | 63.2 | 63.1 | 63.0 |
| 21.800 | 63.1 | 63.1 | 63.1 | 63.1 | 63.2 | 63.3 | 63.4 |
| 23.200 | 63.4 | 63.5 | 63.6 | 63.7 | 63.7 | 62.0 | 58.8 |
| 24.600 | 53.1 | 44.0 | 33.6 | 23.9 | 16.3 | 11.0 | 7.4 |

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Line

| Start Time (hr) | Flow (cfs) | Flow (cfs) | values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow (cfs) | Rate (cfs) |
|-----------------|------------|------------|---------------------|-----------------|-------------------|------------|------------|
| 26.000 | 4.8 | 3.1 | 1.9 | 1.1 | 0.7 | 0.0 | |

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| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| DA4 | 0.450 | | 2.473 | | 12.76 | 322.2 | 715.80 |

Line

| Start Time (hr) | Flow (cfs) | Flow (cfs) | values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow (cfs) | Rate (cfs) |
|-----------------|------------|------------|---------------------|-----------------|-------------------|------------|------------|
| 8.800 | 0.0 | 0.8 | 1.3 | 2.1 | 3.2 | 4.5 | 5.9 |
| 10.200 | 7.4 | 8.8 | 10.1 | 11.4 | 12.6 | 14.1 | 17.0 |
| 11.600 | 22.3 | 31.8 | 54.7 | 115.0 | 215.5 | 299.8 | 320.3 |
| 13.000 | 286.8 | 227.2 | 175.3 | 135.0 | 105.0 | 84.1 | 70.6 |
| 14.400 | 62.6 | 57.7 | 54.6 | 52.8 | 51.2 | 48.7 | 45.0 |
| 15.800 | 41.1 | 38.0 | 35.8 | 34.6 | 33.8 | 33.4 | 33.1 |
| 17.200 | 33.0 | 33.0 | 33.0 | 33.0 | 33.0 | 32.6 | 31.0 |
| 18.600 | 27.6 | 23.7 | 20.3 | 18.0 | 16.7 | 15.8 | 15.2 |
| 20.000 | 14.9 | 14.7 | 14.5 | 14.5 | 14.4 | 14.4 | 14.4 |
| 21.400 | 14.4 | 14.4 | 14.4 | 14.4 | 14.4 | 14.4 | 14.4 |
| 22.800 | 14.4 | 14.5 | 14.5 | 14.5 | 14.5 | 14.5 | 14.5 |
| 24.200 | 14.2 | 12.9 | 10.3 | 7.3 | 4.7 | 2.9 | 1.9 |
| 25.600 | 1.2 | 0.7 | 0.0 | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|

Eccelston POI 1-4 Ultimate.out

DA2 1.323 2.388 12.91 798.4 603.48

| Line Start Time (hr) | Flow (cfs) | values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Peak Flow Rate (cfs) | Rate (csm) |
|----------------------|------------|---------------------|-----------------|-------------------|----------------------|------------|
| 8.800 | 0.0 | 0.5 | 1.3 | 2.6 | 4.7 | 10.7 |
| 10.200 | 14.4 | 18.1 | 21.9 | 25.6 | 29.2 | 39.4 |
| 11.600 | 50.1 | 69.7 | 115.5 | 228.7 | 423.2 | 774.2 |
| 13.000 | 791.7 | 716.4 | 592.9 | 473.5 | 379.2 | 254.7 |
| 14.400 | 218.0 | 193.8 | 177.5 | 166.5 | 158.5 | 141.4 |
| 15.800 | 130.8 | 120.5 | 111.6 | 105.2 | 101.4 | 97.4 |
| 17.200 | 96.4 | 95.9 | 95.6 | 95.5 | 95.4 | 91.7 |
| 18.600 | 85.2 | 76.4 | 67.2 | 59.3 | 53.5 | 47.0 |
| 20.000 | 45.2 | 44.0 | 43.1 | 42.6 | 42.2 | 41.8 |
| 21.400 | 41.7 | 41.6 | 41.6 | 41.6 | 41.6 | 41.7 |
| 22.800 | 41.7 | 41.8 | 41.8 | 41.8 | 41.9 | 41.9 |
| 24.200 | 41.3 | 39.1 | 34.1 | 27.2 | 20.1 | 9.5 |
| 25.600 | 6.5 | 4.5 | 3.1 | 2.1 | 1.4 | 0.6 |
| 27.000 | 0.0 | | | | | |

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Eccelston Mitigation POI 1-4 Ultimate

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| DA3 | 0.920 | | 1.901 | | 12.82 | 459.7 | 499.57 |

| Line Start Time (hr) | Flow (cfs) | values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Peak Flow Rate (cfs) | Rate (csm) |
|----------------------|------------|---------------------|-----------------|-------------------|----------------------|------------|
| 10.200 | 0.3 | 1.3 | 2.5 | 4.1 | 5.9 | 11.4 |
| 11.600 | 17.1 | 27.3 | 53.8 | 126.0 | 256.7 | 456.1 |
| 13.000 | 444.9 | 381.1 | 304.6 | 241.0 | 191.7 | 130.2 |
| 14.400 | 114.2 | 104.2 | 97.8 | 93.7 | 90.6 | 81.2 |
| 15.800 | 74.6 | 68.7 | 64.3 | 61.7 | 60.1 | 58.6 |
| 17.200 | 58.2 | 58.1 | 58.1 | 58.2 | 58.3 | 55.5 |
| 18.600 | 50.6 | 44.3 | 38.4 | 33.9 | 31.0 | 27.8 |
| 20.000 | 27.0 | 26.5 | 26.1 | 25.9 | 25.8 | 25.7 |
| 21.400 | 25.6 | 25.6 | 25.7 | 25.7 | 25.7 | 25.8 |
| 22.800 | 25.8 | 25.9 | 25.9 | 25.9 | 26.0 | 26.0 |
| 24.200 | 25.5 | 23.7 | 19.8 | 14.9 | 10.3 | 4.4 |
| 25.600 | 2.9 | 1.9 | 1.3 | 0.8 | 0.5 | 0.0 |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| CON-1 | 2.693 | Upstream | 2.236 | 364.39 | 12.90 | 1565.7 | 581.33 |

| Line Start Time (hr) | Flow (cfs) | values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Peak Flow Rate (cfs) | Rate (csm) |
|----------------------|------------|---------------------|-----------------|-------------------|----------------------|------------|
| 8.800 | 0.0 | 1.3 | 2.6 | 4.7 | 7.8 | 16.7 |
| 10.200 | 22.0 | 28.2 | 34.6 | 41.2 | 47.7 | 67.8 |
| 11.600 | 89.8 | 129.6 | 224.8 | 471.5 | 895.8 | 1548.5 |
| 13.000 | 1520.2 | 1324.6 | 1072.8 | 850.1 | 676.4 | 455.9 |
| 14.400 | 394.9 | 355.8 | 330.0 | 313.1 | 300.3 | 267.6 |

Eccelston POI 1-4 Ultimate.out

| | | | | | | | |
|--------|-------|-------|-------|-------|-------|-------|-------|
| 15.800 | 246.5 | 227.1 | 211.8 | 201.5 | 195.4 | 191.5 | 189.1 |
| 17.200 | 187.7 | 187.0 | 186.7 | 186.6 | 186.6 | 184.9 | 178.2 |
| 18.600 | 163.3 | 144.3 | 126.0 | 111.2 | 101.1 | 94.5 | 90.1 |
| 20.000 | 87.0 | 85.1 | 83.8 | 83.0 | 82.4 | 82.1 | 81.8 |
| 21.400 | 81.7 | 81.6 | 81.7 | 81.7 | 81.8 | 81.9 | 81.9 |
| 22.800 | 82.0 | 82.1 | 82.2 | 82.3 | 82.3 | 82.3 | 82.3 |
| 24.200 | 81.0 | 75.6 | 64.2 | 49.4 | 35.2 | 23.7 | 15.8 |
| 25.600 | 10.6 | 7.1 | 4.6 | 2.9 | 1.9 | 1.0 | 0.6 |
| 27.000 | 0.0 | | | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| CON-1 | 2.693 | Downstream | 2.235 | 364.32 | 12.98 | 1500.7 | 557.16 |

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Eccelston Mitigation POI 1-4 Ultimate

| Line Start Time (hr) | Flow values @ time increment of 0.200 hr | | | | | | |
|----------------------|--|--------|-------|-------|--------|--------|--------|
| (hr) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) |
| 9.000 | 0.2 | 1.7 | 3.4 | 6.0 | 9.5 | 13.8 | 18.7 |
| 10.400 | 24.5 | 30.7 | 37.1 | 43.6 | 50.6 | 60.5 | 77.2 |
| 11.800 | 106.8 | 170.8 | 334.9 | 657.9 | 1072.8 | 1388.8 | 1499.3 |
| 13.200 | 1413.7 | 1212.8 | 988.5 | 791.7 | 636.2 | 520.4 | 439.3 |
| 14.600 | 385.2 | 349.5 | 325.9 | 309.6 | 295.5 | 278.8 | 259.2 |
| 16.000 | 239.4 | 221.9 | 208.8 | 200.1 | 194.5 | 191.0 | 188.8 |
| 17.400 | 187.6 | 187.0 | 186.7 | 186.6 | 185.9 | 181.8 | 171.4 |
| 18.800 | 155.3 | 137.3 | 120.9 | 108.2 | 99.4 | 93.4 | 89.3 |
| 20.200 | 86.6 | 84.8 | 83.6 | 82.9 | 82.3 | 82.0 | 81.8 |
| 21.600 | 81.7 | 81.7 | 81.7 | 81.8 | 81.8 | 81.9 | 81.9 |
| 23.000 | 82.0 | 82.1 | 82.2 | 82.3 | 82.3 | 82.3 | 81.7 |
| 24.400 | 78.5 | 70.4 | 57.9 | 44.0 | 31.2 | 21.3 | 14.4 |
| 25.800 | 9.7 | 6.5 | 4.1 | 2.7 | 1.5 | 0.9 | 0.0 |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| DA1 | 0.090 | | 2.645 | | 12.19 | 146.8 | 1630.38 |

| Line Start Time (hr) | Flow values @ time increment of 0.200 hr | | | | | | |
|----------------------|--|-------|-------|-------|-------|-------|-------|
| (hr) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) |
| 8.400 | 0.0 | 0.6 | 0.8 | 0.9 | 1.4 | 1.9 | 2.2 |
| 9.800 | 2.5 | 2.8 | 3.1 | 3.3 | 3.6 | 3.6 | 3.8 |
| 11.200 | 6.7 | 9.1 | 11.8 | 24.3 | 65.4 | 146.4 | 83.1 |
| 12.600 | 45.1 | 24.0 | 20.3 | 14.1 | 10.1 | 9.7 | 10.1 |
| 14.000 | 10.1 | 10.2 | 10.3 | 10.3 | 10.3 | 10.4 | 8.3 |
| 15.400 | 6.9 | 6.8 | 6.7 | 6.7 | 6.8 | 6.8 | 6.8 |
| 16.800 | 6.8 | 6.9 | 6.8 | 6.9 | 6.8 | 6.9 | 6.9 |
| 18.200 | 4.6 | 3.2 | 2.9 | 3.0 | 2.9 | 3.0 | 2.9 |
| 19.600 | 3.0 | 2.9 | 3.0 | 3.0 | 2.9 | 3.0 | 2.9 |
| 21.000 | 3.0 | 2.9 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| 22.400 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| 23.800 | 3.0 | 3.0 | 1.3 | 0.0 | | | |

Eccelston POI 1-4 Ultimate.out

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| OUTLET | 2.783 | | 2.249 | | 12.97 | 1520.5 | 546.28 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow Rate (cfs) | Rate (cfs) |
|----------------------|------------|------------|---------------------|-----------------|-------------------|-----------------|------------|
| 8.400 | 0.0 | 0.6 | 0.8 | 1.1 | 3.1 | 5.4 | 8.3 |
| 9.800 | 12.1 | 16.6 | 21.8 | 27.8 | 34.2 | 40.7 | 47.5 |
| 11.200 | 57.3 | 69.6 | 89.1 | 131.1 | 236.2 | 481.6 | 741.3 |
| 12.600 | 1118.0 | 1412.9 | 1519.7 | 1427.5 | 1222.8 | 998.0 | 801.7 |
| 14.000 | 646.2 | 530.6 | 449.5 | 395.5 | 359.8 | 336.2 | 317.9 |

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Eccelston Mitigation POI 1-4 Ultimate

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow Rate (cfs) | Rate (cfs) |
|----------------------|------------|------------|---------------------|-----------------|-------------------|-----------------|------------|
| 15.400 | 302.4 | 285.6 | 265.9 | 246.1 | 228.7 | 215.6 | 206.9 |
| 16.800 | 201.3 | 197.8 | 195.6 | 194.5 | 193.8 | 193.6 | 193.5 |
| 18.200 | 190.5 | 185.0 | 174.3 | 158.3 | 140.2 | 123.9 | 111.1 |
| 19.600 | 102.3 | 96.3 | 92.2 | 89.6 | 87.7 | 86.6 | 85.8 |
| 21.000 | 85.4 | 84.9 | 84.8 | 84.6 | 84.6 | 84.7 | 84.8 |
| 22.400 | 84.8 | 84.9 | 85.0 | 85.0 | 85.2 | 85.2 | 85.3 |
| 23.800 | 85.3 | 85.4 | 83.0 | 78.5 | 70.4 | 58.0 | 44.0 |
| 25.200 | 31.3 | 21.4 | 14.4 | 9.7 | 6.5 | 4.1 | 2.7 |
| 26.600 | 1.5 | 0.9 | 0.0 | | | | |

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| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| DA4 | 0.450 | | 3.530 | | 12.76 | 434.7 | 965.82 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow Rate (cfs) | Rate (cfs) |
|----------------------|------------|------------|---------------------|-----------------|-------------------|-----------------|------------|
| 7.600 | 0.4 | 1.1 | 1.9 | 2.8 | 3.8 | 4.8 | 5.8 |
| 9.000 | 6.8 | 7.9 | 9.4 | 11.7 | 14.2 | 16.7 | 19.0 |
| 10.400 | 21.1 | 23.0 | 24.8 | 26.2 | 28.3 | 32.9 | 41.8 |
| 11.800 | 57.2 | 91.6 | 173.6 | 303.5 | 408.9 | 431.7 | 385.6 |
| 13.200 | 307.1 | 238.3 | 184.1 | 143.6 | 115.1 | 96.8 | 85.9 |
| 14.600 | 79.2 | 75.0 | 72.4 | 70.2 | 67.0 | 62.0 | 56.9 |
| 16.000 | 52.7 | 49.9 | 48.3 | 47.4 | 46.8 | 46.4 | 46.2 |
| 17.400 | 46.1 | 46.1 | 46.1 | 46.2 | 45.6 | 43.3 | 38.6 |
| 18.800 | 33.3 | 28.7 | 25.5 | 23.6 | 22.4 | 21.6 | 21.2 |
| 20.200 | 20.8 | 20.7 | 20.6 | 20.5 | 20.4 | 20.4 | 20.4 |
| 21.600 | 20.5 | 20.4 | 20.4 | 20.5 | 20.5 | 20.5 | 20.5 |
| 23.000 | 20.5 | 20.6 | 20.6 | 20.5 | 20.5 | 20.6 | 20.2 |
| 24.400 | 18.3 | 14.6 | 10.3 | 6.6 | 4.1 | 2.6 | 1.6 |
| 25.800 | 1.0 | 0.6 | 0.0 | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|

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| Reach Identifier | Area (sq mi) | ID or Location | Amount (in) | Elevation (ft) | Time (hr) | Rate (cfs) | Rate (csm) |
|------------------|--------------|----------------|-------------|----------------|-----------|------------|------------|
| DA2 | 1.323 | | 3.430 | | 12.92 | 1093.4 | 826.46 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|------------|------------|------------|------------|------------|
| 7.600 | 0.0 | 0.9 | 2.1 | 3.9 | 6.0 | 8.5 | 11.1 |
| 9.000 | 13.8 | 16.8 | 20.5 | 25.4 | 31.3 | 37.8 | 44.3 |
| 10.400 | 50.6 | 56.4 | 61.7 | 66.5 | 72.1 | 81.8 | 99.6 |
| 11.800 | 131.5 | 201.3 | 359.8 | 617.5 | 899.5 | 1064.6 | 1080.5 |
| 13.200 | 977.4 | 810.7 | 650.3 | 521.2 | 423.3 | 351.2 | 300.5 |

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Eccelston Mitigation POI 1-4 Ultimate

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|------------|------------|------------|------------|------------|
| 14.600 | 267.3 | 244.9 | 229.7 | 218.5 | 208.0 | 195.4 | 181.2 |
| 16.000 | 167.4 | 155.6 | 147.2 | 142.3 | 139.1 | 136.9 | 135.5 |
| 17.400 | 134.7 | 134.2 | 134.1 | 134.0 | 132.9 | 128.8 | 119.8 |
| 18.800 | 107.5 | 94.9 | 83.9 | 75.8 | 70.5 | 66.9 | 64.4 |
| 20.200 | 62.7 | 61.5 | 60.8 | 60.3 | 59.9 | 59.6 | 59.5 |
| 21.600 | 59.4 | 59.4 | 59.3 | 59.3 | 59.4 | 59.5 | 59.5 |
| 23.000 | 59.5 | 59.6 | 59.6 | 59.6 | 59.7 | 59.7 | 58.9 |
| 24.400 | 55.7 | 48.6 | 38.7 | 28.6 | 19.9 | 13.5 | 9.3 |
| 25.800 | 6.4 | 4.4 | 3.0 | 2.0 | 1.4 | 0.9 | 0.6 |
| 27.200 | 0.0 | | | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Peak Rate (cfs) | Peak Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| DA3 | 0.920 | | 2.845 | | 12.83 | 665.3 | 722.99 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|------------|------------|------------|------------|------------|
| 9.000 | 0.1 | 1.2 | 2.5 | 4.4 | 7.0 | 10.1 | 13.3 |
| 10.400 | 16.6 | 19.9 | 23.1 | 26.0 | 29.6 | 35.6 | 46.6 |
| 11.800 | 65.9 | 110.6 | 218.3 | 400.6 | 581.0 | 661.3 | 638.5 |
| 13.200 | 545.6 | 437.1 | 346.4 | 275.4 | 222.9 | 186.8 | 163.6 |
| 14.600 | 149.2 | 139.8 | 133.7 | 129.2 | 123.9 | 116.0 | 106.8 |
| 16.000 | 98.7 | 92.8 | 89.2 | 87.1 | 85.7 | 84.9 | 84.4 |
| 17.400 | 84.1 | 84.1 | 84.2 | 84.3 | 83.6 | 80.3 | 73.2 |
| 18.800 | 64.3 | 56.0 | 49.4 | 45.2 | 42.5 | 40.8 | 39.6 |
| 20.200 | 38.8 | 38.4 | 38.1 | 37.9 | 37.7 | 37.7 | 37.7 |
| 21.600 | 37.7 | 37.7 | 37.7 | 37.7 | 37.8 | 37.8 | 37.9 |
| 23.000 | 37.9 | 38.0 | 38.0 | 38.0 | 38.0 | 38.1 | 37.5 |
| 24.400 | 34.7 | 29.0 | 21.8 | 15.1 | 9.8 | 6.5 | 4.3 |
| 25.800 | 2.8 | 1.8 | 1.2 | 0.8 | 0.0 | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Peak Rate (cfs) | Peak Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| CON-1 | 2.693 | Upstream | 3.247 | 364.98 | 12.83 | 2173.2 | 806.86 |

Eccelston POI 1-4 Ultimate.out

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|---------------------|-----------------|-------------------|------------|------------|
| 7.600 | 0.4 | 2.1 | 4.0 | 6.7 | 9.8 | 13.3 | 16.9 |
| 9.000 | 20.8 | 25.9 | 32.4 | 41.5 | 52.6 | 64.6 | 76.7 |
| 10.400 | 88.3 | 99.3 | 109.5 | 118.8 | 129.9 | 150.3 | 188.0 |
| 11.800 | 256.1 | 403.6 | 754.2 | 1321.6 | 1885.4 | 2157.1 | 2100.7 |
| 13.200 | 1829.9 | 1486.1 | 1181.0 | 941.3 | 761.9 | 635.2 | 550.0 |
| 14.600 | 495.9 | 459.8 | 435.9 | 417.9 | 398.9 | 373.4 | 345.1 |
| 16.000 | 318.9 | 298.4 | 284.8 | 276.8 | 271.6 | 268.2 | 266.0 |

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Eccelston Mitigation POI 1-4 Ultimate

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|---------------------|-----------------|-------------------|------------|------------|
| 17.400 | 264.8 | 264.4 | 264.4 | 264.5 | 262.0 | 252.4 | 231.5 |
| 18.800 | 205.1 | 179.6 | 158.8 | 144.6 | 135.4 | 129.4 | 125.2 |
| 20.200 | 122.4 | 120.6 | 119.5 | 118.7 | 118.0 | 117.7 | 117.6 |
| 21.600 | 117.6 | 117.5 | 117.4 | 117.5 | 117.7 | 117.8 | 117.9 |
| 23.000 | 118.0 | 118.2 | 118.2 | 118.2 | 118.2 | 118.3 | 116.5 |
| 24.400 | 108.7 | 92.1 | 70.9 | 50.4 | 34.0 | 22.6 | 15.2 |
| 25.800 | 10.2 | 6.8 | 4.5 | 2.8 | 1.9 | 0.9 | 0.6 |
| 27.200 | 0.0 | | | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| CON-1 | 2.693 | Downstream | 3.247 | 364.92 | 12.97 | 2076.7 | 771.04 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|---------------------|-----------------|-------------------|------------|------------|
| 7.600 | 0.0 | 1.0 | 2.9 | 5.2 | 8.0 | 11.3 | 14.8 |
| 9.000 | 18.5 | 23.1 | 28.8 | 36.6 | 46.5 | 57.8 | 69.6 |
| 10.400 | 81.4 | 92.6 | 103.3 | 113.1 | 123.4 | 139.5 | 168.6 |
| 11.800 | 220.9 | 327.8 | 579.0 | 1029.1 | 1571.2 | 1959.4 | 2071.6 |
| 13.200 | 1936.6 | 1659.9 | 1357.6 | 1092.1 | 880.3 | 722.1 | 610.5 |
| 14.600 | 536.3 | 486.7 | 453.7 | 430.7 | 410.8 | 387.7 | 361.1 |
| 16.000 | 334.4 | 311.4 | 294.1 | 282.8 | 275.5 | 270.8 | 267.7 |
| 17.400 | 265.8 | 264.9 | 264.6 | 264.5 | 263.2 | 257.0 | 241.8 |
| 18.800 | 219.1 | 194.3 | 171.7 | 154.2 | 142.0 | 133.8 | 128.2 |
| 20.200 | 124.4 | 121.9 | 120.3 | 119.3 | 118.5 | 118.0 | 117.7 |
| 21.600 | 117.6 | 117.5 | 117.5 | 117.5 | 117.6 | 117.7 | 117.8 |
| 23.000 | 117.9 | 118.1 | 118.2 | 118.2 | 118.2 | 118.3 | 117.3 |
| 24.400 | 112.4 | 100.3 | 82.1 | 62.2 | 44.2 | 30.3 | 20.5 |
| 25.800 | 13.9 | 9.3 | 6.2 | 3.9 | 2.6 | 1.5 | 0.9 |
| 27.200 | 0.0 | | | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| DA1 | 0.090 | | 3.731 | | 12.19 | 187.5 | 2082.06 |

Line

| Start Time (hr) | Eccelston POI 1-4 Ultimate.out Flow Values @ time increment of 0.200 hr | | | | | | |
|-----------------|--|-------|-------|-------|-------|-------|-------|
| (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) |
| 7.000 | 0.0 | 0.6 | 0.9 | 1.1 | 1.3 | 1.6 | 1.8 |
| 8.400 | 2.0 | 2.2 | 2.4 | 2.6 | 3.6 | 4.5 | 5.0 |
| 9.800 | 5.3 | 5.7 | 6.0 | 6.4 | 6.6 | 6.6 | 6.8 |
| 11.200 | 11.7 | 15.6 | 19.7 | 38.5 | 91.8 | 186.5 | 107.9 |
| 12.600 | 60.8 | 32.9 | 28.2 | 19.3 | 13.8 | 13.2 | 13.7 |
| 14.000 | 13.9 | 13.9 | 13.9 | 13.9 | 14.1 | 14.1 | 11.4 |
| 15.400 | 9.6 | 9.3 | 9.3 | 9.3 | 9.5 | 9.4 | 9.4 |

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Eccelston Mitigation POI 1-4 Ultimate

| Line Start Time (hr) | Flow values @ time increment of 0.200 hr | | | | | | |
|----------------------|--|-------|-------|-------|-------|-------|-------|
| (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) |
| 16.800 | 9.4 | 9.4 | 9.4 | 9.6 | 9.5 | 9.5 | 9.5 |
| 18.200 | 6.4 | 4.5 | 4.2 | 4.1 | 4.1 | 4.1 | 4.3 |
| 19.600 | 4.2 | 4.1 | 4.1 | 4.3 | 4.2 | 4.2 | 4.2 |
| 21.000 | 4.2 | 4.2 | 4.2 | 4.2 | 4.2 | 4.3 | 4.2 |
| 22.400 | 4.2 | 4.2 | 4.3 | 4.2 | 4.2 | 4.2 | 4.2 |
| 23.800 | 4.3 | 4.2 | 1.8 | 0.0 | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| OUTLET | 2.783 | | 3.262 | | 12.98 | 2103.7 | 755.80 |

| Line Start Time (hr) | Flow values @ time increment of 0.200 hr | | | | | | |
|----------------------|--|--------|--------|--------|--------|--------|--------|
| (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) |
| 7.000 | 0.0 | 0.6 | 0.9 | 1.1 | 2.3 | 4.4 | 7.0 |
| 8.400 | 10.0 | 13.5 | 17.2 | 21.1 | 26.7 | 33.3 | 41.5 |
| 9.800 | 51.8 | 63.5 | 75.6 | 87.7 | 99.3 | 109.9 | 119.9 |
| 11.200 | 135.2 | 155.1 | 188.3 | 259.4 | 419.7 | 765.6 | 1137.5 |
| 12.600 | 1632.2 | 1992.4 | 2099.8 | 1955.9 | 1673.4 | 1370.7 | 1105.7 |
| 14.000 | 894.1 | 736.0 | 624.7 | 550.2 | 500.7 | 467.8 | 442.1 |
| 15.400 | 420.4 | 397.0 | 370.4 | 343.7 | 320.9 | 303.6 | 292.2 |
| 16.800 | 284.9 | 280.2 | 277.1 | 275.4 | 274.4 | 274.0 | 274.0 |
| 18.200 | 269.6 | 261.5 | 246.0 | 223.3 | 198.4 | 175.8 | 158.5 |
| 19.600 | 146.2 | 138.0 | 132.4 | 128.7 | 126.1 | 124.5 | 123.4 |
| 21.000 | 122.7 | 122.2 | 121.9 | 121.8 | 121.7 | 121.8 | 121.7 |
| 22.400 | 121.8 | 121.9 | 122.1 | 122.1 | 122.3 | 122.4 | 122.4 |
| 23.800 | 122.5 | 122.5 | 119.2 | 112.4 | 100.3 | 82.2 | 62.2 |
| 25.200 | 44.2 | 30.3 | 20.5 | 13.9 | 9.3 | 6.2 | 4.0 |
| 26.600 | 2.6 | 1.5 | 0.9 | 0.0 | | | |

STORM 50_yr_sm

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| DA4 | 0.450 | | 4.512 | | 12.75 | 526.7 | 1170.14 |

| Line Start Time (hr) | Flow values @ time increment of 0.200 hr | | | | | | |
|----------------------|--|-------|-------|-------|-------|-------|-------|
| (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) |

Eccelston POI 1-4 Ultimate.out

| | | | | | | | |
|--------|-------|-------|-------|-------|-------|-------|-------|
| 6.800 | 0.0 | 1.0 | 1.9 | 3.2 | 4.5 | 6.0 | 7.5 |
| 8.200 | 8.9 | 10.4 | 11.8 | 13.2 | 14.5 | 16.0 | 18.2 |
| 9.600 | 21.4 | 25.0 | 28.6 | 31.7 | 34.4 | 36.8 | 38.8 |
| 11.000 | 40.4 | 42.9 | 49.1 | 61.6 | 82.8 | 127.3 | 226.8 |
| 12.400 | 378.3 | 499.3 | 522.8 | 466.8 | 374.3 | 292.6 | 226.9 |
| 13.800 | 177.5 | 142.6 | 120.3 | 107.0 | 98.9 | 93.8 | 90.5 |
| 15.200 | 87.9 | 83.9 | 78.0 | 71.9 | 66.9 | 63.6 | 61.6 |

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Eccelston Mitigation POI 1-4 Ultimate

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|------------|------------|------------|------------|------------|
| 16.600 | 60.3 | 59.6 | 59.2 | 59.0 | 58.8 | 58.8 | 58.8 |
| 18.000 | 58.9 | 58.2 | 55.2 | 49.2 | 42.4 | 36.5 | 32.5 |
| 19.400 | 30.1 | 28.5 | 27.5 | 26.9 | 26.5 | 26.3 | 26.1 |
| 20.800 | 26.0 | 25.9 | 25.9 | 25.9 | 25.9 | 26.0 | 26.0 |
| 22.200 | 26.0 | 26.0 | 26.0 | 26.1 | 26.1 | 26.1 | 26.1 |
| 23.600 | 26.1 | 26.1 | 26.1 | 25.6 | 23.2 | 18.5 | 13.1 |
| 25.000 | 8.4 | 5.3 | 3.3 | 2.1 | 1.3 | 0.8 | 0.5 |
| 26.400 | 0.0 | | | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| DA2 | 1.323 | | 4.401 | | 12.93 | 1337.3 | 1010.82 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|------------|------------|------------|------------|------------|
| 6.800 | 0.0 | 0.8 | 2.1 | 4.3 | 7.1 | 10.5 | 14.3 |
| 8.200 | 18.3 | 22.3 | 26.3 | 30.2 | 34.1 | 38.3 | 43.6 |
| 9.600 | 50.7 | 59.4 | 68.8 | 77.9 | 86.3 | 93.8 | 100.5 |
| 11.000 | 106.2 | 113.0 | 125.9 | 150.7 | 194.6 | 285.5 | 481.3 |
| 12.400 | 788.6 | 1118.2 | 1306.8 | 1320.1 | 1196.0 | 995.4 | 802.5 |
| 13.800 | 644.9 | 525.0 | 436.5 | 374.3 | 333.6 | 306.4 | 287.7 |
| 15.200 | 273.9 | 260.9 | 245.6 | 228.5 | 212.0 | 197.9 | 187.6 |
| 16.600 | 181.5 | 177.6 | 175.0 | 173.3 | 172.4 | 171.8 | 171.5 |
| 18.000 | 171.3 | 170.0 | 164.8 | 153.3 | 137.5 | 121.2 | 107.1 |
| 19.400 | 96.8 | 90.0 | 85.4 | 82.2 | 80.0 | 78.5 | 77.5 |
| 20.800 | 76.7 | 76.2 | 75.9 | 75.7 | 75.6 | 75.6 | 75.6 |
| 22.200 | 75.6 | 75.6 | 75.7 | 75.8 | 75.8 | 75.8 | 75.9 |
| 23.600 | 75.9 | 76.0 | 76.0 | 74.9 | 70.8 | 61.8 | 49.3 |
| 25.000 | 36.5 | 25.4 | 17.2 | 11.8 | 8.1 | 5.5 | 3.8 |
| 26.400 | 2.6 | 1.7 | 1.2 | 0.8 | 0.5 | 0.0 | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| DA3 | 0.920 | | 3.744 | | 12.84 | 840.4 | 913.21 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|------------|------------|------------|------------|------------|
| 8.000 | 0.1 | 1.3 | 2.5 | 4.2 | 6.2 | 8.3 | 10.7 |

Eccelston POI 1-4 Ultimate.out

| | | | | | | | |
|--------|-------|-------|-------|-------|-------|-------|-------|
| 9.400 | 13.6 | 17.7 | 22.4 | 27.5 | 32.5 | 37.2 | 41.6 |
| 10.800 | 45.7 | 49.3 | 53.8 | 62.5 | 78.8 | 107.6 | 168.1 |
| 12.200 | 306.6 | 527.9 | 743.4 | 835.6 | 804.7 | 688.0 | 554.0 |
| 13.600 | 440.8 | 350.6 | 284.3 | 238.2 | 209.0 | 190.8 | 178.9 |
| 15.000 | 171.2 | 165.4 | 158.7 | 148.9 | 137.7 | 127.8 | 120.5 |
| 16.400 | 116.1 | 113.3 | 111.6 | 110.6 | 110.0 | 109.7 | 109.6 |

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Eccelston Mitigation POI 1-4 Ultimate

| Line Start Time (hr) | Flow values @ time increment of 0.200 hr | | | | | | |
|----------------------|--|-------|-------|-------|-------|-------|-------|
| | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) |
| 17.800 | 109.6 | 109.7 | 108.8 | 104.5 | 95.3 | 83.7 | 72.8 |
| 19.200 | 64.3 | 58.8 | 55.3 | 52.9 | 51.4 | 50.4 | 49.8 |
| 20.600 | 49.4 | 49.1 | 48.9 | 48.8 | 48.7 | 48.7 | 48.8 |
| 22.000 | 48.9 | 48.9 | 49.0 | 49.0 | 49.0 | 49.1 | 49.1 |
| 23.400 | 49.2 | 49.2 | 49.2 | 49.3 | 48.4 | 44.9 | 37.6 |
| 24.800 | 28.3 | 19.5 | 12.8 | 8.4 | 5.5 | 3.6 | 2.4 |
| 26.200 | 1.5 | 1.0 | 0.6 | 0.0 | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| CON-1 | 2.693 | Upstream | 4.195 | 365.33 | 12.82 | 2676.1 | 993.58 |

| Line Start Time (hr) | Flow values @ time increment of 0.200 hr | | | | | | |
|----------------------|--|--------|--------|--------|--------|--------|--------|
| | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) |
| 6.800 | 0.0 | 1.8 | 4.1 | 7.4 | 11.7 | 16.6 | 22.0 |
| 8.200 | 28.5 | 35.2 | 42.3 | 49.5 | 56.9 | 65.0 | 75.4 |
| 9.600 | 89.8 | 106.9 | 124.8 | 142.0 | 157.9 | 172.2 | 185.0 |
| 11.000 | 196.0 | 209.8 | 237.6 | 291.2 | 386.2 | 583.6 | 1017.3 |
| 12.400 | 1694.9 | 2359.2 | 2662.8 | 2586.7 | 2256.3 | 1842.0 | 1470.4 |
| 13.800 | 1174.5 | 952.6 | 795.1 | 690.8 | 623.4 | 579.1 | 549.5 |
| 15.200 | 527.2 | 503.4 | 472.5 | 438.1 | 406.8 | 382.1 | 365.3 |
| 16.600 | 355.1 | 348.8 | 344.8 | 342.3 | 340.9 | 340.2 | 340.0 |
| 18.000 | 339.9 | 336.9 | 324.3 | 297.8 | 263.6 | 230.5 | 204.1 |
| 19.400 | 185.7 | 173.8 | 165.9 | 160.5 | 156.9 | 154.6 | 153.0 |
| 20.800 | 151.8 | 151.0 | 150.6 | 150.4 | 150.3 | 150.4 | 150.4 |
| 22.200 | 150.5 | 150.6 | 150.7 | 150.8 | 151.0 | 151.1 | 151.2 |
| 23.600 | 151.3 | 151.4 | 151.3 | 148.8 | 138.8 | 117.8 | 90.7 |
| 25.000 | 64.5 | 43.5 | 28.9 | 19.5 | 13.1 | 8.8 | 5.8 |
| 26.400 | 3.6 | 2.4 | 1.2 | 0.8 | 0.5 | 0.0 | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| CON-1 | 2.693 | Downstream | 4.195 | 365.26 | 12.96 | 2574.1 | 955.72 |

| Line Start Time (hr) | Flow values @ time increment of 0.200 hr | | | | | | |
|----------------------|--|-------|-------|-------|-------|-------|-------|
| | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) |
| 6.800 | 0.0 | 0.9 | 2.9 | 5.8 | 9.6 | 14.1 | 19.2 |
| 8.200 | 25.2 | 31.7 | 38.5 | 45.7 | 53.0 | 60.7 | 70.1 |
| 9.600 | 82.7 | 98.3 | 115.5 | 132.8 | 149.2 | 164.3 | 177.9 |
| 11.000 | 189.8 | 202.5 | 224.3 | 266.0 | 341.4 | 490.5 | 818.0 |

Eccelston POI 1-4 Ultimate.out

| | | | | | | | |
|--------|--------|--------|--------|--------|--------|--------|--------|
| 12.400 | 1374.1 | 2021.3 | 2459.9 | 2563.9 | 2379.1 | 2034.6 | 1665.3 |
| 13.800 | 1341.9 | 1084.1 | 891.9 | 757.4 | 667.8 | 608.6 | 569.2 |
| 15.200 | 541.4 | 516.8 | 488.3 | 455.8 | 423.7 | 396.2 | 375.6 |
| 16.600 | 361.9 | 353.1 | 347.6 | 344.0 | 341.9 | 340.7 | 340.2 |

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Eccelston Mitigation POI 1-4 Ultimate

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|------------|------------|------------|------------|------------|
| 18.000 | 340.0 | 338.3 | 329.9 | 309.8 | 280.1 | 247.7 | 218.9 |
| 19.400 | 196.8 | 181.4 | 171.1 | 164.0 | 159.3 | 156.1 | 154.0 |
| 20.800 | 152.6 | 151.5 | 150.9 | 150.5 | 150.4 | 150.4 | 150.4 |
| 22.200 | 150.5 | 150.6 | 150.7 | 150.8 | 150.9 | 151.0 | 151.1 |
| 23.600 | 151.2 | 151.3 | 151.3 | 149.9 | 143.2 | 127.4 | 103.8 |
| 25.000 | 78.2 | 55.3 | 37.8 | 25.5 | 17.2 | 11.6 | 7.8 |
| 26.400 | 4.9 | 3.2 | 1.9 | 1.1 | 0.7 | 0.0 | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| DA1 | 0.090 | | 4.734 | | 12.19 | 218.5 | 2427.19 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|------------|------------|------------|------------|------------|
| 6.400 | 0.2 | 0.9 | 1.2 | 1.6 | 1.9 | 2.3 | 2.6 |
| 7.800 | 2.9 | 3.2 | 3.5 | 3.7 | 4.0 | 4.2 | 4.5 |
| 9.200 | 6.0 | 7.3 | 7.8 | 8.3 | 8.7 | 9.1 | 9.4 |
| 10.600 | 9.7 | 9.5 | 9.7 | 16.8 | 22.3 | 27.5 | 51.4 |
| 12.000 | 113.4 | 217.3 | 127.7 | 73.9 | 41.2 | 35.5 | 24.2 |
| 13.400 | 17.1 | 16.4 | 17.1 | 17.3 | 17.4 | 17.4 | 17.4 |
| 14.800 | 17.4 | 17.5 | 14.3 | 12.2 | 11.9 | 12.0 | 11.9 |
| 16.200 | 11.9 | 12.0 | 12.0 | 11.9 | 12.0 | 12.0 | 12.1 |
| 17.600 | 12.0 | 12.1 | 12.0 | 8.2 | 5.6 | 5.3 | 5.3 |
| 19.000 | 5.2 | 5.3 | 5.3 | 5.2 | 5.3 | 5.3 | 5.2 |
| 20.400 | 5.3 | 5.3 | 5.3 | 5.2 | 5.3 | 5.3 | 5.3 |
| 21.800 | 5.3 | 5.3 | 5.3 | 5.4 | 5.3 | 5.3 | 5.4 |
| 23.200 | 5.3 | 5.3 | 5.4 | 5.4 | 5.3 | 2.3 | 0.0 |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| OUTLET | 2.783 | | 4.213 | | 12.96 | 2609.6 | 937.56 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|------------|------------|------------|------------|------------|
| 6.400 | 0.2 | 0.9 | 1.2 | 2.5 | 4.8 | 8.1 | 12.1 |
| 7.800 | 17.0 | 22.3 | 28.7 | 35.4 | 42.5 | 49.9 | 57.4 |
| 9.200 | 66.7 | 77.4 | 90.5 | 106.6 | 124.2 | 141.9 | 158.6 |
| 10.600 | 174.0 | 187.4 | 199.5 | 219.3 | 246.6 | 293.6 | 392.8 |
| 12.000 | 604.0 | 1035.4 | 1502.2 | 2095.3 | 2501.2 | 2599.4 | 2403.2 |
| 13.400 | 2051.5 | 1681.6 | 1358.9 | 1101.2 | 909.2 | 774.8 | 685.2 |
| 14.800 | 626.0 | 586.6 | 555.7 | 528.9 | 500.2 | 467.7 | 435.5 |
| 16.200 | 408.1 | 387.5 | 373.9 | 365.0 | 359.5 | 356.1 | 354.0 |

Eccelston POI 1-4 Ultimate.out

| | | | | | | | |
|--------|-------|-------|-------|-------|-------|-------|-------|
| 17.600 | 352.7 | 352.3 | 352.1 | 346.5 | 335.5 | 315.1 | 285.4 |
| 19.000 | 253.0 | 224.2 | 202.1 | 186.7 | 176.4 | 169.3 | 164.5 |

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Eccelston Mitigation POI 1-4 Ultimate

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | values @ time (cfs) | increment (cfs) | of 0.200 (cfs) | hr (cfs) | Flow (cfs) |
|----------------------|------------|------------|---------------------|-----------------|----------------|----------|------------|
| 20.400 | 161.5 | 159.3 | 157.9 | 156.8 | 156.2 | 155.8 | 155.6 |
| 21.800 | 155.7 | 155.7 | 155.7 | 155.9 | 156.0 | 156.0 | 156.3 |
| 23.200 | 156.3 | 156.4 | 156.6 | 156.7 | 156.6 | 152.3 | 143.2 |
| 24.600 | 127.4 | 103.8 | 78.2 | 55.3 | 37.8 | 25.6 | 17.2 |
| 26.000 | 11.6 | 7.8 | 4.9 | 3.2 | 1.9 | 1.1 | 0.7 |
| 27.400 | 0.0 | | | | | | |

STORM 100_yr_sm

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| DA4 | 0.450 | | 5.658 | | 12.72 | 622.1 | 1382.12 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | values @ time (cfs) | increment (cfs) | of 0.200 (cfs) | hr (cfs) | Flow (cfs) |
|----------------------|------------|------------|---------------------|-----------------|----------------|----------|------------|
| 6.200 | 0.3 | 1.1 | 2.2 | 3.9 | 5.9 | 8.0 | 10.1 |
| 7.600 | 12.2 | 14.3 | 16.3 | 18.3 | 20.1 | 21.9 | 23.7 |
| 9.000 | 25.3 | 27.2 | 30.2 | 34.5 | 39.4 | 44.1 | 48.1 |
| 10.400 | 51.4 | 54.3 | 56.6 | 58.2 | 60.9 | 69.0 | 85.6 |
| 11.800 | 113.1 | 168.3 | 285.8 | 457.6 | 592.4 | 618.7 | 552.5 |
| 13.200 | 446.0 | 351.2 | 273.6 | 214.3 | 172.6 | 146.3 | 130.7 |
| 14.600 | 121.1 | 115.1 | 111.3 | 108.2 | 103.5 | 96.6 | 89.4 |
| 16.000 | 83.5 | 79.6 | 77.2 | 75.8 | 75.0 | 74.5 | 74.2 |
| 17.400 | 74.0 | 74.0 | 74.0 | 74.0 | 73.2 | 69.4 | 61.9 |
| 18.800 | 53.3 | 45.9 | 40.9 | 37.8 | 35.8 | 34.6 | 33.9 |
| 20.200 | 33.4 | 33.1 | 32.9 | 32.8 | 32.7 | 32.7 | 32.7 |
| 21.600 | 32.7 | 32.7 | 32.7 | 32.8 | 32.8 | 32.8 | 32.8 |
| 23.000 | 32.8 | 32.8 | 32.8 | 32.8 | 32.8 | 32.9 | 32.2 |
| 24.400 | 29.2 | 23.2 | 16.4 | 10.5 | 6.6 | 4.2 | 2.6 |
| 25.800 | 1.7 | 1.0 | 0.6 | 0.0 | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| DA2 | 1.323 | | 5.538 | | 12.89 | 1593.4 | 1204.38 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | values @ time (cfs) | increment (cfs) | of 0.200 (cfs) | hr (cfs) | Flow (cfs) |
|----------------------|------------|------------|---------------------|-----------------|----------------|----------|------------|
| 6.200 | 0.0 | 1.0 | 2.6 | 5.4 | 9.5 | 14.3 | 19.7 |
| 7.600 | 25.4 | 31.2 | 36.9 | 42.5 | 48.1 | 53.4 | 58.6 |
| 9.000 | 63.6 | 69.0 | 76.0 | 85.8 | 97.7 | 110.2 | 122.3 |
| 10.400 | 133.1 | 142.4 | 150.3 | 156.7 | 164.5 | 180.3 | 213.1 |
| 11.800 | 272.0 | 385.7 | 621.0 | 980.4 | 1353.7 | 1567.3 | 1570.2 |
| 13.200 | 1421.4 | 1189.4 | 964.7 | 779.5 | 635.3 | 529.3 | 456.1 |
| 14.600 | 407.7 | 375.3 | 353.5 | 337.2 | 321.9 | 303.7 | 283.6 |

Eccelston POI 1-4 Ultimate.out

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Eccelston Mitigation POI 1-4 Ultimate

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|---------------------|-----------------|-------------------|------------|------------|
| 16.000 | 264.0 | 247.3 | 235.4 | 228.1 | 223.4 | 220.4 | 218.4 |
| 17.400 | 217.2 | 216.5 | 216.1 | 216.0 | 214.3 | 207.6 | 193.1 |
| 18.800 | 173.3 | 152.7 | 135.1 | 122.0 | 113.5 | 107.7 | 103.6 |
| 20.200 | 100.9 | 99.0 | 97.7 | 96.9 | 96.3 | 95.9 | 95.6 |
| 21.600 | 95.5 | 95.4 | 95.3 | 95.4 | 95.5 | 95.5 | 95.5 |
| 23.000 | 95.6 | 95.6 | 95.6 | 95.7 | 95.7 | 95.7 | 94.4 |
| 24.400 | 89.2 | 77.8 | 62.1 | 46.0 | 32.0 | 21.6 | 14.9 |
| 25.800 | 10.2 | 7.0 | 4.8 | 3.2 | 2.2 | 1.5 | 1.0 |
| 27.200 | 0.6 | 0.0 | | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| DA3 | 0.920 | | 4.812 | | 12.81 | 1025.9 | 1114.81 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|---------------------|-----------------|-------------------|------------|------------|
| 7.200 | 0.3 | 1.4 | 3.1 | 5.4 | 8.2 | 11.3 | 14.4 |
| 8.600 | 17.7 | 20.9 | 24.0 | 27.4 | 31.9 | 37.9 | 45.0 |
| 10.000 | 52.3 | 59.2 | 65.4 | 71.1 | 76.1 | 80.1 | 85.4 |
| 11.400 | 96.7 | 120.0 | 159.5 | 239.4 | 410.4 | 673.2 | 919.4 |
| 12.800 | 1024.0 | 978.8 | 840.0 | 680.0 | 542.8 | 433.3 | 352.0 |
| 14.200 | 295.6 | 260.2 | 238.1 | 223.8 | 214.4 | 207.4 | 199.4 |
| 15.600 | 187.6 | 174.0 | 162.1 | 153.4 | 148.0 | 144.7 | 142.6 |
| 17.000 | 141.4 | 140.7 | 140.4 | 140.2 | 140.3 | 140.4 | 139.1 |
| 18.400 | 133.6 | 121.8 | 107.0 | 93.0 | 82.2 | 75.2 | 70.7 |
| 19.800 | 67.7 | 65.8 | 64.5 | 63.7 | 63.2 | 62.8 | 62.6 |
| 21.200 | 62.5 | 62.4 | 62.4 | 62.4 | 62.5 | 62.5 | 62.6 |
| 22.600 | 62.7 | 62.7 | 62.7 | 62.8 | 62.8 | 62.8 | 62.9 |
| 24.000 | 62.9 | 61.8 | 57.4 | 47.9 | 36.1 | 25.0 | 16.2 |
| 25.400 | 10.7 | 7.0 | 4.6 | 3.0 | 2.0 | 1.3 | 0.8 |
| 26.800 | 0.5 | 0.0 | | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| CON-1 | 2.693 | Upstream | 5.310 | 365.69 | 12.87 | 3215.2 | 1193.73 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|------------|---------------------|-----------------|-------------------|------------|------------|
| 6.200 | 0.3 | 2.0 | 4.9 | 9.3 | 15.3 | 22.6 | 31.3 |
| 7.600 | 40.8 | 50.9 | 61.5 | 72.1 | 82.6 | 93.0 | 103.1 |
| 9.000 | 113.0 | 123.7 | 138.1 | 158.2 | 182.1 | 206.6 | 229.6 |
| 10.400 | 249.9 | 267.8 | 283.0 | 295.0 | 310.7 | 346.9 | 418.8 |
| 11.800 | 544.7 | 793.5 | 1322.7 | 2110.6 | 2862.3 | 3207.4 | 3099.1 |
| 13.200 | 2706.9 | 2221.4 | 1781.6 | 1427.4 | 1160.2 | 972.2 | 847.2 |

Eccelston POI 1-4 Ultimate.out

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Eccelston Mitigation POI 1-4 Ultimate

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Values @ time (cfs) | increment (cfs) | of 0.200 (cfs) | hr (cfs) | (cfs) |
|----------------------|------------|------------|---------------------|-----------------|----------------|----------|-------|
| 14.600 | 767.3 | 714.3 | 679.3 | 652.8 | 624.6 | 587.9 | 547.0 |
| 16.000 | 509.5 | 480.4 | 460.7 | 448.7 | 441.0 | 436.3 | 433.3 |
| 17.400 | 431.6 | 430.7 | 430.4 | 430.3 | 426.4 | 410.5 | 376.8 |
| 18.800 | 333.5 | 291.6 | 258.2 | 235.3 | 220.1 | 210.0 | 203.3 |
| 20.200 | 198.8 | 195.7 | 193.8 | 192.5 | 191.6 | 191.1 | 190.7 |
| 21.600 | 190.6 | 190.5 | 190.5 | 190.7 | 190.8 | 191.0 | 191.0 |
| 23.000 | 191.1 | 191.2 | 191.2 | 191.3 | 191.4 | 191.5 | 188.2 |
| 24.400 | 175.5 | 148.9 | 114.6 | 81.5 | 54.9 | 36.6 | 24.6 |
| 25.800 | 16.5 | 11.0 | 7.4 | 4.7 | 3.0 | 1.9 | 1.0 |
| 27.200 | 0.6 | 0.0 | | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| CON-1 | 2.693 | Downstream | 5.310 | 365.62 | 12.94 | 3101.4 | 1151.47 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Values @ time (cfs) | increment (cfs) | of 0.200 (cfs) | hr (cfs) | (cfs) |
|----------------------|------------|------------|---------------------|-----------------|----------------|----------|--------|
| 6.200 | 0.0 | 1.0 | 3.5 | 7.3 | 12.6 | 19.2 | 27.3 |
| 7.600 | 36.3 | 46.0 | 56.3 | 66.9 | 77.4 | 87.9 | 98.1 |
| 9.000 | 108.1 | 118.5 | 131.4 | 149.1 | 171.0 | 194.9 | 218.2 |
| 10.400 | 239.6 | 258.6 | 275.1 | 288.6 | 303.0 | 331.2 | 387.8 |
| 11.800 | 489.7 | 684.9 | 1098.2 | 1765.3 | 2507.7 | 2998.1 | 3085.1 |
| 13.200 | 2843.9 | 2430.4 | 1993.9 | 1610.4 | 1304.7 | 1078.3 | 920.4 |
| 14.600 | 815.7 | 746.3 | 700.5 | 668.2 | 639.2 | 605.2 | 566.3 |
| 16.000 | 528.1 | 495.8 | 471.8 | 456.0 | 445.7 | 439.2 | 435.1 |
| 17.400 | 432.7 | 431.3 | 430.7 | 430.4 | 428.0 | 417.0 | 390.9 |
| 18.800 | 352.9 | 311.7 | 275.5 | 248.1 | 229.0 | 216.0 | 207.3 |
| 20.200 | 201.5 | 197.5 | 195.0 | 193.3 | 192.1 | 191.4 | 190.9 |
| 21.600 | 190.7 | 190.5 | 190.5 | 190.6 | 190.8 | 190.9 | 190.9 |
| 23.000 | 191.0 | 191.1 | 191.2 | 191.3 | 191.4 | 191.4 | 189.5 |
| 24.400 | 180.7 | 160.0 | 129.9 | 97.4 | 68.6 | 46.8 | 31.6 |
| 25.800 | 21.3 | 14.3 | 9.6 | 6.3 | 4.0 | 2.6 | 1.4 |
| 27.200 | 0.9 | 0.0 | | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| DA1 | 0.090 | | 5.897 | | 12.19 | 249.3 | 2768.55 |

| Line Start Time (hr) | Flow (cfs) | Flow (cfs) | Values @ time (cfs) | increment (cfs) | of 0.200 (cfs) | hr (cfs) | (cfs) |
|----------------------|------------|------------|---------------------|-----------------|----------------|----------|-------|
| 5.800 | 0.0 | 0.6 | 1.2 | 2.0 | 2.5 | 3.0 | 3.5 |
| 7.200 | 3.9 | 4.3 | 4.7 | 5.1 | 5.4 | 5.7 | 6.1 |
| 8.600 | 6.3 | 6.7 | 7.0 | 9.1 | 10.8 | 11.5 | 12.0 |
| 10.000 | 12.5 | 12.9 | 13.2 | 13.5 | 13.0 | 13.1 | 23.0 |

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Eccelston POI 1-4 Ultimate.out

| Line Start Time (hr) | Flow (cfs) | Values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|---------------------|-----------------|-------------------|------------|------------|
| 11.400 | 30.2 | 36.7 | 65.9 | 135.9 | 247.6 | 88.1 |
| 12.800 | 50.4 | 43.8 | 29.7 | 20.6 | 19.8 | 21.2 |
| 14.200 | 21.3 | 21.4 | 21.4 | 21.5 | 21.5 | 15.2 |
| 15.600 | 15.0 | 14.9 | 15.0 | 15.0 | 14.9 | 14.9 |
| 17.000 | 15.0 | 15.0 | 15.1 | 15.1 | 15.1 | 10.2 |
| 18.400 | 7.2 | 6.6 | 6.7 | 6.6 | 6.6 | 6.6 |
| 19.800 | 6.7 | 6.5 | 6.7 | 6.6 | 6.6 | 6.6 |
| 21.200 | 6.7 | 6.6 | 6.7 | 6.6 | 6.7 | 6.6 |
| 22.600 | 6.7 | 6.6 | 6.7 | 6.6 | 6.7 | 6.6 |
| 24.000 | 6.7 | 2.9 | 0.0 | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| OUTLET | 2.783 | | 5.329 | | 12.94 | 3144.3 | 1129.65 |

| Line Start Time (hr) | Flow (cfs) | Values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|---------------------|-----------------|-------------------|------------|------------|
| 5.800 | 0.0 | 0.6 | 1.2 | 3.0 | 6.1 | 16.1 |
| 7.200 | 23.1 | 31.6 | 41.0 | 51.1 | 61.8 | 83.5 |
| 8.600 | 94.2 | 104.8 | 115.0 | 127.6 | 142.3 | 183.0 |
| 10.000 | 207.3 | 231.1 | 252.8 | 272.1 | 288.0 | 326.0 |
| 11.400 | 361.4 | 424.5 | 555.7 | 820.8 | 1346.0 | 2595.9 |
| 12.800 | 3048.5 | 3128.9 | 2873.5 | 2450.8 | 2013.5 | 1325.9 |
| 14.200 | 1099.6 | 941.7 | 837.0 | 767.8 | 722.1 | 654.4 |
| 15.600 | 620.1 | 581.2 | 543.0 | 510.7 | 486.7 | 460.6 |
| 17.000 | 454.3 | 450.2 | 447.8 | 446.4 | 445.8 | 438.3 |
| 18.400 | 424.2 | 397.4 | 359.5 | 318.3 | 282.1 | 235.6 |
| 19.800 | 222.7 | 213.9 | 208.2 | 204.2 | 201.6 | 198.8 |
| 21.200 | 198.1 | 197.5 | 197.4 | 197.2 | 197.2 | 197.3 |
| 22.600 | 197.6 | 197.6 | 197.7 | 197.7 | 197.8 | 198.0 |
| 24.000 | 198.2 | 192.4 | 180.9 | 160.1 | 129.9 | 68.6 |
| 25.400 | 46.8 | 31.6 | 21.3 | 14.3 | 9.6 | 4.0 |
| 26.800 | 2.6 | 1.4 | 0.9 | 0.0 | | |

STORM 500_yr_sm

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| DA4 | 0.450 | | 9.089 | | 12.71 | 853.7 | 1896.50 |

| Line Start Time (hr) | Flow (cfs) | Values @ time (cfs) | increment (cfs) | of 0.200 hr (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|---------------------|-----------------|-------------------|------------|------------|
| 4.000 | 0.0 | 0.7 | 1.4 | 2.3 | 3.3 | 5.4 |
| 5.400 | 6.5 | 7.5 | 8.5 | 9.5 | 10.9 | 18.5 |

Eccelston POI 1-4 Ultimate.out

| Start Time (hr) | Flow Values @ time increment of 0.200 hr | | | | | | |
|-----------------|--|-------|-------|-------|-------|-------|-------|
| | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) |
| 6.800 | 24.3 | 30.3 | 35.6 | 40.3 | 44.5 | 48.3 | 51.7 |
| 8.200 | 54.9 | 57.9 | 60.6 | 63.3 | 65.7 | 68.6 | 73.4 |
| 9.600 | 80.8 | 89.1 | 96.7 | 102.8 | 107.6 | 111.5 | 114.2 |
| 11.000 | 115.1 | 117.8 | 131.2 | 160.4 | 206.9 | 288.7 | 444.1 |
| 12.400 | 658.1 | 819.9 | 848.0 | 764.7 | 629.7 | 506.1 | 399.9 |
| 13.800 | 316.4 | 256.8 | 219.9 | 198.7 | 185.6 | 177.3 | 172.1 |
| 15.200 | 167.8 | 161.4 | 152.0 | 142.4 | 134.3 | 129.0 | 125.8 |
| 16.600 | 123.9 | 122.7 | 122.1 | 121.7 | 121.7 | 121.7 | 121.6 |
| 18.000 | 121.5 | 120.0 | 113.7 | 101.3 | 87.2 | 75.1 | 66.9 |
| 19.400 | 61.9 | 58.7 | 56.7 | 55.4 | 54.6 | 54.1 | 53.8 |
| 20.800 | 53.6 | 53.4 | 53.4 | 53.4 | 53.4 | 53.4 | 53.4 |
| 22.200 | 53.4 | 53.4 | 53.4 | 53.4 | 53.5 | 53.5 | 53.6 |
| 23.600 | 53.5 | 53.5 | 53.5 | 52.4 | 47.5 | 37.9 | 26.8 |
| 25.000 | 17.2 | 10.7 | 6.8 | 4.3 | 2.7 | 1.7 | 1.0 |
| 26.400 | 0.6 | 0.0 | | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| DA2 | 1.323 | | 8.948 | | 12.92 | 2229.0 | 1684.87 |

| Line Start Time (hr) | Flow Values @ time increment of 0.200 hr | | | | | | |
|----------------------|--|--------|--------|--------|--------|--------|--------|
| | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) |
| 4.200 | 0.4 | 1.4 | 2.9 | 4.9 | 7.3 | 10.0 | 12.8 |
| 5.600 | 15.6 | 18.5 | 21.4 | 25.0 | 30.6 | 40.2 | 53.2 |
| 7.000 | 67.9 | 82.8 | 96.9 | 109.7 | 121.5 | 132.3 | 142.4 |
| 8.400 | 151.8 | 160.6 | 168.8 | 176.7 | 185.2 | 196.6 | 213.1 |
| 9.800 | 233.4 | 254.4 | 273.9 | 290.6 | 304.1 | 314.5 | 321.2 |
| 11.200 | 330.1 | 355.0 | 411.2 | 509.9 | 686.6 | 1008.7 | 1470.5 |
| 12.600 | 1936.0 | 2193.8 | 2199.4 | 2004.5 | 1702.1 | 1399.9 | 1141.5 |
| 14.000 | 939.6 | 789.6 | 685.3 | 619.0 | 574.6 | 544.0 | 521.4 |
| 15.400 | 500.1 | 475.2 | 447.5 | 420.9 | 398.3 | 382.0 | 372.2 |
| 16.800 | 365.7 | 361.5 | 359.0 | 357.6 | 356.9 | 356.4 | 355.8 |
| 18.200 | 352.6 | 341.6 | 317.4 | 284.7 | 251.0 | 222.0 | 200.7 |
| 19.600 | 186.5 | 176.8 | 170.1 | 165.5 | 162.3 | 160.3 | 158.8 |
| 21.000 | 157.8 | 157.2 | 156.8 | 156.6 | 156.4 | 156.3 | 156.2 |
| 22.400 | 156.2 | 156.2 | 156.3 | 156.3 | 156.4 | 156.5 | 156.6 |
| 23.800 | 156.6 | 156.5 | 154.3 | 145.9 | 127.2 | 101.5 | 75.1 |
| 25.200 | 52.3 | 35.5 | 24.3 | 16.7 | 11.4 | 7.8 | 5.3 |
| 26.600 | 3.6 | 2.4 | 1.6 | 1.0 | 0.6 | 0.0 | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| DA3 | 0.920 | | 8.077 | | 12.84 | 1497.0 | 1626.71 |

| Line Start Time (hr) | Flow Values @ time increment of 0.200 hr | | | | | | |
|----------------------|--|-------|-------|-------|-------|-------|-------|
| | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) |

Eccelston POI 1-4 Ultimate.out

| | | | | | | | |
|--------|--------|--------|--------|--------|--------|--------|-------|
| 5.400 | 0.0 | 0.8 | 1.7 | 2.9 | 4.5 | 7.3 | 11.9 |
| 6.800 | 18.1 | 25.4 | 33.0 | 40.5 | 47.9 | 54.9 | 61.7 |
| 8.200 | 68.1 | 74.3 | 80.2 | 85.8 | 91.2 | 97.2 | 105.2 |
| 9.600 | 116.9 | 130.5 | 144.0 | 156.2 | 166.3 | 174.9 | 181.8 |
| 11.000 | 186.1 | 192.5 | 212.5 | 255.6 | 328.4 | 457.3 | 700.8 |
| 12.400 | 1049.8 | 1368.9 | 1493.1 | 1430.6 | 1239.6 | 1020.8 | 825.7 |
| 13.800 | 664.1 | 543.0 | 459.4 | 407.8 | 376.1 | 355.2 | 341.7 |
| 15.200 | 331.4 | 319.7 | 303.1 | 284.2 | 267.6 | 255.4 | 247.9 |
| 16.600 | 243.2 | 240.2 | 238.5 | 237.7 | 237.4 | 237.3 | 237.2 |
| 18.000 | 237.1 | 234.7 | 225.3 | 205.1 | 180.1 | 156.7 | 138.3 |
| 19.400 | 126.6 | 118.9 | 113.9 | 110.5 | 108.3 | 106.9 | 106.0 |
| 20.800 | 105.4 | 105.0 | 104.9 | 104.8 | 104.8 | 104.7 | 104.7 |
| 22.200 | 104.8 | 104.8 | 104.9 | 104.9 | 105.0 | 105.1 | 105.2 |
| 23.600 | 105.2 | 105.2 | 105.2 | 103.4 | 95.8 | 80.2 | 60.3 |
| 25.000 | 41.7 | 27.2 | 17.8 | 11.8 | 7.7 | 5.0 | 3.3 |
| 26.400 | 2.1 | 1.4 | 0.9 | 0.5 | 0.0 | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| CON-1 | 2.693 | Upstream | 8.674 | 366.44 | 12.85 | 4550.9 | 1689.65 |

| Line Start Time (hr) | Flow (cfs) | Flow values @ time increment of 0.200 hr (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|--|------------|------------|------------|------------|------------|
| 4.000 | 0.0 | 1.2 | 2.9 | 5.2 | 8.2 | 11.7 | 15.4 |
| 5.400 | 19.2 | 24.0 | 28.8 | 33.9 | 40.5 | 51.8 | 70.6 |
| 6.800 | 95.7 | 123.5 | 151.4 | 177.7 | 202.0 | 224.6 | 245.7 |
| 8.200 | 265.4 | 283.9 | 301.4 | 317.9 | 333.7 | 351.0 | 375.4 |
| 9.600 | 410.9 | 453.0 | 495.1 | 532.9 | 564.4 | 590.5 | 610.3 |
| 11.000 | 622.4 | 640.8 | 698.8 | 828.7 | 1047.2 | 1432.9 | 2153.6 |
| 12.400 | 3178.8 | 4116.4 | 4531.6 | 4392.5 | 3871.9 | 3229.7 | 2626.7 |
| 13.800 | 2123.4 | 1739.8 | 1469.3 | 1293.2 | 1180.9 | 1107.5 | 1057.9 |
| 15.200 | 1020.6 | 981.3 | 930.3 | 874.2 | 822.9 | 782.8 | 756.0 |
| 16.600 | 739.4 | 728.7 | 722.1 | 718.4 | 716.7 | 715.8 | 715.2 |
| 18.000 | 714.5 | 707.3 | 680.0 | 623.7 | 552.1 | 482.9 | 427.4 |
| 19.400 | 389.2 | 364.2 | 347.4 | 336.0 | 328.4 | 323.4 | 320.1 |
| 20.800 | 317.8 | 316.3 | 315.4 | 314.9 | 314.7 | 314.5 | 314.4 |
| 22.200 | 314.3 | 314.5 | 314.5 | 314.6 | 314.8 | 315.0 | 315.3 |
| 23.600 | 315.4 | 315.4 | 315.2 | 310.2 | 289.0 | 244.9 | 188.6 |
| 25.000 | 134.1 | 90.3 | 60.2 | 40.5 | 27.2 | 18.2 | 12.1 |
| 26.400 | 8.1 | 5.1 | 3.3 | 2.0 | 1.0 | 0.7 | 0.0 |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| CON-1 | 2.693 | Downstream | 8.674 | 366.37 | 12.92 | 4417.7 | 1640.22 |

Eccelston Mitigation POI 1-4 Ultimate

| Line Start Time (hr) | Flow (cfs) | Flow values @ time increment of 0.200 hr (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) | Flow (cfs) |
|----------------------|------------|--|------------|------------|------------|------------|------------|
| 4.200 | 0.5 | 2.2 | 4.3 | 7.0 | 10.3 | 13.9 | 17.6 |

Eccelston POI 1-4 Ultimate.out

| | | | | | | | |
|--------|--------|--------|--------|--------|--------|--------|--------|
| 5.600 | 22.1 | 26.8 | 31.7 | 37.8 | 47.4 | 63.4 | 85.9 |
| 7.000 | 112.2 | 139.7 | 166.4 | 191.4 | 214.8 | 236.5 | 256.8 |
| 8.400 | 275.8 | 293.8 | 310.7 | 326.8 | 343.7 | 365.7 | 397.1 |
| 9.800 | 436.2 | 477.6 | 516.5 | 550.3 | 578.6 | 601.0 | 616.3 |
| 11.200 | 632.8 | 677.6 | 781.4 | 964.8 | 1285.8 | 1884.3 | 2787.5 |
| 12.600 | 3728.9 | 4307.8 | 4382.5 | 4030.7 | 3469.6 | 2876.7 | 2345.3 |
| 14.000 | 1917.4 | 1600.3 | 1383.1 | 1240.0 | 1146.2 | 1083.7 | 1039.4 |
| 15.400 | 998.9 | 951.0 | 897.2 | 844.9 | 801.0 | 769.1 | 748.0 |
| 16.800 | 734.4 | 725.7 | 720.5 | 717.8 | 716.4 | 715.5 | 714.8 |
| 18.200 | 709.9 | 689.6 | 644.1 | 579.8 | 511.6 | 452.1 | 407.6 |
| 19.600 | 376.9 | 356.0 | 341.9 | 332.3 | 326.0 | 321.8 | 319.0 |
| 21.000 | 317.1 | 315.9 | 315.2 | 314.9 | 314.6 | 314.5 | 314.4 |
| 22.400 | 314.5 | 314.5 | 314.6 | 314.7 | 314.9 | 315.2 | 315.3 |
| 23.800 | 315.3 | 315.3 | 312.0 | 296.4 | 260.8 | 210.3 | 156.7 |
| 25.200 | 109.7 | 74.7 | 50.5 | 34.0 | 22.8 | 15.2 | 10.2 |
| 26.600 | 6.6 | 4.2 | 2.7 | 1.5 | 0.9 | 0.0 | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| DA1 | 0.090 | | 9.368 | | 12.18 | 315.9 | 3508.55 |

Line Start Time (hr) ----- Flow values @ time increment of 0.200 hr -----

| Start Time (hr) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) |
|-----------------|-------|-------|-------|-------|-------|-------|-------|
| 3.600 | 0.0 | 0.7 | 1.0 | 1.2 | 1.5 | 1.7 | 2.0 |
| 5.000 | 2.1 | 2.4 | 2.6 | 2.8 | 3.0 | 3.2 | 5.8 |
| 6.400 | 8.2 | 9.2 | 10.0 | 10.7 | 11.5 | 12.1 | 12.6 |
| 7.800 | 13.2 | 13.7 | 14.2 | 14.6 | 15.0 | 15.4 | 15.8 |
| 9.200 | 19.6 | 22.5 | 23.2 | 23.9 | 24.4 | 24.9 | 25.4 |
| 10.600 | 25.3 | 23.5 | 23.4 | 41.7 | 54.5 | 64.0 | 105.1 |
| 12.000 | 189.5 | 313.3 | 196.7 | 125.2 | 76.8 | 68.2 | 45.6 |
| 13.400 | 31.2 | 29.9 | 32.2 | 33.0 | 32.9 | 33.2 | 33.0 |
| 14.800 | 33.1 | 33.2 | 28.1 | 24.8 | 24.4 | 24.4 | 24.4 |
| 16.200 | 24.4 | 24.4 | 24.4 | 24.5 | 24.6 | 24.7 | 24.5 |
| 17.600 | 24.5 | 24.5 | 24.6 | 16.5 | 11.7 | 10.7 | 10.9 |
| 19.000 | 10.6 | 10.8 | 10.7 | 10.8 | 10.8 | 10.6 | 10.9 |
| 20.400 | 10.7 | 10.8 | 10.8 | 10.8 | 10.8 | 10.9 | 10.8 |
| 21.800 | 10.7 | 10.9 | 10.7 | 10.8 | 10.8 | 10.9 | 10.8 |
| 23.200 | 10.9 | 10.8 | 10.7 | 10.9 | 10.7 | 4.7 | 0.6 |
| 24.600 | 0.0 | | | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Flow Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|-----------------|
| OUTLET | 2.783 | | 8.696 | | 12.93 | 4484.3 | 1611.09 |

♀

Eccelston Mitigation POI 1-4 Ultimate

Line Start Time (hr) ----- Flow values @ time increment of 0.200 hr -----

| Start Time (hr) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) | (cfs) |
|-----------------|-------|-------|-------|-------|-------|-------|-------|
| 3.600 | 0.0 | 0.7 | 1.0 | 1.7 | 3.6 | 6.0 | 9.0 |
| 5.000 | 12.4 | 16.2 | 20.2 | 24.8 | 29.7 | 34.9 | 43.6 |
| 6.400 | 55.6 | 72.7 | 95.9 | 123.0 | 151.2 | 178.4 | 204.0 |

| Eccelston POI 1-4 Ultimate.out | | | | | | | |
|--------------------------------|--------|--------|--------|--------|--------|--------|--------|
| 7.800 | 227.9 | 250.2 | 270.9 | 290.4 | 308.8 | 326.2 | 342.6 |
| 9.200 | 363.2 | 388.2 | 420.3 | 460.0 | 502.0 | 541.3 | 575.6 |
| 10.600 | 603.9 | 624.6 | 639.6 | 674.6 | 732.1 | 845.5 | 1069.9 |
| 12.000 | 1475.9 | 2197.7 | 2984.3 | 3854.2 | 4384.7 | 4450.7 | 4076.1 |
| 13.400 | 3500.6 | 2906.4 | 2377.4 | 1950.4 | 1633.3 | 1416.2 | 1272.9 |
| 14.800 | 1179.3 | 1116.9 | 1067.5 | 1023.7 | 975.4 | 921.5 | 869.2 |
| 16.200 | 825.4 | 793.5 | 772.5 | 758.8 | 750.2 | 745.2 | 742.3 |
| 17.600 | 740.9 | 740.1 | 739.4 | 726.4 | 701.2 | 654.9 | 590.7 |
| 19.000 | 522.3 | 462.9 | 418.3 | 387.7 | 366.8 | 352.5 | 343.2 |
| 20.400 | 336.7 | 332.6 | 329.7 | 327.9 | 326.7 | 326.1 | 325.7 |
| 21.800 | 325.3 | 325.4 | 325.0 | 325.3 | 325.3 | 325.4 | 325.5 |
| 23.200 | 325.8 | 326.0 | 326.0 | 326.3 | 326.0 | 316.6 | 297.0 |
| 24.600 | 260.9 | 210.4 | 156.8 | 109.9 | 74.8 | 50.5 | 34.0 |
| 26.000 | 22.8 | 15.3 | 10.2 | 6.6 | 4.2 | 2.7 | 1.5 |
| 27.400 | 0.9 | 0.0 | | | | | |

Eccelston Mitigation POI 1-4 Ultimate

| Area or Reach Identifier | Drainage Area (sq mi) | ----- Peak Flow by Storm ----- | | | | |
|--------------------------|-----------------------|--------------------------------|---------------|---------------|----------------|----------------|
| | | 1_yr_sm (cfs) | 2_yr_sm (cfs) | 5_yr_sm (cfs) | 10_yr_sm (cfs) | 25_yr_sm (cfs) |
| DA1 | 0.090 | 52.5 | 77.9 | 116.5 | 146.8 | 187.5 |
| DA4 | 0.450 | 97.0 | 151.7 | 243.7 | 322.2 | 434.7 |
| DA2 | 1.323 | 228.3 | 363.3 | 597.5 | 798.4 | 1093.4 |
| DA3 | 0.920 | 96.7 | 175.5 | 325.1 | 459.7 | 665.3 |
| CON-1 | 2.693 | 416.3 | 682.1 | 1154.4 | 1565.7 | 2173.2 |

| | | Eccelston POI 1-4 Ultimate.out | | | | |
|--------------------------------|-----------------------------|--------------------------------|--------------------|--------------------|--------|--------|
| | | 381.8 | 645.7 | 1106.3 | 1500.7 | 2076.7 |
| | | 387.2 | 655.4 | 1121.1 | 1520.5 | 2103.7 |
| Area or Reach Identifier | Drainage Area (sq mi) | ----- Peak Flow by Storm ----- | | | | |
| | | 50_yr_sm (cfs) | 100_yr_sm (cfs) | 500_yr_sm (cfs) | (cfs) | (cfs) |
| DA1 | 0.090 | 218.5 | 249.3 | 315.9 | | |
| DA4 | 0.450 | 526.7 | 622.1 | 853.7 | | |
| DA2 | 1.323 | 1337.3 | 1593.4 | 2229.0 | | |
| DA3 | 0.920 | 840.4 | 1025.9 | 1497.0 | | |
| CON-1 | 2.693 | 2676.1 | 3215.2 | 4550.9 | | |
| DOWNSTREAM | | 2574.1 | 3101.4 | 4417.7 | | |
| OUTLET | 2.783 | 2609.6 | 3144.3 | 4484.3 | | |

| | | | | |
|----------------------------|--------|---------------|------|---|
| WinTR-20: version 3.20 | 0 | 0 | 0 | |
| Eccelston Mitigation POI 5 | | | | |
| SUB-AREA: | | | | |
| DA5 | OUTLET | 0.1392984374. | .609 | Y |

STORM ANALYSIS:

| | | | | |
|-----------|-------|-----------|---|------|
| 1_yr_sm | 2.71 | 1_yr_sm | 2 | 3.28 |
| 2_yr_sm | 3.28 | 2_yr_sm | 2 | 3.28 |
| 5_yr_sm | 4.22 | 5_yr_sm | 2 | 3.28 |
| 10_yr_sm | 5.04 | 10_yr_sm | 2 | 3.28 |
| 25_yr_sm | 6.31 | 25_yr_sm | 2 | 3.28 |
| 50_yr_sm | 7.43 | 50_yr_sm | 2 | 3.28 |
| 100_yr_sm | 8.71 | 100_yr_sm | 2 | 3.28 |
| 500_yr_sm | 12.39 | 500_yr_sm | 2 | 3.28 |

RAINFALL DISTRIBUTION:

| | | | | |
|---------|--------|--------|--------|--------|
| 1_yr_sm | 0.1 | | | |
| 0.0000 | 0.0011 | 0.0022 | 0.0033 | 0.0044 |
| 0.0056 | 0.0067 | 0.0078 | 0.0089 | 0.0100 |
| 0.0111 | 0.0122 | 0.0133 | 0.0144 | 0.0155 |
| 0.0167 | 0.0178 | 0.0189 | 0.0200 | 0.0211 |
| 0.0222 | 0.0233 | 0.0244 | 0.0255 | 0.0267 |
| 0.0278 | 0.0289 | 0.0300 | 0.0311 | 0.0322 |
| 0.0333 | 0.0344 | 0.0355 | 0.0366 | 0.0378 |
| 0.0389 | 0.0400 | 0.0411 | 0.0422 | 0.0433 |
| 0.0444 | 0.0455 | 0.0466 | 0.0478 | 0.0489 |
| 0.0500 | 0.0511 | 0.0522 | 0.0533 | 0.0544 |
| 0.0555 | 0.0566 | 0.0578 | 0.0589 | 0.0600 |
| 0.0611 | 0.0622 | 0.0633 | 0.0644 | 0.0655 |
| 0.0666 | 0.0694 | 0.0721 | 0.0749 | 0.0776 |
| 0.0804 | 0.0831 | 0.0859 | 0.0886 | 0.0914 |
| 0.0941 | 0.0969 | 0.0996 | 0.1024 | 0.1051 |
| 0.1079 | 0.1106 | 0.1134 | 0.1161 | 0.1189 |
| 0.1216 | 0.1244 | 0.1271 | 0.1299 | 0.1326 |
| 0.1354 | 0.1381 | 0.1409 | 0.1436 | 0.1464 |
| 0.1491 | 0.1537 | 0.1584 | 0.1630 | 0.1677 |
| 0.1723 | 0.1770 | 0.1816 | 0.1863 | 0.1909 |
| 0.1956 | 0.2002 | 0.2049 | 0.2095 | 0.2142 |
| 0.2188 | 0.2230 | 0.2271 | 0.2312 | 0.2353 |
| 0.2394 | 0.2480 | 0.2566 | 0.2652 | 0.2738 |

Eccelston POI 5 Ultimate.out

| | | | | |
|---------|--------|--------|--------|--------|
| 0.2824 | 0.2996 | 0.3169 | 0.3444 | 0.3880 |
| 0.5000 | 0.6120 | 0.6556 | 0.6831 | 0.7004 |
| 0.7176 | 0.7262 | 0.7348 | 0.7434 | 0.7520 |
| 0.7606 | 0.7647 | 0.7688 | 0.7729 | 0.7770 |
| 0.7812 | 0.7858 | 0.7905 | 0.7951 | 0.7998 |
| 0.8044 | 0.8091 | 0.8137 | 0.8184 | 0.8230 |
| 0.8277 | 0.8323 | 0.8370 | 0.8416 | 0.8463 |
| 0.8509 | 0.8536 | 0.8564 | 0.8591 | 0.8619 |
| 0.8646 | 0.8674 | 0.8701 | 0.8729 | 0.8756 |
| 0.8784 | 0.8811 | 0.8839 | 0.8866 | 0.8894 |
| 0.8921 | 0.8949 | 0.8976 | 0.9004 | 0.9031 |
| 0.9059 | 0.9086 | 0.9114 | 0.9141 | 0.9169 |
| 0.9196 | 0.9224 | 0.9251 | 0.9279 | 0.9306 |
| 0.9334 | 0.9345 | 0.9356 | 0.9367 | 0.9378 |
| 0.9389 | 0.9400 | 0.9411 | 0.9422 | 0.9434 |
| 0.9445 | 0.9456 | 0.9467 | 0.9478 | 0.9489 |
| 0.9500 | 0.9511 | 0.9522 | 0.9534 | 0.9545 |
| 0.9556 | 0.9567 | 0.9578 | 0.9589 | 0.9600 |
| 0.9611 | 0.9622 | 0.9634 | 0.9645 | 0.9656 |
| 0.9667 | 0.9678 | 0.9689 | 0.9700 | 0.9711 |
| 0.9722 | 0.9733 | 0.9745 | 0.9756 | 0.9767 |
| 0.9778 | 0.9789 | 0.9800 | 0.9811 | 0.9822 |
| 0.9833 | 0.9845 | 0.9856 | 0.9867 | 0.9878 |
| 0.9889 | 0.9900 | 0.9911 | 0.9922 | 0.9933 |
| 0.9944 | 0.9956 | 0.9967 | 0.9978 | 0.9989 |
| 1.0000 | | | | |
| 2_yr_sm | 0.1 | | | |
| 0.0000 | 0.0011 | 0.0022 | 0.0033 | 0.0044 |
| 0.0055 | 0.0066 | 0.0077 | 0.0088 | 0.0099 |
| 0.0110 | 0.0121 | 0.0132 | 0.0143 | 0.0154 |
| 0.0166 | 0.0177 | 0.0188 | 0.0199 | 0.0210 |
| 0.0221 | 0.0232 | 0.0243 | 0.0254 | 0.0265 |
| 0.0276 | 0.0287 | 0.0298 | 0.0309 | 0.0320 |
| 0.0331 | 0.0342 | 0.0353 | 0.0364 | 0.0375 |
| 0.0386 | 0.0397 | 0.0408 | 0.0419 | 0.0430 |
| 0.0441 | 0.0452 | 0.0463 | 0.0474 | 0.0486 |
| 0.0497 | 0.0508 | 0.0519 | 0.0530 | 0.0541 |
| 0.0552 | 0.0563 | 0.0574 | 0.0585 | 0.0596 |
| 0.0607 | 0.0618 | 0.0629 | 0.0640 | 0.0651 |
| 0.0662 | 0.0689 | 0.0717 | 0.0744 | 0.0771 |
| 0.0799 | 0.0826 | 0.0853 | 0.0880 | 0.0908 |
| 0.0935 | 0.0962 | 0.0990 | 0.1017 | 0.1044 |
| 0.1072 | 0.1099 | 0.1126 | 0.1153 | 0.1181 |
| 0.1208 | 0.1235 | 0.1263 | 0.1290 | 0.1317 |
| 0.1344 | 0.1372 | 0.1399 | 0.1426 | 0.1454 |
| 0.1481 | 0.1527 | 0.1573 | 0.1619 | 0.1665 |
| 0.1711 | 0.1757 | 0.1802 | 0.1848 | 0.1894 |
| 0.1940 | 0.1986 | 0.2032 | 0.2078 | 0.2124 |
| 0.2170 | 0.2211 | 0.2252 | 0.2293 | 0.2334 |
| 0.2375 | 0.2461 | 0.2547 | 0.2632 | 0.2718 |
| 0.2803 | 0.2982 | 0.3160 | 0.3443 | 0.3888 |
| 0.5000 | 0.6112 | 0.6557 | 0.6840 | 0.7018 |
| 0.7197 | 0.7282 | 0.7368 | 0.7453 | 0.7539 |
| 0.7625 | 0.7666 | 0.7707 | 0.7748 | 0.7789 |
| 0.7830 | 0.7876 | 0.7922 | 0.7968 | 0.8014 |
| 0.8060 | 0.8106 | 0.8152 | 0.8198 | 0.8243 |
| 0.8289 | 0.8335 | 0.8381 | 0.8427 | 0.8473 |
| 0.8519 | 0.8546 | 0.8574 | 0.8601 | 0.8628 |
| 0.8656 | 0.8683 | 0.8710 | 0.8737 | 0.8765 |
| 0.8792 | 0.8819 | 0.8847 | 0.8874 | 0.8901 |
| 0.8928 | 0.8956 | 0.8983 | 0.9010 | 0.9038 |
| 0.9065 | 0.9092 | 0.9120 | 0.9147 | 0.9174 |
| 0.9201 | 0.9229 | 0.9256 | 0.9283 | 0.9311 |

| | Eccelston POI 5 Ultimate.out | | | | |
|---------|------------------------------|--------|--------|--------|--------|
| | 0.9338 | 0.9349 | 0.9360 | 0.9371 | 0.9382 |
| | 0.9393 | 0.9404 | 0.9415 | 0.9426 | 0.9437 |
| | 0.9448 | 0.9459 | 0.9470 | 0.9481 | 0.9492 |
| | 0.9503 | 0.9514 | 0.9526 | 0.9537 | 0.9548 |
| | 0.9559 | 0.9570 | 0.9581 | 0.9592 | 0.9603 |
| | 0.9614 | 0.9625 | 0.9636 | 0.9647 | 0.9658 |
| | 0.9669 | 0.9680 | 0.9691 | 0.9702 | 0.9713 |
| | 0.9724 | 0.9735 | 0.9746 | 0.9757 | 0.9768 |
| | 0.9779 | 0.9790 | 0.9801 | 0.9812 | 0.9823 |
| | 0.9834 | 0.9846 | 0.9857 | 0.9868 | 0.9879 |
| | 0.9890 | 0.9901 | 0.9912 | 0.9923 | 0.9934 |
| | 0.9945 | 0.9956 | 0.9967 | 0.9978 | 0.9989 |
| | 1.0000 | | | | |
| 5_yr_sm | 0.1 | | | | |
| | 0.0000 | 0.0012 | 0.0023 | 0.0035 | 0.0047 |
| | 0.0059 | 0.0070 | 0.0082 | 0.0094 | 0.0106 |
| | 0.0117 | 0.0129 | 0.0141 | 0.0153 | 0.0164 |
| | 0.0176 | 0.0188 | 0.0200 | 0.0211 | 0.0223 |
| | 0.0235 | 0.0246 | 0.0258 | 0.0270 | 0.0282 |
| | 0.0293 | 0.0305 | 0.0317 | 0.0329 | 0.0340 |
| | 0.0352 | 0.0364 | 0.0376 | 0.0387 | 0.0399 |
| | 0.0411 | 0.0422 | 0.0434 | 0.0446 | 0.0458 |
| | 0.0469 | 0.0481 | 0.0493 | 0.0505 | 0.0516 |
| | 0.0528 | 0.0540 | 0.0552 | 0.0563 | 0.0575 |
| | 0.0587 | 0.0599 | 0.0610 | 0.0622 | 0.0634 |
| | 0.0645 | 0.0657 | 0.0669 | 0.0681 | 0.0692 |
| | 0.0704 | 0.0732 | 0.0760 | 0.0787 | 0.0815 |
| | 0.0843 | 0.0871 | 0.0898 | 0.0926 | 0.0954 |
| | 0.0982 | 0.1009 | 0.1037 | 0.1065 | 0.1093 |
| | 0.1120 | 0.1148 | 0.1176 | 0.1204 | 0.1232 |
| | 0.1259 | 0.1287 | 0.1315 | 0.1343 | 0.1370 |
| | 0.1398 | 0.1426 | 0.1454 | 0.1481 | 0.1509 |
| | 0.1537 | 0.1582 | 0.1626 | 0.1671 | 0.1716 |
| | 0.1760 | 0.1805 | 0.1850 | 0.1894 | 0.1939 |
| | 0.1984 | 0.2029 | 0.2073 | 0.2118 | 0.2163 |
| | 0.2207 | 0.2249 | 0.2291 | 0.2333 | 0.2375 |
| | 0.2416 | 0.2504 | 0.2592 | 0.2679 | 0.2767 |
| | 0.2854 | 0.3043 | 0.3232 | 0.3524 | 0.3970 |
| | 0.5000 | 0.6030 | 0.6476 | 0.6768 | 0.6957 |
| | 0.7146 | 0.7233 | 0.7321 | 0.7408 | 0.7496 |
| | 0.7584 | 0.7625 | 0.7667 | 0.7709 | 0.7751 |
| | 0.7793 | 0.7837 | 0.7882 | 0.7927 | 0.7971 |
| | 0.8016 | 0.8061 | 0.8106 | 0.8150 | 0.8195 |
| | 0.8240 | 0.8284 | 0.8329 | 0.8374 | 0.8418 |
| | 0.8463 | 0.8491 | 0.8519 | 0.8546 | 0.8574 |
| | 0.8602 | 0.8630 | 0.8657 | 0.8685 | 0.8713 |
| | 0.8741 | 0.8768 | 0.8796 | 0.8824 | 0.8852 |
| | 0.8880 | 0.8907 | 0.8935 | 0.8963 | 0.8991 |
| | 0.9018 | 0.9046 | 0.9074 | 0.9102 | 0.9129 |
| | 0.9157 | 0.9185 | 0.9213 | 0.9240 | 0.9268 |
| | 0.9296 | 0.9308 | 0.9319 | 0.9331 | 0.9343 |
| | 0.9355 | 0.9366 | 0.9378 | 0.9390 | 0.9401 |
| | 0.9413 | 0.9425 | 0.9437 | 0.9448 | 0.9460 |
| | 0.9472 | 0.9484 | 0.9495 | 0.9507 | 0.9519 |
| | 0.9531 | 0.9542 | 0.9554 | 0.9566 | 0.9578 |
| | 0.9589 | 0.9601 | 0.9613 | 0.9624 | 0.9636 |
| | 0.9648 | 0.9660 | 0.9671 | 0.9683 | 0.9695 |
| | 0.9707 | 0.9718 | 0.9730 | 0.9742 | 0.9754 |
| | 0.9765 | 0.9777 | 0.9789 | 0.9800 | 0.9812 |
| | 0.9824 | 0.9836 | 0.9847 | 0.9859 | 0.9871 |
| | 0.9883 | 0.9894 | 0.9906 | 0.9918 | 0.9930 |
| | 0.9941 | 0.9953 | 0.9965 | 0.9977 | 0.9988 |
| | 1.0000 | | | | |

| | Eccelston POI 5 Ultimate.out | | | | |
|----------|------------------------------|--------|--------|--------|--------|
| 10_yr_sm | 0.0000 | 0.0012 | 0.0025 | 0.0037 | 0.0049 |
| | 0.0061 | 0.0074 | 0.0086 | 0.0098 | 0.0110 |
| | 0.0123 | 0.0135 | 0.0147 | 0.0159 | 0.0172 |
| | 0.0184 | 0.0196 | 0.0208 | 0.0221 | 0.0233 |
| | 0.0245 | 0.0257 | 0.0270 | 0.0282 | 0.0294 |
| | 0.0306 | 0.0319 | 0.0331 | 0.0343 | 0.0355 |
| | 0.0368 | 0.0380 | 0.0392 | 0.0404 | 0.0417 |
| | 0.0429 | 0.0441 | 0.0453 | 0.0466 | 0.0478 |
| | 0.0490 | 0.0502 | 0.0515 | 0.0527 | 0.0539 |
| | 0.0552 | 0.0564 | 0.0576 | 0.0588 | 0.0601 |
| | 0.0613 | 0.0625 | 0.0637 | 0.0650 | 0.0662 |
| | 0.0674 | 0.0686 | 0.0699 | 0.0711 | 0.0723 |
| | 0.0735 | 0.0764 | 0.0793 | 0.0822 | 0.0851 |
| | 0.0879 | 0.0908 | 0.0937 | 0.0966 | 0.0995 |
| | 0.1023 | 0.1052 | 0.1081 | 0.1110 | 0.1139 |
| | 0.1167 | 0.1196 | 0.1225 | 0.1254 | 0.1283 |
| | 0.1311 | 0.1340 | 0.1369 | 0.1398 | 0.1427 |
| | 0.1455 | 0.1484 | 0.1513 | 0.1542 | 0.1570 |
| | 0.1599 | 0.1644 | 0.1689 | 0.1734 | 0.1779 |
| | 0.1824 | 0.1869 | 0.1914 | 0.1958 | 0.2003 |
| | 0.2048 | 0.2093 | 0.2138 | 0.2183 | 0.2228 |
| | 0.2273 | 0.2315 | 0.2357 | 0.2399 | 0.2441 |
| | 0.2483 | 0.2573 | 0.2663 | 0.2752 | 0.2842 |
| | 0.2931 | 0.3123 | 0.3315 | 0.3608 | 0.4041 |
| | 0.5000 | 0.5959 | 0.6392 | 0.6685 | 0.6877 |
| | 0.7069 | 0.7158 | 0.7248 | 0.7337 | 0.7427 |
| | 0.7517 | 0.7559 | 0.7601 | 0.7643 | 0.7685 |
| | 0.7727 | 0.7772 | 0.7817 | 0.7862 | 0.7907 |
| | 0.7952 | 0.7997 | 0.8042 | 0.8086 | 0.8131 |
| | 0.8176 | 0.8221 | 0.8266 | 0.8311 | 0.8356 |
| | 0.8401 | 0.8430 | 0.8458 | 0.8487 | 0.8516 |
| | 0.8545 | 0.8573 | 0.8602 | 0.8631 | 0.8660 |
| | 0.8689 | 0.8717 | 0.8746 | 0.8775 | 0.8804 |
| | 0.8833 | 0.8861 | 0.8890 | 0.8919 | 0.8948 |
| | 0.8977 | 0.9005 | 0.9034 | 0.9063 | 0.9092 |
| | 0.9121 | 0.9149 | 0.9178 | 0.9207 | 0.9236 |
| | 0.9265 | 0.9277 | 0.9289 | 0.9301 | 0.9314 |
| | 0.9326 | 0.9338 | 0.9350 | 0.9363 | 0.9375 |
| | 0.9387 | 0.9399 | 0.9412 | 0.9424 | 0.9436 |
| | 0.9448 | 0.9461 | 0.9473 | 0.9485 | 0.9498 |
| | 0.9510 | 0.9522 | 0.9534 | 0.9547 | 0.9559 |
| | 0.9571 | 0.9583 | 0.9596 | 0.9608 | 0.9620 |
| | 0.9632 | 0.9645 | 0.9657 | 0.9669 | 0.9681 |
| | 0.9694 | 0.9706 | 0.9718 | 0.9730 | 0.9743 |
| | 0.9755 | 0.9767 | 0.9779 | 0.9792 | 0.9804 |
| | 0.9816 | 0.9828 | 0.9841 | 0.9853 | 0.9865 |
| | 0.9877 | 0.9890 | 0.9902 | 0.9914 | 0.9926 |
| | 0.9939 | 0.9951 | 0.9963 | 0.9975 | 0.9988 |
| | 1.0000 | | | | |
| 25_yr_sm | | 0.1 | | | |
| | 0.0000 | 0.0013 | 0.0026 | 0.0039 | 0.0052 |
| | 0.0065 | 0.0079 | 0.0092 | 0.0105 | 0.0118 |
| | 0.0131 | 0.0144 | 0.0157 | 0.0170 | 0.0183 |
| | 0.0196 | 0.0210 | 0.0223 | 0.0236 | 0.0249 |
| | 0.0262 | 0.0275 | 0.0288 | 0.0301 | 0.0314 |
| | 0.0327 | 0.0340 | 0.0354 | 0.0367 | 0.0380 |
| | 0.0393 | 0.0406 | 0.0419 | 0.0432 | 0.0445 |
| | 0.0458 | 0.0471 | 0.0485 | 0.0498 | 0.0511 |
| | 0.0524 | 0.0537 | 0.0550 | 0.0563 | 0.0576 |
| | 0.0589 | 0.0602 | 0.0616 | 0.0629 | 0.0642 |
| | 0.0655 | 0.0668 | 0.0681 | 0.0694 | 0.0707 |
| | 0.0720 | 0.0733 | 0.0746 | 0.0760 | 0.0773 |

Eccelston POI 5 Ultimate.out

| | | | | |
|--------|--------|--------|--------|--------|
| 0.0786 | 0.0816 | 0.0846 | 0.0876 | 0.0906 |
| 0.0937 | 0.0967 | 0.0997 | 0.1027 | 0.1057 |
| 0.1087 | 0.1118 | 0.1148 | 0.1178 | 0.1208 |
| 0.1238 | 0.1268 | 0.1299 | 0.1329 | 0.1359 |
| 0.1389 | 0.1419 | 0.1449 | 0.1480 | 0.1510 |
| 0.1540 | 0.1570 | 0.1600 | 0.1630 | 0.1661 |
| 0.1691 | 0.1737 | 0.1782 | 0.1828 | 0.1874 |
| 0.1920 | 0.1966 | 0.2011 | 0.2057 | 0.2103 |
| 0.2149 | 0.2195 | 0.2241 | 0.2286 | 0.2332 |
| 0.2378 | 0.2421 | 0.2464 | 0.2507 | 0.2549 |
| 0.2592 | 0.2685 | 0.2777 | 0.2869 | 0.2961 |
| 0.3054 | 0.3248 | 0.3441 | 0.3728 | 0.4138 |
| 0.5000 | 0.5862 | 0.6272 | 0.6559 | 0.6752 |
| 0.6946 | 0.7039 | 0.7131 | 0.7223 | 0.7315 |
| 0.7408 | 0.7451 | 0.7493 | 0.7536 | 0.7579 |
| 0.7622 | 0.7668 | 0.7714 | 0.7759 | 0.7805 |
| 0.7851 | 0.7897 | 0.7943 | 0.7989 | 0.8034 |
| 0.8080 | 0.8126 | 0.8172 | 0.8218 | 0.8263 |
| 0.8309 | 0.8339 | 0.8370 | 0.8400 | 0.8430 |
| 0.8460 | 0.8490 | 0.8520 | 0.8551 | 0.8581 |
| 0.8611 | 0.8641 | 0.8671 | 0.8701 | 0.8732 |
| 0.8762 | 0.8792 | 0.8822 | 0.8852 | 0.8882 |
| 0.8913 | 0.8943 | 0.8973 | 0.9003 | 0.9033 |
| 0.9063 | 0.9094 | 0.9124 | 0.9154 | 0.9184 |
| 0.9214 | 0.9227 | 0.9240 | 0.9254 | 0.9267 |
| 0.9280 | 0.9293 | 0.9306 | 0.9319 | 0.9332 |
| 0.9345 | 0.9358 | 0.9371 | 0.9384 | 0.9398 |
| 0.9411 | 0.9424 | 0.9437 | 0.9450 | 0.9463 |
| 0.9476 | 0.9489 | 0.9502 | 0.9515 | 0.9529 |
| 0.9542 | 0.9555 | 0.9568 | 0.9581 | 0.9594 |
| 0.9607 | 0.9620 | 0.9633 | 0.9646 | 0.9660 |
| 0.9673 | 0.9686 | 0.9699 | 0.9712 | 0.9725 |
| 0.9738 | 0.9751 | 0.9764 | 0.9777 | 0.9790 |
| 0.9804 | 0.9817 | 0.9830 | 0.9843 | 0.9856 |
| 0.9869 | 0.9882 | 0.9895 | 0.9908 | 0.9921 |
| 0.9935 | 0.9948 | 0.9961 | 0.9974 | 0.9987 |
| 1.0000 | | | | |

50_yr_sm

| | | | | |
|--------|--------|--------|--------|--------|
| | 0.1 | | | |
| 0.0000 | 0.0014 | 0.0027 | 0.0041 | 0.0055 |
| 0.0068 | 0.0082 | 0.0095 | 0.0109 | 0.0123 |
| 0.0136 | 0.0150 | 0.0164 | 0.0177 | 0.0191 |
| 0.0205 | 0.0218 | 0.0232 | 0.0246 | 0.0259 |
| 0.0273 | 0.0286 | 0.0300 | 0.0314 | 0.0327 |
| 0.0341 | 0.0355 | 0.0368 | 0.0382 | 0.0396 |
| 0.0409 | 0.0423 | 0.0436 | 0.0450 | 0.0464 |
| 0.0477 | 0.0491 | 0.0505 | 0.0518 | 0.0532 |
| 0.0546 | 0.0559 | 0.0573 | 0.0587 | 0.0600 |
| 0.0614 | 0.0627 | 0.0641 | 0.0655 | 0.0668 |
| 0.0682 | 0.0696 | 0.0709 | 0.0723 | 0.0737 |
| 0.0750 | 0.0764 | 0.0777 | 0.0791 | 0.0805 |
| 0.0818 | 0.0850 | 0.0881 | 0.0913 | 0.0944 |
| 0.0976 | 0.1007 | 0.1039 | 0.1070 | 0.1102 |
| 0.1133 | 0.1165 | 0.1196 | 0.1227 | 0.1259 |
| 0.1290 | 0.1322 | 0.1353 | 0.1385 | 0.1416 |
| 0.1448 | 0.1479 | 0.1511 | 0.1542 | 0.1574 |
| 0.1605 | 0.1636 | 0.1668 | 0.1699 | 0.1731 |
| 0.1762 | 0.1809 | 0.1856 | 0.1903 | 0.1949 |
| 0.1996 | 0.2043 | 0.2089 | 0.2136 | 0.2183 |
| 0.2230 | 0.2276 | 0.2323 | 0.2370 | 0.2417 |
| 0.2463 | 0.2507 | 0.2550 | 0.2593 | 0.2636 |
| 0.2679 | 0.2774 | 0.2869 | 0.2964 | 0.3059 |
| 0.3154 | 0.3348 | 0.3541 | 0.3821 | 0.4210 |
| 0.5000 | 0.5790 | 0.6179 | 0.6459 | 0.6652 |

Eccelston POI 5 Ultimate.out

| | | | | |
|--------|--------|--------|--------|--------|
| 0.6846 | 0.6941 | 0.7036 | 0.7131 | 0.7226 |
| 0.7321 | 0.7364 | 0.7407 | 0.7450 | 0.7493 |
| 0.7537 | 0.7583 | 0.7630 | 0.7677 | 0.7724 |
| 0.7770 | 0.7817 | 0.7864 | 0.7911 | 0.7957 |
| 0.8004 | 0.8051 | 0.8097 | 0.8144 | 0.8191 |
| 0.8238 | 0.8269 | 0.8301 | 0.8332 | 0.8364 |
| 0.8395 | 0.8426 | 0.8458 | 0.8489 | 0.8521 |
| 0.8552 | 0.8584 | 0.8615 | 0.8647 | 0.8678 |
| 0.8710 | 0.8741 | 0.8773 | 0.8804 | 0.8835 |
| 0.8867 | 0.8898 | 0.8930 | 0.8961 | 0.8993 |
| 0.9024 | 0.9056 | 0.9087 | 0.9119 | 0.9150 |
| 0.9182 | 0.9195 | 0.9209 | 0.9223 | 0.9236 |
| 0.9250 | 0.9263 | 0.9277 | 0.9291 | 0.9304 |
| 0.9318 | 0.9332 | 0.9345 | 0.9359 | 0.9373 |
| 0.9386 | 0.9400 | 0.9413 | 0.9427 | 0.9441 |
| 0.9454 | 0.9468 | 0.9482 | 0.9495 | 0.9509 |
| 0.9523 | 0.9536 | 0.9550 | 0.9564 | 0.9577 |
| 0.9591 | 0.9604 | 0.9618 | 0.9632 | 0.9645 |
| 0.9659 | 0.9673 | 0.9686 | 0.9700 | 0.9714 |
| 0.9727 | 0.9741 | 0.9754 | 0.9768 | 0.9782 |
| 0.9795 | 0.9809 | 0.9823 | 0.9836 | 0.9850 |
| 0.9864 | 0.9877 | 0.9891 | 0.9905 | 0.9918 |
| 0.9932 | 0.9945 | 0.9959 | 0.9973 | 0.9986 |
| 1.0000 | | | | |

100_yr_sm

| | | | | |
|--------|--------|--------|--------|--------|
| | 0.1 | | | |
| 0.0000 | 0.0014 | 0.0029 | 0.0043 | 0.0057 |
| 0.0071 | 0.0086 | 0.0100 | 0.0114 | 0.0128 |
| 0.0143 | 0.0157 | 0.0171 | 0.0185 | 0.0200 |
| 0.0214 | 0.0228 | 0.0243 | 0.0257 | 0.0271 |
| 0.0285 | 0.0300 | 0.0314 | 0.0328 | 0.0342 |
| 0.0357 | 0.0371 | 0.0385 | 0.0399 | 0.0414 |
| 0.0428 | 0.0442 | 0.0457 | 0.0471 | 0.0485 |
| 0.0499 | 0.0514 | 0.0528 | 0.0542 | 0.0556 |
| 0.0571 | 0.0585 | 0.0599 | 0.0613 | 0.0628 |
| 0.0642 | 0.0656 | 0.0671 | 0.0685 | 0.0699 |
| 0.0713 | 0.0728 | 0.0742 | 0.0756 | 0.0770 |
| 0.0785 | 0.0799 | 0.0813 | 0.0827 | 0.0842 |
| 0.0856 | 0.0889 | 0.0922 | 0.0954 | 0.0987 |
| 0.1020 | 0.1053 | 0.1086 | 0.1118 | 0.1151 |
| 0.1184 | 0.1217 | 0.1250 | 0.1282 | 0.1315 |
| 0.1348 | 0.1381 | 0.1414 | 0.1447 | 0.1479 |
| 0.1512 | 0.1545 | 0.1578 | 0.1611 | 0.1643 |
| 0.1676 | 0.1709 | 0.1742 | 0.1775 | 0.1807 |
| 0.1840 | 0.1888 | 0.1935 | 0.1983 | 0.2031 |
| 0.2078 | 0.2126 | 0.2174 | 0.2221 | 0.2269 |
| 0.2317 | 0.2364 | 0.2412 | 0.2459 | 0.2507 |
| 0.2555 | 0.2598 | 0.2641 | 0.2684 | 0.2727 |
| 0.2770 | 0.2867 | 0.2964 | 0.3062 | 0.3159 |
| 0.3256 | 0.3447 | 0.3638 | 0.3910 | 0.4277 |
| 0.5000 | 0.5723 | 0.6090 | 0.6362 | 0.6553 |
| 0.6744 | 0.6841 | 0.6938 | 0.7036 | 0.7133 |
| 0.7230 | 0.7273 | 0.7316 | 0.7359 | 0.7402 |
| 0.7445 | 0.7493 | 0.7541 | 0.7588 | 0.7636 |
| 0.7683 | 0.7731 | 0.7779 | 0.7826 | 0.7874 |
| 0.7922 | 0.7969 | 0.8017 | 0.8065 | 0.8112 |
| 0.8160 | 0.8193 | 0.8225 | 0.8258 | 0.8291 |
| 0.8324 | 0.8357 | 0.8389 | 0.8422 | 0.8455 |
| 0.8488 | 0.8521 | 0.8553 | 0.8586 | 0.8619 |
| 0.8652 | 0.8685 | 0.8718 | 0.8750 | 0.8783 |
| 0.8816 | 0.8849 | 0.8882 | 0.8914 | 0.8947 |
| 0.8980 | 0.9013 | 0.9046 | 0.9078 | 0.9111 |
| 0.9144 | 0.9158 | 0.9173 | 0.9187 | 0.9201 |
| 0.9215 | 0.9230 | 0.9244 | 0.9258 | 0.9272 |

| | Eccelston POI 5 Ultimate.out | | | | |
|-----------|------------------------------|--------|--------|--------|--|
| 0.9287 | 0.9301 | 0.9315 | 0.9329 | 0.9344 | |
| 0.9358 | 0.9372 | 0.9387 | 0.9401 | 0.9415 | |
| 0.9429 | 0.9444 | 0.9458 | 0.9472 | 0.9486 | |
| 0.9501 | 0.9515 | 0.9529 | 0.9543 | 0.9558 | |
| 0.9572 | 0.9586 | 0.9601 | 0.9615 | 0.9629 | |
| 0.9643 | 0.9658 | 0.9672 | 0.9686 | 0.9700 | |
| 0.9715 | 0.9729 | 0.9743 | 0.9757 | 0.9772 | |
| 0.9786 | 0.9800 | 0.9815 | 0.9829 | 0.9843 | |
| 0.9857 | 0.9872 | 0.9886 | 0.9900 | 0.9914 | |
| 0.9929 | 0.9943 | 0.9957 | 0.9971 | 0.9986 | |
| 1.0000 | | | | | |
| 500_yr_sm | 0.1 | | | | |
| 0.0000 | 0.0016 | 0.0031 | 0.0047 | 0.0063 | |
| 0.0078 | 0.0094 | 0.0110 | 0.0126 | 0.0141 | |
| 0.0157 | 0.0173 | 0.0188 | 0.0204 | 0.0220 | |
| 0.0235 | 0.0251 | 0.0267 | 0.0283 | 0.0298 | |
| 0.0314 | 0.0330 | 0.0345 | 0.0361 | 0.0377 | |
| 0.0392 | 0.0408 | 0.0424 | 0.0439 | 0.0455 | |
| 0.0471 | 0.0487 | 0.0502 | 0.0518 | 0.0534 | |
| 0.0549 | 0.0565 | 0.0581 | 0.0596 | 0.0612 | |
| 0.0628 | 0.0643 | 0.0659 | 0.0675 | 0.0691 | |
| 0.0706 | 0.0722 | 0.0738 | 0.0753 | 0.0769 | |
| 0.0785 | 0.0800 | 0.0816 | 0.0832 | 0.0848 | |
| 0.0863 | 0.0879 | 0.0895 | 0.0910 | 0.0926 | |
| 0.0942 | 0.0978 | 0.1014 | 0.1050 | 0.1086 | |
| 0.1122 | 0.1158 | 0.1195 | 0.1231 | 0.1267 | |
| 0.1303 | 0.1339 | 0.1375 | 0.1411 | 0.1447 | |
| 0.1483 | 0.1520 | 0.1556 | 0.1592 | 0.1628 | |
| 0.1664 | 0.1700 | 0.1736 | 0.1772 | 0.1809 | |
| 0.1845 | 0.1881 | 0.1917 | 0.1953 | 0.1989 | |
| 0.2025 | 0.2075 | 0.2124 | 0.2174 | 0.2223 | |
| 0.2272 | 0.2322 | 0.2371 | 0.2421 | 0.2470 | |
| 0.2520 | 0.2569 | 0.2618 | 0.2668 | 0.2717 | |
| 0.2767 | 0.2810 | 0.2853 | 0.2896 | 0.2940 | |
| 0.2983 | 0.3084 | 0.3185 | 0.3287 | 0.3388 | |
| 0.3489 | 0.3673 | 0.3856 | 0.4104 | 0.4420 | |
| 0.5000 | 0.5580 | 0.5896 | 0.6144 | 0.6327 | |
| 0.6511 | 0.6612 | 0.6713 | 0.6815 | 0.6916 | |
| 0.7017 | 0.7060 | 0.7104 | 0.7147 | 0.7190 | |
| 0.7233 | 0.7283 | 0.7332 | 0.7382 | 0.7431 | |
| 0.7480 | 0.7530 | 0.7579 | 0.7629 | 0.7678 | |
| 0.7728 | 0.7777 | 0.7826 | 0.7876 | 0.7925 | |
| 0.7975 | 0.8011 | 0.8047 | 0.8083 | 0.8119 | |
| 0.8155 | 0.8191 | 0.8228 | 0.8264 | 0.8300 | |
| 0.8336 | 0.8372 | 0.8408 | 0.8444 | 0.8480 | |
| 0.8517 | 0.8553 | 0.8589 | 0.8625 | 0.8661 | |
| 0.8697 | 0.8733 | 0.8769 | 0.8805 | 0.8842 | |
| 0.8878 | 0.8914 | 0.8950 | 0.8986 | 0.9022 | |
| 0.9058 | 0.9074 | 0.9090 | 0.9105 | 0.9121 | |
| 0.9137 | 0.9152 | 0.9168 | 0.9184 | 0.9200 | |
| 0.9215 | 0.9231 | 0.9247 | 0.9262 | 0.9278 | |
| 0.9294 | 0.9309 | 0.9325 | 0.9341 | 0.9357 | |
| 0.9372 | 0.9388 | 0.9404 | 0.9419 | 0.9435 | |
| 0.9451 | 0.9466 | 0.9482 | 0.9498 | 0.9513 | |
| 0.9529 | 0.9545 | 0.9561 | 0.9576 | 0.9592 | |
| 0.9608 | 0.9623 | 0.9639 | 0.9655 | 0.9670 | |
| 0.9686 | 0.9702 | 0.9717 | 0.9733 | 0.9749 | |
| 0.9765 | 0.9780 | 0.9796 | 0.9812 | 0.9827 | |
| 0.9843 | 0.9859 | 0.9874 | 0.9890 | 0.9906 | |
| 0.9922 | 0.9937 | 0.9953 | 0.9969 | 0.9984 | |
| 1.0000 | | | | | |

Eccelston POI 5 Ultimate.out

GLOBAL OUTPUT:

.2 NN N NN N

winTR-20 Printed Page File End of Input Data List

Eccelston Mitigation POI 5

Name of printed page file:
C:\Users\cwagner\Desktop\Eccelston POI 5 Ultimate.out

STORM 1_yr_sm

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| OUTLET | 0.139 | | 0.728 | | 12.46 | 42.0 | 301.19 |

STORM 2_yr_sm

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| OUTLET | 0.139 | | 1.088 | | 12.44 | 66.3 | 475.87 |

STORM 5_yr_sm

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| OUTLET | 0.139 | | 1.757 | | 12.44 | 106.0 | 761.04 |

STORM 10_yr_sm

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| OUTLET | 0.139 | | 2.393 | | 12.44 | 138.9 | 997.17 |

STORM 25_yr_sm

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| OUTLET | 0.139 | | 3.445 | | 12.43 | 186.0 | 1335.10 |

STORM 50_yr_sm

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|----------------|----------------|-----------------|------------|
| OUTLET | 0.139 | | | | | | |

| Identifier | (sq mi) | Location | Eccelston POI 5 (in) | Ultimate.out (ft) | (hr) | (cfs) | (csm) |
|-----------------|---------|----------|-------------------------|----------------------|-------|-------|---------|
| OUTLET | 0.139 | | 4.417 | | 12.41 | 223.3 | 1603.02 |
| STORM 100_yr_sm | | | | | | | |

WinTR-20 Version 3.20
♀

Page 1

06/18/2018 16:10

Eccelston Mitigation POI 5

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | ----- Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | ----- Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|-------------------------|----------------|-----------------|---------------------|
| OUTLET | 0.139 | | 5.563 | | 12.43 | 261.2 | 1875.46 |
| STORM 500_yr_sm | | | | | | | |

| Area or Reach Identifier | Drainage Area (sq mi) | Rain Gage ID or Location | Runoff Amount (in) | ----- Elevation (ft) | Peak Time (hr) | Flow Rate (cfs) | ----- Rate (csm) |
|--------------------------|-----------------------|--------------------------|--------------------|-------------------------|----------------|-----------------|---------------------|
| OUTLET | 0.139 | | 8.984 | | 12.42 | 349.2 | 2507.02 |

Eccelston Mitigation POI 5

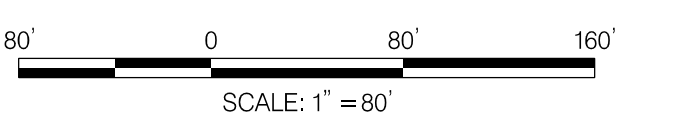
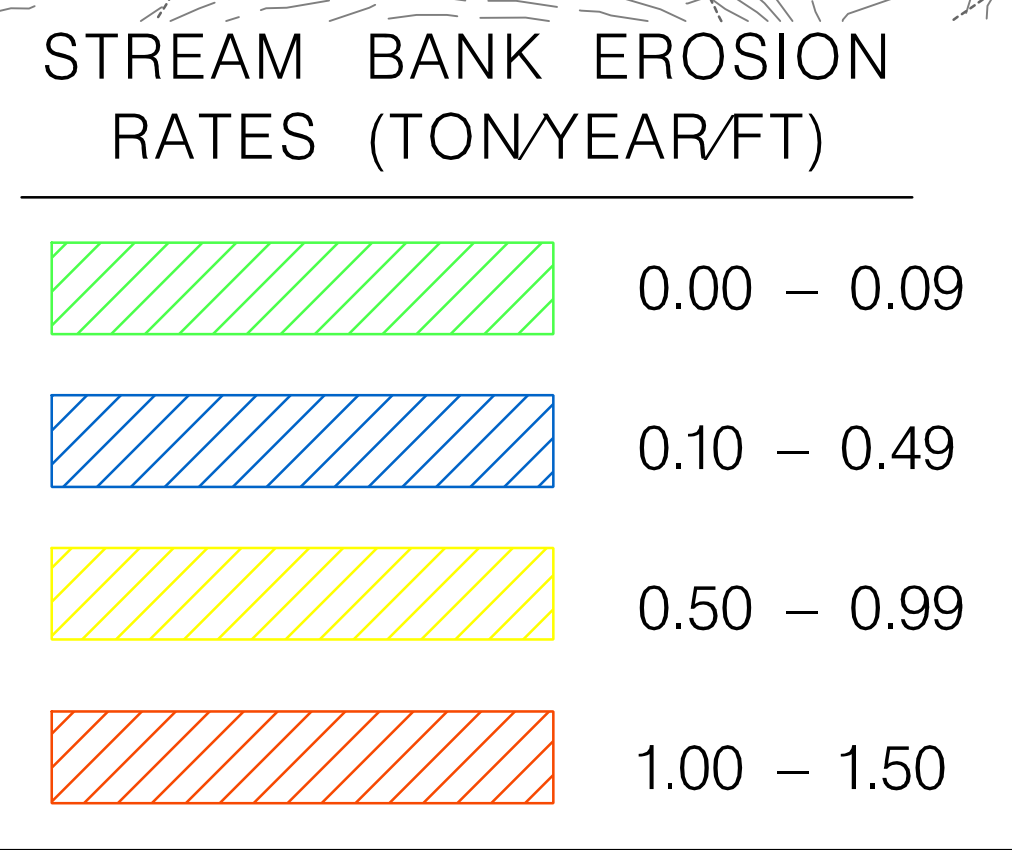
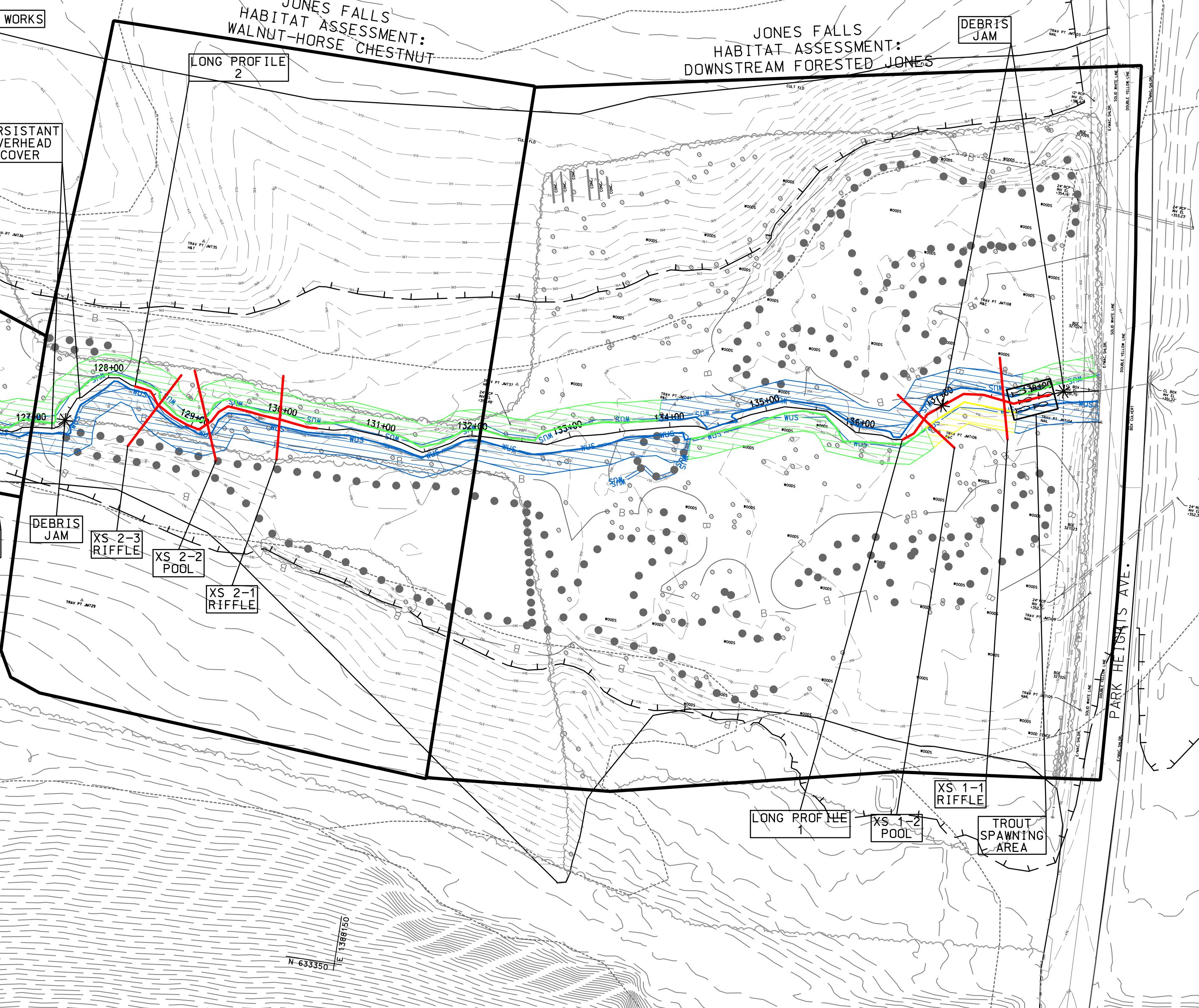
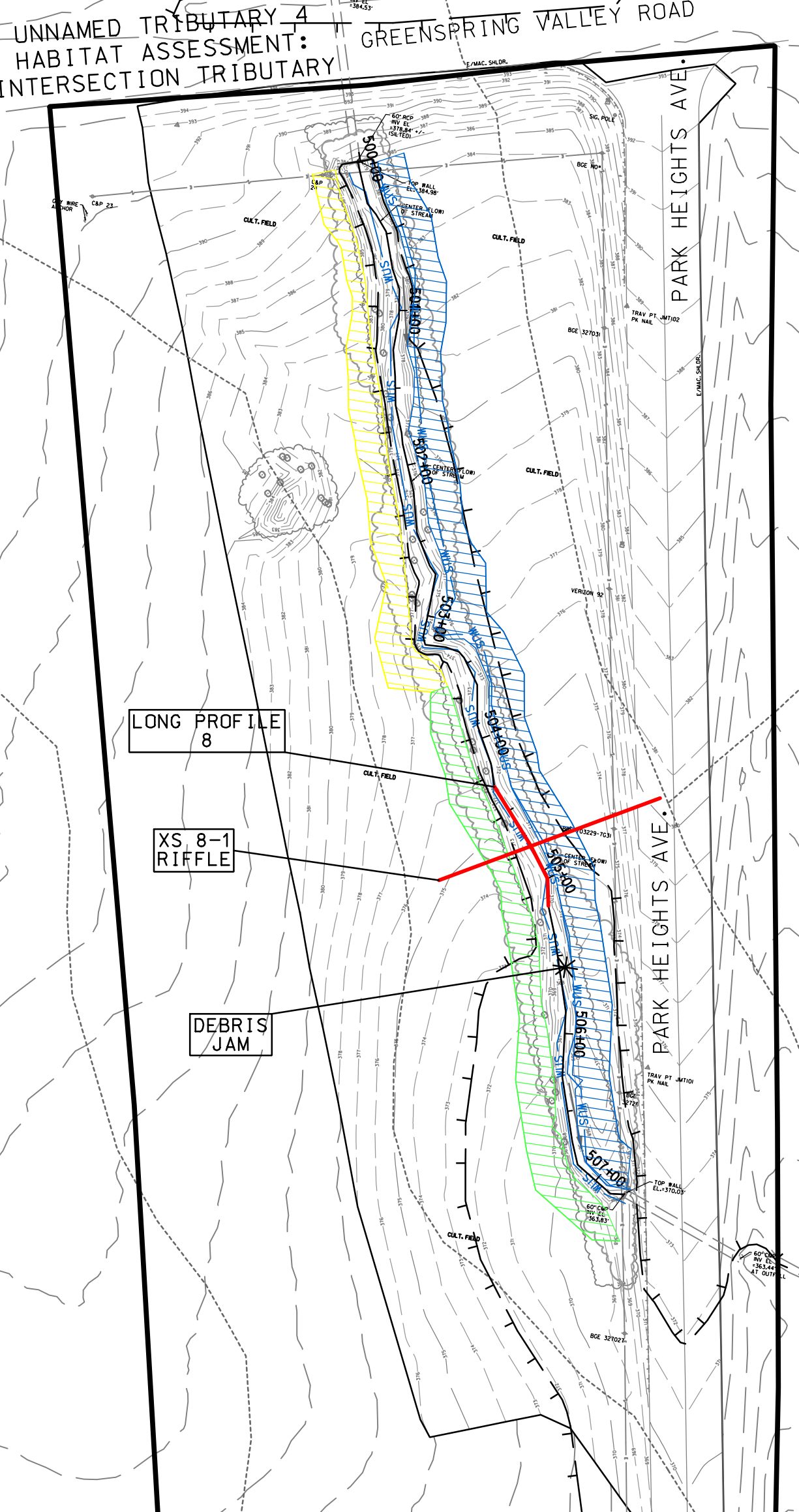
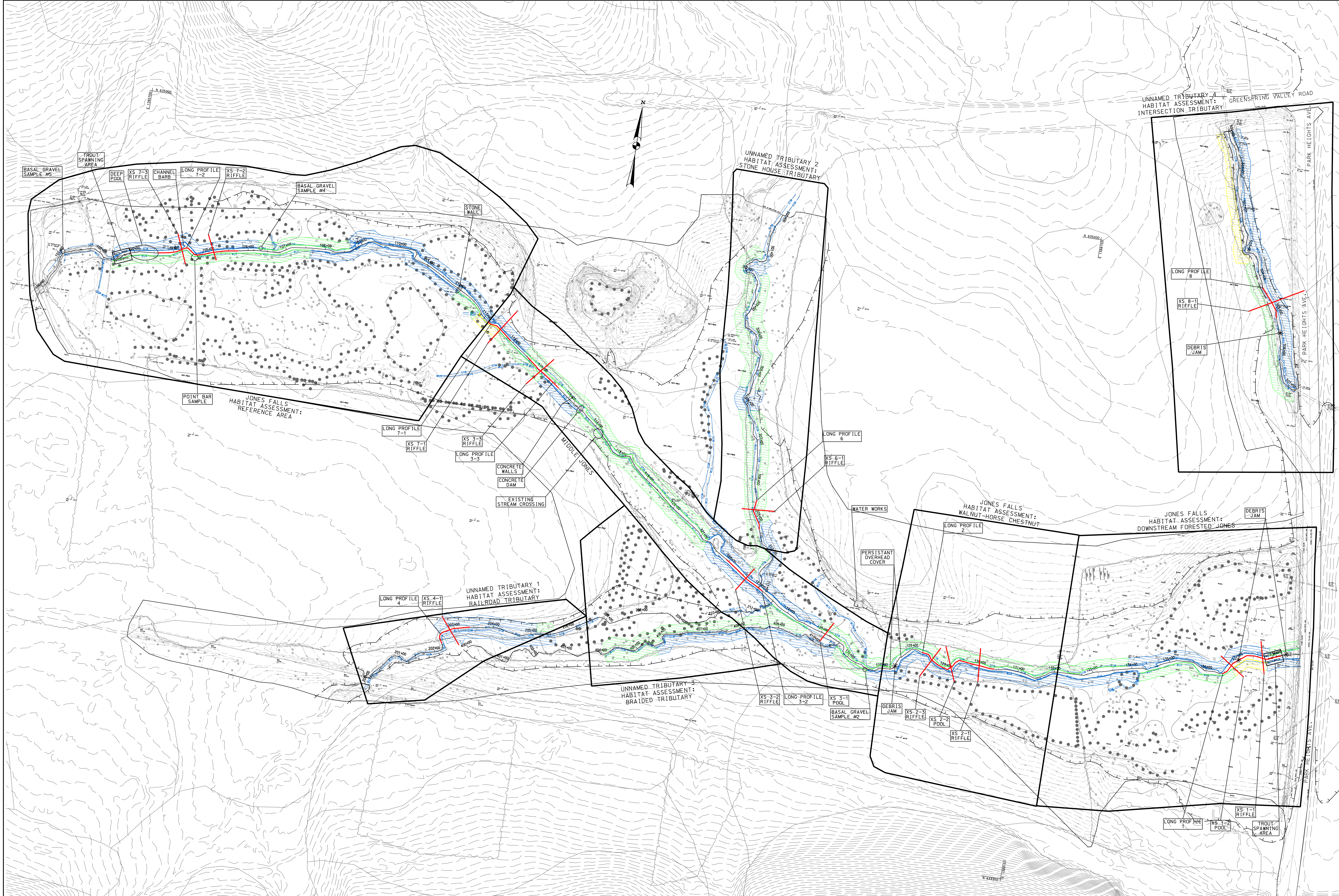
| Area or Reach Identifier | Drainage Area (sq mi) | ----- Peak Flow by Storm ----- | | | | |
|--------------------------|-----------------------|--------------------------------|---------------|---------------|----------------|----------------|
| | | 1_yr_sm (cfs) | 2_yr_sm (cfs) | 5_yr_sm (cfs) | 10_yr_sm (cfs) | 25_yr_sm (cfs) |
| DA5 | 0.139 | 42.0 | 66.3 | 106.0 | 138.9 | 186.0 |
| OUTLET | 0.139 | 42.0 | 66.3 | 106.0 | 138.9 | 186.0 |

| Area or Reach Identifier | Drainage Area (sq mi) | ----- Peak Flow by Storm ----- | | | |
|--------------------------|-----------------------|--------------------------------|-----------------|-----------------|-------|
| | | 50_yr_sm (cfs) | 100_yr_sm (cfs) | 500_yr_sm (cfs) | (cfs) |
| DA5 | 0.139 | 223.3 | 261.2 | 349.2 | |
| OUTLET | 0.139 | 223.3 | 261.2 | 349.2 | |



APPENDIX D

Existing Conditions Geomorphic Data



ECCLESTON MITIGATION SITE

| REVISIONS | | SITE ASSESSMENT MAP | |
|----------------------|----------------------------|----------------------|-----------------|
| CONCEPT SUBMISSION | SCALE AS SHOWN | DATE MAY, 2018 | CONTRACT NO. |
| NOT FOR CONSTRUCTION | DESIGNED BY MRG | COUNTY | |
| | DRAWN BY MRG | LOGMILE | |
| | CHECKED BY FAB | HORIZONTAL SCALE N/A | |
| | F.A.P. NO. SEE TITLE SHEET | VERTICAL SCALE N/A | |
| | DRAWING NO. SAM - 1 | OF 1 | SHEET NO. OF XX |

PLOTTED: Wednesday, November 07, 2018 AT 10:51 PM
FILE: G:\2017\101871_01_Eccleston_Mitigation\GIS\Map\010_Eccleston.dwg

XS 1-1 (Riffle)

○ Ground Points

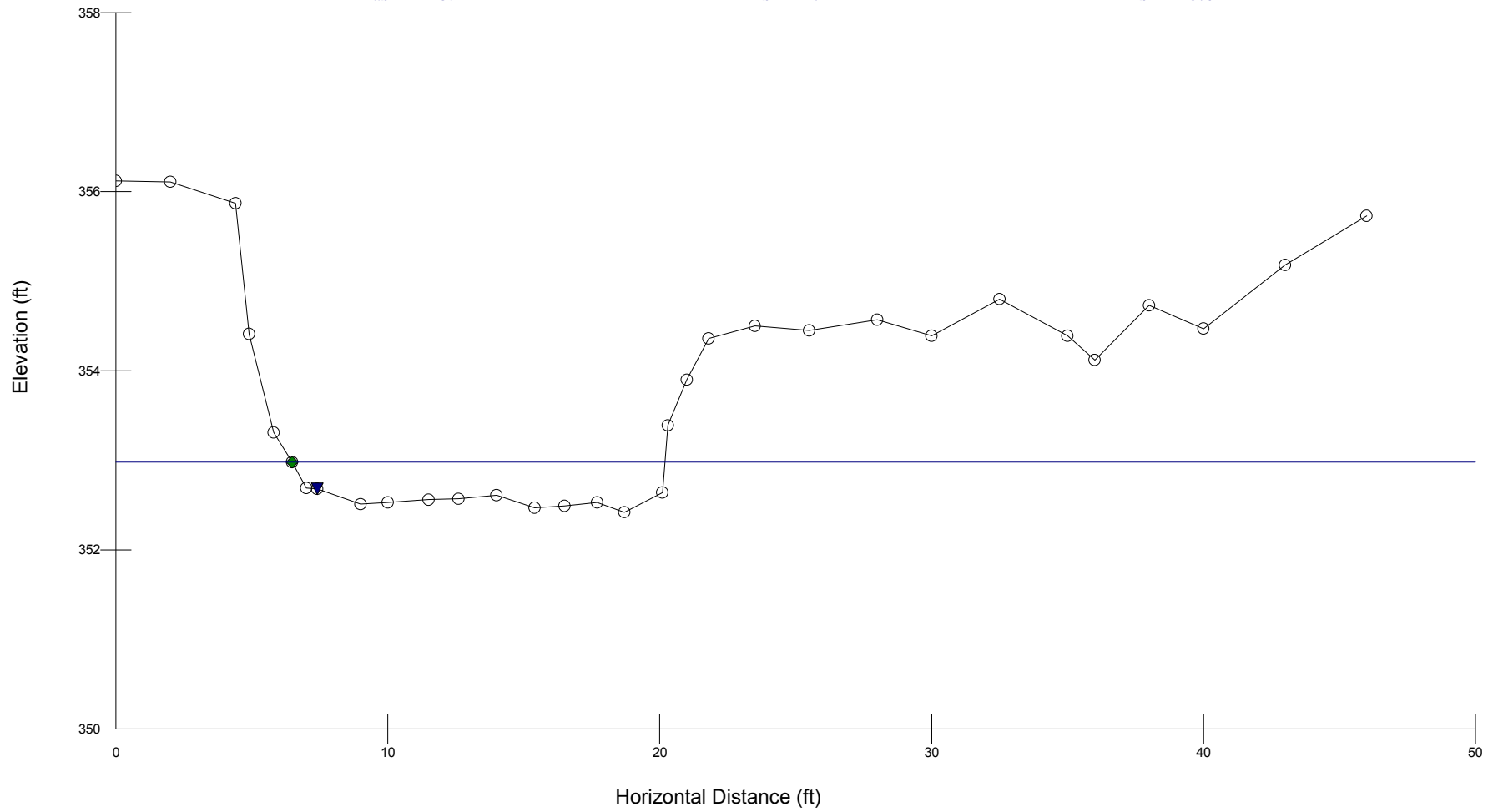
◆ Bankfull Indicators

▼ Water Surface Points

Wbkf = 13.7

Dbkf = .42

Abkf = 5.8



XS 1-2 (Pool)

○ Ground Points

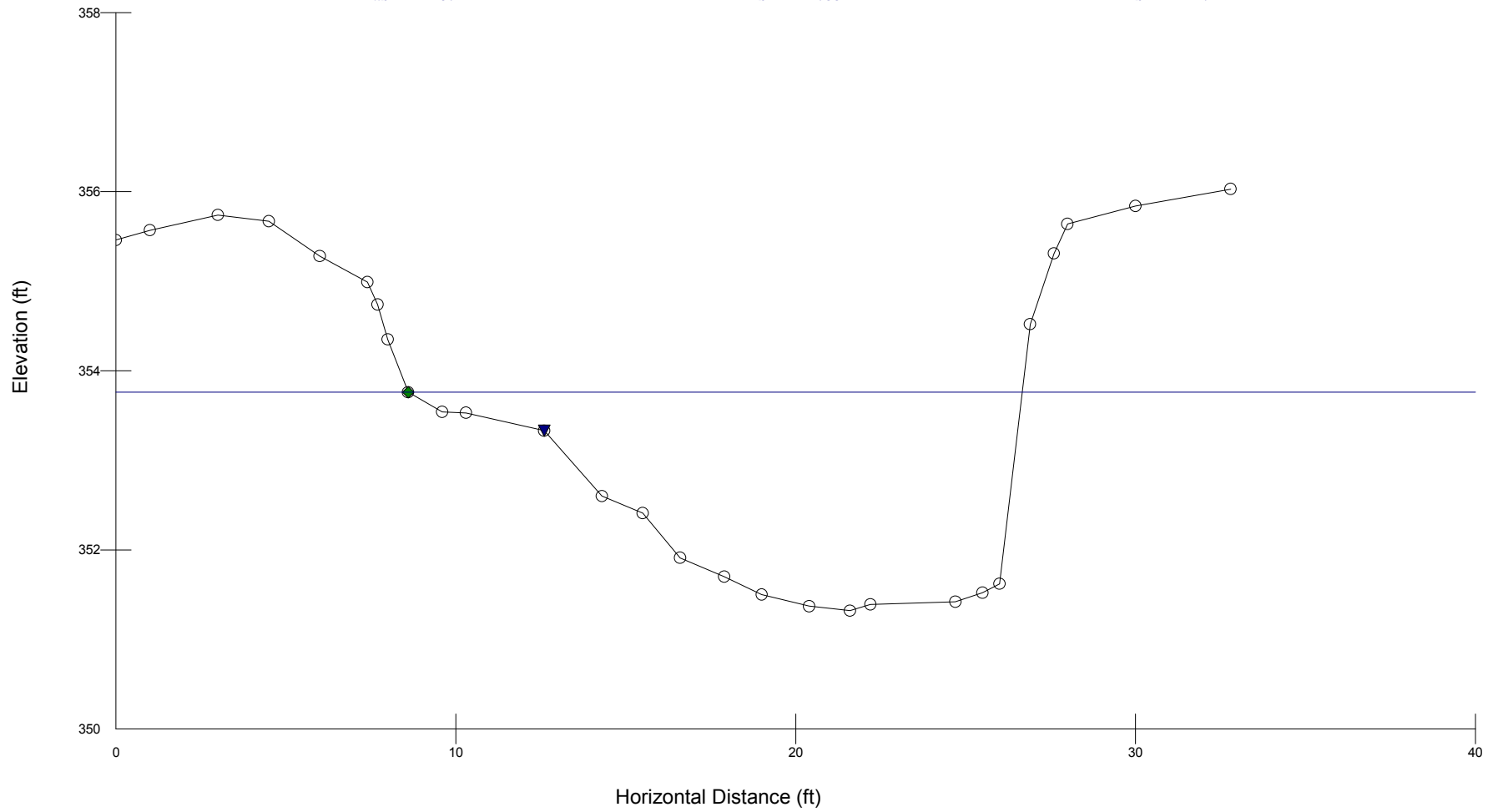
◆ Bankfull Indicators

▼ Water Surface Points

Wbkf = 18.1

Dbkf = 1.53

Abkf = 27.7



XS 2-1 (Riffle)

○ Ground Points

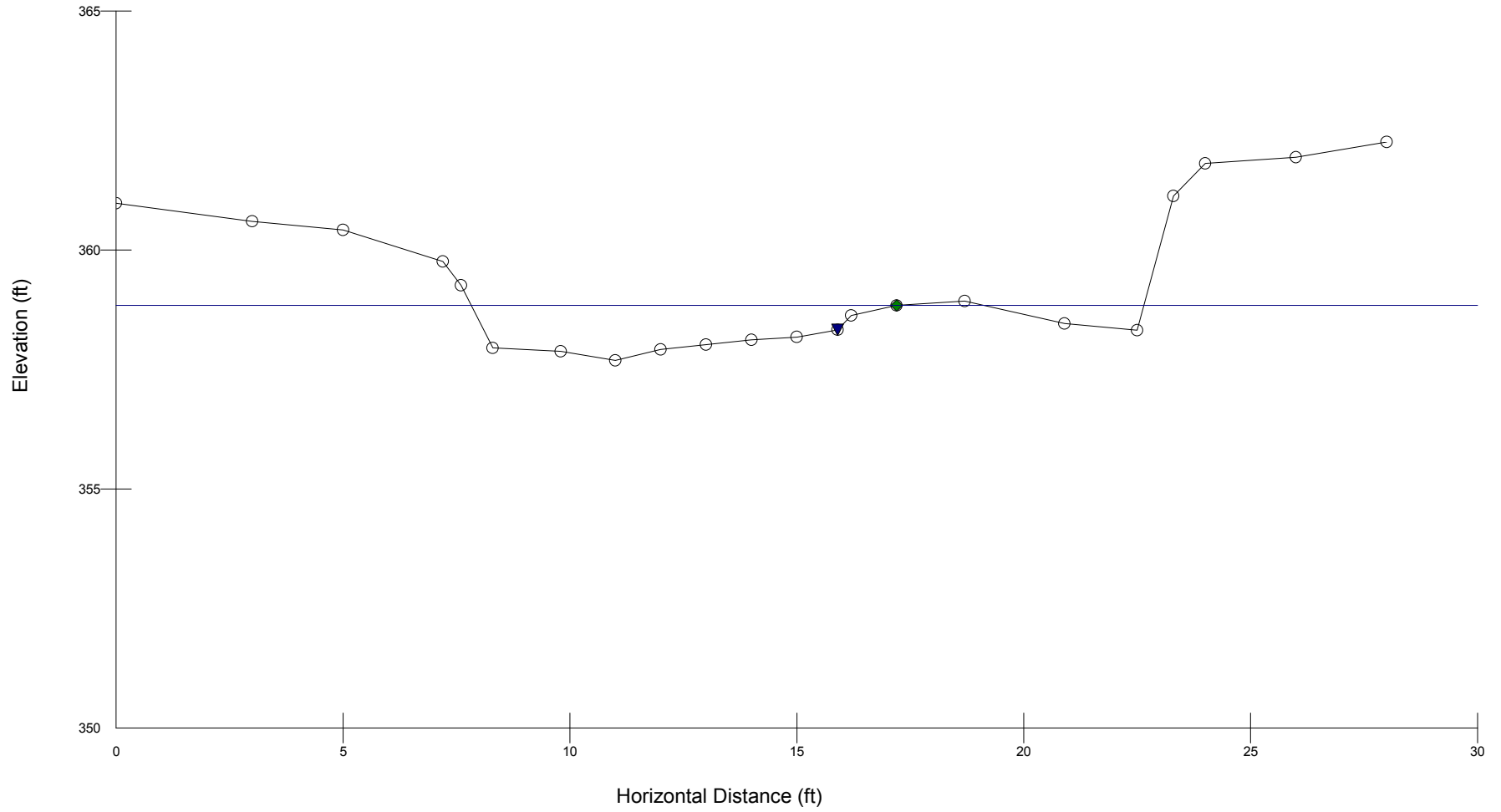
◆ Bankfull Indicators

▼ Water Surface Points

Wbkf = 12.9

Dbkf = .63

Abkf = 8.07



XS 2-2 (Pool)

○ Ground Points

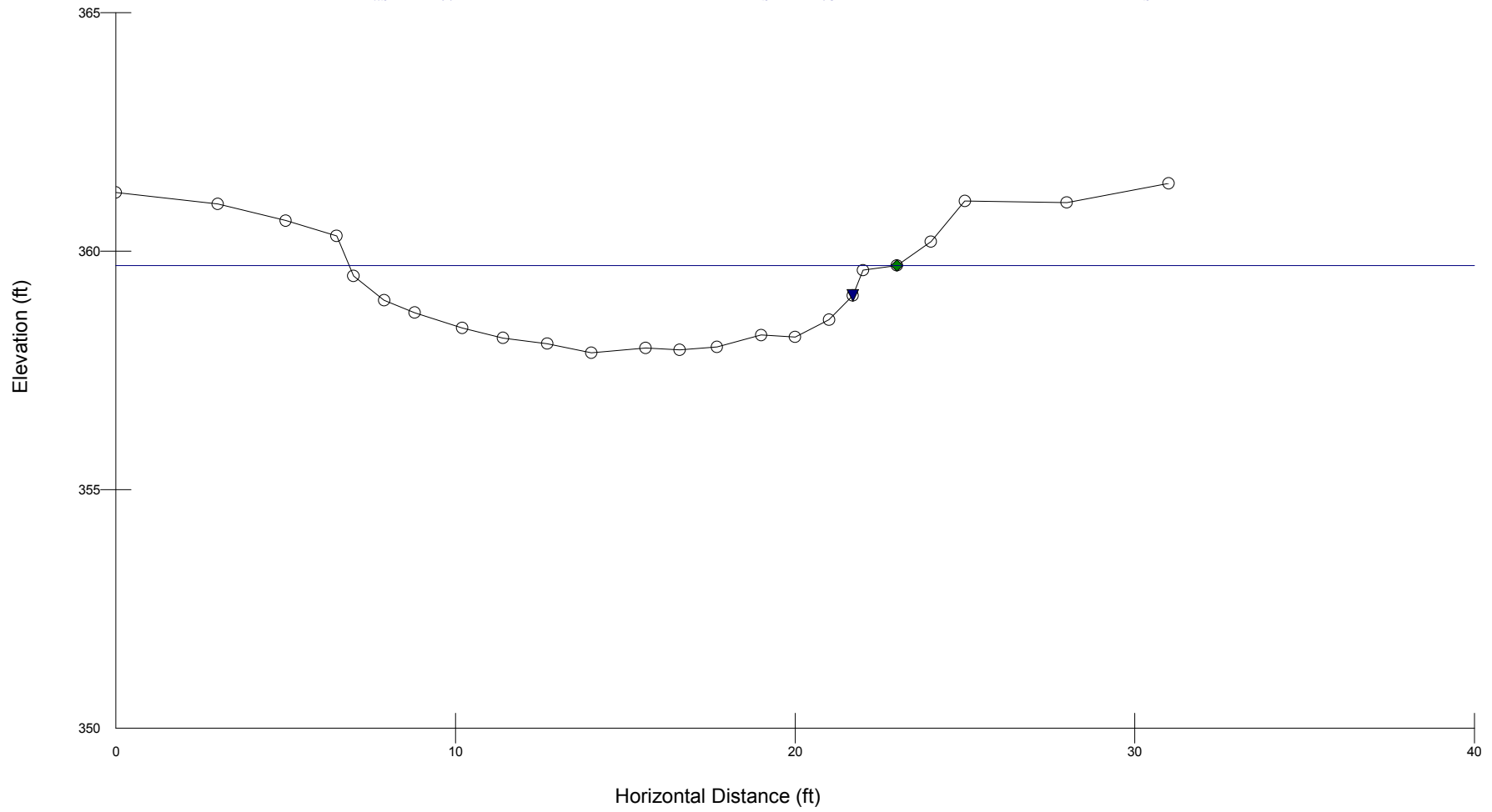
◆ Bankfull Indicators

▼ Water Surface Points

Wbkf = 16.1

Dbkf = 1.3

Abkf = 21



XS 2-3 (Riffle)

○ Ground Points

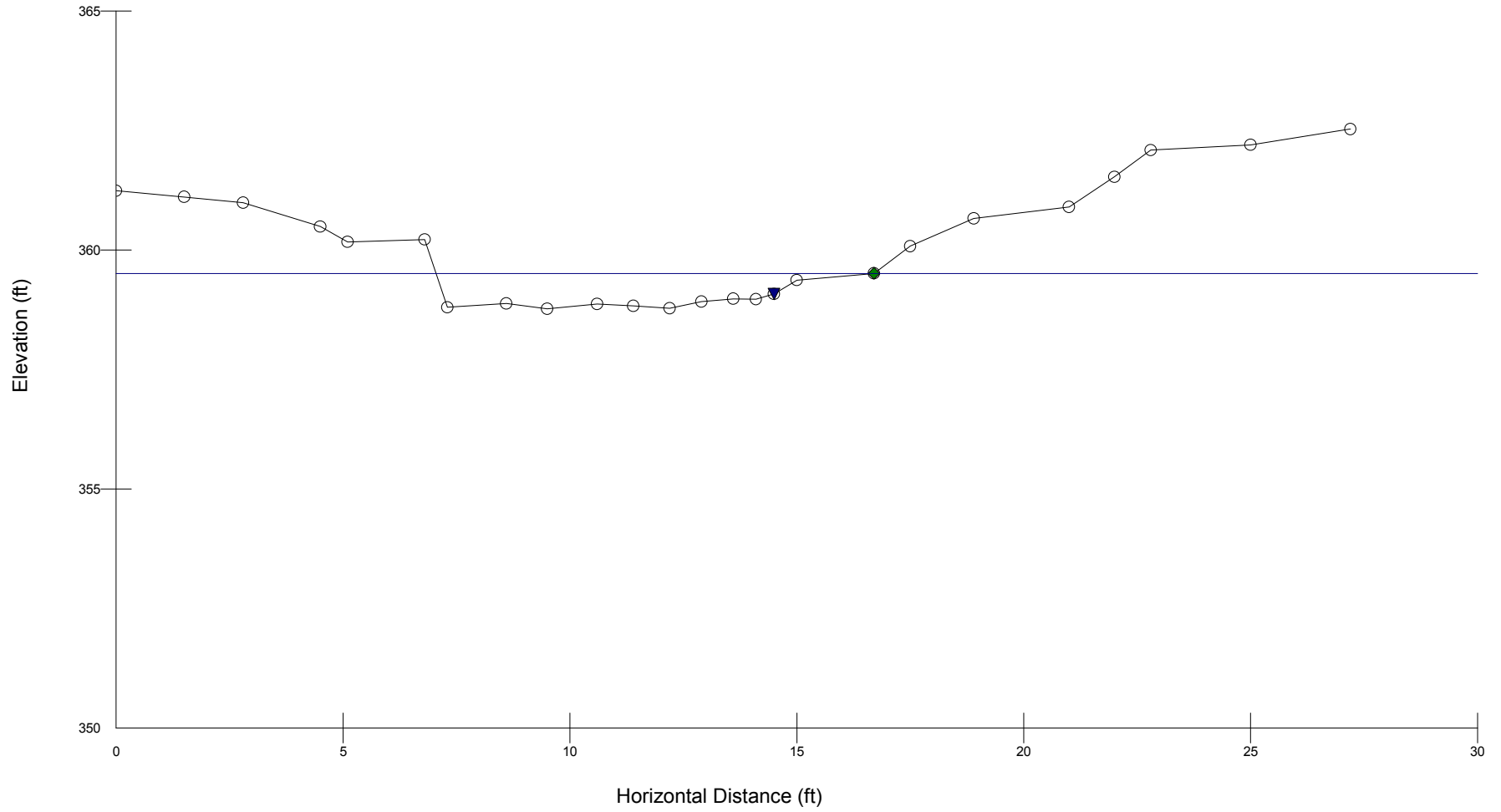
◆ Bankfull Indicators

▼ Water Surface Points

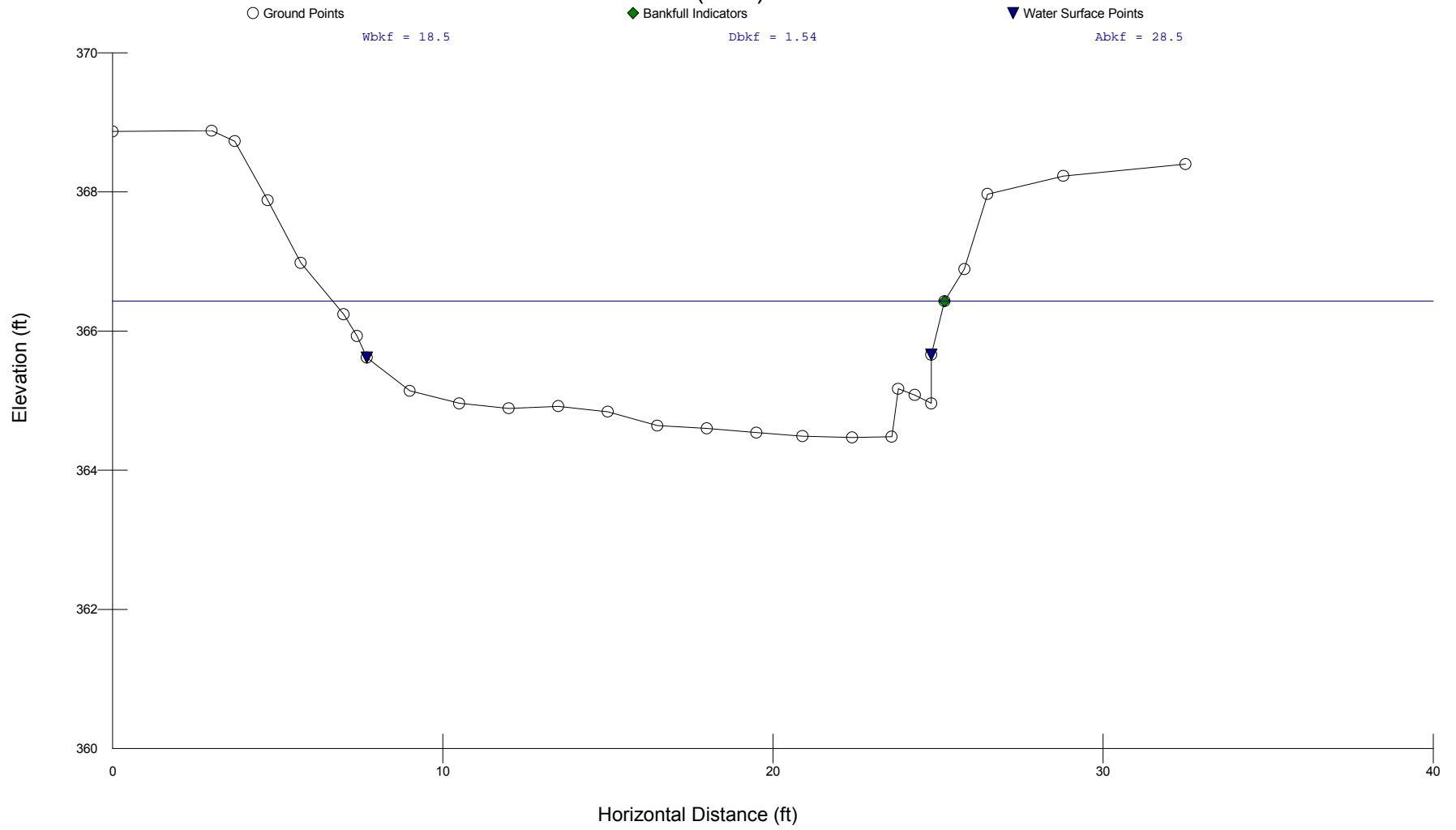
Wbkf = 9.65

Dbkf = .52

Abkf = 5



XS 3-1 (Pool)



XS 3-2 (Riffle)

○ Ground Points

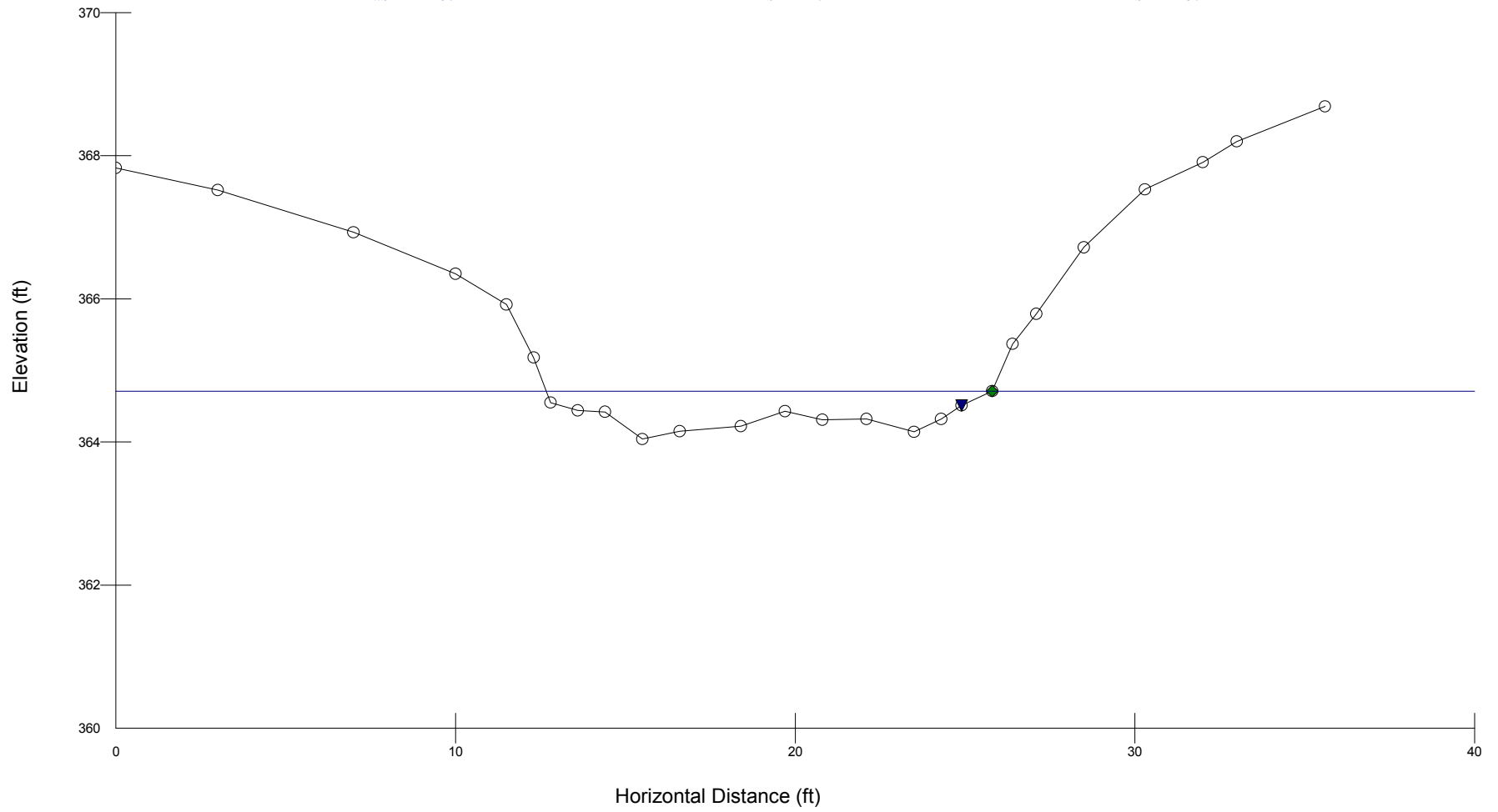
Wbkf = 13.1

◆ Bankfull Indicators

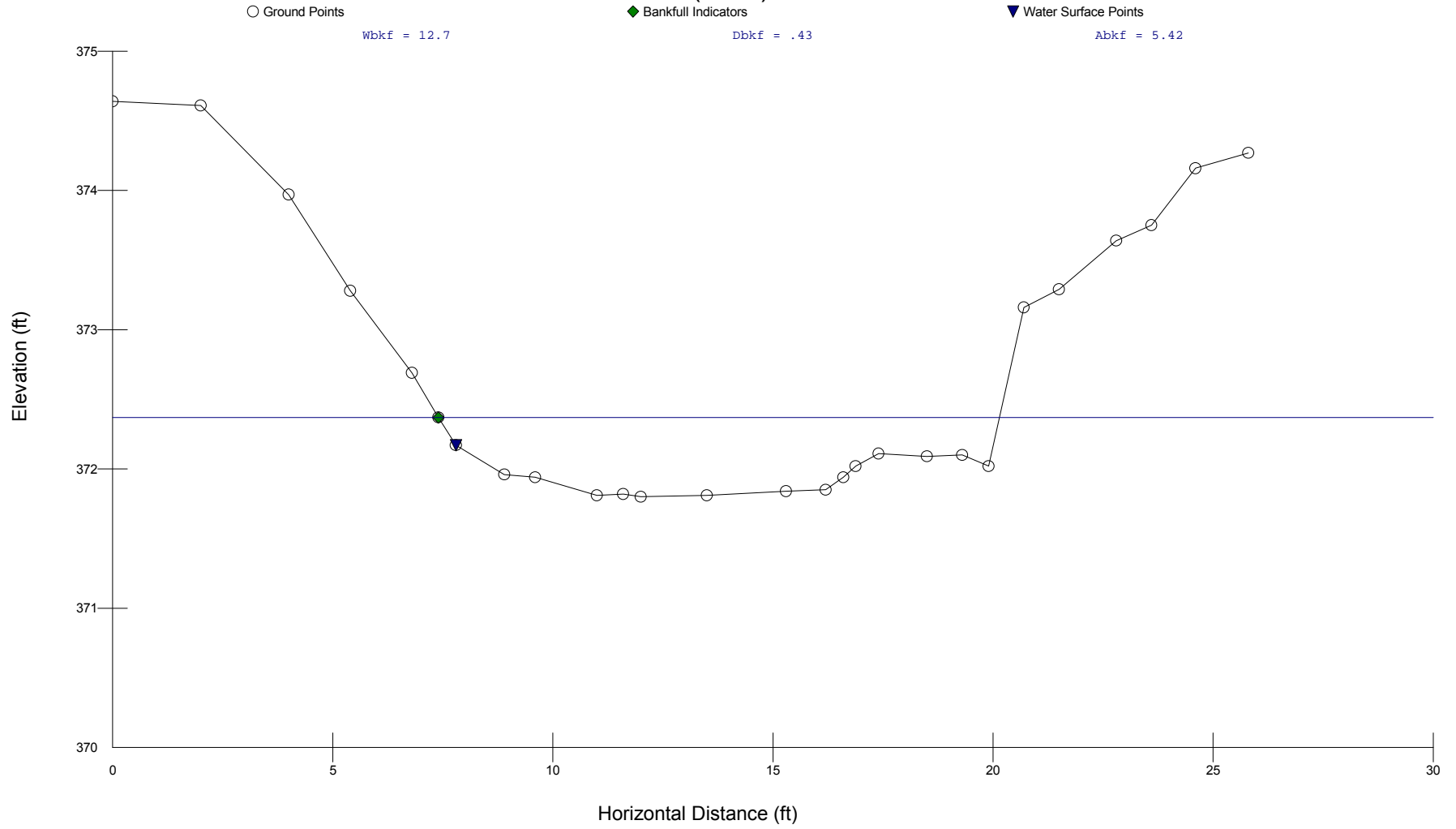
Dbkf = .4

▼ Water Surface Points

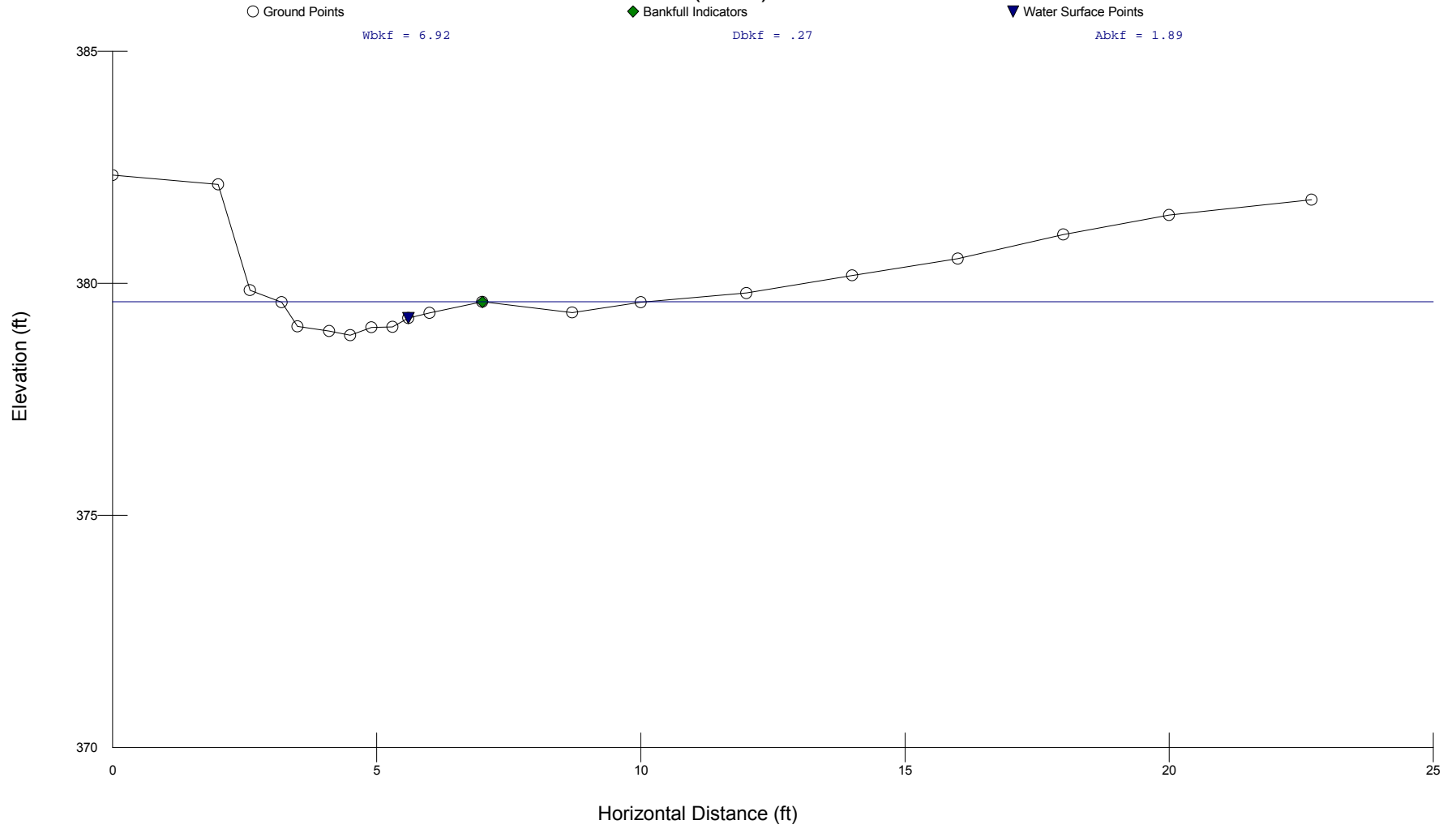
Abkf = 5.27



XS 3-3 (Riffle)



XS 4-1 (Riffle)



XS 6-1 (Riffle)

○ Ground Points

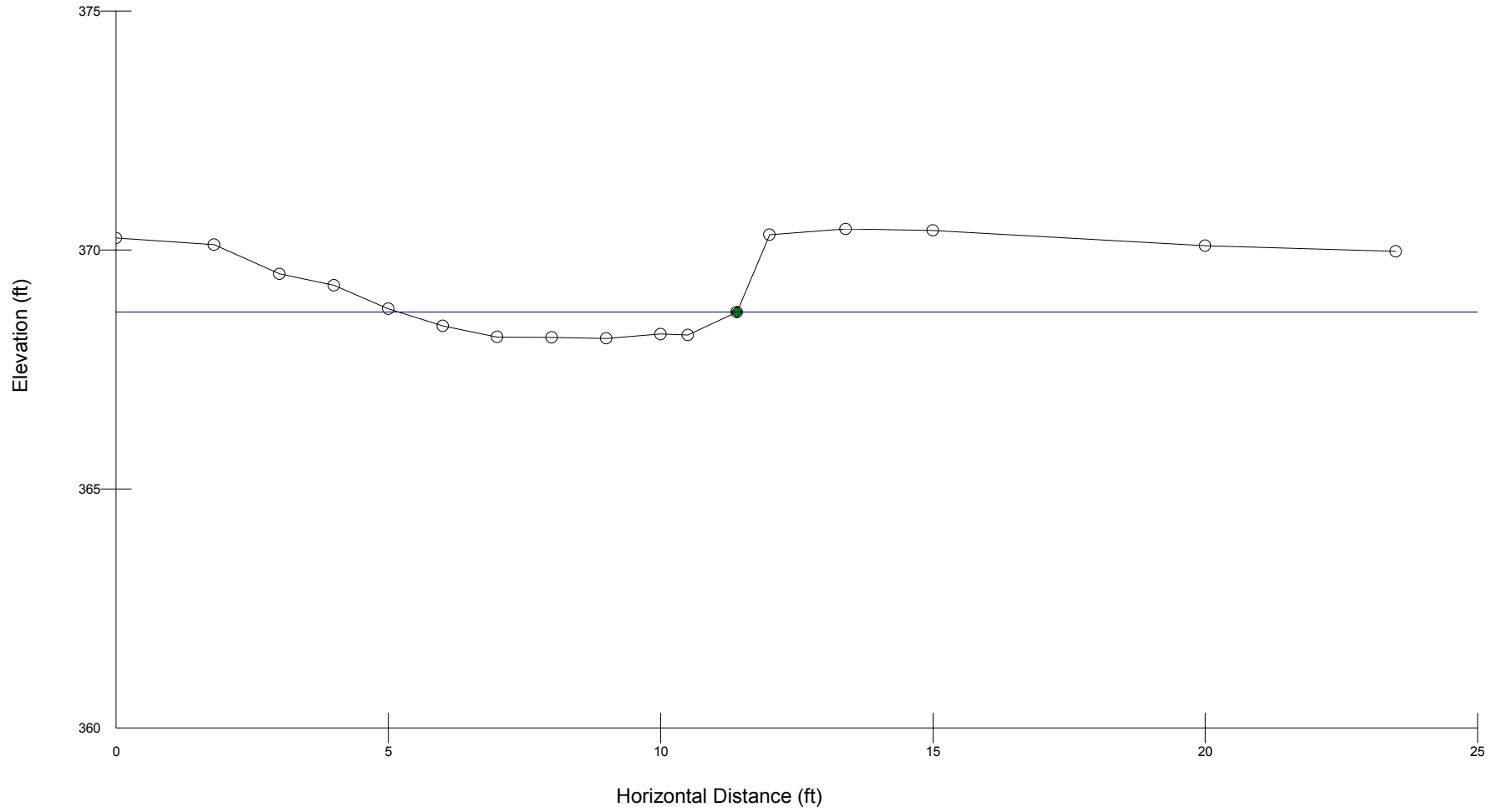
◆ Bankfull Indicators

▼ Water Surface Points

Wbkf = 6.21

Dbkf = .41

Abkf = 2.54



XS 7-1 (Riffle)

○ Ground Points

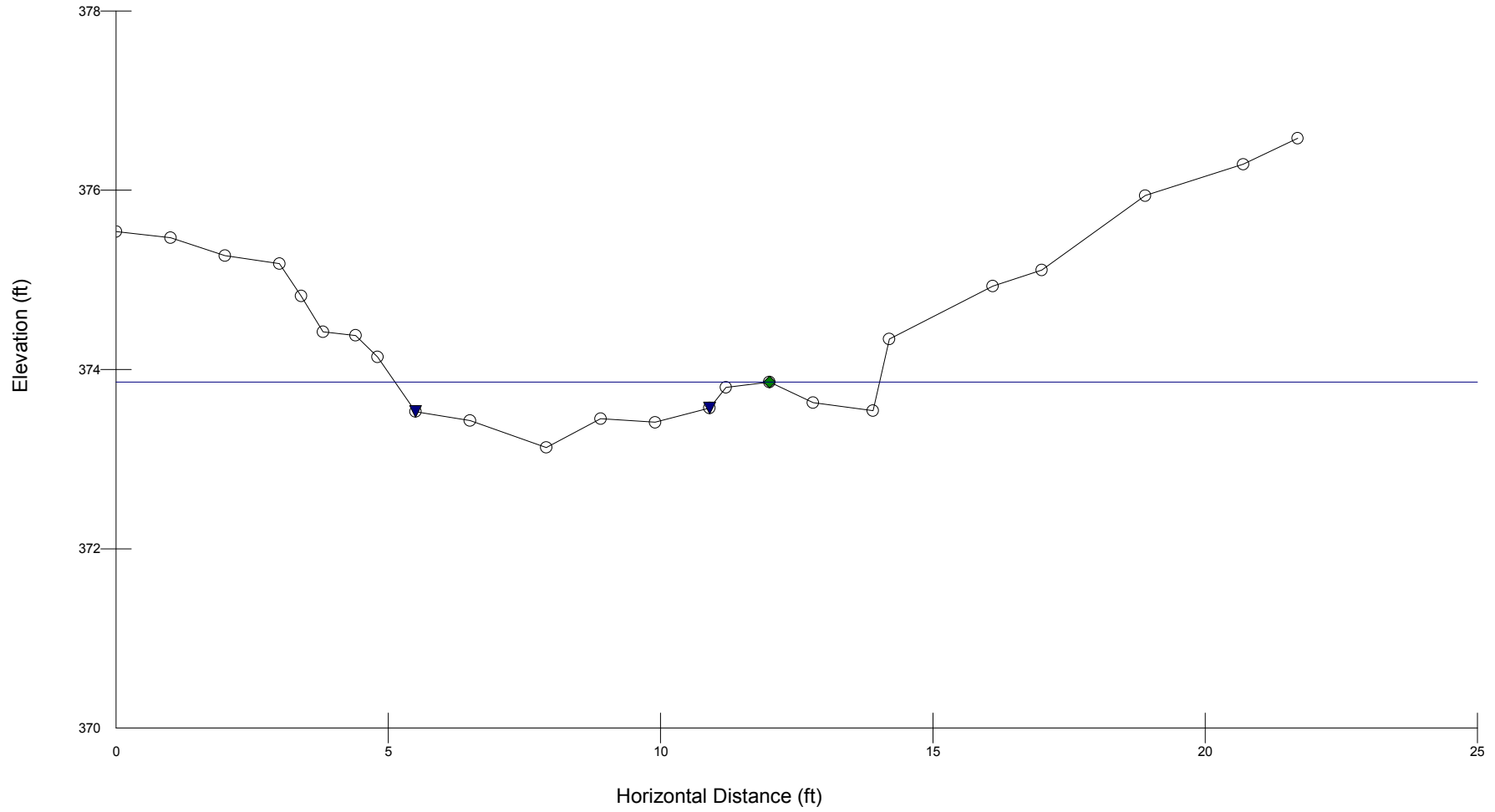
◆ Bankfull Indicators

▼ Water Surface Points

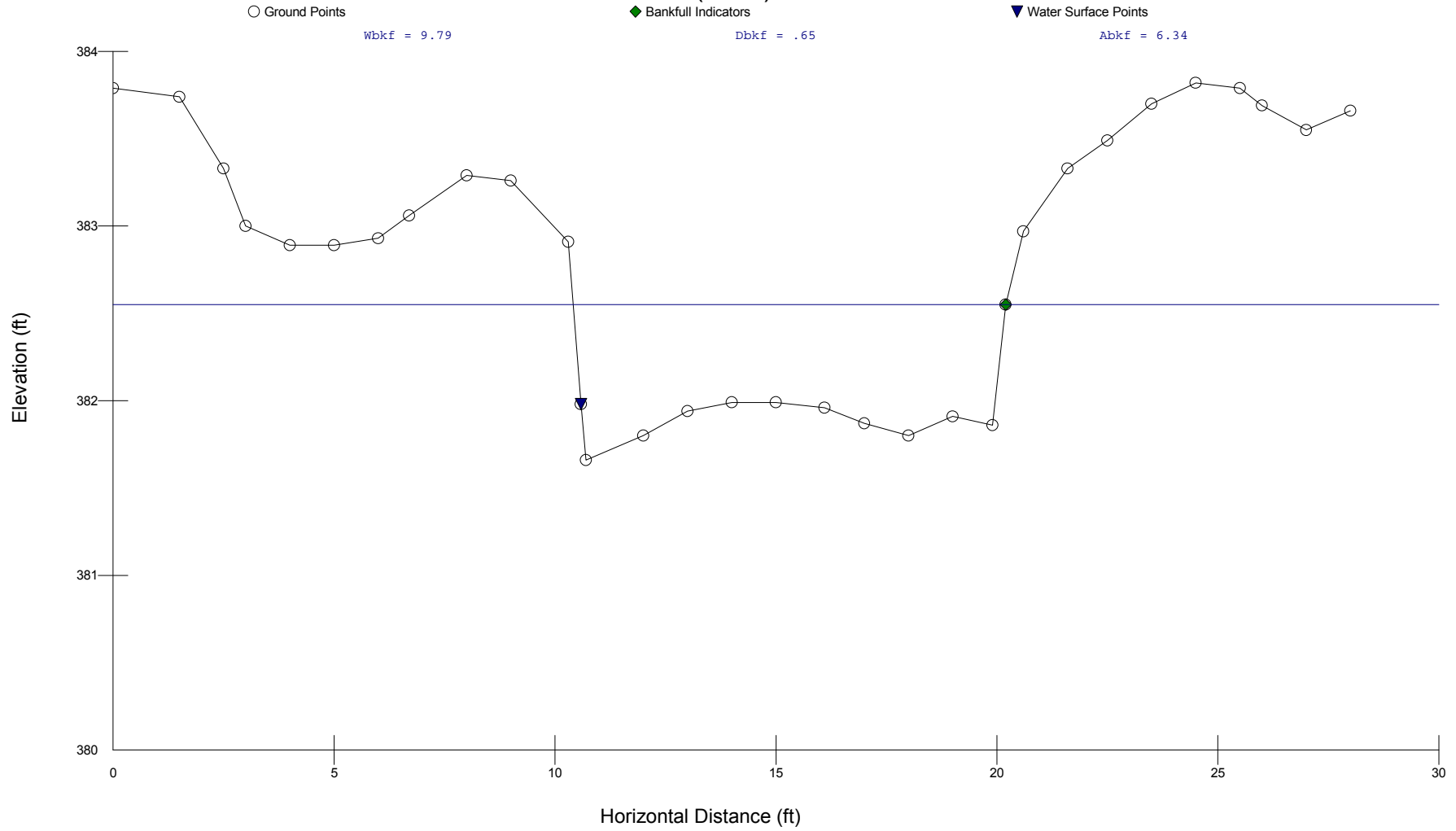
wbkf = 8.9

Dbkf = .35

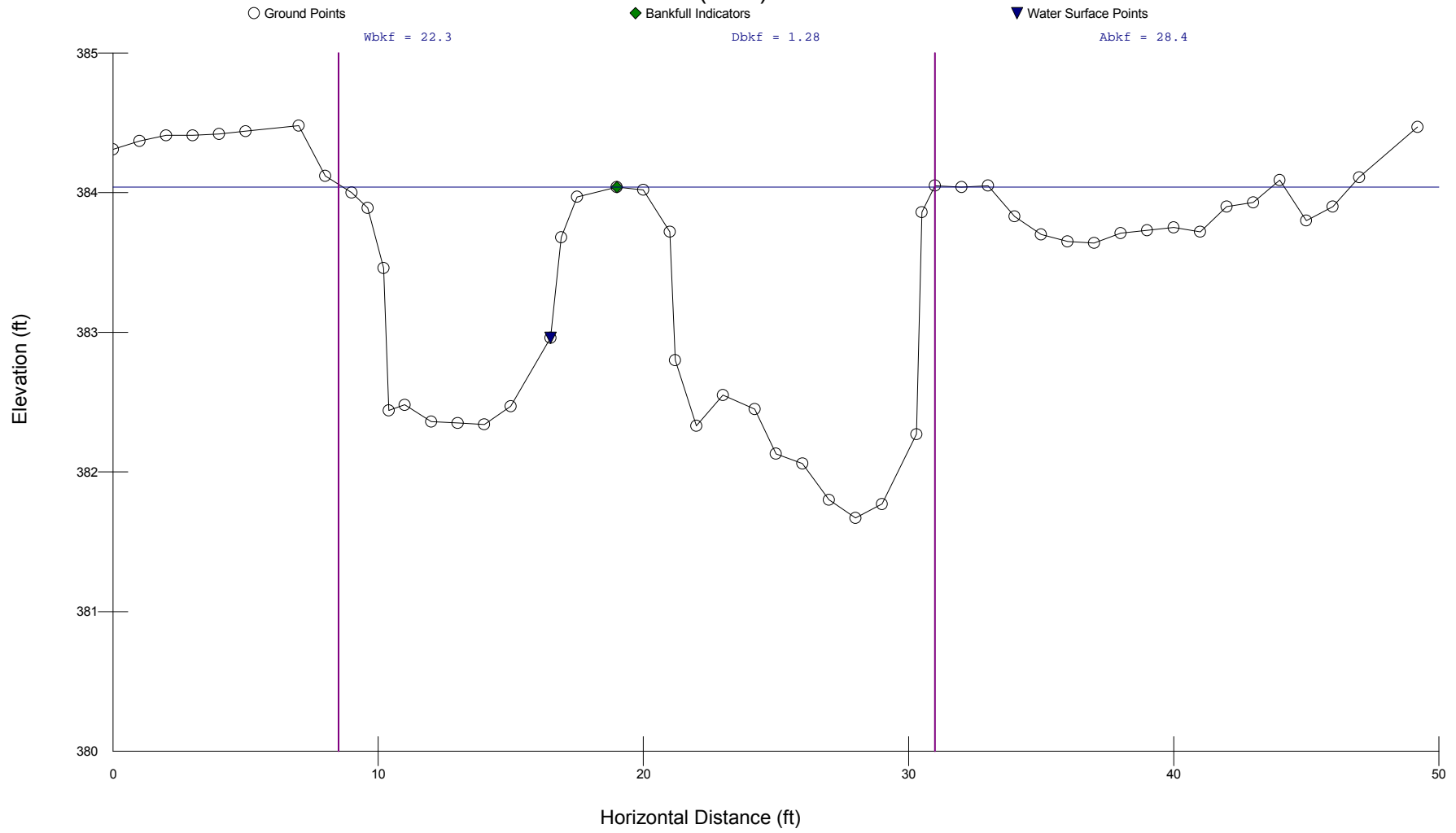
Abkf = 3.11



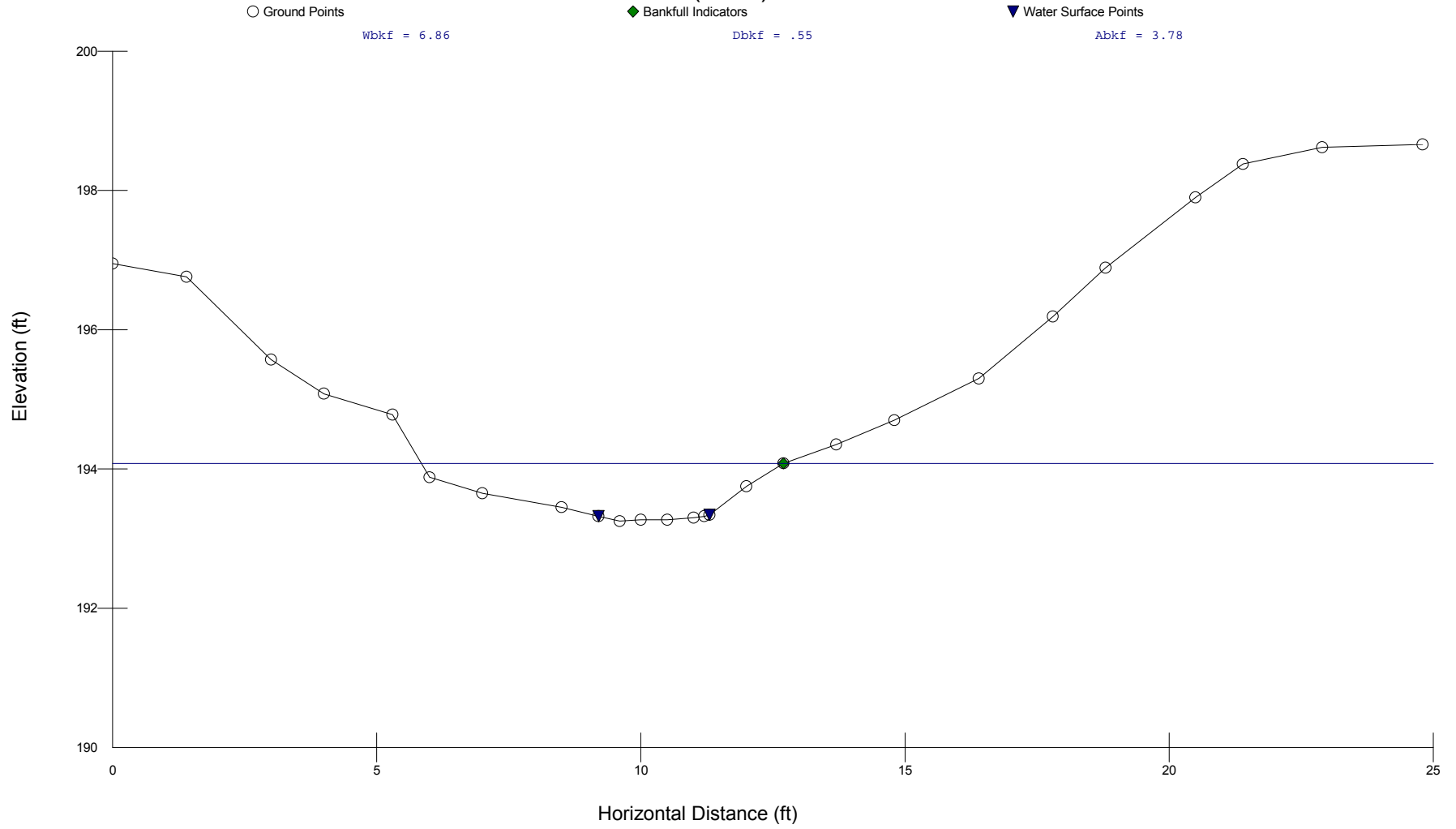
XS 7-2 (Riffle)



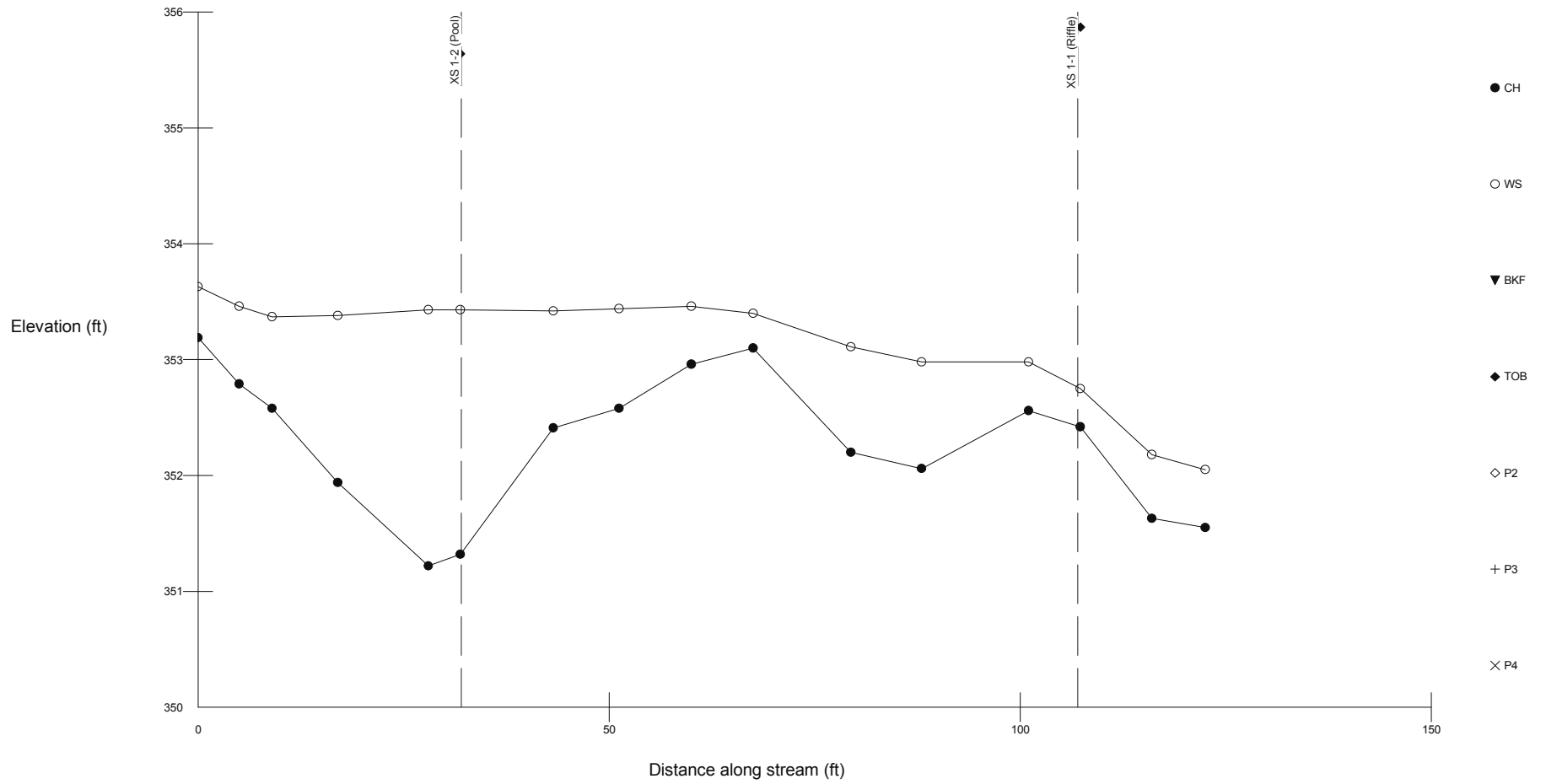
XS 7-3 (Pool)



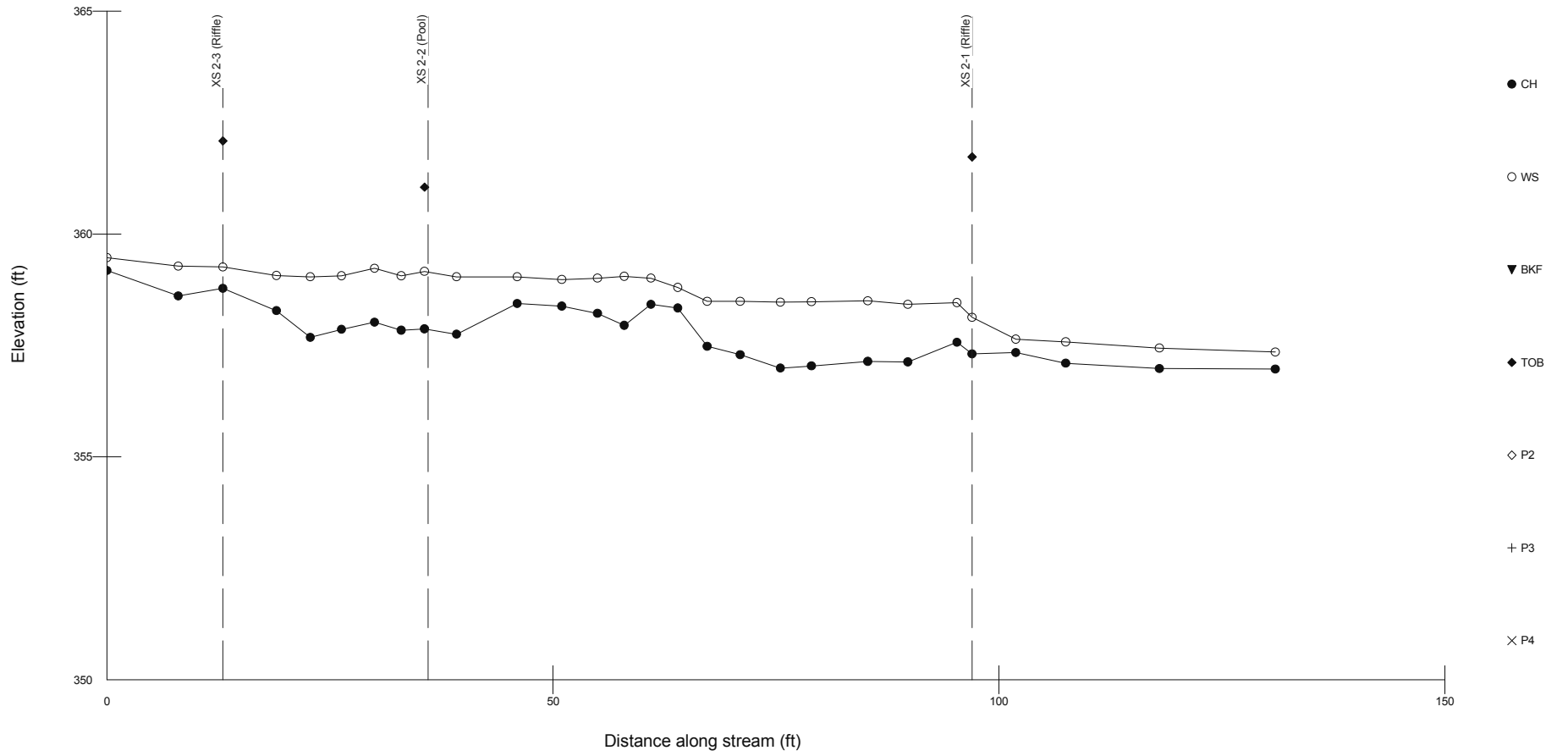
XS 8-1 (Riffle)



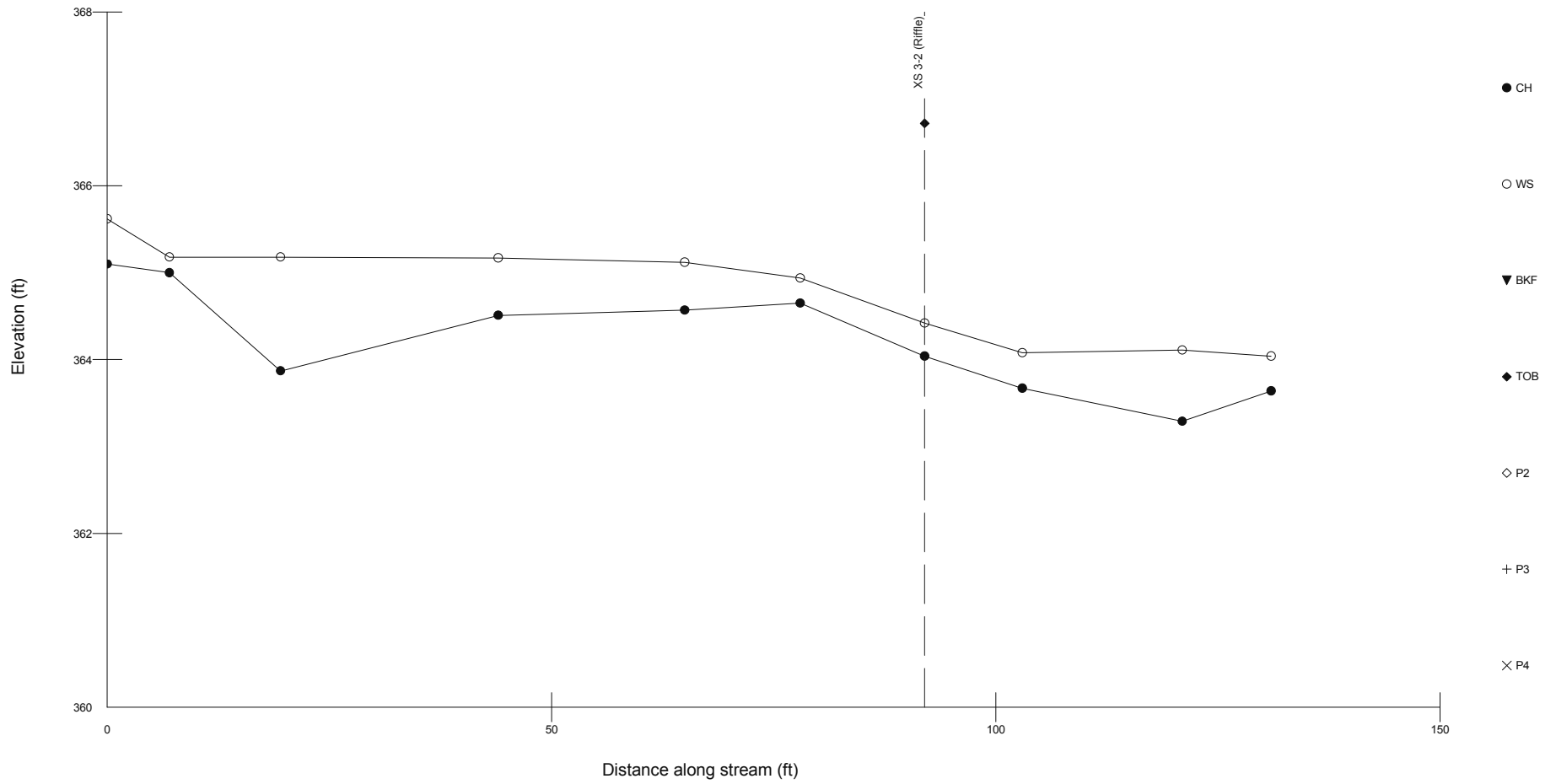
Long Profile 1



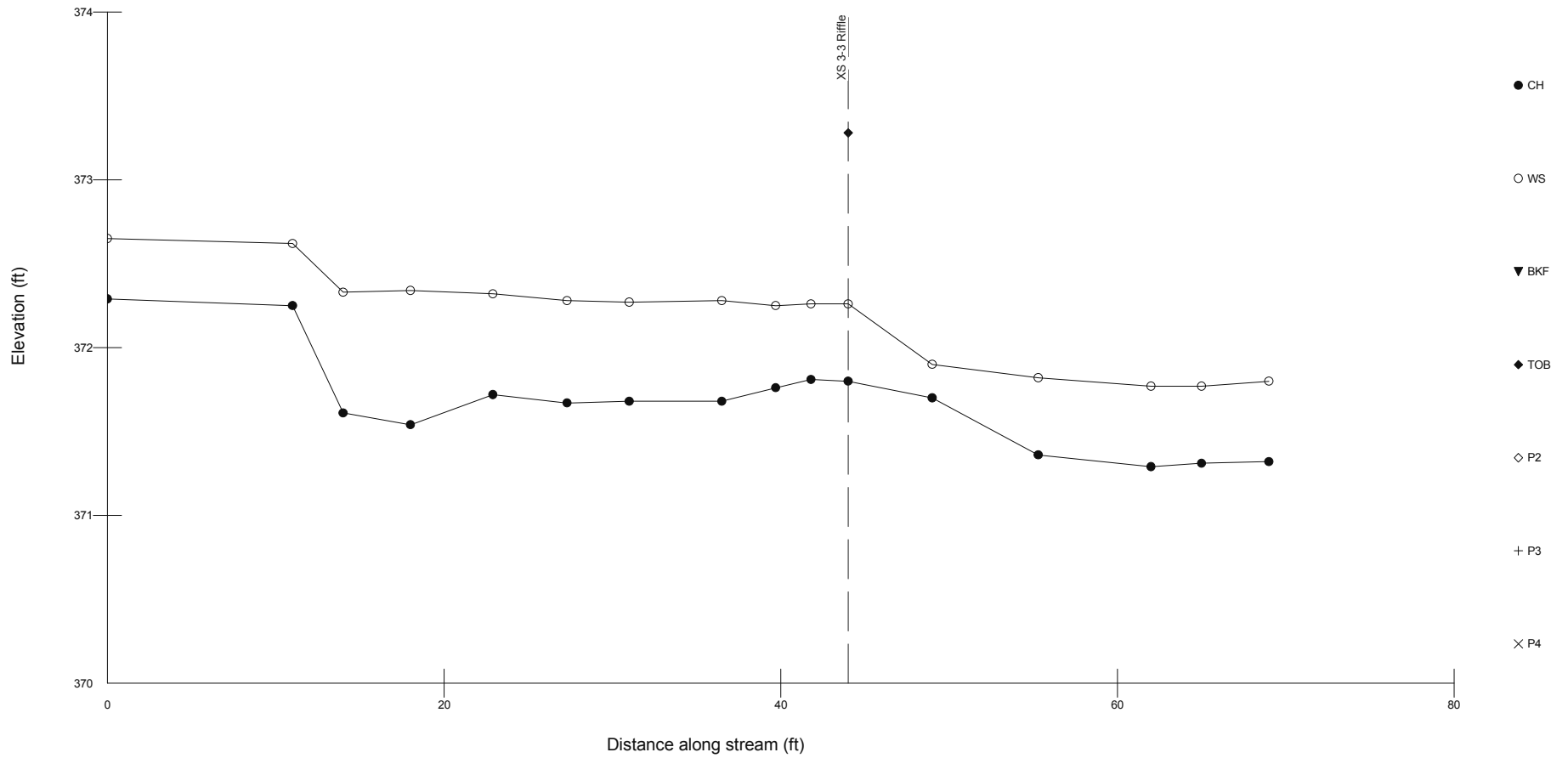
Long Profile 2



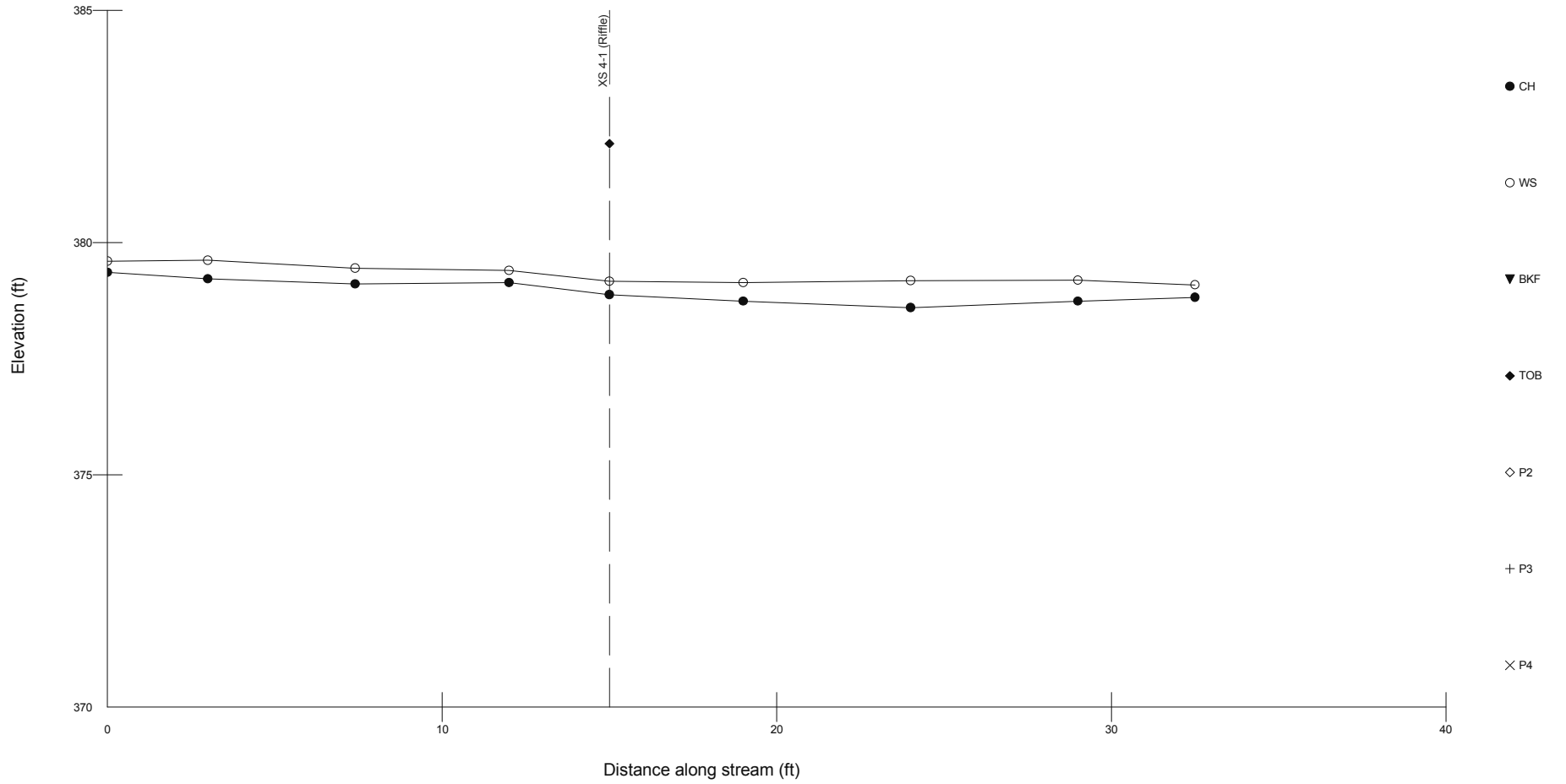
Long Profile 3-2



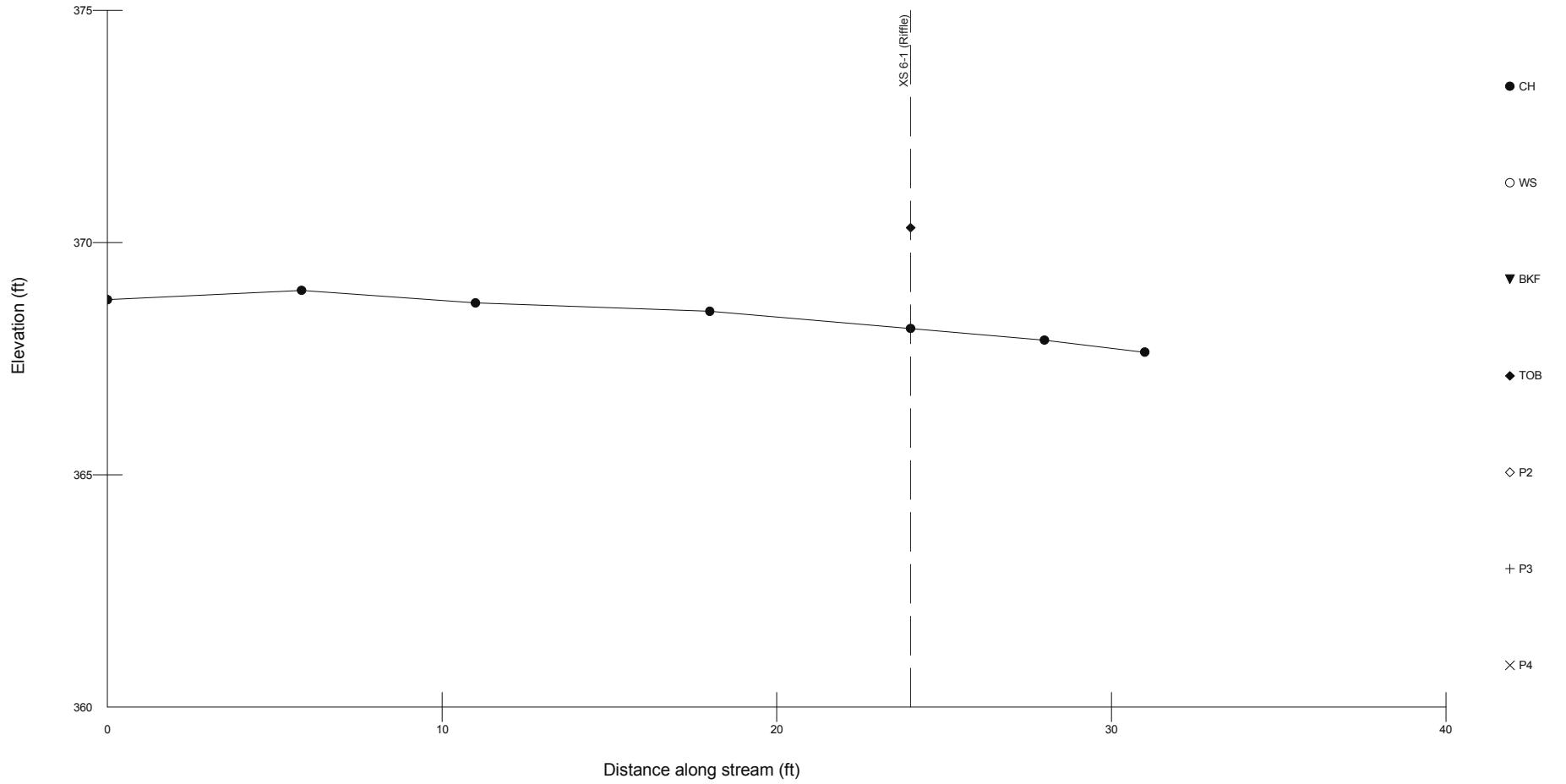
Long Profile 3-3



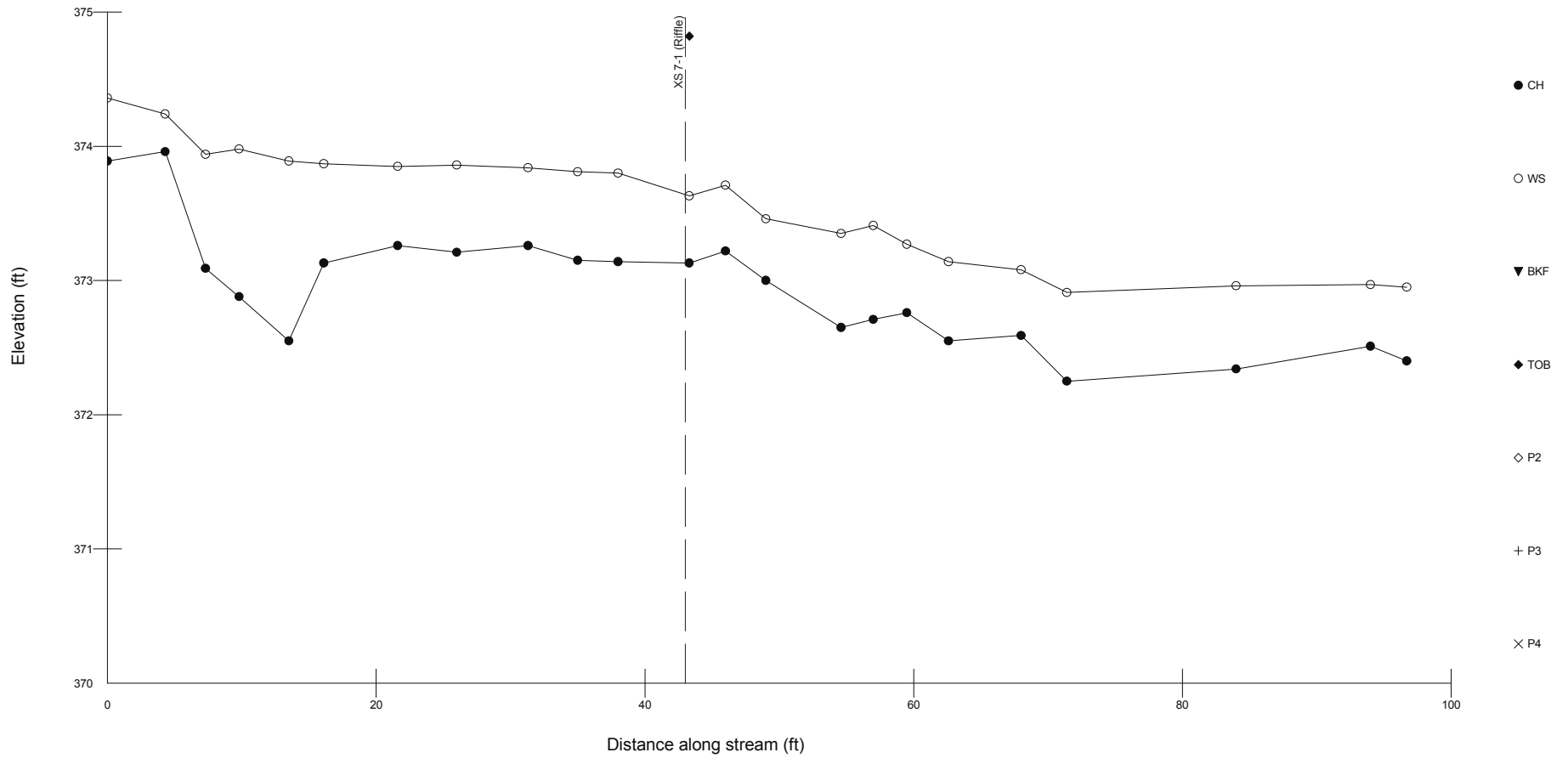
Long Profile 4



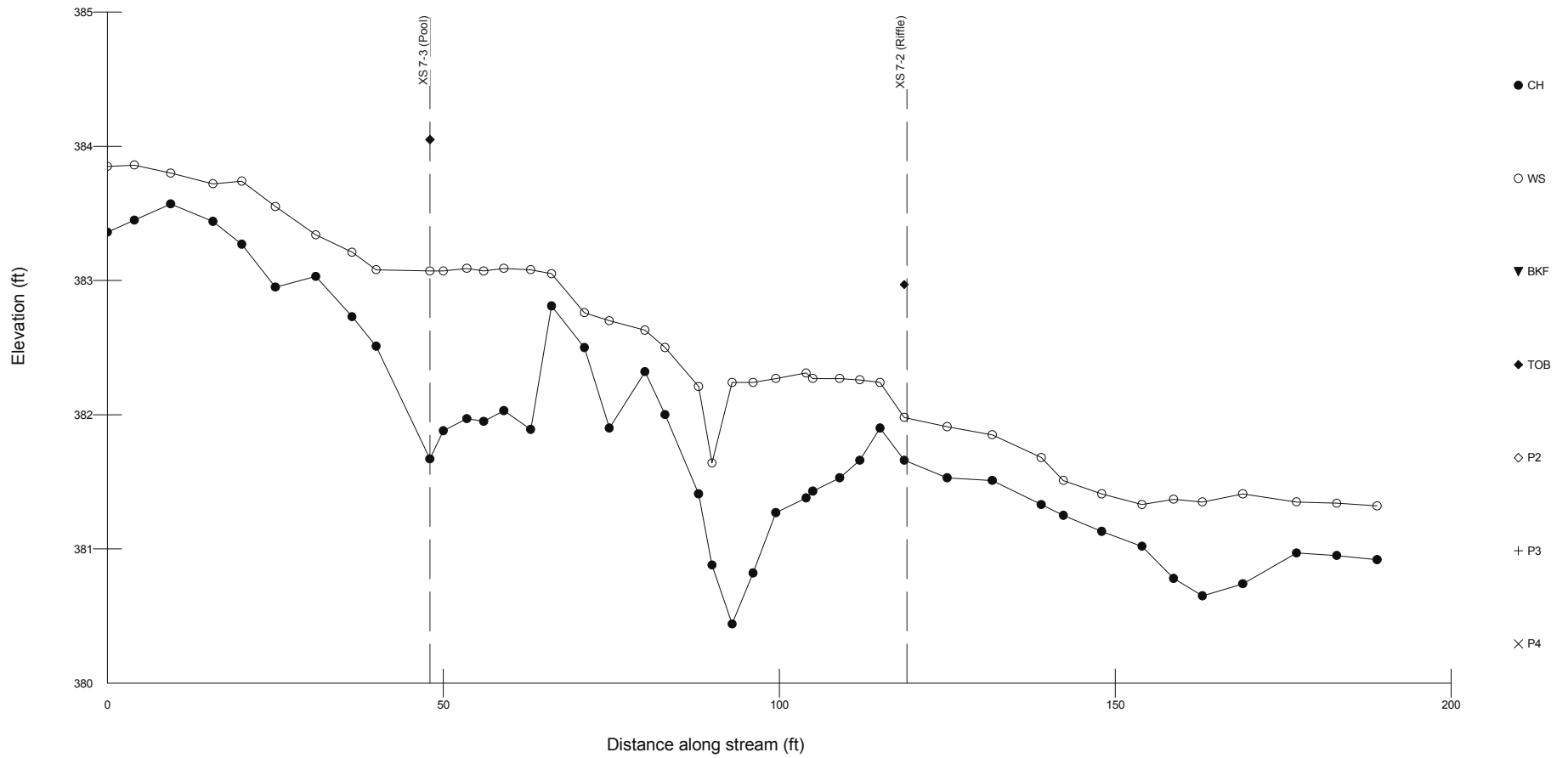
Long Profile 6



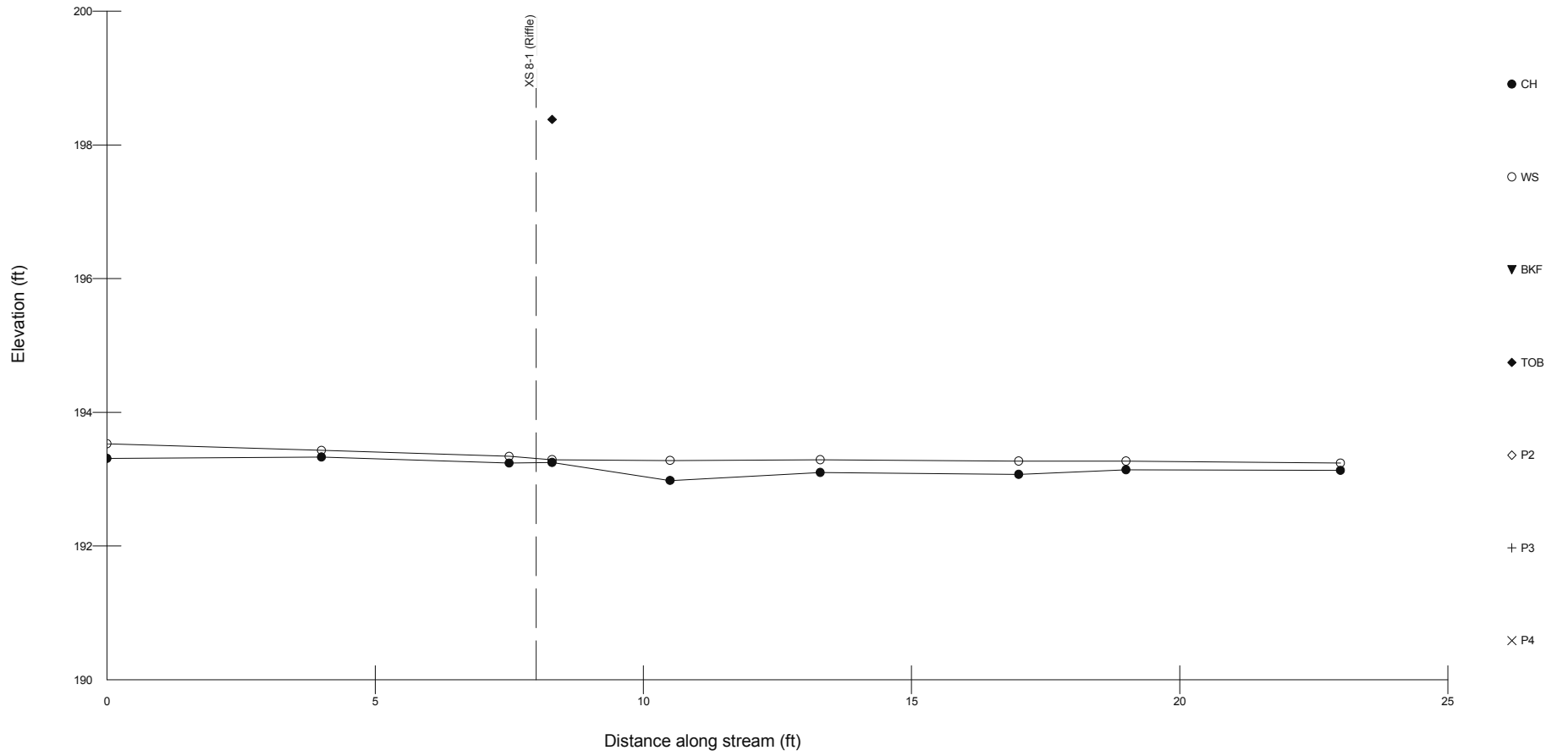
Long Profile 7-1



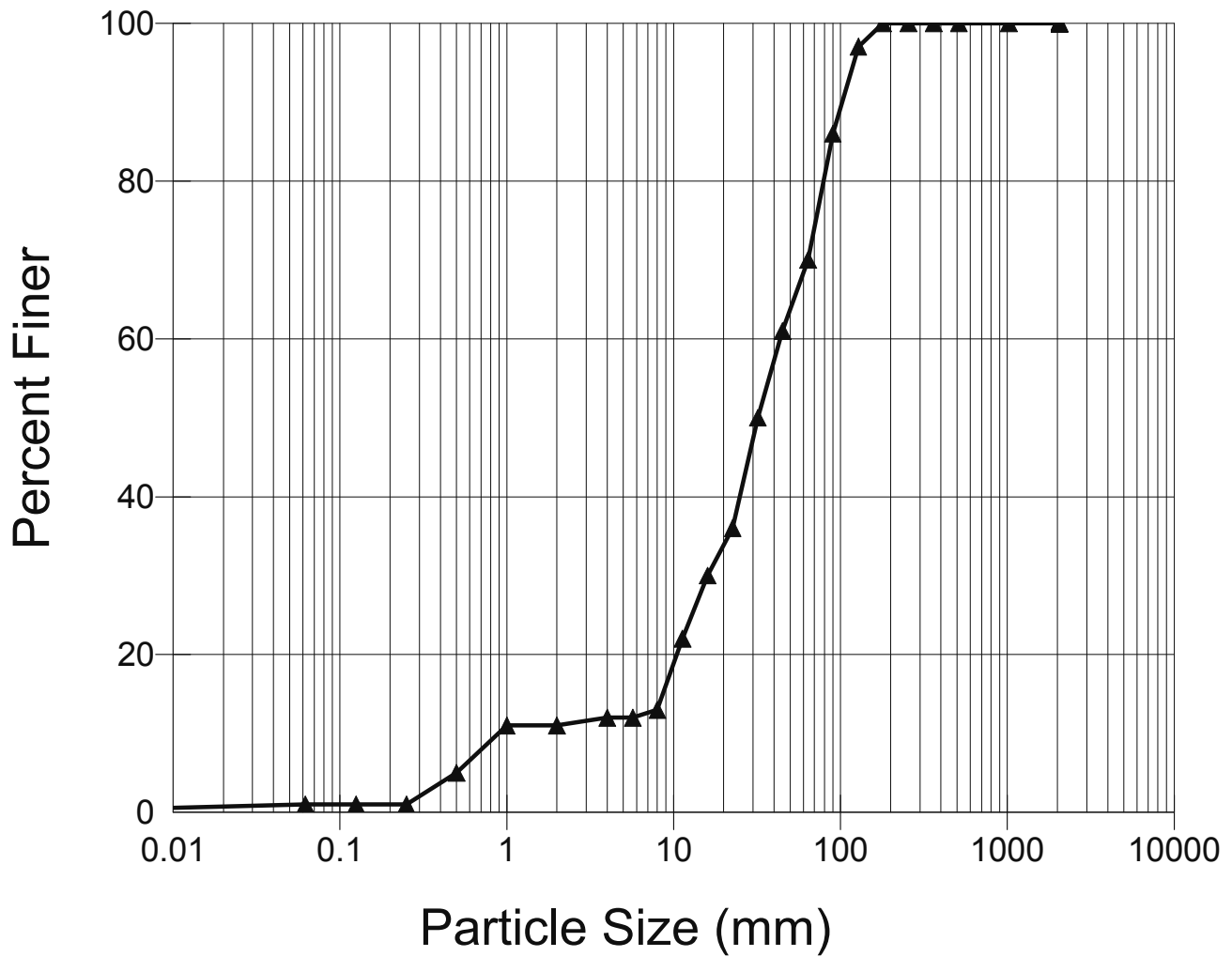
Long Profile 7-2



Long Profile 8



XS 1-1 (Riffle)

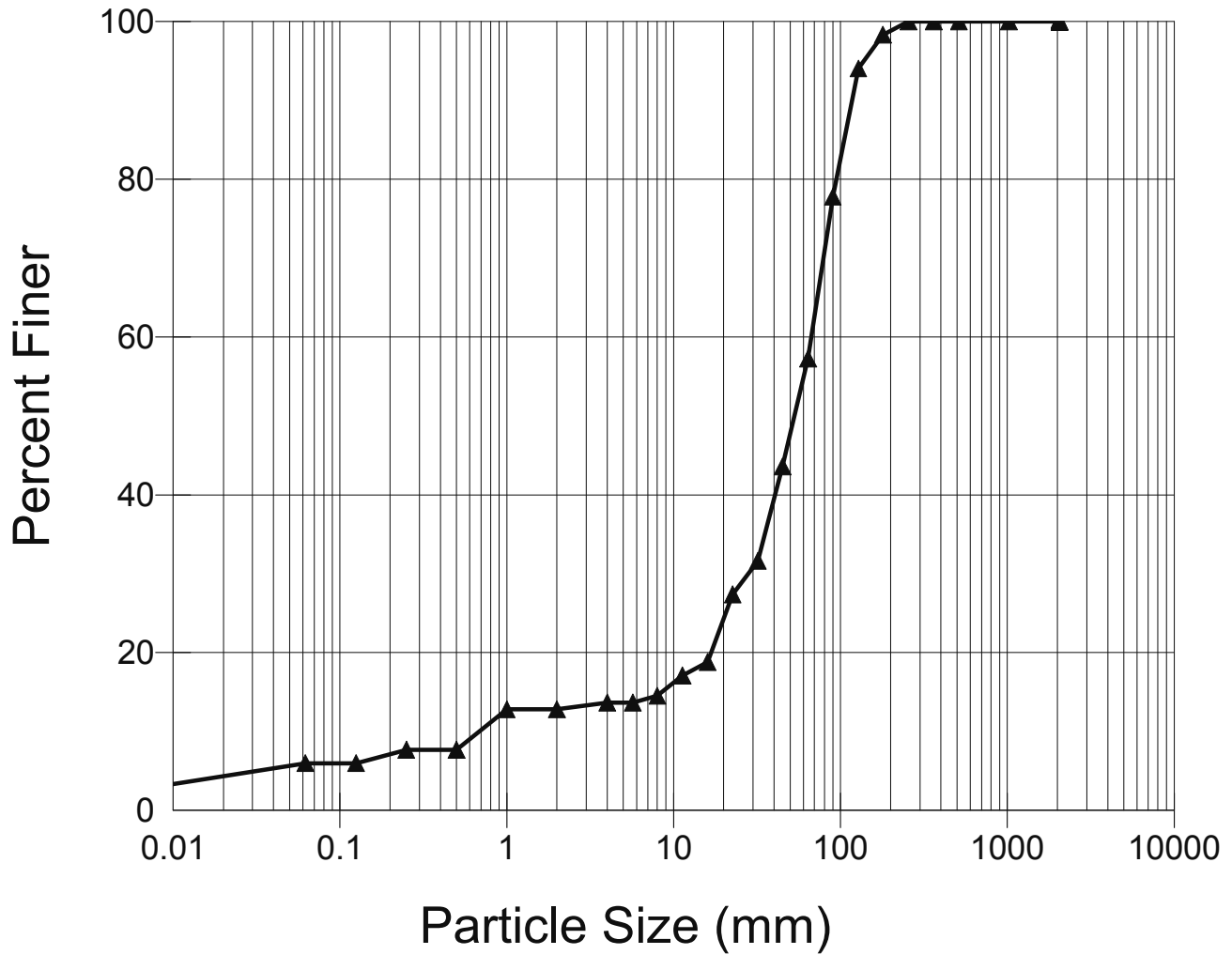


Particle Size Analysis

| | |
|---------------|--------|
| D16 (mm) | 9.1 |
| D35 (mm) | 21.5 |
| D50 (mm) | 32 |
| D84 (mm) | 86.75 |
| D95 (mm) | 121.09 |
| D100 (mm) | 180 |
| Silt/Clay (%) | 1 |
| Sand (%) | 10 |
| Gravel (%) | 59 |
| Cobble (%) | 30 |
| Boulder (%) | 0 |
| Bedrock (%) | 0 |

Total Particles = 100

XS 3-2 (Riffle)

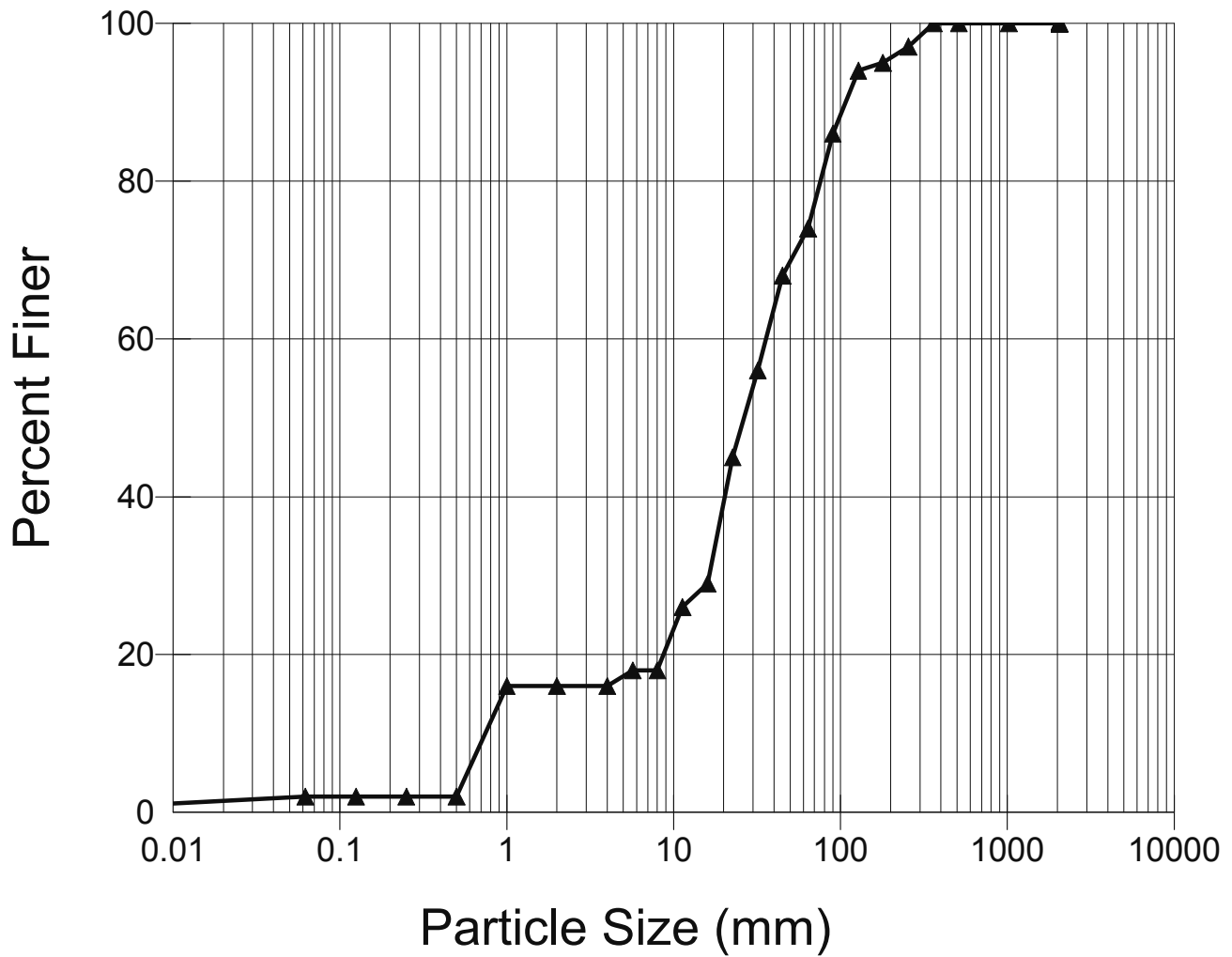


Particle Size Analysis

| | |
|---------------|--------|
| D16 (mm) | 9.89 |
| D35 (mm) | 35.67 |
| D50 (mm) | 53.91 |
| D84 (mm) | 104.55 |
| D95 (mm) | 139.93 |
| D100 (mm) | 256 |
| Silt/Clay (%) | 5.98 |
| Sand (%) | 6.84 |
| Gravel (%) | 44.44 |
| Cobble (%) | 42.74 |
| Boulder (%) | 0 |
| Bedrock (%) | 0 |

Total Particles = 117

XS 3-3 (Riffle)

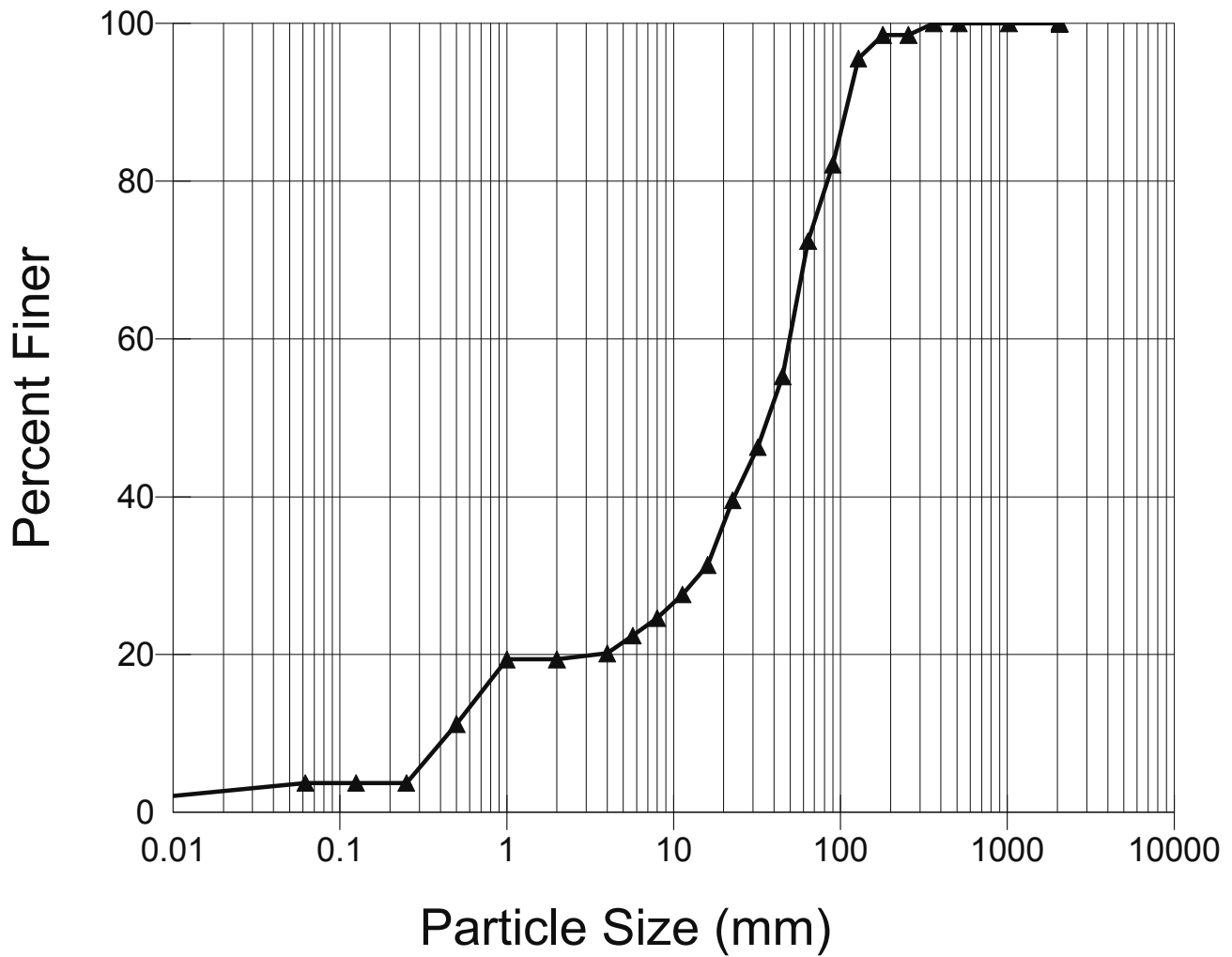


Particle Size Analysis

| | |
|---------------|-------|
| D16 (mm) | 1 |
| D35 (mm) | 18.48 |
| D50 (mm) | 26.87 |
| D84 (mm) | 85.67 |
| D95 (mm) | 180 |
| D100 (mm) | 362 |
| Silt/Clay (%) | 2 |
| Sand (%) | 14 |
| Gravel (%) | 58 |
| Cobble (%) | 23 |
| Boulder (%) | 3 |
| Bedrock (%) | 0 |

Total Particles = 100

XS 4-1 (Riffle)

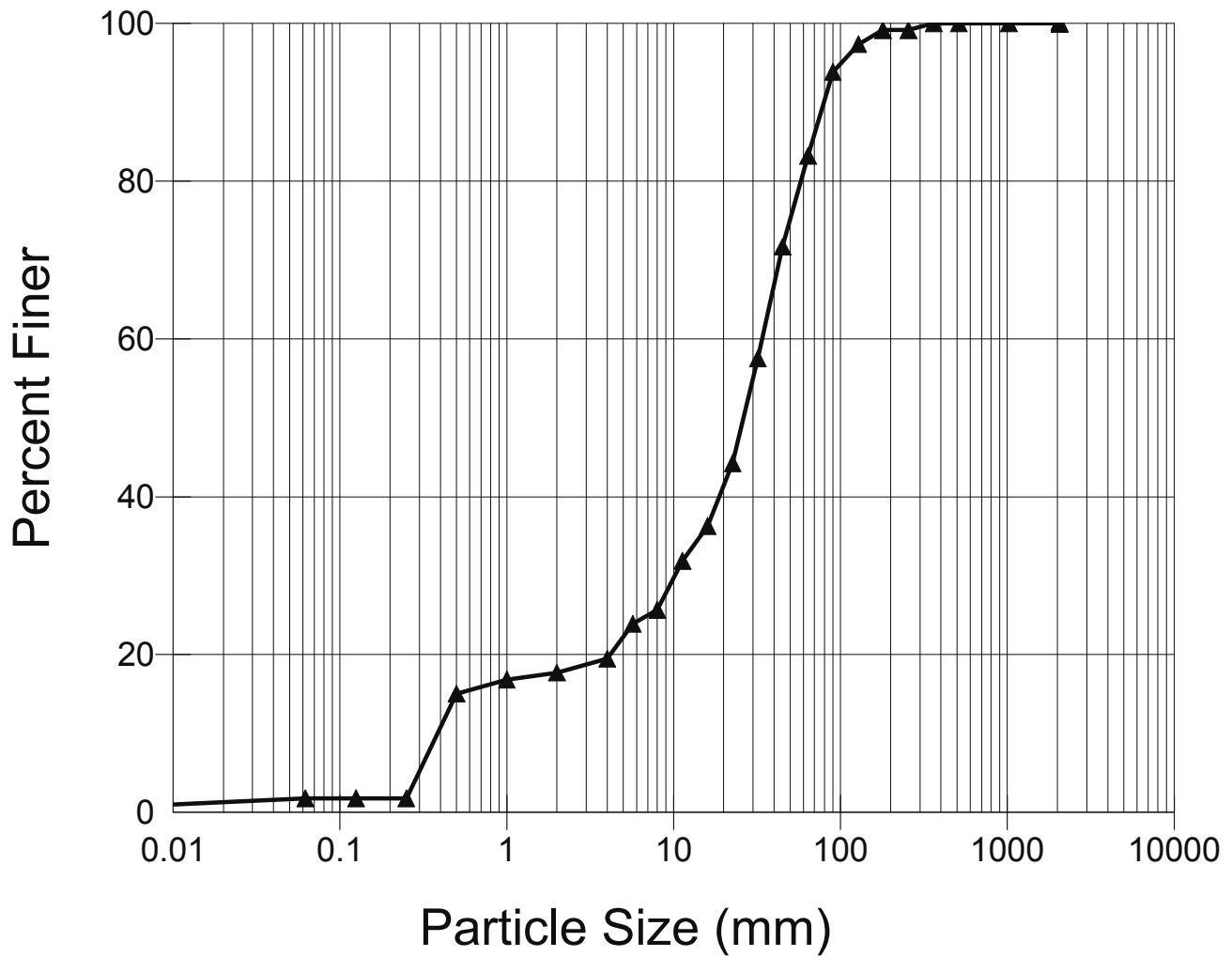


Particle Size Analysis

| | |
|---------------|--------|
| D16 (mm) | 0.79 |
| D35 (mm) | 18.94 |
| D50 (mm) | 37.42 |
| D84 (mm) | 95.4 |
| D95 (mm) | 126.53 |
| D100 (mm) | 361.99 |
| Silt/Clay (%) | 3.73 |
| Sand (%) | 15.67 |
| Gravel (%) | 52.99 |
| Cobble (%) | 26.12 |
| Boulder (%) | 1.49 |
| Bedrock (%) | 0 |

Total Particles = 134

XS 6-1 (Riffle)

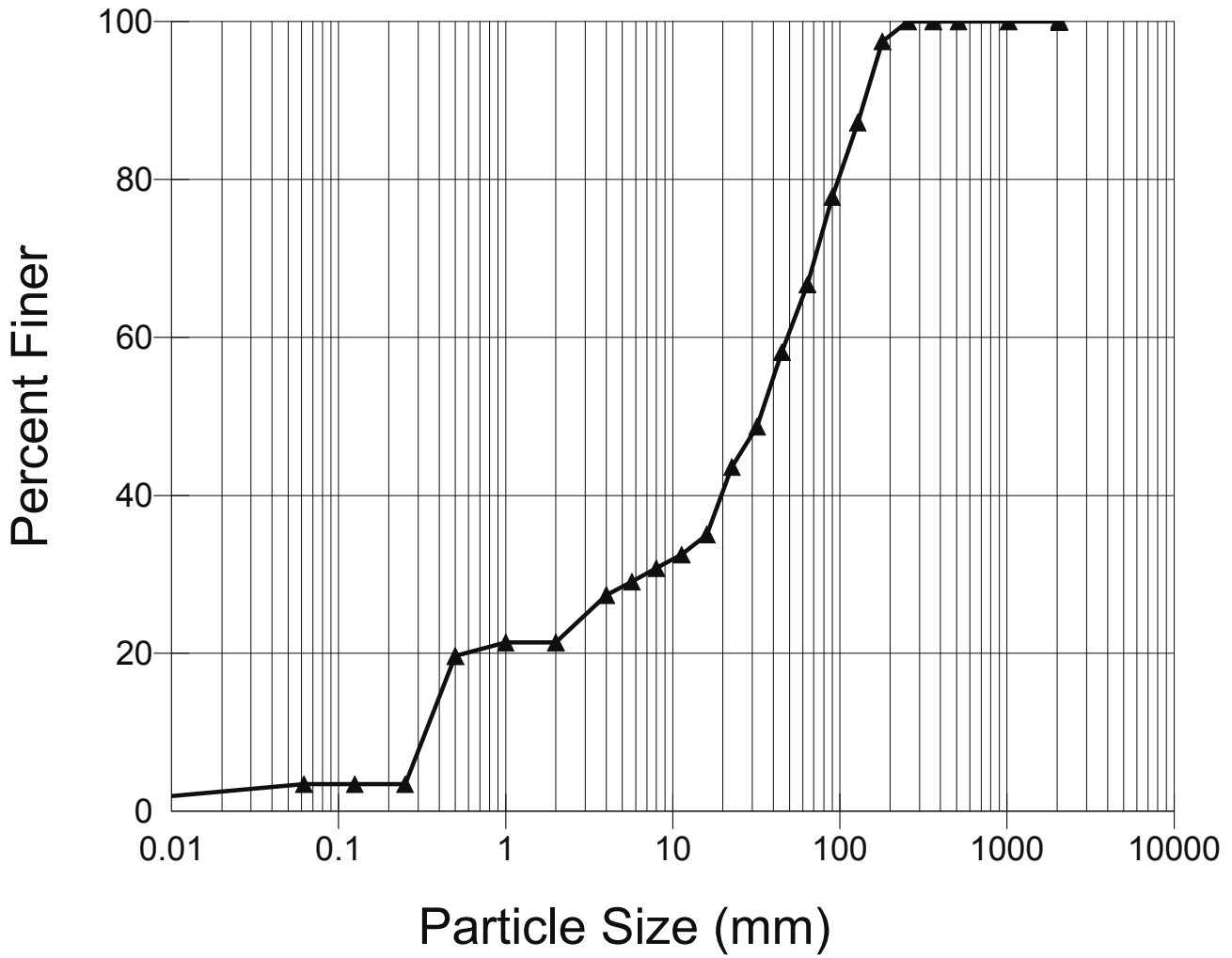


Particle Size Analysis

| | |
|---------------|--------|
| D16 (mm) | 0.77 |
| D35 (mm) | 14.64 |
| D50 (mm) | 26.67 |
| D84 (mm) | 65.98 |
| D95 (mm) | 102.77 |
| D100 (mm) | 361.99 |
| Silt/Clay (%) | 1.77 |
| Sand (%) | 15.93 |
| Gravel (%) | 65.49 |
| Cobble (%) | 15.93 |
| Boulder (%) | 0.88 |
| Bedrock (%) | 0 |

Total Particles = 113

XS 7-1 (Riffle)

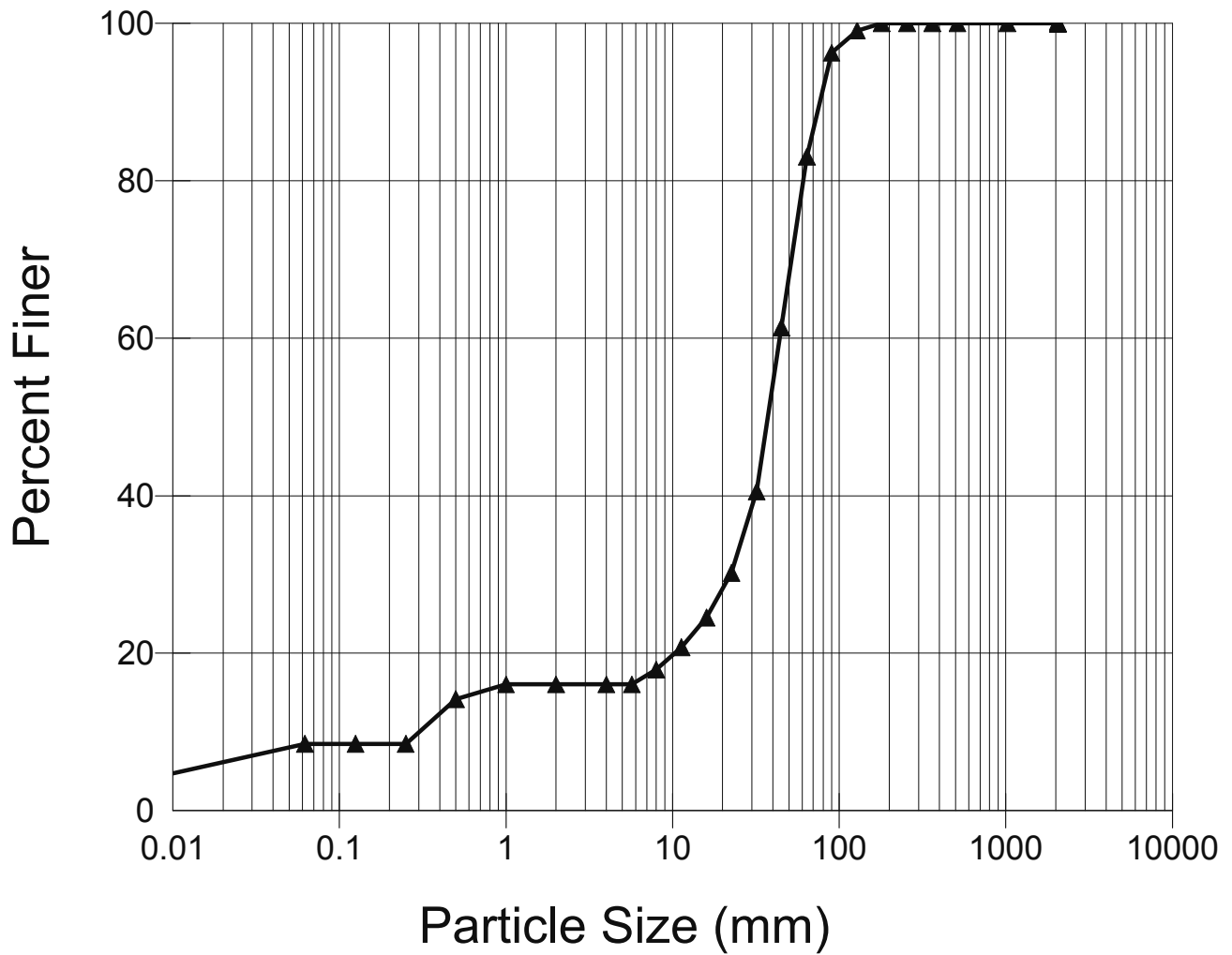


Particle Size Analysis

| | |
|---------------|--------|
| D16 (mm) | 0.44 |
| D35 (mm) | 15.93 |
| D50 (mm) | 33.77 |
| D84 (mm) | 115.14 |
| D95 (mm) | 167.63 |
| D100 (mm) | 256 |
| Silt/Clay (%) | 3.42 |
| Sand (%) | 17.95 |
| Gravel (%) | 45.3 |
| Cobble (%) | 33.33 |
| Boulder (%) | 0 |
| Bedrock (%) | 0 |

Total Particles = 117

XS 7-2 (Riffle)

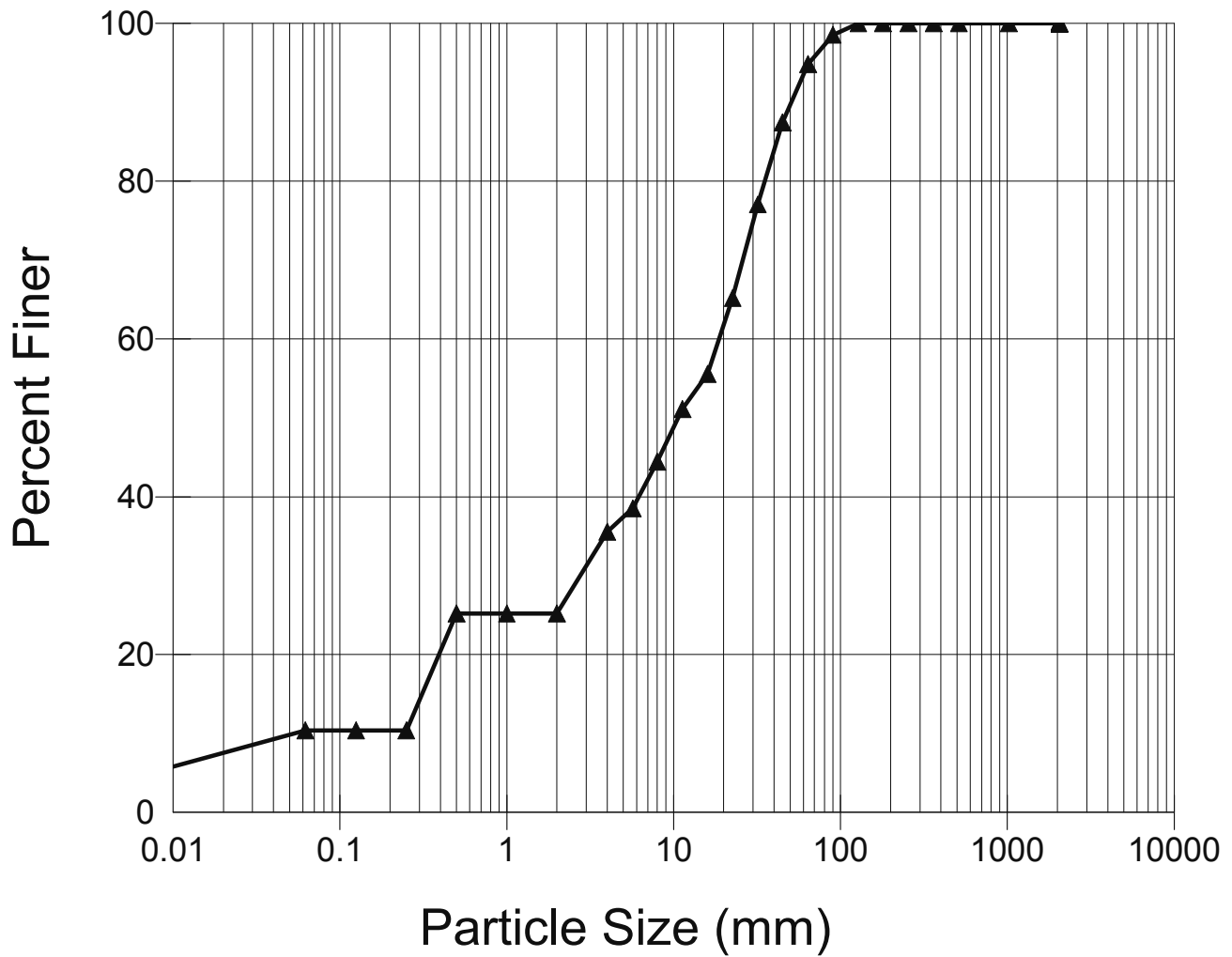


Particle Size Analysis

| | |
|---------------|--------|
| D16 (mm) | 0.99 |
| D35 (mm) | 26.96 |
| D50 (mm) | 37.91 |
| D84 (mm) | 65.93 |
| D95 (mm) | 87.58 |
| D100 (mm) | 179.99 |
| Silt/Clay (%) | 8.49 |
| Sand (%) | 7.55 |
| Gravel (%) | 66.98 |
| Cobble (%) | 16.98 |
| Boulder (%) | 0 |
| Bedrock (%) | 0 |

Total Particles = 106

XS 8-1 (Riffle)

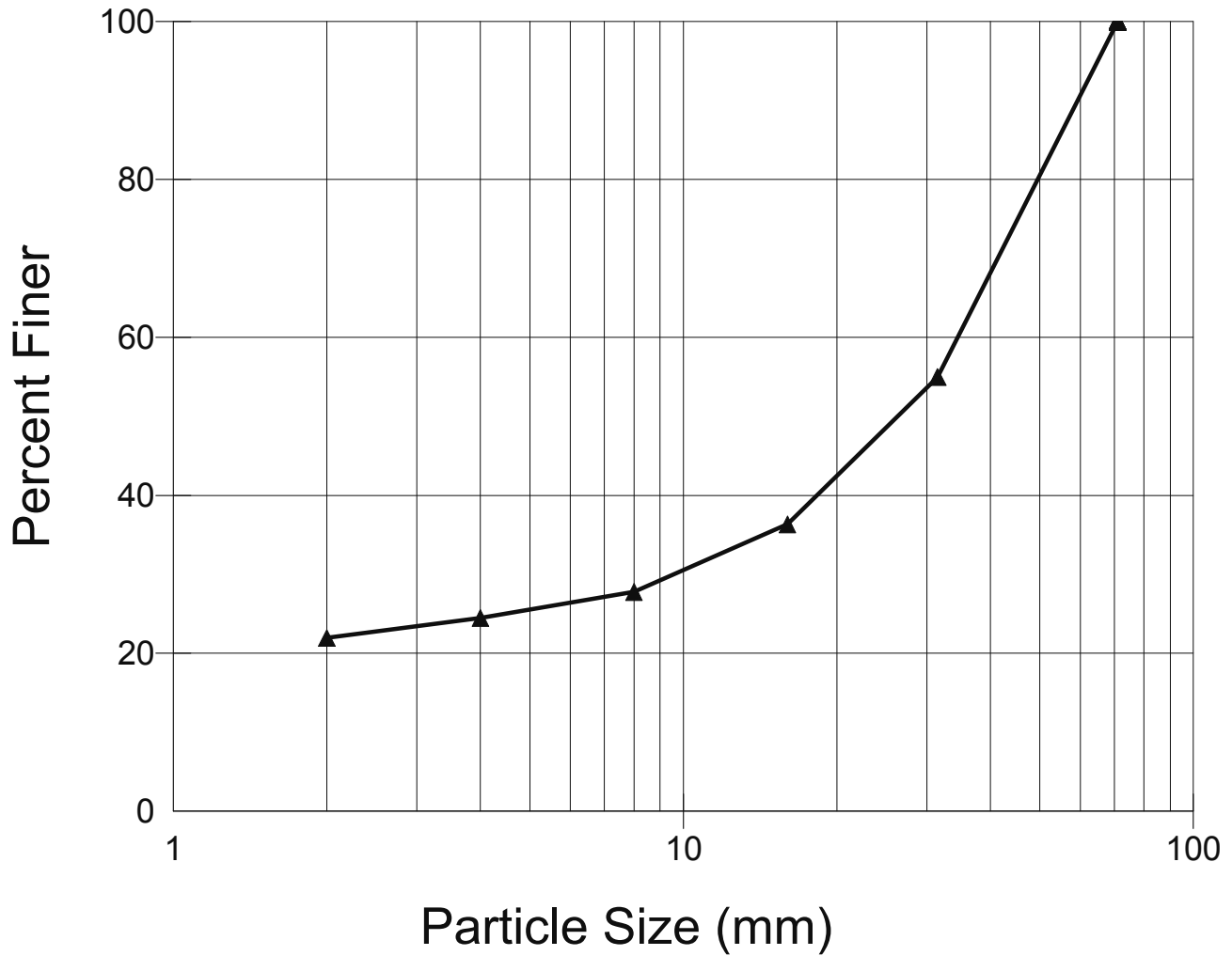


Particle Size Analysis

| | |
|---------------|-------|
| D16 (mm) | 0.34 |
| D35 (mm) | 3.89 |
| D50 (mm) | 10.75 |
| D84 (mm) | 40.73 |
| D95 (mm) | 65.33 |
| D100 (mm) | 128 |
| Silt/Clay (%) | 10.37 |
| Sand (%) | 14.82 |
| Gravel (%) | 69.62 |
| Cobble (%) | 5.19 |
| Boulder (%) | 0 |
| Bedrock (%) | 0 |

Total Particles = 135

Basal Gravel 2

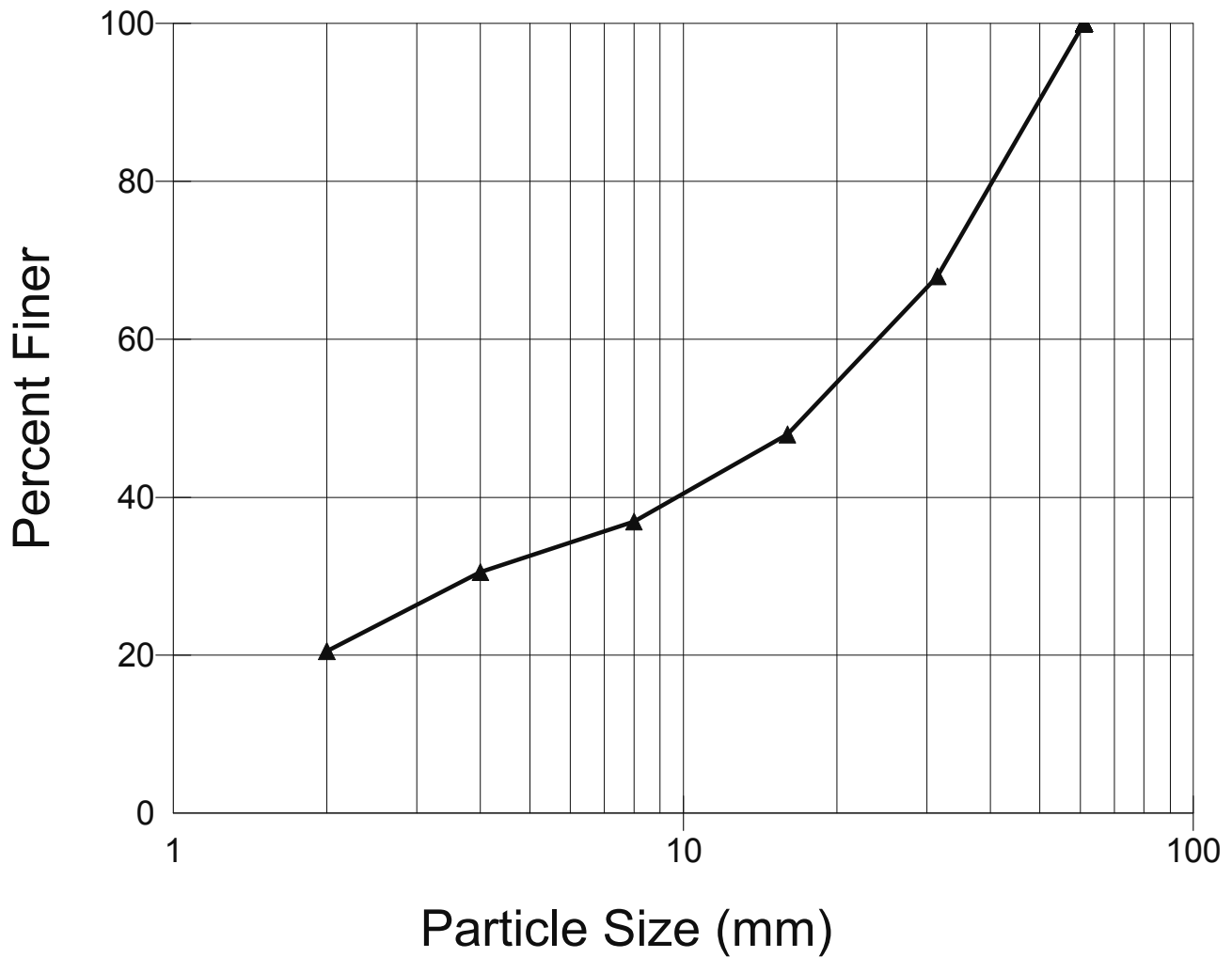


Particle Size Analysis

| | |
|---------------|-------|
| D16 (mm) | 0 |
| D35 (mm) | 14.77 |
| D50 (mm) | 27.38 |
| D84 (mm) | 56.97 |
| D95 (mm) | 66.62 |
| D100 (mm) | 71 |
| Silt/Clay (%) | 0 |
| Sand (%) | 21.94 |
| Gravel (%) | 72.3 |
| Cobble (%) | 5.75 |
| Boulder (%) | 0 |
| Bedrock (%) | 0 |

Total Weight = 10.30

Basal Gravel 4

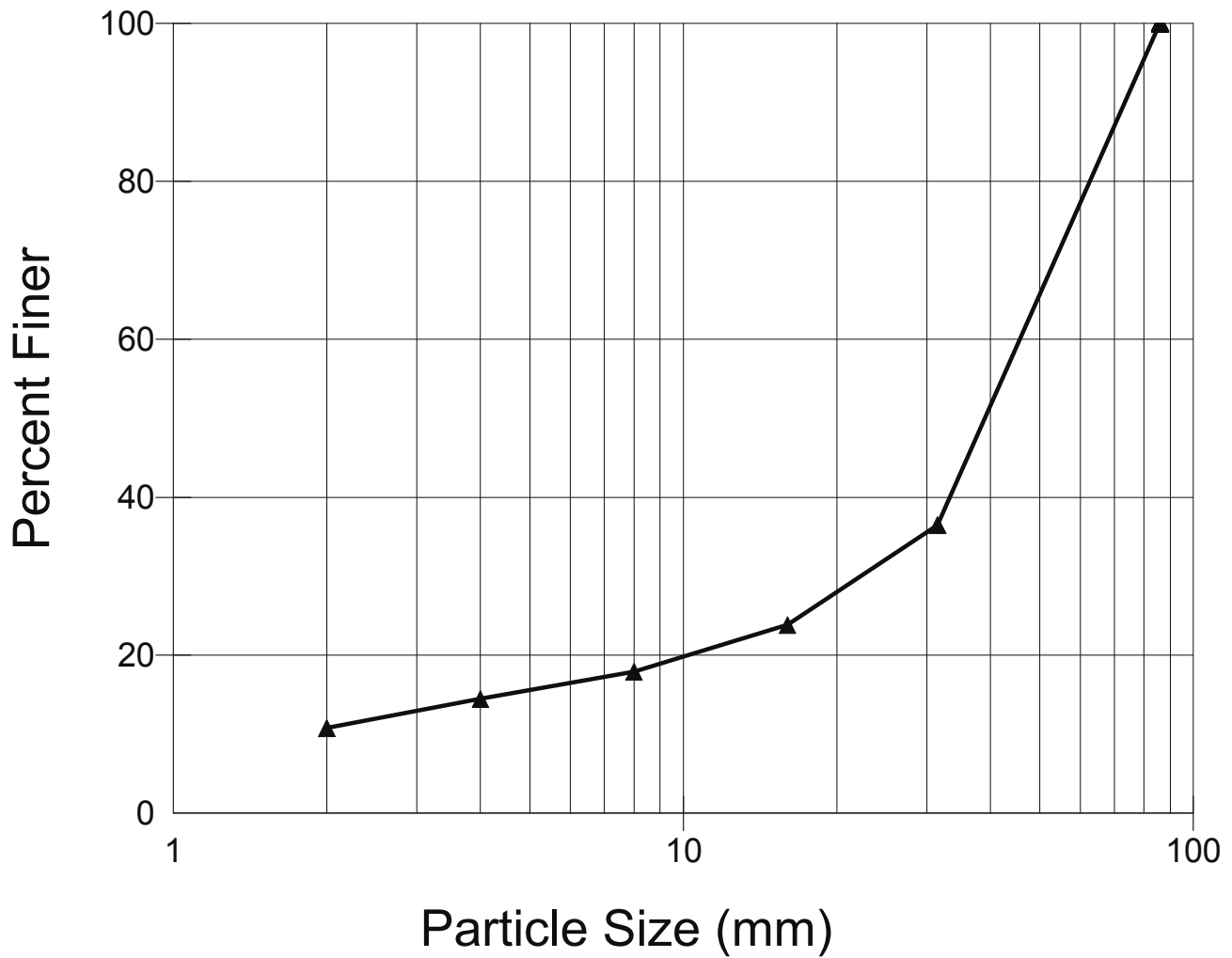


Particle Size Analysis

| | |
|---------------|-------|
| D16 (mm) | 0 |
| D35 (mm) | 6.8 |
| D50 (mm) | 17.59 |
| D84 (mm) | 46.27 |
| D95 (mm) | 56.4 |
| D100 (mm) | 64 |
| Silt/Clay (%) | 0 |
| Sand (%) | 20.51 |
| Gravel (%) | 79.49 |
| Cobble (%) | 0 |
| Boulder (%) | 0 |
| Bedrock (%) | 0 |

Total Weight = 7.80

Basal Gravel 5

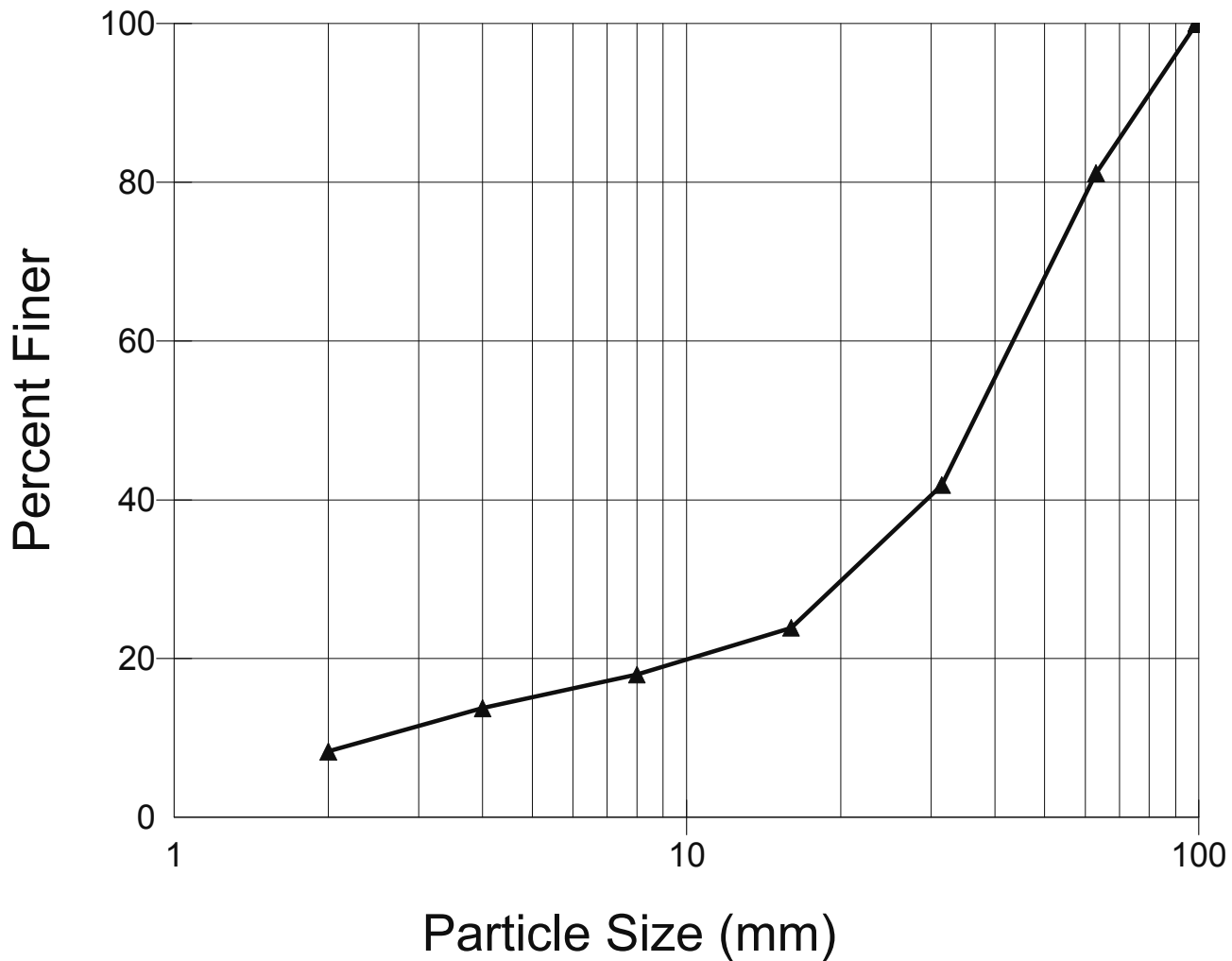


Particle Size Analysis

| | |
|---------------|-------|
| D16 (mm) | 5.78 |
| D35 (mm) | 29.71 |
| D50 (mm) | 43.12 |
| D84 (mm) | 72.28 |
| D95 (mm) | 81.71 |
| D100 (mm) | 86 |
| Silt/Clay (%) | 0 |
| Sand (%) | 10.79 |
| Gravel (%) | 70.51 |
| Cobble (%) | 18.69 |
| Boulder (%) | 0 |
| Bedrock (%) | 0 |

Total Weight = 9.82

Point Bar



Particle Size Analysis

| | |
|---------------|-------|
| D16 (mm) | 6.13 |
| D35 (mm) | 25.6 |
| D50 (mm) | 38.04 |
| D84 (mm) | 68.5 |
| D95 (mm) | 89.47 |
| D100 (mm) | 99 |
| Silt/Clay (%) | 0 |
| Sand (%) | 8.31 |
| Gravel (%) | 73.47 |
| Cobble (%) | 18.22 |
| Boulder (%) | 0 |
| Bedrock (%) | 0 |

Total Weight = 13.24

RIVERMORPH PARTICLE SUMMARY

 River Name: Eccleston Mitigation Bank
 Reach Name: Basal Gravel Samples
 Sample Name: Combined Basal Gravel
 Survey Date: 11/06/2018

| SIEVE (mm) | NET WT |
|---------------|--------|
| 31.5 | 10.18 |
| 16 | 4.72 |
| 8 | 2.32 |
| 4 | 1.18 |
| 2 | 1.4 |
| PAN | 4.92 |
| D16 (mm) | 0 |
| D35 (mm) | 13.81 |
| D50 (mm) | 26.84 |
| D84 (mm) | 66.44 |
| D95 (mm) | 79.89 |
| D100 (mm) | 86 |
| Silt/Clay (%) | 0 |
| Sand (%) | 18.75 |
| Gravel (%) | 68.13 |
| Cobble (%) | 13.12 |
| Boulder (%) | 0 |
| Bedrock (%) | 0 |

Total weight = 26.2400.

Largest Surface Particles:

| | Size(mm) | weight |
|-------------|----------|--------|
| Particle 1: | 86 | 0.52 |
| Particle 2: | 74 | 1 |

RIVERMORPH PARTICLE SUMMARY

River Name: Eccleston Mitigation Bank
 Reach Name: Combined MainStem
 Sample Name: Combined Riffle Pebble Count
 Survey Date: 11/07/2018

| Size (mm) | TOT # | ITEM % | CUM % |
|---------------|--------|--------|--------|
| 0 - 0.062 | 23 | 4.26 | 4.26 |
| 0.062 - 0.125 | 0 | 0.00 | 4.26 |
| 0.125 - 0.25 | 2 | 0.37 | 4.63 |
| 0.25 - 0.50 | 29 | 5.37 | 10.00 |
| 0.50 - 1.0 | 30 | 5.56 | 15.56 |
| 1.0 - 2.0 | 0 | 0.00 | 15.56 |
| 2.0 - 4.0 | 9 | 1.67 | 17.22 |
| 4.0 - 5.7 | 4 | 0.74 | 17.96 |
| 5.7 - 8.0 | 6 | 1.11 | 19.07 |
| 8.0 - 11.3 | 25 | 4.63 | 23.70 |
| 11.3 - 16.0 | 20 | 3.70 | 27.41 |
| 16.0 - 22.6 | 48 | 8.89 | 36.30 |
| 22.6 - 32.0 | 47 | 8.70 | 45.00 |
| 32 - 45 | 70 | 12.96 | 57.96 |
| 45 - 64 | 64 | 11.85 | 69.81 |
| 64 - 90 | 79 | 14.63 | 84.44 |
| 90 - 128 | 52 | 9.63 | 94.07 |
| 128 - 180 | 22 | 4.07 | 98.15 |
| 180 - 256 | 7 | 1.30 | 99.44 |
| 256 - 362 | 3 | 0.56 | 100.00 |
| 362 - 512 | 0 | 0.00 | 100.00 |
| 512 - 1024 | 0 | 0.00 | 100.00 |
| 1024 - 2048 | 0 | 0.00 | 100.00 |
| Bedrock | 0 | 0.00 | 100.00 |
| D16 (mm) | 2.53 | | |
| D35 (mm) | 21.63 | | |
| D50 (mm) | 37.02 | | |
| D84 (mm) | 89.22 | | |
| D95 (mm) | 139.85 | | |
| D100 (mm) | 361.98 | | |
| Silt/Clay (%) | 4.26 | | |
| Sand (%) | 11.3 | | |
| Gravel (%) | 54.25 | | |
| Cobble (%) | 29.63 | | |
| Boulder (%) | 0.56 | | |
| Bedrock (%) | 0 | | |

Total Particles = 540.



APPENDIX E

TMDL and NPDES Credit Calculations

Only enter data in the green cells. All other cells are either linked to other worksheets or have equations.

| Eccleston Mitigation Bank | | | | | | | | | | | |
|---|---|---------------------------------|---------------------------------------|------------------------------------|-------------|------------|---|---|---|---|-------------------------|
| Project Name | | | | | | | | | | | |
| Feature | Lat/Long | | Length, ft (Bank or deposition) | Height, ft (Bank or Headcut) | BEHI Rating | NBS Rating | Predicted Rate of Bank Erosion (ft/year) | Predicted Erosion Amount (ft ³ /year) | Predicted Erosion Amount (tons/year) | Predicted Erosion Rate (tons/year/ft) | Comments |
| Feature I.D. (Bank., Headcut or Deposition I.D.) | Start | End | | | | | | | | | |
| | Headcut Location or Start of Bank/Deposition | For Banks or Deposition only | | | | | | | | | |
| Left Bank, LB1 | 137+81.38 to | 138+57.64 | 79 | 5.00 | High | Low | 0.40 | 158.00 | 7.61 | 0.096 | Jones Falls - Main Stem |
| Right Bank, RB1 | 137+75.04 to | 138+58.10 | 81 | 5.00 | Very High | Very High | 1.75 | 708.75 | 34.13 | 0.421 | Jones Falls - Main Stem |
| Left Bank, LB2 | 136+80.59 to | 137+81.38 | 109 | 4.00 | High | Extreme | 2.50 | 1090.00 | 52.48 | 0.481 | Jones Falls - Main Stem |
| Right Bank, RB2 | 136+68.35 to | 137+75.04 | 101 | 3.00 | Extreme | Extreme | 4.50 | 1363.50 | 65.65 | 0.650 | Jones Falls - Main Stem |
| Left Bank, LB3 | 135+84.96 to | 136+80.59 | 90 | 2.70 | Very High | High | 1.00 | 243.00 | 11.70 | 0.130 | Jones Falls - Main Stem |
| Right Bank, RB3 | 135+92.67 to | 136+68.35 | 87 | 4.30 | High | Low | 0.40 | 149.64 | 7.20 | 0.083 | Jones Falls - Main Stem |
| Left Bank, LB4 | 135+2.07 to | 135+84.96 | 87 | 3.20 | Extreme | High | 2.50 | 696.00 | 33.51 | 0.385 | Jones Falls - Main Stem |
| Right Bank, RB4 | 135+7.97 to | 135+92.67 | 83 | 2.20 | High | Low | 0.40 | 73.04 | 3.52 | 0.042 | Jones Falls - Main Stem |
| Left Bank, LB5 | 133+88.95 to | 135+2.07 | 133 | 4.00 | Very High | Very High | 1.75 | 931.00 | 44.83 | 0.337 | Jones Falls - Main Stem |
| Right Bank, RB5 | 134+20.79 to | 135+7.97 | 88 | 2.50 | High | Low | 0.40 | 88.00 | 4.24 | 0.048 | Jones Falls - Main Stem |
| Right Bank, RB6 | 133+33.43 to | 134+20.79 | 92 | 4.00 | Very High | High | 1.00 | 368.00 | 17.72 | 0.193 | Jones Falls - Main Stem |
| Left Bank, LB6 | 132+65.40 to | 133+88.95 | 124 | 4.00 | High | Low | 0.40 | 198.40 | 9.55 | 0.077 | Jones Falls - Main Stem |
| Right Bank, RB7 | 126+61.74 to | 133+33.43 | 686 | 3.50 | Extreme | High | 2.50 | 6002.50 | 289.01 | 0.421 | Jones Falls - Main Stem |
| Left Bank, LB7 | 126+57.48 to | 132+65.40 | 621 | 4.50 | High | Low | 0.40 | 1117.80 | 53.82 | 0.087 | Jones Falls - Main Stem |
| Right Bank, RB8 | 123+57.45 to | 126+61.74 | 301 | 3.50 | Very High | Low | 0.40 | 421.40 | 20.29 | 0.067 | Jones Falls - Main Stem |
| Left Bank, LB8 | 124+88.11 to | 126+57.48 | 194 | 3.00 | High | Low | 0.40 | 232.80 | 11.21 | 0.058 | Jones Falls - Main Stem |
| Right Bank, RB9 | 121+21.11 to | 123+57.45 | 239 | 5.00 | High | Moderate | 0.64 | 764.80 | 36.82 | 0.154 | Jones Falls - Main Stem |
| Left Bank, LB9 | 121+23.56 to | 124+88.11 | 409 | 3.50 | Very High | Moderate | 0.64 | 916.16 | 44.11 | 0.108 | Jones Falls - Main Stem |
| Right Bank, RB10 | 119+64.19 to | 121+21.11 | 160 | 2.50 | High | Moderate | 0.64 | 256.00 | 12.33 | 0.077 | Jones Falls - Main Stem |

| Feature | Lat/Long | | Length, ft (Bank or deposition) | Height, ft (Bank or Headcut) | BEHI Rating | NBS Rating | Predicted Rate of Bank Erosion (ft/year) | Predicted Erosion Amount (ft ³ /year) | Predicted Erosion Amount (tons/year) | Predicted Erosion Rate (tons/year/ft) | Comments |
|---|---|---------------------------------|---------------------------------------|------------------------------------|-------------|------------|---|---|---|---|-------------------------|
| | Start | End | | | | | | | | | |
| Feature I.D. (Bank., Headcut or Deposition I.D.) | Headcut Location or Start of Bank/Deposition | For Banks or Deposition only | | | | | | | | | |
| Left Bank, LB10 | 120+25.66 to 121+23.56 | | 97 | 3.00 | Very High | Moderate | 0.64 | 186.24 | 8.97 | 0.092 | Jones Falls - Main Stem |
| Right Bank, RB11 | 116+39.48 to 119+64.19 | | 325 | 4.50 | High | Low | 0.40 | 585.00 | 28.17 | 0.087 | Jones Falls - Main Stem |
| Left Bank, LB11 | 114+61.16 to 120+25.66 | | 595 | 4.50 | High | Low | 0.40 | 1071.00 | 51.57 | 0.087 | Jones Falls - Main Stem |
| Right Bank, RB12 | 115+14.22 to 116+39.48 | | 124 | 5.50 | High | Low | 0.40 | 272.80 | 13.13 | 0.106 | Jones Falls - Main Stem |
| Left Bank, LB12 | 111+99.76 to 114+61.16 | | 246 | 3.00 | High | Extreme | 2.50 | 1845.00 | 88.83 | 0.361 | Jones Falls - Main Stem |
| Right Bank, RB13 | 113+44.63 to 115+14.22 | | 160 | 2.20 | Very High | Moderate | 0.64 | 225.28 | 10.85 | 0.068 | Jones Falls - Main Stem |
| Left Bank, LB13 | 110+41.23 to 111+99.76 | | 147 | 3.50 | High | Moderate | 0.64 | 329.28 | 15.85 | 0.108 | Jones Falls - Main Stem |
| Right Bank, RB14 | 112+84.76 to 113+44.63 | | 76 | 2.50 | Extreme | Extreme | 4.50 | 855.00 | 41.17 | 0.542 | Jones Falls - Main Stem |
| Left Bank, LB14 | 108+67.52 to 110+41.23 | | 188 | 3.00 | Extreme | Moderate | 1.75 | 987.00 | 47.52 | 0.253 | Jones Falls - Main Stem |
| Right Bank, RB15 | 112+3.47 to 112+84.76 | | 79 | 3.00 | Very High | Moderate | 0.64 | 151.68 | 7.30 | 0.092 | Jones Falls - Main Stem |
| Left Bank, LB15 | 107+61.02 to 108+67.52 | | 103 | 2.50 | Very High | Low | 0.40 | 103.00 | 4.96 | 0.048 | Jones Falls - Main Stem |
| Right Bank, RB16 | 110+65.05 to 112+3.47 | | 140 | 3.50 | High | Moderate | 0.64 | 313.60 | 15.10 | 0.108 | Jones Falls - Main Stem |
| Left Bank, LB16 | 106+23.76 to 107+61.02 | | 138 | 2.50 | Very High | Low | 0.40 | 138.00 | 6.64 | 0.048 | Jones Falls - Main Stem |
| Right Bank, RB17 | 107+61.59 to 110+65.05 | | 298 | 2.00 | Very High | Very High | 1.75 | 1043.00 | 50.22 | 0.169 | Jones Falls - Main Stem |
| Left Bank, LB17 | 102+41.73 to 106+23.76 | | 419 | 2.50 | High | High | 1.00 | 1047.50 | 50.44 | 0.120 | Jones Falls - Main Stem |
| Right Bank, RB18 | 106+3.93 to 107+61.59 | | 157 | 2.50 | High | Low | 0.40 | 157.00 | 7.56 | 0.048 | Jones Falls - Main Stem |
| Right Bank, RB19 | 102+40.18 to 106+3.93 | | 362 | 2.50 | Very High | Low | 0.40 | 362.00 | 17.43 | 0.048 | Jones Falls - Main Stem |
| Left Bank, LB18 | 202+64.02 to 205+15.89 | | 279 | 3.50 | Extreme | Low | 1.30 | 1269.45 | 61.12 | 0.219 | Rail Road Tributary |
| Left Bank, LB19 | 205+15.89 to 205+62.34 | | 43 | 2.00 | Very High | Low | 0.40 | 34.40 | 1.66 | 0.039 | Rail Road Tributary |
| Right Bank, RB20 | 202+64.58 to 205+11.94 | | 244 | 3.00 | Very High | Extreme | 2.50 | 1830.00 | 88.11 | 0.361 | Rail Road Tributary |
| Right Bank, RB21 | 205+11.94 to 205+58.48 | | 47 | 2.00 | Very High | Extreme | 2.50 | 235.00 | 11.31 | 0.241 | Rail Road Tributary |

| Feature | Lat/Long | | Length, ft (Bank or deposition) | Height, ft (Bank or Headcut) | BEHI Rating | NBS Rating | Predicted Rate of Bank Erosion (ft/year) | Predicted Erosion Amount (ft ³ /year) | Predicted Erosion Amount (tons/year) | Predicted Erosion Rate (tons/year/ft) | Comments |
|---|---|---------------------------------|---------------------------------------|------------------------------------|-------------|------------|---|---|---|---|------------------------|
| | Start | End | | | | | | | | | |
| Feature I.D. (Bank., Headcut or Deposition I.D.) | Headcut Location or Start of Bank/Deposition | For Banks or Deposition only | | | | | | | | | |
| Left Bank, LB20 | 404+4.57 to 405+60.53 | | 155 | 0.50 | High | Low | 0.40 | 31.00 | 1.49 | 0.010 | Braided Tributary |
| | | | | | | | | | | | |
| Left Bank, LB21 | 405+60.53 to 410+65.09 | | 517 | 2.80 | High | Low | 0.40 | 579.04 | 27.88 | 0.054 | Braided Tributary |
| | | | | | | | | | | | |
| Right Bank, RB22 | 404+7.41 to 405+56.34 | | 147 | 0.50 | High | Extreme | 2.50 | 183.75 | 8.85 | 0.060 | Braided Tributary |
| | | | | | | | | | | | |
| Right Bank, RB23 | 405+56.34 to 410+65.81 | | 516 | 2.00 | High | Extreme | 2.50 | 2580.00 | 124.22 | 0.241 | Braided Tributary |
| | | | | | | | | | | | |
| Left Bank, LB22 | 309+20.39 to 311+1.38 | | 178 | 2.50 | Extreme | Low | 1.30 | 578.50 | 27.85 | 0.156 | Stone House Tributary |
| | | | | | | | | | | | |
| Left Bank, LB23 | 307+55.25 to 309+20.39 | | 163 | 2.50 | Very High | Low | 0.40 | 163.00 | 7.85 | 0.048 | Stone House Tributary |
| | | | | | | | | | | | |
| Right Bank, RB24 | 306+16.05 to 310+97.33 | | 486 | 2.50 | High | Low | 0.40 | 486.00 | 23.40 | 0.048 | Stone House Tributary |
| | | | | | | | | | | | |
| Left Bank, LB24 | 306+18.16 to 307+55.25 | | 137 | 2.50 | High | Low | 0.40 | 137.00 | 6.60 | 0.048 | Stone House Tributary |
| | | | | | | | | | | | |
| Right Bank, RB25 | 305+52.82 to 306+16.05 | | 62 | 2.50 | Extreme | Low | 1.30 | 201.50 | 9.70 | 0.156 | Stone House Tributary |
| | | | | | | | | | | | |
| Left Bank, LB25 | 305+51.43 to 306+18.16 | | 65 | 2.50 | Extreme | Low | 1.30 | 211.25 | 10.17 | 0.156 | Stone House Tributary |
| | | | | | | | | | | | |
| Right Bank, RB26 | 302+31.22 to 305+52.82 | | 335 | 2.50 | High | Low | 0.40 | 335.00 | 16.13 | 0.048 | Stone House Tributary |
| | | | | | | | | | | | |
| Left Bank, LB26 | 302+30.62 to 305+51.43 | | 322 | 2.50 | High | Low | 0.40 | 322.00 | 15.50 | 0.048 | Stone House Tributary |
| | | | | | | | | | | | |
| Right Bank, RB27 | 301+33.97 to 302+31.22 | | 111 | 4.00 | High | Low | 0.40 | 177.60 | 8.55 | 0.077 | Stone House Tributary |
| | | | | | | | | | | | |
| Left Bank, LB27 | 301+25.14 to 302+30.62 | | 107 | 2.00 | Very High | Very High | 1.75 | 374.50 | 18.03 | 0.169 | Stone House Tributary |
| | | | | | | | | | | | |
| Right Bank, RB28 | 500+3.19 to 503+63.08 | | 345 | 6.00 | Very High | Very High | 1.75 | 3622.50 | 174.42 | 0.506 | Intersection Tributary |
| | | | | | | | | | | | |
| Left Bank, LB28 | 500+2.38 to 503+65.54 | | 367 | 6.00 | Very High | Moderate | 0.64 | 1409.28 | 67.85 | 0.185 | Intersection Tributary |
| | | | | | | | | | | | |
| Right Bank, RB29 | 503+63.08 to 507+15.6 | | 358 | 5.00 | Very High | Low | 0.40 | 716.00 | 34.47 | 0.096 | Intersection Tributary |
| | | | | | | | | | | | |
| Left Bank, LB29 | 503+65.54 to 507+20.72 | | 352 | 5.00 | Very High | Moderate | 0.64 | 1126.40 | 54.23 | 0.154 | Intersection Tributary |
| | | | | | | | | | | | |
| TOTAL OF ALL GRIDS | | | 12754.0 | N/A | N/A | N/A | 64.1 | 42054.3 | 2024.8 | 9.4 | |

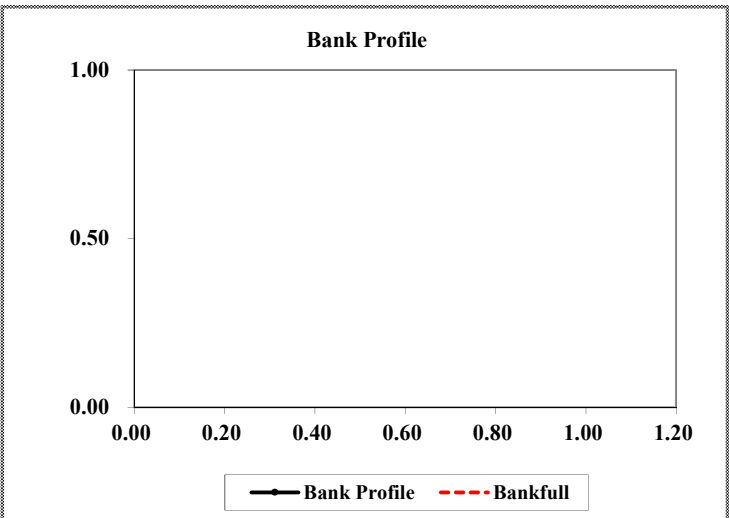
BANK EROSION HAZARD INDEX

| | | | | | | | | | | | | | | | |
|-----------|---------------------------|--------------|-----|-------|----|--------|--|--------------|-------------|----------|-------|----------|-------|-----------|---------|
| Stream: | Eccleston Mitigation Site | Observer(s): | PVC | Data: | SH | QA/QC: | | Total Score: | 39.88 | | | | | | |
| Reach: | 137+81.38 to 138+57.64 | Comments: | | | | | | | High | | | | | | |
| Location: | Left Bank 1 | Bank Length | 79 | | | | | | Total Score | Very Low | Low | Moderate | High | Very High | Extreme |
| Date: | 5/4/2018 | | | | | | | Values: | 5-10 | 10-20 | 20-30 | 30-40 | 40-45 | 45-50 | |

| Erodibility Variables | | | | | |
|--|--------------------------|-------|--------------|------------------------|-------|
| Bank Height / Bankfull Height Ratio | | | | | |
| Bank Height | Bankfull Height | Value | Index | Bank Erosion Potential | Notes |
| 5.00 | 1.50 | 3.33 | 10.00 | Extreme | |
| Root Depth / Bank Height Ratio | | | | | |
| Root Depth | Bank Height | Value | Index | Bank Erosion Potential | Notes |
| 0.25 | 5.00 | 0.05 | 9.00 | Very High | |
| Weighted Root Density | | | | | |
| Root Density (%) | Root Depth / Bank Height | Value | Index | Bank Erosion Potential | Notes |
| 70.00 | 0.05 | 3.50 | 10.00 | Extreme | |
| Bank Angle | | | | | |
| Bank Angle (°) | | | Index | Bank Erosion Potential | Notes |
| 45.00 | | | 3.17 | Low | |
| Surface Protection | | | | | |
| Surface Protection (%) | | | Index | Bank Erosion Potential | Notes |
| 70.00 | | | 2.71 | Low | |
| | | | Adjustment | | Notes |
| Bank Materials | | | | | |
| | | | 5.00 | | |
| | | | Adjustment | | Notes |
| Bank Stratification | | | | | |
| | | | 0.00 | | |
| TOTAL SCORE | | | 39.88 | | |

| Bank Erosion Potential | | | | | | | |
|---|--|-----------|-----------|-----------|-----------|-----------|---------|
| | | Very Low | Low | Moderate | High | Very High | Extreme |
| Bank Height / Bankfull Height | Value | 1.00-1.10 | 1.11-1.19 | 1.20-1.50 | 1.60-2.00 | 2.10-2.80 | >2.80 |
| | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| Root Depth / Bank Height | Value | 1.00-0.90 | 0.89-0.50 | 0.49-0.30 | 0.29-0.15 | 0.14-0.05 | <0.05 |
| | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| Weighted Root Density | Value | 100-80 | 79-55 | 54-30 | 29-15 | 14-5 | <5 |
| | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| Bank Angle | Value | 0-20 | 21-60 | 61-80 | 81-90 | 91-119 | >119 |
| | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| Surface Protection | Value | 100-80 | 79-55 | 54-30 | 29-15 | 14-10 | <10 |
| | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| Adjustments | | | | | | | |
| Bedrock | Bedrock banks have a very low erosion potential. | | | | | | |
| Boulders | Boulder banks have a low erosion potential. | | | | | | |
| Cobble | Subtract 10 points. No adjustment if sand/gravel compose greater than 50% of bank. | | | | | | |
| Clay/Silt Loam | Add 5 points. | | | | | | |
| Gravel | Add 5-10 points depending on percentage of bank material composed of sand. | | | | | | |
| Sand | Add 10 points. | | | | | | |
| Silt / Clay | No adjustment. | | | | | | |
| Stratification | | | | | | | |
| Add 5-10 points depending on position of unstable layers in relation to bankfull stage. | | | | | | | |

| Bank Profile | | |
|---------------------|-----------------|-------|
| Horizontal Distance | Vertical Height | Notes |
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| | | |
| | | |
| Bankfull | | |
| Horizontal Distance | Vertical Height | Notes |
| | | |
| | | |
| | | |



Estimating Near-Bank Stress (NBS)

Stream: **Eccleston** Location: **Left Bank 1**
 Station: **137+81.38 to 138+57.64** Stream Type: Valley Type:
 Observers: Date: **5/4/2018**

Methods for Estimating Near-Bank Stress (NBS)

| | | |
|---|-----------|---------------------|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | Level II | General prediction |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | Level III | Detailed prediction |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | Level III | Detailed prediction |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | | | |
|-----------------|---------------------------|--------------------------------|-------------------------------|------------------------|------------------------|--|--------|---|---------------------------|-----|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | <table border="1" style="margin: auto;"> <tr><td style="background-color: #ADD8E6;">Method</td><td style="background-color: #ADD8E6;">5</td></tr> <tr><td style="background-color: #ADD8E6;">Dominant Near-Bank Stress</td><td style="background-color: #ADD8E6;">Low</td></tr> </table> | Method | 5 | Dominant Near-Bank Stress | Low |
| | Method | 5 | | | | | | | | |
| | Dominant Near-Bank Stress | Low | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | |

| | | | | | | | | | |
|------------------|-----|-----------------------------------|---------------------------|--|---------------------------|-------------------|--|--------------------------------|------------------------|
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | | | | |
| | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} | Near-Bank Stress (NBS) |

| | | | |
|-----------------|-----|-------------------------------------|------------------------|
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | Near-Bank Stress (NBS) |
|-----------------|-----|-------------------------------------|------------------------|

Converting Values to a Near-Bank Stress (NBS) Rating

| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
|--------------------------------|---------------|-------------|-------------|-------------|-------------|-------------|-------------|
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N / A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N / A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N / A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |

Overall Near-Bank Stress (NBS) rating Low

Estimating Near-Bank Stress (NBS)

Stream: **Eccleston** Location: **Right Bank 1**

Station: **137+75.04 to 138+58.10** Stream Type: Valley Type:

Observers: Date: **5/4/2018**

Methods for Estimating Near-Bank Stress (NBS)

| | | |
|---|-----------|---------------------|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | Level II | General prediction |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | Level III | Detailed prediction |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | Level III | Detailed prediction |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | | | | | | | |
|------------------|---------------------------|-------------------------------------|-------------------------------|--|---------------------------|---|--|--------------------------------|------------------------|---|---------------------------|--|-----------|--|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | <table border="1"> <tr> <td>Method</td> <td>1</td> </tr> <tr> <td colspan="2">Dominant Near-Bank Stress</td> </tr> <tr> <td colspan="2">Very High</td> </tr> </table> | | | Method | 1 | Dominant Near-Bank Stress | | Very High | |
| | Method | 1 | | | | | | | | | | | | |
| | Dominant Near-Bank Stress | | | | | | | | | | | | | |
| Very High | | | | | | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | | | | | | | | | |
| | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} | Near-Bank Stress (NBS) | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | Near-Bank Stress (NBS) | | | | | | | | | | | |

Converting Values to a Near-Bank Stress (NBS) Rating

| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
|--------------------------------|---------------|-------------|-------------|-------------|-------------|-------------|-------------|
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |

Overall Near-Bank Stress (NBS) rating **Very High**

Estimating Near-Bank Stress (NBS)

Stream: **Eccleston** Location: **Left Bank 2**
 Station: **136+80.59 to 137+81.38** Stream Type: Valley Type:
 Observers: Date: **5/4/2018**

Methods for Estimating Near-Bank Stress (NBS)

| | | |
|---|-----------|---------------------|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | Level II | General prediction |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | Level III | Detailed prediction |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | Level III | Detailed prediction |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | | | | | |
|------------------|-----------------------------------|-------------------------------------|--|---------------------------|------------------------|--|--------------------------------|------------------------|---------------------------|--|---------|--|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | <table border="1" style="margin: auto;"> <tr><td style="text-align: center;">Method</td><td style="text-align: center;">2</td></tr> <tr><td colspan="2" style="text-align: center;">Dominant Near-Bank Stress</td></tr> <tr><td colspan="2" style="text-align: center;">Extreme</td></tr> </table> | Method | 2 | Dominant Near-Bank Stress | | Extreme | |
| | | Method | 2 | | | | | | | | | |
| | Dominant Near-Bank Stress | | | | | | | | | | | |
| Extreme | | | | | | | | | | | | |
| 0.36 | 6.83 | 0.0527086 | Extreme | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | |
| | | | | | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | |
| | | | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | | | | | | | |
| | | | | | | | | | | | | |
| (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} | Near-Bank Stress (NBS) | | | | |
| | | | | | | | | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | Near-Bank Stress (NBS) | | | | | | | | | |
| | | | | | | | | | | | | |

Converting Values to a Near-Bank Stress (NBS) Rating

| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
|--|---------------|-------------|-------------|-------------|-------------|----------------|-------------|
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |
| Overall Near-Bank Stress (NBS) rating | | | | | | Extreme | |

| Estimating Near-Bank Stress (NBS) | | | |
|--|-------------------------------|--------------|--|
| Stream: Eccleston | Location: Right Bank 2 | | |
| Station: 136+68.35 to 137+75.04 | Stream Type: | Valley Type: | |
| Observers: | Date: 5/4/2018 | | |

| Methods for Estimating Near-Bank Stress (NBS) | | | |
|---|-----------|---------------------|--|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance | |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | Level II | General prediction | |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction | |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction | |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | Level III | Detailed prediction | |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | Level III | Detailed prediction | |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation | |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | | | | | | | |
|------------------|-----------------------------------|-------------------------------------|--|---------------------------|------------------------|---|--------------------------------|------------------------|--------|---|---------------------------|--|---------|--|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | <table border="1"> <tr> <td>Method</td> <td>2</td> </tr> <tr> <td colspan="2">Dominant Near-Bank Stress</td> </tr> <tr> <td colspan="2">Extreme</td> </tr> </table> | | | Method | 2 | Dominant Near-Bank Stress | | Extreme | |
| | Method | 2 | | | | | | | | | | | | |
| | Dominant Near-Bank Stress | | | | | | | | | | | | | |
| Extreme | | | | | | | | | | | | | | |
| | | 0.42 | 6.88 | 0.0610465 | Extreme | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | | | |
| | | | | | | | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | | | |
| | | | | | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | | | | | | | | | |
| | | | | | | | | | | | | | | |
| (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} | Near-Bank Stress (NBS) | | | | | | |
| | | | | | | | | | | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | Near-Bank Stress (NBS) | | | | | | | | | | | |
| | | | | | | | | | | | | | | |

| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | |
|--|---------------|-------------|-------------|-------------|-------------|----------------|-------------|
| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |
| Overall Near-Bank Stress (NBS) rating | | | | | | Extreme | |

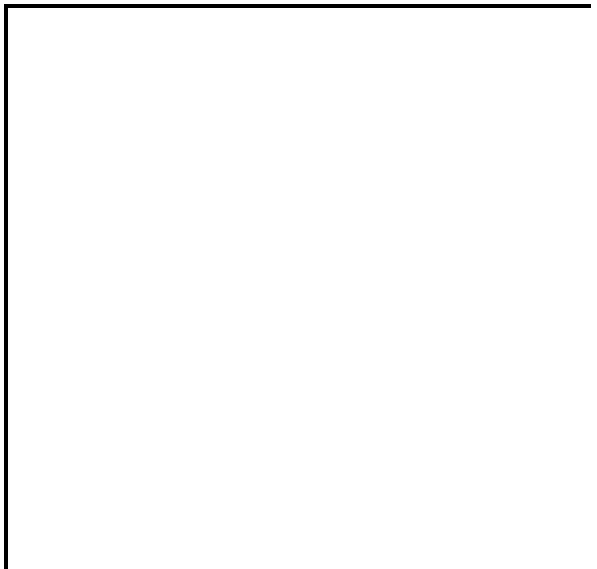
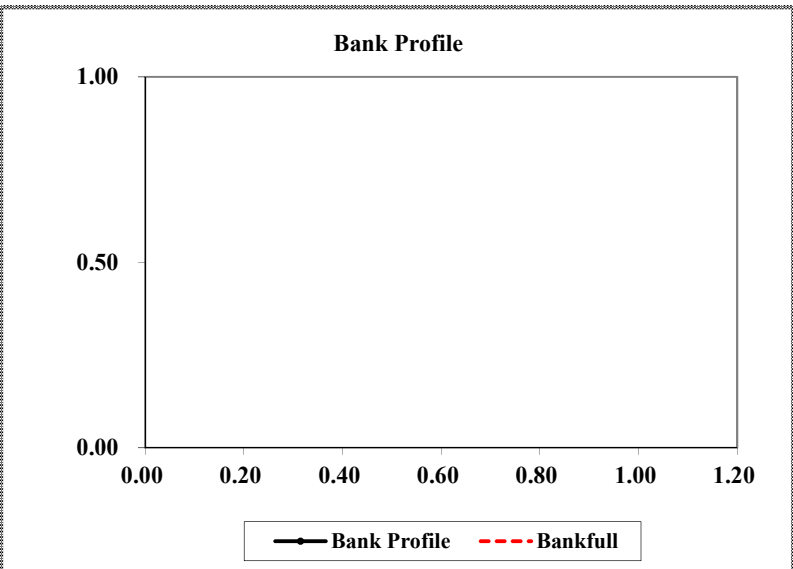
BANK EROSION HAZARD INDEX

| | | | | | | | | | | | | | | |
|------------------|---------------------------|---------------------|-----|--------------|----|---------------|--|---------------------|-----------------|------------|-----------------|-------------|------------------|----------------|
| Stream: | Eccleston Mitigation Site | Observer(s): | PVC | Data: | SH | QA/QC: | | Total Score: | 40.81 | | | | | |
| Reach: | 135+84.96 to 136+80.59 | Comments: | | | | | | Very High | | | | | | |
| Location: | Left Bank 3 | Bank Length | 90 | | | | | Total Score | Very Low | Low | Moderate | High | Very High | Extreme |
| Date: | 5/4/2018 | | | | | | | Values: | 5-10 | 10-20 | 20-30 | 30-40 | 40-45 | 45-50 |

| Erodibility Variables | | | | | |
|-------------------------------------|--------------------------|-------|--------------|------------------------|-------|
| Bank Height / Bankfull Height Ratio | | | | | |
| Bank Height | Bankfull Height | Value | Index | Bank Erosion Potential | Notes |
| 2.70 | 1.50 | 1.80 | 6.95 | High | |
| Root Depth / Bank Height Ratio | | | | | |
| Root Depth | Bank Height | Value | Index | Bank Erosion Potential | Notes |
| 0.17 | 2.70 | 0.06 | 8.86 | Very High | |
| Weighted Root Density | | | | | |
| Root Density (%) | Root Depth / Bank Height | Value | Index | Bank Erosion Potential | Notes |
| 30.00 | 0.06 | 1.89 | 10.00 | Extreme | |
| Bank Angle | | | | | |
| Bank Angle (°) | | | Index | Bank Erosion Potential | Notes |
| 70.00 | | | 4.90 | Moderate | |
| Surface Protection | | | | | |
| Surface Protection (%) | | | Index | Bank Erosion Potential | Notes |
| 40.00 | | | 5.11 | Moderate | |
| | | | Adjustment | | Notes |
| | | | 5.00 | | |
| | | | Adjustment | | Notes |
| | | | 0.00 | | |
| TOTAL SCORE | | | 40.81 | | |

| Bank Erosion Potential | | | | | | | | | |
|---|-------------------------------|----------------|--|-----------|-----------|-----------|-----------|-------|--|
| | | Very Low | Low | Moderate | High | Very High | Extreme | | |
| Erodibility Variables | Bank Height / Bankfull Height | Value | 1.00-1.10 | 1.11-1.19 | 1.20-1.50 | 1.60-2.00 | 2.10-2.80 | >2.80 | |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 | |
| | Root Depth / Bank Height | Value | 1.00-0.90 | 0.89-0.50 | 0.49-0.30 | 0.29-0.15 | 0.14-0.05 | <0.05 | |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 | |
| | Weighted Root Density | Value | 100-80 | 79-55 | 54-30 | 29-15 | 14-5 | <5 | |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 | |
| | Bank Angle | Value | 0-20 | 21-60 | 61-80 | 81-90 | 91-119 | >119 | |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 | |
| | Surface Protection | Value | 100-80 | 79-55 | 54-30 | 29-15 | 14-10 | <10 | |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 | |
| | Adjustments | | | | | | | | |
| | Bank Material | Bedrock | Bedrock banks have a very low erosion potential. | | | | | | |
| | | Boulders | Boulder banks have a low erosion potential. | | | | | | |
| | | Cobble | Subtract 10 points. No adjustment if sand/gravel compose greater than 50% of bank. | | | | | | |
| | | Clay/Silt Loam | Add 5 points. | | | | | | |
| | | Gravel | Add 5-10 points depending on percentage of bank material composed of sand. | | | | | | |
| | Sand | Add 10 points. | | | | | | | |
| | Silt / Clay | No adjustment. | | | | | | | |
| Stratification | | | | | | | | | |
| Add 5-10 points depending on position of unstable layers in relation to bankfull stage. | | | | | | | | | |

| Bank Profile | | |
|---------------------|-----------------|-------|
| Horizontal Distance | Vertical Height | Notes |
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| Bankfull | | |
| Horizontal Distance | Vertical Height | Notes |
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| Estimating Near-Bank Stress (NBS) | | | |
|--|------------------------------|--------------|--|
| Stream: Eccleston | Location: Left Bank 3 | | |
| Station: 135+84.96 to 136+80.59 | Stream Type: | Valley Type: | |
| Observers: | Date: 5/4/2018 | | |

| Methods for Estimating Near-Bank Stress (NBS) | | | |
|---|-----------|---------------------|--|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance | |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | Level II | General prediction | |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction | |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction | |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | Level III | Detailed prediction | |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | Level III | Detailed prediction | |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation | |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | | | | | |
|------------------|---------------------------|-------------------------------------|-------------------------------|--|---------------------------|---|--|--------------------------------|------------------------|------|---------------------------|------|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | <table border="1"> <tr><td>Method</td><td>5</td></tr> <tr><td>Dominant Near-Bank Stress</td><td>High</td></tr> </table> | | | Method | 5 | Dominant Near-Bank Stress | High |
| | Method | 5 | | | | | | | | | | |
| | Dominant Near-Bank Stress | High | | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | | | | 1.98 | 0.81 | 2.4444444 | High |
| | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} | Near-Bank Stress (NBS) | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | Near-Bank Stress (NBS) | | | | | | | | | |

| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | |
|--|---------------|-------------|-------------|-------------|-------------|-------------|-------------|
| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |
| Overall Near-Bank Stress (NBS) rating | | | | | | High | |

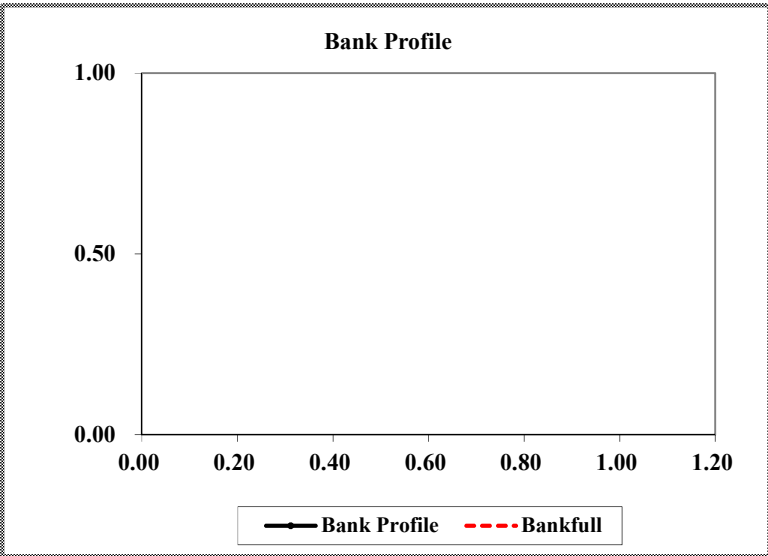
BANK EROSION HAZARD INDEX

| | | | | | | | | | | | | | | | |
|------------------|---------------------------|---------------------|-----|--------------|----|---------------|------|---------------------|--------------------|----------|-------|----------|------|-----------|---------|
| Stream: | Eccleston Mitigation Site | Observer(s): | PVC | Data: | SH | QA/QC: | | Total Score: | 37.87 | | | | | | |
| Reach: | 135+92.67 to 136+68.35 | Comments: | | | | | | | High | | | | | | |
| Location: | Right Bank 3 | Bank Length | 87 | | | | | | Total Score | Very Low | Low | Moderate | High | Very High | Extreme |
| Date: | 5/4/2018 | | | Values: | | | 5-10 | 10-20 | 20-30 | 30-40 | 40-45 | 45-50 | | | |

| Erodibility Variables | | | | | |
|-------------------------------------|--------------------------|-------|--------------|------------------------|-------|
| Bank Height / Bankfull Height Ratio | | | | | |
| Bank Height | Bankfull Height | Value | Index | Bank Erosion Potential | Notes |
| 4.30 | 3.00 | 1.43 | 5.48 | Moderate | |
| Root Depth / Bank Height Ratio | | | | | |
| Root Depth | Bank Height | Value | Index | Bank Erosion Potential | Notes |
| 0.50 | 4.30 | 0.12 | 8.26 | Very High | |
| Weighted Root Density | | | | | |
| Root Density (%) | Root Depth / Bank Height | Value | Index | Bank Erosion Potential | Notes |
| 50.00 | 0.12 | 5.81 | 8.91 | Very High | |
| Bank Angle | | | | | |
| Bank Angle (°) | | | Index | Bank Erosion Potential | Notes |
| 80.00 | | | 5.90 | Moderate | |
| Surface Protection | | | | | |
| Surface Protection (%) | | | Index | Bank Erosion Potential | Notes |
| 50.00 | | | 4.32 | Moderate | |
| | | | Adjustment | | Notes |
| Bank Materials | | | | | |
| | | | 5.00 | | |
| | | | Adjustment | | Notes |
| Bank Stratification | | | | | |
| | | | 0.00 | | |
| TOTAL SCORE | | | 37.87 | | |

| Bank Erosion Potential | | | | | | | | |
|---|--|----------|-----------|-----------|-----------|-----------|-----------|-------|
| | | Very Low | Low | Moderate | High | Very High | Extreme | |
| Erodibility Variables | Bank Height / Bankfull Height | Value | 1.00-1.10 | 1.11-1.19 | 1.20-1.50 | 1.60-2.00 | 2.10-2.80 | >2.80 |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| | Root Depth / Bank Height | Value | 1.00-0.90 | 0.89-0.50 | 0.49-0.30 | 0.29-0.15 | 0.14-0.05 | <0.05 |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| | Weighted Root Density | Value | 100-80 | 79-55 | 54-30 | 29-15 | 14-5 | <5 |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| | Bank Angle | Value | 0-20 | 21-60 | 61-80 | 81-90 | 91-119 | >119 |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| Surface Protection | Value | 100-80 | 79-55 | 54-30 | 29-15 | 14-10 | <10 | |
| | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 | |
| Adjustments | | | | | | | | |
| Bedrock | Bedrock banks have a very low erosion potential. | | | | | | | |
| Boulders | Boulder banks have a low erosion potential. | | | | | | | |
| Cobble | Subtract 10 points. No adjustment if sand/gravel compose greater than 50% of bank. | | | | | | | |
| Clay/Silt Loam | Add 5 points. | | | | | | | |
| Gravel | Add 5-10 points depending on percentage of bank material composed of sand. | | | | | | | |
| Sand | Add 10 points. | | | | | | | |
| Silt / Clay | No adjustment. | | | | | | | |
| Stratification | | | | | | | | |
| Add 5-10 points depending on position of unstable layers in relation to bankfull stage. | | | | | | | | |

| Bank Profile | | |
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| Horizontal Distance | Vertical Height | Notes |
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| Bankfull | | |
| Horizontal Distance | Vertical Height | Notes |
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| Estimating Near-Bank Stress (NBS) | | | |
|--|-------------------------------|--------------|--|
| Stream: Eccleston | Location: Right Bank 3 | | |
| Station: 135+92.67 to 136+68.35 | Stream Type: | Valley Type: | |
| Observers: | Date: 5/4/2018 | | |

| Methods for Estimating Near-Bank Stress (NBS) | | | |
|---|-----------|---------------------|--|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance | |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | Level II | General prediction | |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction | |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction | |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | Level III | Detailed prediction | |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | Level III | Detailed prediction | |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation | |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | | | | | | | |
|------------------|---------------------------|-------------------------------------|-------------------------------|--|---------------------------|--|--|--------------------------------|------------------------|---|---------------------------|--|-----|--|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | <table border="1"> <tr><td>Method</td><td>5</td></tr> <tr><td>Dominant Near-Bank Stress</td><td></td></tr> <tr><td>Low</td><td></td></tr> </table> | | | Method | 5 | Dominant Near-Bank Stress | | Low | |
| | Method | 5 | | | | | | | | | | | | |
| | Dominant Near-Bank Stress | | | | | | | | | | | | | |
| Low | | | | | | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | 2.44 | 2.21 | 1.1040724 | Low | | | | | |
| | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} | Near-Bank Stress (NBS) | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | Near-Bank Stress (NBS) | | | | | | | | | | | |

| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | |
|--|---------------|-------------|-------------|-------------|-------------|-------------|-------------|
| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |
| Overall Near-Bank Stress (NBS) rating | | | | | | Low | |

| Estimating Near-Bank Stress (NBS) | | | |
|---------------------------------------|------------------------------|--------------|--|
| Stream: Eccleston | Location: Left Bank 4 | | |
| Station: 135+2.07 to 135+84.96 | Stream Type: | Valley Type: | |
| Observers: | Date: 5/4/2018 | | |

| Methods for Estimating Near-Bank Stress (NBS) | | |
|---|-----------|---------------------|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkr}) | Level II | General prediction |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkr}) | Level III | Detailed prediction |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkr}) | Level III | Detailed prediction |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | | | | | | | | |
|-----------|-----------------------------------|-------------------------------------|---|---------------------------|------------------------|---|--------------------------------|------------------------|--|--------|---|---------------------------|--|------|--|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkr} (ft) | Ratio R_c / W_{bkr} | Near-Bank Stress (NBS) | <table border="1"> <tr><td>Method</td><td>5</td></tr> <tr><td colspan="2">Dominant Near-Bank Stress</td></tr> <tr><td colspan="2">High</td></tr> </table> | | | | Method | 5 | Dominant Near-Bank Stress | | High | |
| | Method | 5 | | | | | | | | | | | | | |
| | Dominant Near-Bank Stress | | | | | | | | | | | | | | |
| High | | | | | | | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkr} (ft) | Ratio d_{nb} / d_{bkr} | Near-Bank Stress (NBS) | | | | | | | | | | |
| | | 1.98 | 0.81 | 2.444444 | High | | | | | | | | | | |
| (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkr} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkr} (lb/ft ²) | Ratio τ_{nb} / τ_{bkr} | Near-Bank Stress (NBS) | | | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | | Near-Bank Stress (NBS) | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |

| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | |
|--|---------------|-------------|-------------|-------------|-------------|-------------|-------------|
| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |
| Overall Near-Bank Stress (NBS) rating | | | | | | High | |

Estimating Near-Bank Stress (NBS)

Stream: **Eccleston** Location: **Right Bank 4**

Station: **135+7.97 to 135+92.67** Stream Type: Valley Type:

Observers: Date: **5/4/2018**

Methods for Estimating Near-Bank Stress (NBS)

| | | |
|---|-----------|---------------------|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | Level II | General prediction |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | Level III | Detailed prediction |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | Level III | Detailed prediction |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | | | | | | | |
|------------------|---------------------------|-------------------------------------|-------------------------------|--|---------------------------|---|--|--------------------------------|------------------------|---|---------------------------|--|-----|--|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | <table border="1"> <tr> <td>Method</td> <td>5</td> </tr> <tr> <td colspan="2">Dominant Near-Bank Stress</td> </tr> <tr> <td colspan="2">Low</td> </tr> </table> | | | Method | 5 | Dominant Near-Bank Stress | | Low | |
| | Method | 5 | | | | | | | | | | | | |
| | Dominant Near-Bank Stress | | | | | | | | | | | | | |
| Low | | | | | | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | 2.44 | 2.21 | 1.1040724 | Low | | | | | |
| | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} | Near-Bank Stress (NBS) | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | Near-Bank Stress (NBS) | | | | | | | | | | | |

Converting Values to a Near-Bank Stress (NBS) Rating

| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
|--------------------------------|---------------|-------------|-------------|-------------|-------------|-------------|-------------|
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |

Overall Near-Bank Stress (NBS) rating **Low**

| Estimating Near-Bank Stress (NBS) | | | | | | | | |
|--|---|---|-------------------------------|--|---------------------------|-------------------|--|--------------------------------|
| Stream: Eccleston | | Location: Left Bank 5 | | | | | | |
| Station: 133+88.95 to 135+2.07 | | Stream Type: | | Valley Type: | | | | |
| Observers: | | Date: 5/4/2018 | | | | | | |
| Methods for Estimating Near-Bank Stress (NBS) | | | | | | | | |
| (1) | Channel pattern, transverse bar or split channel/central bar creating NBS | | | Level I | Reconnaissance | | | |
| (2) | Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | | | Level II | General prediction | | | |
| (3) | Ratio of pool slope to average water surface slope (S_p / S) | | | Level II | General prediction | | | |
| (4) | Ratio of pool slope to riffle slope (S_p / S_{rif}) | | | Level II | General prediction | | | |
| (5) | Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | | | Level III | Detailed prediction | | | |
| (6) | Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | | | Level III | Detailed prediction | | | |
| (7) | Velocity profiles / Isovels / Velocity gradient | | | Level IV | Validation | | | |
| Level I | (1) | Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High Extensive deposition (continuous, cross-channel).....NBS = Extreme Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme | | | | | | |
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | | | |
| | (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | |
| | (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | | | |
| | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | | Near-Bank Stress (NBS) | | | | |
| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | | |
| Near-Bank Stress (NBS) ratings | Method number | | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) | |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 | |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 | |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 | |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 | |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 | |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 | |
| Overall Near-Bank Stress (NBS) rating | | | | | | Very High | | |

| | |
|----------------------------------|----------|
| Method | 1 |
| Dominant Near-Bank Stress | |
| Very High | |

Estimating Near-Bank Stress (NBS)

Stream: **Eccleston** Location: **Right Bank 5**

Station: **134+20.79 to 135+7.97** Stream Type: Valley Type:

Observers: Date: **5/4/2018**

Methods for Estimating Near-Bank Stress (NBS)

| | | |
|---|-----------|---------------------|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | Level II | General prediction |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | Level III | Detailed prediction |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | Level III | Detailed prediction |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | | | | | | | |
|------------------|----------------------------------|-------------------------------------|-------------------------------|--|---------------------------|--|--|--------------------------------|------------------------|----------|----------------------------------|--|------------|--|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | <table border="1"> <tr> <td>Method</td> <td>5</td> </tr> <tr> <td colspan="2">Dominant Near-Bank Stress</td> </tr> <tr> <td colspan="2">Low</td> </tr> </table> | | | Method | 5 | Dominant Near-Bank Stress | | Low | |
| | Method | 5 | | | | | | | | | | | | |
| | Dominant Near-Bank Stress | | | | | | | | | | | | | |
| Low | | | | | | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | | | | | | | | | |
| | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} | Near-Bank Stress (NBS) | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | Near-Bank Stress (NBS) | | | | | | | | | | | |

Converting Values to a Near-Bank Stress (NBS) Rating

| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
|--------------------------------|---------------|-------------|-------------|-------------|-------------|-------------|-------------|
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |

Overall Near-Bank Stress (NBS) rating **Low**

Estimating Near-Bank Stress (NBS)

Stream: **Eccleston** Location: **Right Bank 6**

Station: **133+33.43 to 134+20.79** Stream Type: Valley Type:

Observers: Date: **5/4/2018**

Methods for Estimating Near-Bank Stress (NBS)

| | | |
|---|-----------|---------------------|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | Level II | General prediction |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | Level III | Detailed prediction |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | Level III | Detailed prediction |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | | | | | | | |
|------------------|-----------------------------------|-------------------------------------|--|---------------------------|------------------------|--|--------------------------------|------------------------|--------|---|---------------------------|--|------|--|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | <table border="1" style="margin-left: auto; margin-right: auto;"> <tr><td>Method</td><td>5</td></tr> <tr><td align="center" colspan="2">Dominant Near-Bank Stress</td></tr> <tr><td align="center" colspan="2">High</td></tr> </table> | | | Method | 5 | Dominant Near-Bank Stress | | High | |
| | Method | 5 | | | | | | | | | | | | |
| | Dominant Near-Bank Stress | | | | | | | | | | | | | |
| High | | | | | | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | | | | | | | | | |
| | | 0.77 | 0.4 | 1.925 | High | | | | | | | | | |
| (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} | Near-Bank Stress (NBS) | | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | Near-Bank Stress (NBS) | | | | | | | | | | | |

Converting Values to a Near-Bank Stress (NBS) Rating

| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
|--------------------------------|---------------|-------------|-------------|-------------|-------------|-------------|-------------|
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |

Overall Near-Bank Stress (NBS) rating **High**

| Estimating Near-Bank Stress (NBS) | | | |
|---------------------------------------|------------------------------|--------------|--|
| Stream: Eccleston | Location: Left Bank 6 | | |
| Station: 133+88.95 to 135+2.07 | Stream Type: | Valley Type: | |
| Observers: | Date: 5/4/2018 | | |

| Methods for Estimating Near-Bank Stress (NBS) | | | |
|---|-----------|---------------------|--|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance | |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | Level II | General prediction | |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction | |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction | |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | Level III | Detailed prediction | |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | Level III | Detailed prediction | |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation | |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | | | | | | | |
|------------------|----------------------------------|-------------------------------------|-------------------------------|--|---------------------------|--|--|--------------------------------|------------------------|----------|----------------------------------|--|------------|--|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | <table border="1"> <tr> <td>Method</td> <td>5</td> </tr> <tr> <td colspan="2">Dominant Near-Bank Stress</td> </tr> <tr> <td colspan="2">Low</td> </tr> </table> | | | Method | 5 | Dominant Near-Bank Stress | | Low | |
| | Method | 5 | | | | | | | | | | | | |
| | Dominant Near-Bank Stress | | | | | | | | | | | | | |
| Low | | | | | | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | 1.15 | 0.91 | 1.2637363 | Low | | | | | |
| | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} | Near-Bank Stress (NBS) | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | | Near-Bank Stress (NBS) | | | | | | | | | | |

| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | |
|--|---------------|-------------|-------------|-------------|-------------|-------------|-------------|
| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |
| Overall Near-Bank Stress (NBS) rating | | | | | | Low | |

Estimating Near-Bank Stress (NBS)

Stream: **Eccleston** Location: **Right Bank 7**

Station: **126+61.74 to 133+33.43** Stream Type: Valley Type:

Observers: Date: **5/4/2018**

Methods for Estimating Near-Bank Stress (NBS)

| | | |
|---|-----------|---------------------|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | Level II | General prediction |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | Level III | Detailed prediction |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | Level III | Detailed prediction |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | | | | | | | |
|------------------|-----------------------------------|-------------------------------------|--|---------------------------|------------------------|--|--------------------------------|------------------------|--------|---|---------------------------|--|------|--|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | <table border="1" style="margin-left: auto; margin-right: auto;"> <tr><td>Method</td><td>5</td></tr> <tr><td align="center" colspan="2">Dominant Near-Bank Stress</td></tr> <tr><td align="center" colspan="2">High</td></tr> </table> | | | Method | 5 | Dominant Near-Bank Stress | | High | |
| | Method | 5 | | | | | | | | | | | | |
| | Dominant Near-Bank Stress | | | | | | | | | | | | | |
| High | | | | | | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | | | | | | | | | |
| | | 0.77 | 0.4 | 1.925 | High | | | | | | | | | |
| (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} | Near-Bank Stress (NBS) | | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | Near-Bank Stress (NBS) | | | | | | | | | | | |

Converting Values to a Near-Bank Stress (NBS) Rating

| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
|--------------------------------|---------------|-------------|-------------|-------------|-------------|-------------|-------------|
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |

Overall Near-Bank Stress (NBS) rating **High**

| Estimating Near-Bank Stress (NBS) | | | |
|--|------------------------------|--------------|--|
| Stream: Eccleston | Location: Left Bank 7 | | |
| Station: 126+57.48 to 132+65.40 | Stream Type: | Valley Type: | |
| Observers: | Date: 5/4/2018 | | |

| Methods for Estimating Near-Bank Stress (NBS) | | | |
|---|-----------|---------------------|--|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance | |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | Level II | General prediction | |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction | |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction | |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | Level III | Detailed prediction | |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | Level III | Detailed prediction | |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation | |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | |
|------------------|-----|-------------------------------------|-------------------------------|--|---------------------------|-------------------|--|--------------------------------|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | | | |
| | (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | |
| | (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | | | |
| | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | | Near-Bank Stress (NBS) | | | | |

| | |
|---------------------------|---|
| Method | 5 |
| Dominant Near-Bank Stress | |
| Low | |

| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | |
|--|---------------|-------------|-------------|-------------|-------------|-------------|-------------|
| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |
| Overall Near-Bank Stress (NBS) rating | | | | | | Low | |

| Estimating Near-Bank Stress (NBS) | | | | | | | | |
|--|---|---|-------------------------------|--|---------------------------|-------------------|--|--------------------------------|
| Stream: Eccleston | | | | Location: Right Bank 8 | | | | |
| Station: 123+57.45 to 126+61.74 | | | Stream Type: | | Valley Type: | | | |
| Observers: | | | | Date: 5/4/2018 | | | | |
| Methods for Estimating Near-Bank Stress (NBS) | | | | | | | | |
| (1) | Channel pattern, transverse bar or split channel/central bar creating NBS | | | Level I | Reconnaissance | | | |
| (2) | Ratio of radius of curvature to bankfull width (R_c / W_{bkr}) | | | Level II | General prediction | | | |
| (3) | Ratio of pool slope to average water surface slope (S_p / S) | | | Level II | General prediction | | | |
| (4) | Ratio of pool slope to riffle slope (S_p / S_{rif}) | | | Level II | General prediction | | | |
| (5) | Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkr}) | | | Level III | Detailed prediction | | | |
| (6) | Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkr}) | | | Level III | Detailed prediction | | | |
| (7) | Velocity profiles / Isovels / Velocity gradient | | | Level IV | Validation | | | |
| Level I | (1) | Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High Extensive deposition (continuous, cross-channel).....NBS = Extreme Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme | | | | | | |
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkr} (ft) | Ratio R_c / W_{bkr} | Near-Bank Stress (NBS) | | | |
| | (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | |
| | (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkr} (ft) | Ratio d_{nb} / d_{bkr} | Near-Bank Stress (NBS) | | | |
| | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft^2) | Mean Depth d_{bkr} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkr} (lb/ft^2) | Ratio τ_{nb} / τ_{bkr} |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | | Near-Bank Stress (NBS) | | | | |
| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | | |
| Near-Bank Stress (NBS) ratings | Method number | | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) | |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 | |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 | |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 | |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 | |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 | |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 | |
| Overall Near-Bank Stress (NBS) rating | | | | | | Low | | |

| | |
|------------------|---|
| Method | 5 |
| Dominant | |
| Near-Bank Stress | |
| Low | |

| Estimating Near-Bank Stress (NBS) | | | | | | | | |
|--|---|---|-------------------------------|--|---------------------------|-------------------|--|--------------------------------|
| Stream: Eccleston | | Location: Left Bank 8 | | | | | | |
| Station: 124+88.11 to 126+57.48 | | Stream Type: | | Valley Type: | | | | |
| Observers: | | Date: 5/4/2018 | | | | | | |
| Methods for Estimating Near-Bank Stress (NBS) | | | | | | | | |
| (1) | Channel pattern, transverse bar or split channel/central bar creating NBS | | | Level I | Reconnaissance | | | |
| (2) | Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | | | Level II | General prediction | | | |
| (3) | Ratio of pool slope to average water surface slope (S_p / S) | | | Level II | General prediction | | | |
| (4) | Ratio of pool slope to riffle slope (S_p / S_{rif}) | | | Level II | General prediction | | | |
| (5) | Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | | | Level III | Detailed prediction | | | |
| (6) | Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | | | Level III | Detailed prediction | | | |
| (7) | Velocity profiles / Isovels / Velocity gradient | | | Level IV | Validation | | | |
| Level I | (1) | Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High Extensive deposition (continuous, cross-channel).....NBS = Extreme Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme | | | | | | |
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | | | |
| | (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | |
| | (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | | | |
| | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | | Near-Bank Stress (NBS) | | | | |
| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | | |
| Near-Bank Stress (NBS) ratings | Method number | | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) | |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 | |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 | |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 | |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 | |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 | |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 | |
| Overall Near-Bank Stress (NBS) rating | | | | | | Low | | |

| | |
|----------------------------------|----------|
| Method | 5 |
| Dominant Near-Bank Stress | |
| Low | |

Estimating Near-Bank Stress (NBS)

Stream: **Eccleston** Location: **Right Bank 9**

Station: **121+21.11 to 123+57.45** Stream Type: Valley Type:

Observers: Date: **5/4/2018**

Methods for Estimating Near-Bank Stress (NBS)

| | | |
|---|-----------|---------------------|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | Level II | General prediction |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | Level III | Detailed prediction |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | Level III | Detailed prediction |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | | | | | | | |
|------------------|---------------------------|-------------------------------------|-------------------------------|--|---------------------------|---|--|--------------------------------|------------------------|---|---------------------------|--|----------|--|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | <table border="1"> <tr><td>Method</td><td>5</td></tr> <tr><td>Dominant Near-Bank Stress</td><td></td></tr> <tr><td>Moderate</td><td></td></tr> </table> | | | Method | 5 | Dominant Near-Bank Stress | | Moderate | |
| | Method | 5 | | | | | | | | | | | | |
| | Dominant Near-Bank Stress | | | | | | | | | | | | | |
| Moderate | | | | | | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | 0.57 | 0.36 | 1.5833333 | Moderate | | | | | |
| | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} | Near-Bank Stress (NBS) | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | Near-Bank Stress (NBS) | | | | | | | | | | | |

Converting Values to a Near-Bank Stress (NBS) Rating

| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
|--------------------------------|---------------|-------------|-------------|-------------|-------------|-------------|-------------|
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |

Overall Near-Bank Stress (NBS) rating **Moderate**

| Estimating Near-Bank Stress (NBS) | | | |
|--|------------------------------|--------------|--|
| Stream: Eccleston | Location: Left Bank 9 | | |
| Station: 121+23.56 to 124+88.11 | Stream Type: | Valley Type: | |
| Observers: | Date: 5/4/2018 | | |

| Methods for Estimating Near-Bank Stress (NBS) | | | |
|---|-----------|---------------------|--|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance | |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | Level II | General prediction | |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction | |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction | |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | Level III | Detailed prediction | |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | Level III | Detailed prediction | |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation | |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | | | | | | | |
|------------------|---------------------------|-------------------------------------|-------------------------------|--|---------------------------|---|--|--------------------------------|------------------------|---|---------------------------|--|----------|--|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | <table border="1"> <tr><td>Method</td><td>5</td></tr> <tr><td>Dominant Near-Bank Stress</td><td></td></tr> <tr><td>Moderate</td><td></td></tr> </table> | | | Method | 5 | Dominant Near-Bank Stress | | Moderate | |
| | Method | 5 | | | | | | | | | | | | |
| | Dominant Near-Bank Stress | | | | | | | | | | | | | |
| Moderate | | | | | | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | 0.67 | 0.44 | 1.5227273 | Moderate | | | | | |
| | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} | Near-Bank Stress (NBS) | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | | Near-Bank Stress (NBS) | | | | | | | | | | |

| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | |
|--|---------------|-------------|-------------|-------------|-------------|-----------------|-------------|
| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |
| Overall Near-Bank Stress (NBS) rating | | | | | | Moderate | |

| Estimating Near-Bank Stress (NBS) | | | |
|--|--------------------------------|--------------|--|
| Stream: Eccleston | Location: Right Bank 10 | | |
| Station: 119+64.19 to 121+21.11 | Stream Type: | Valley Type: | |
| Observers: | Date: 5/4/2018 | | |

| Methods for Estimating Near-Bank Stress (NBS) | | |
|---|-----------|---------------------|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkr}) | Level II | General prediction |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkr}) | Level III | Detailed prediction |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkr}) | Level III | Detailed prediction |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | | | | | | | |
|------------------|---------------------------|-------------------------------------|-------------------------------|--|---------------------------|---|--|--------------------------------|------------------------|---|---------------------------|--|----------|--|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkr} (ft) | Ratio R_c / W_{bkr} | Near-Bank Stress (NBS) | <table border="1"> <tr><td>Method</td><td>5</td></tr> <tr><td colspan="2">Dominant Near-Bank Stress</td></tr> <tr><td colspan="2">Moderate</td></tr> </table> | | | Method | 5 | Dominant Near-Bank Stress | | Moderate | |
| | Method | 5 | | | | | | | | | | | | |
| | Dominant Near-Bank Stress | | | | | | | | | | | | | |
| Moderate | | | | | | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkr} (ft) | Ratio d_{nb} / d_{bkr} | Near-Bank Stress (NBS) | | | | | | | | | |
| | | 0.57 | 0.36 | 1.5833333 | Moderate | | | | | | | | | |
| | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft^2) | Mean Depth d_{bkr} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkr} (lb/ft^2) | Ratio τ_{nb} / τ_{bkr} | Near-Bank Stress (NBS) | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | | Near-Bank Stress (NBS) | | | | | | | | | | |

| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | |
|--|---------------|-------------|-------------|-------------|-------------|-----------------|-------------|
| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |
| Overall Near-Bank Stress (NBS) rating | | | | | | Moderate | |

Estimating Near-Bank Stress (NBS)

Stream: **Eccleston** Location: **Left Bank 10**

Station: **120+25.66 to 121+23.56** Stream Type: Valley Type:

Observers: Date: **5/4/2018**

Methods for Estimating Near-Bank Stress (NBS)

| | | |
|---|-----------|---------------------|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | Level II | General prediction |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | Level III | Detailed prediction |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | Level III | Detailed prediction |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | | | | | | | |
|------------------|---------------------------|-------------------------------------|-------------------------------|--|---------------------------|---|--|--------------------------------|------------------------|---|---------------------------|--|----------|--|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | <table border="1"> <tr><td>Method</td><td>5</td></tr> <tr><td>Dominant Near-Bank Stress</td><td></td></tr> <tr><td>Moderate</td><td></td></tr> </table> | | | Method | 5 | Dominant Near-Bank Stress | | Moderate | |
| | Method | 5 | | | | | | | | | | | | |
| | Dominant Near-Bank Stress | | | | | | | | | | | | | |
| Moderate | | | | | | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | | | | | | | | | |
| | | 0.67 | 0.44 | 1.5227273 | Moderate | | | | | | | | | |
| Level III | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} | Near-Bank Stress (NBS) | | | | | |
| | | | | | | | | | | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | Near-Bank Stress (NBS) | | | | | | | | | | | |
| | | | | | | | | | | | | | | |

Converting Values to a Near-Bank Stress (NBS) Rating

| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
|--------------------------------|---------------|-------------|-------------|-------------|-------------|-------------|-------------|
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |

Overall Near-Bank Stress (NBS) rating **Moderate**

| Estimating Near-Bank Stress (NBS) | | | |
|--|--------------------------------|--------------|--|
| Stream: Eccleston | Location: Right Bank 11 | | |
| Station: 116+39.48 to 119+64.19 | Stream Type: | Valley Type: | |
| Observers: | Date: 5/4/2018 | | |

| Methods for Estimating Near-Bank Stress (NBS) | | |
|---|-----------|---------------------|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkr}) | Level II | General prediction |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkr}) | Level III | Detailed prediction |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkr}) | Level III | Detailed prediction |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| Level | Method | Input | | Ratio | Near-Bank Stress (NBS) | | | |
|-----------|--------|-------------------------------------|--------------------------------|--|---------------------------|-------------------|--|--------------------------------|
| | | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkr} (ft) | R_c / W_{bkr} | | | |
| Level II | (3) | Pool Slope S_p | Average Slope S | S_p / S | | | | |
| | (4) | Pool Slope S_p | Riffle Slope S_{rif} | S_p / S_{rif} | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkr} (ft) | d_{nb} / d_{bkr} | | | | |
| | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft^2) | Mean Depth d_{bkr} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkr} (lb/ft^2) | Ratio τ_{nb} / τ_{bkr} |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | | Near-Bank Stress (NBS) | | | | |

| | |
|---------------------------|---|
| Method | 5 |
| Dominant Near-Bank Stress | |
| Low | |

| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | |
|--|---------------|-------------|-------------|-------------|-------------|-------------|-------------|
| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |
| Overall Near-Bank Stress (NBS) rating | | | | | | Low | |

Estimating Near-Bank Stress (NBS)

Stream: **Eccleston** Location: **Left Bank 11**

Station: **114+61.16 to 120+25.66** Stream Type: Valley Type:

Observers: Date: **5/4/2018**

Methods for Estimating Near-Bank Stress (NBS)

| | | |
|---|-----------|---------------------|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | Level II | General prediction |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | Level III | Detailed prediction |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | Level III | Detailed prediction |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | | | | | | | |
|------------------|----------------------------------|-------------------------------------|-------------------------------|--|---------------------------|--|--|--------------------------------|------------------------|----------|----------------------------------|--|------------|--|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | <table border="1"> <tr> <td>Method</td> <td>5</td> </tr> <tr> <td colspan="2">Dominant Near-Bank Stress</td> </tr> <tr> <td colspan="2">Low</td> </tr> </table> | | | Method | 5 | Dominant Near-Bank Stress | | Low | |
| | Method | 5 | | | | | | | | | | | | |
| | Dominant Near-Bank Stress | | | | | | | | | | | | | |
| Low | | | | | | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | 0.57 | 0.46 | 1.2391304 | Low | | | | | |
| | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} | Near-Bank Stress (NBS) | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | Near-Bank Stress (NBS) | | | | | | | | | | | |

Converting Values to a Near-Bank Stress (NBS) Rating

| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
|--------------------------------|---------------|-------------|-------------|-------------|-------------|-------------|-------------|
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |

Overall Near-Bank Stress (NBS) rating **Low**

| Estimating Near-Bank Stress (NBS) | | | | | | | | |
|--|---|---|-------------------------------|--|---------------------------|-------------------|--|--------------------------------|
| Stream: Eccleston | | Location: Right Bank 12 | | | | | | |
| Station: 115+14.22 to 116+39.48 | | Stream Type: | | | Valley Type: | | | |
| Observers: | | Date: 5/4/2018 | | | | | | |
| Methods for Estimating Near-Bank Stress (NBS) | | | | | | | | |
| (1) | Channel pattern, transverse bar or split channel/central bar creating NBS | | | Level I | Reconnaissance | | | |
| (2) | Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | | | Level II | General prediction | | | |
| (3) | Ratio of pool slope to average water surface slope (S_p / S) | | | Level II | General prediction | | | |
| (4) | Ratio of pool slope to riffle slope (S_p / S_{rif}) | | | Level II | General prediction | | | |
| (5) | Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | | | Level III | Detailed prediction | | | |
| (6) | Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | | | Level III | Detailed prediction | | | |
| (7) | Velocity profiles / Isovels / Velocity gradient | | | Level IV | Validation | | | |
| Level I | (1) | Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High Extensive deposition (continuous, cross-channel).....NBS = Extreme Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme | | | | | | |
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | | | |
| | (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | |
| | (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | | | |
| | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft^2) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft^2) | Ratio τ_{nb} / τ_{bkf} |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | | Near-Bank Stress (NBS) | | | | |
| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | | |
| Near-Bank Stress (NBS) ratings | Method number | | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) | |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 | |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 | |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 | |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 | |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 | |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 | |
| Overall Near-Bank Stress (NBS) rating | | | | | | Low | | |

| | |
|----------------------------------|----------|
| Method | 5 |
| Dominant Near-Bank Stress | |
| Low | |

Estimating Near-Bank Stress (NBS)

Stream: **Eccleston** Location: **Left Bank 12**

Station: **111+99.76 to 114+61.16** Stream Type: Valley Type:

Observers: Date: **5/4/2018**

Methods for Estimating Near-Bank Stress (NBS)

| | | |
|---|-----------|---------------------|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | Level II | General prediction |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | Level III | Detailed prediction |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | Level III | Detailed prediction |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | | | | | | | |
|------------------|-----------------------------------|-------------------------------------|--|---------------------------|------------------------|---|--------------------------------|------------------------|--------|---|---------------------------|--|---------|--|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | <table border="1"> <tr> <td>Method</td> <td>2</td> </tr> <tr> <td colspan="2">Dominant Near-Bank Stress</td> </tr> <tr> <td colspan="2">Extreme</td> </tr> </table> | | | Method | 2 | Dominant Near-Bank Stress | | Extreme | |
| | Method | 2 | | | | | | | | | | | | |
| | Dominant Near-Bank Stress | | | | | | | | | | | | | |
| Extreme | | | | | | | | | | | | | | |
| | | 0.41 | 3.97 | 0.1032746 | Extreme | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | | | |
| | | | | | | | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | | | |
| | | | | | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | | | | | | | | | |
| | | | | | | | | | | | | | | |
| (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} | Near-Bank Stress (NBS) | | | | | | |
| | | | | | | | | | | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | Near-Bank Stress (NBS) | | | | | | | | | | | |
| | | | | | | | | | | | | | | |

Converting Values to a Near-Bank Stress (NBS) Rating

| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
|--------------------------------|---------------|-------------|-------------|-------------|-------------|-------------|-------------|
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |

Overall Near-Bank Stress (NBS) rating **Extreme**

| Estimating Near-Bank Stress (NBS) | | | |
|--|--------------------------------|--------------|--|
| Stream: Eccleston | Location: Right Bank 13 | | |
| Station: 113+44.63 to 115+14.22 | Stream Type: | Valley Type: | |
| Observers: | Date: 5/4/2018 | | |

| Methods for Estimating Near-Bank Stress (NBS) | | | |
|---|-----------|---------------------|--|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance | |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | Level II | General prediction | |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction | |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction | |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | Level III | Detailed prediction | |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | Level III | Detailed prediction | |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation | |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | | | | | | | |
|------------------|---------------------------|-------------------------------------|-------------------------------|--|---------------------------|---|--|--------------------------------|------------------------|---|---------------------------|--|----------|--|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | <table border="1"> <tr><td>Method</td><td>5</td></tr> <tr><td>Dominant Near-Bank Stress</td><td></td></tr> <tr><td>Moderate</td><td></td></tr> </table> | | | Method | 5 | Dominant Near-Bank Stress | | Moderate | |
| | Method | 5 | | | | | | | | | | | | |
| | Dominant Near-Bank Stress | | | | | | | | | | | | | |
| Moderate | | | | | | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | 0.45 | 0.25 | 1.8 | Moderate | | | | | |
| | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} | Near-Bank Stress (NBS) | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | Near-Bank Stress (NBS) | | | | | | | | | | | |

| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | |
|--|---------------|-------------|-------------|-------------|-------------|-----------------|-------------|
| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |
| Overall Near-Bank Stress (NBS) rating | | | | | | Moderate | |

| Estimating Near-Bank Stress (NBS) | | | |
|--|-------------------------------|--------------|--|
| Stream: Eccleston | Location: Left Bank 13 | | |
| Station: 110+41.23 to 111+99.76 | Stream Type: | Valley Type: | |
| Observers: | Date: 5/4/2018 | | |

| Methods for Estimating Near-Bank Stress (NBS) | | | |
|---|-----------|---------------------|--|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance | |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | Level II | General prediction | |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction | |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction | |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | Level III | Detailed prediction | |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | Level III | Detailed prediction | |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation | |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | | | | | | | |
|------------------|---------------------------|-------------------------------------|-------------------------------|--|---------------------------|---|--|--------------------------------|------------------------|---|---------------------------|--|----------|--|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | <table border="1"> <tr><td>Method</td><td>5</td></tr> <tr><td>Dominant Near-Bank Stress</td><td></td></tr> <tr><td>Moderate</td><td></td></tr> </table> | | | Method | 5 | Dominant Near-Bank Stress | | Moderate | |
| | Method | 5 | | | | | | | | | | | | |
| | Dominant Near-Bank Stress | | | | | | | | | | | | | |
| Moderate | | | | | | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | 0.73 | 0.48 | 1.5208333 | Moderate | | | | | |
| | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} | Near-Bank Stress (NBS) | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | Near-Bank Stress (NBS) | | | | | | | | | | | |

| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | |
|--|---------------|-------------|-------------|-------------|-------------|-----------------|-------------|
| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |
| Overall Near-Bank Stress (NBS) rating | | | | | | Moderate | |

| Estimating Near-Bank Stress (NBS) | | | | | | | | | |
|--|---|---|-------------------------------|---|--------------------------------|---------------------|---|--------------------------------|------------------------|
| Stream: Eccleston | | | | | Location: Right Bank 14 | | | | |
| Station: 112+84.76 to 113+44.63 | | | | | Stream Type: | | | Valley Type: | |
| Observers: | | | | | Date: 5/4/2018 | | | | |
| Methods for Estimating Near-Bank Stress (NBS) | | | | | | | | | |
| (1) | Channel pattern, transverse bar or split channel/central bar creating NBS | | | | Level I | Reconnaissance | | | |
| (2) | Ratio of radius of curvature to bankfull width (R_c / W_{bkr}) | | | | Level II | General prediction | | | |
| (3) | Ratio of pool slope to average water surface slope (S_p / S) | | | | Level II | General prediction | | | |
| (4) | Ratio of pool slope to riffle slope (S_p / S_{rif}) | | | | Level II | General prediction | | | |
| (5) | Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkr}) | | | | Level III | Detailed prediction | | | |
| (6) | Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkr}) | | | | Level III | Detailed prediction | | | |
| (7) | Velocity profiles / Isovels / Velocity gradient | | | | Level IV | Validation | | | |
| Level I | (1) | Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High Extensive deposition (continuous, cross-channel).....NBS = Extreme Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme | | | | | | | |
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkr} (ft) | Ratio R_c / W_{bkr} | Near-Bank Stress (NBS) | | | | |
| | | 0.21 | 4.93 | 0.0425963 | Extreme | | | | |
| | (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | |
| | (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkr} (ft) | Ratio d_{nb} / d_{bkr} | Near-Bank Stress (NBS) | | | | |
| | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkr} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkr} (lb/ft ²) | Ratio τ_{nb} / τ_{bkr} | Near-Bank Stress (NBS) |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | | | Near-Bank Stress (NBS) | | | | |
| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | | | |
| Near-Bank Stress (NBS) ratings | Method number | | | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) | | |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 | | |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 | | |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 | | |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 | | |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 | | |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 | | |
| Overall Near-Bank Stress (NBS) rating | | | | | | Extreme | | | |

| | |
|---------------------------|---|
| Method | 2 |
| Dominant Near-Bank Stress | |
| Extreme | |

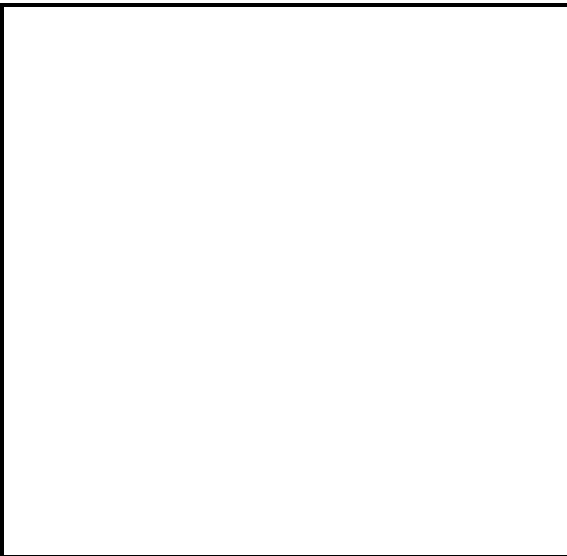
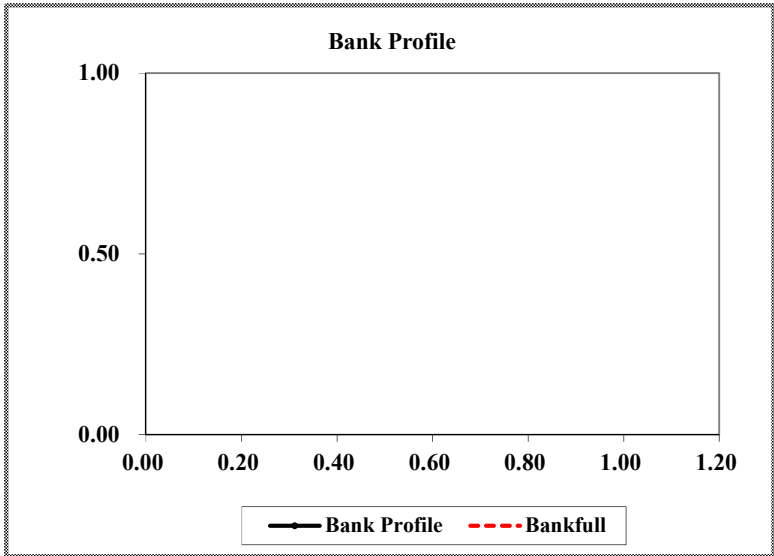
BANK EROSION HAZARD INDEX

| | | | | | | | | | | | | | | |
|-----------|---------------------------|--------------|-----|-------|----|--------|--|---------------------|----------|-------|----------|-------|-----------|---------|
| Stream: | Eccleston Mitigation Site | Observer(s): | PVC | Data: | SH | QA/QC: | | Total Score: | 48.45 | | | | | |
| Reach: | 108+67.52 to 110+41.23 | Comments: | | | | | | | Extreme | | | | | |
| Location: | Left Bank 14 | Bank Length | 188 | | | | | Total Score Values: | Very Low | Low | Moderate | High | Very High | Extreme |
| Date: | 5/4/2018 | | | | | | | | 5-10 | 10-20 | 20-30 | 30-40 | 40-45 | 45-50 |

| Erodibility Variables | | | | | |
|--|--------------------------|-------|--------------|------------------------|-------|
| Bank Height / Bankfull Height Ratio | | | | | |
| Bank Height | Bankfull Height | Value | Index | Bank Erosion Potential | Notes |
| 3.00 | 1.00 | 3.00 | 10.00 | Extreme | |
| Root Depth / Bank Height Ratio | | | | | |
| Root Depth | Bank Height | Value | Index | Bank Erosion Potential | Notes |
| 0.33 | 3.00 | 0.11 | 8.33 | Very High | |
| Weighted Root Density | | | | | |
| Root Density (%) | Root Depth / Bank Height | Value | Index | Bank Erosion Potential | Notes |
| 10.00 | 0.11 | 1.10 | 10.00 | Extreme | |
| Bank Angle | | | | | |
| Bank Angle (°) | | | Index | Bank Erosion Potential | Notes |
| 90.00 | | | 7.90 | High | |
| Surface Protection | | | | | |
| Surface Protection (%) | | | Index | Bank Erosion Potential | Notes |
| 20.00 | | | 7.22 | High | |
| | | | Adjustment | | Notes |
| Bank Materials | | | | | |
| | | | 0.00 | | |
| | | | Adjustment | | Notes |
| Bank Stratification | | | | | |
| | | | 5.00 | | |
| TOTAL SCORE | | | 48.45 | | |

| Bank Erosion Potential | | | | | | | |
|---|--|-----------|-----------|-----------|-----------|-----------|---------|
| | | Very Low | Low | Moderate | High | Very High | Extreme |
| Bank Height / Bankfull Height | Value | 1.00-1.10 | 1.11-1.19 | 1.20-1.50 | 1.60-2.00 | 2.10-2.80 | >2.80 |
| | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| Root Depth / Bank Height | Value | 1.00-0.90 | 0.89-0.50 | 0.49-0.30 | 0.29-0.15 | 0.14-0.05 | <0.05 |
| | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| Weighted Root Density | Value | 100-80 | 79-55 | 54-30 | 29-15 | 14-5 | <5 |
| | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| Bank Angle | Value | 0-20 | 21-60 | 61-80 | 81-90 | 91-119 | >119 |
| | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| Surface Protection | Value | 100-80 | 79-55 | 54-30 | 29-15 | 14-10 | <10 |
| | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| Adjustments | | | | | | | |
| Bedrock | Bedrock banks have a very low erosion potential. | | | | | | |
| Boulders | Boulder banks have a low erosion potential. | | | | | | |
| Cobble | Subtract 10 points. No adjustment if sand/gravel compose greater than 50% of bank. | | | | | | |
| Clay/Silt Loam | Add 5 points. | | | | | | |
| Gravel | Add 5-10 points depending on percentage of bank material composed of sand. | | | | | | |
| Sand | Add 10 points. | | | | | | |
| Silt / Clay | No adjustment. | | | | | | |
| Stratification | | | | | | | |
| Add 5-10 points depending on position of unstable layers in relation to bankfull stage. | | | | | | | |

| Bank Profile | | |
|---------------------|-----------------|-------|
| Horizontal Distance | Vertical Height | Notes |
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| | | |
| | | |
| Bankfull | | |
| Horizontal Distance | Vertical Height | Notes |
| | | |
| | | |



Estimating Near-Bank Stress (NBS)

Stream: **Eccleston** Location: **Left Bank 14**

Station: **108+67.52 to 110+41.23** Stream Type: Valley Type:

Observers: Date: **5/4/2018**

Methods for Estimating Near-Bank Stress (NBS)

| | | |
|---|-----------|---------------------|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | Level II | General prediction |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | Level III | Detailed prediction |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | Level III | Detailed prediction |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | | | | | | | |
|------------------|---------------------------|-------------------------------------|-------------------------------|--|---------------------------|---|--|--------------------------------|------------------------|---|---------------------------|--|----------|--|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | <table border="1"> <tr><td>Method</td><td>5</td></tr> <tr><td>Dominant Near-Bank Stress</td><td></td></tr> <tr><td>Moderate</td><td></td></tr> </table> | | | Method | 5 | Dominant Near-Bank Stress | | Moderate | |
| | Method | 5 | | | | | | | | | | | | |
| | Dominant Near-Bank Stress | | | | | | | | | | | | | |
| Moderate | | | | | | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | 0.73 | 0.48 | 1.5208333 | Moderate | | | | | |
| | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} | Near-Bank Stress (NBS) | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | Near-Bank Stress (NBS) | | | | | | | | | | | |

Converting Values to a Near-Bank Stress (NBS) Rating

| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
|--------------------------------|---------------|-------------|-------------|-------------|-------------|-------------|-------------|
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |

Overall Near-Bank Stress (NBS) rating **Moderate**

| Estimating Near-Bank Stress (NBS) | | | |
|---------------------------------------|--------------------------------|--------------|--|
| Stream: Eccleston | Location: Right Bank 15 | | |
| Station: 112+3.47 to 112+84.76 | Stream Type: | Valley Type: | |
| Observers: | Date: 5/4/2018 | | |

| Methods for Estimating Near-Bank Stress (NBS) | | | |
|---|-----------|---------------------|--|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance | |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | Level II | General prediction | |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction | |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction | |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | Level III | Detailed prediction | |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | Level III | Detailed prediction | |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation | |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | | | | | | | |
|------------------|---------------------------|-------------------------------------|-------------------------------|--|---------------------------|---|--|--------------------------------|------------------------|---|---------------------------|--|----------|--|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | <table border="1"> <tr><td>Method</td><td>5</td></tr> <tr><td>Dominant Near-Bank Stress</td><td></td></tr> <tr><td>Moderate</td><td></td></tr> </table> | | | Method | 5 | Dominant Near-Bank Stress | | Moderate | |
| | Method | 5 | | | | | | | | | | | | |
| | Dominant Near-Bank Stress | | | | | | | | | | | | | |
| Moderate | | | | | | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | 0.45 | 0.25 | 1.8 | Moderate | | | | | |
| | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} | Near-Bank Stress (NBS) | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | Near-Bank Stress (NBS) | | | | | | | | | | | |

| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | |
|--|---------------|-------------|-------------|-------------|-------------|-----------------|-------------|
| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |
| Overall Near-Bank Stress (NBS) rating | | | | | | Moderate | |

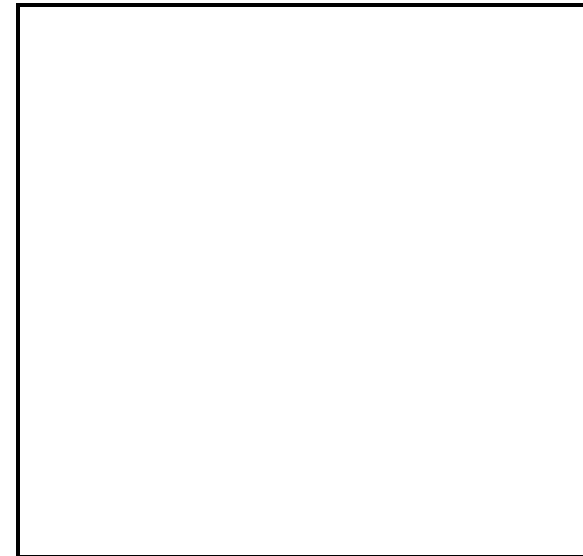
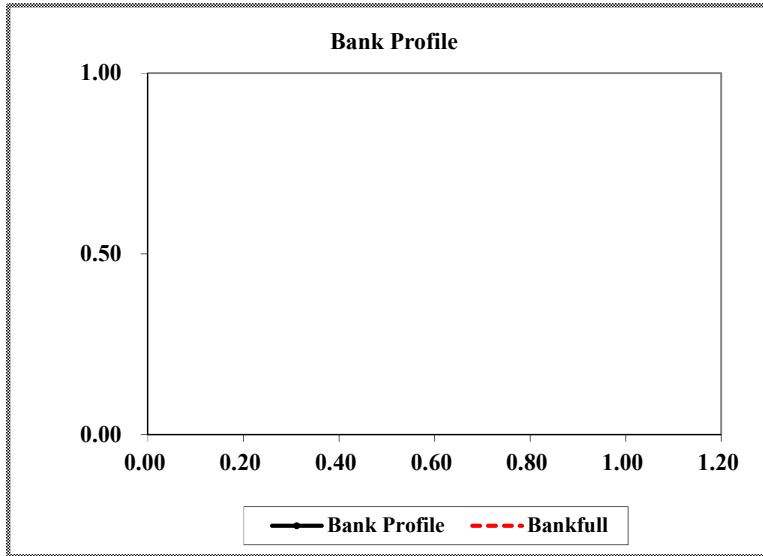
BANK EROSION HAZARD INDEX

| | | | | | | | | | | | | | | |
|------------------|---------------------------|---------------------|-----|--------------|----|---------------|----------------|---------------------|------------------|------------|-----------------|-------------|------------------|----------------|
| Stream: | Eccleston Mitigation Site | Observer(s): | PVC | Data: | SH | QA/QC: | | Total Score: | 45.10 | | | | | |
| Reach: | 107+61.02 to 108+67.52 | Comments: | | | | | | | Very High | | | | | |
| Location: | Left Bank 15 | Bank Length | 103 | | | | | Total Score | Very Low | Low | Moderate | High | Very High | Extreme |
| Date: | 5/4/2018 | | | | | | Values: | 5-10 | 10-20 | 20-30 | 30-40 | 40-45 | 45-50 | |

| Erodibility Variables | | | | | |
|-------------------------------------|--------------------------|-------|--------------|------------------------|-------|
| Bank Height / Bankfull Height Ratio | | | | | |
| Bank Height | Bankfull Height | Value | Index | Bank Erosion Potential | Notes |
| 2.50 | 1.00 | 2.50 | 8.57 | Very High | |
| Root Depth / Bank Height Ratio | | | | | |
| Root Depth | Bank Height | Value | Index | Bank Erosion Potential | Notes |
| 0.17 | 2.50 | 0.07 | 8.80 | Very High | |
| Weighted Root Density | | | | | |
| Root Density (%) | Root Depth / Bank Height | Value | Index | Bank Erosion Potential | Notes |
| 50.00 | 0.07 | 3.40 | 10.00 | Extreme | |
| Bank Angle | | | | | |
| Bank Angle (°) | | | Index | Bank Erosion Potential | Notes |
| 50.00 | | | 3.41 | Low | |
| Surface Protection | | | | | |
| Surface Protection (%) | | | Index | Bank Erosion Potential | Notes |
| 50.00 | | | 4.32 | Moderate | |
| | | | Adjustment | | Notes |
| Bank Materials | | | 10.00 | | |
| | | | Adjustment | | Notes |
| Bank Stratification | | | 0.00 | | |
| TOTAL SCORE | | | 45.10 | | |

| Bank Erosion Potential | | | | | | | |
|---|-------------------------------|--|------------|-----------------|-------------|------------------|----------------|
| | | Very Low | Low | Moderate | High | Very High | Extreme |
| Erodibility Variables | Bank Height / Bankfull Height | Value | 1.00-1.10 | 1.11-1.19 | 1.20-1.50 | 1.60-2.00 | 2.10-2.80 |
| | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | >2.80 |
| Erodibility Variables | Root Depth / Bank Height | Value | 1.00-0.90 | 0.89-0.50 | 0.49-0.30 | 0.29-0.15 | 0.14-0.05 |
| | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | <0.05 |
| Erodibility Variables | Weighted Root Density | Value | 100-80 | 79-55 | 54-30 | 29-15 | 14-5 |
| | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | <5 |
| Erodibility Variables | Bank Angle | Value | 0-20 | 21-60 | 61-80 | 81-90 | 91-119 |
| | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | >119 |
| Erodibility Variables | Surface Protection | Value | 100-80 | 79-55 | 54-30 | 29-15 | 14-10 |
| | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | <10 |
| Adjustments | | | | | | | |
| Bank Material | Bedrock | Bedrock banks have a very low erosion potential. | | | | | |
| | Boulders | Boulder banks have a low erosion potential. | | | | | |
| | Cobble | Subtract 10 points. No adjustment if sand/gravel compose greater than 50% of bank. | | | | | |
| | Clay/Silt Loam | Add 5 points. | | | | | |
| | Gravel | Add 5-10 points depending on percentage of bank material composed of sand. | | | | | |
| | Sand | Add 10 points. | | | | | |
| | Silt / Clay | No adjustment. | | | | | |
| Stratification | | | | | | | |
| Add 5-10 points depending on position of unstable layers in relation to bankfull stage. | | | | | | | |

| Bank Profile | | |
|---------------------|-----------------|-------|
| Horizontal Distance | Vertical Height | Notes |
| | | |
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| | | |
| | | |
| | | |
| | | |
| Bankfull | | |
| Horizontal Distance | Vertical Height | Notes |
| | | |
| | | |



Estimating Near-Bank Stress (NBS)

Stream: **Eccleston** Location: **Left Bank 15**

Station: **107+61.02 to 108+67.52** Stream Type: Valley Type:

Observers: Date: **5/4/2018**

Methods for Estimating Near-Bank Stress (NBS)

| | | |
|---|-----------|---------------------|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | Level II | General prediction |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | Level III | Detailed prediction |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | Level III | Detailed prediction |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | | | | | |
|------------------|---------------------------|-------------------------------------|-------------------------------|--|---------------------------|---|--|--------------------------------|---------------------------|--|-----|--|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | <table border="1"> <tr> <td>Method</td> <td>5</td> </tr> <tr> <td colspan="2">Dominant Near-Bank Stress</td> </tr> <tr> <td colspan="2">Low</td> </tr> </table> | Method | 5 | Dominant Near-Bank Stress | | Low | |
| | Method | 5 | | | | | | | | | | |
| | Dominant Near-Bank Stress | | | | | | | | | | | |
| Low | | | | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | | | | | | | |
| | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} | Near-Bank Stress (NBS) | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | Near-Bank Stress (NBS) | | | | | | | | | |

Converting Values to a Near-Bank Stress (NBS) Rating

| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
|--------------------------------|---------------|-------------|-------------|-------------|-------------|-------------|-------------|
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |

Overall Near-Bank Stress (NBS) rating **Low**

| Estimating Near-Bank Stress (NBS) | | | |
|---------------------------------------|--------------------------------|--------------|--|
| Stream: Eccleston | Location: Right Bank 16 | | |
| Station: 110+65.05 to 112+3.47 | Stream Type: | Valley Type: | |
| Observers: | Date: 5/4/2018 | | |

| Methods for Estimating Near-Bank Stress (NBS) | | | |
|---|-----------|---------------------|--|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance | |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | Level II | General prediction | |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction | |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction | |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | Level III | Detailed prediction | |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | Level III | Detailed prediction | |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation | |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | | | | | | | |
|------------------|---------------------------|-------------------------------------|-------------------------------|--|---------------------------|---|--|--------------------------------|------------------------|---|---------------------------|--|----------|--|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | <table border="1"> <tr><td>Method</td><td>5</td></tr> <tr><td>Dominant Near-Bank Stress</td><td></td></tr> <tr><td>Moderate</td><td></td></tr> </table> | | | Method | 5 | Dominant Near-Bank Stress | | Moderate | |
| | Method | 5 | | | | | | | | | | | | |
| | Dominant Near-Bank Stress | | | | | | | | | | | | | |
| Moderate | | | | | | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | 0.45 | 0.25 | 1.8 | Moderate | | | | | |
| | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} | Near-Bank Stress (NBS) | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | | Near-Bank Stress (NBS) | | | | | | | | | | |

| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | |
|--|---------------|-------------|-------------|-------------|-------------|-----------------|-------------|
| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |
| Overall Near-Bank Stress (NBS) rating | | | | | | Moderate | |

| Estimating Near-Bank Stress (NBS) | | | | | | | | | | | | | | | |
|--|---|---|-------------------------------|--|-------------------------------|--|--|--------------------------------|------------------------|--------|---|---------------------------|--|-----|--|
| Stream: Eccleston | | | | | Location: Left Bank 16 | | | | | | | | | | |
| Station: 106+23.76 to 107+61.02 | | | Stream Type: | | Valley Type: | | | | | | | | | | |
| Observers: | | | | | Date: 5/4/2018 | | | | | | | | | | |
| Methods for Estimating Near-Bank Stress (NBS) | | | | | | | | | | | | | | | |
| (1) | Channel pattern, transverse bar or split channel/central bar creating NBS | | | | Level I | Reconnaissance | | | | | | | | | |
| (2) | Ratio of radius of curvature to bankfull width (R_c / W_{bkr}) | | | | Level II | General prediction | | | | | | | | | |
| (3) | Ratio of pool slope to average water surface slope (S_p / S) | | | | Level II | General prediction | | | | | | | | | |
| (4) | Ratio of pool slope to riffle slope (S_p / S_{rif}) | | | | Level II | General prediction | | | | | | | | | |
| (5) | Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkr}) | | | | Level III | Detailed prediction | | | | | | | | | |
| (6) | Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkr}) | | | | Level III | Detailed prediction | | | | | | | | | |
| (7) | Velocity profiles / Isovels / Velocity gradient | | | | Level IV | Validation | | | | | | | | | |
| Level I | (1) | Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High Extensive deposition (continuous, cross-channel).....NBS = Extreme Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme | | | | | | | | | | | | | |
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkr} (ft) | Ratio R_c / W_{bkr} | Near-Bank Stress (NBS) | <table border="1"> <tr><td>Method</td><td>5</td></tr> <tr><td colspan="2">Dominant Near-Bank Stress</td></tr> <tr><td colspan="2">Low</td></tr> </table> | | | | Method | 5 | Dominant Near-Bank Stress | | Low | |
| | Method | 5 | | | | | | | | | | | | | |
| | Dominant Near-Bank Stress | | | | | | | | | | | | | | |
| Low | | | | | | | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkr} (ft) | Ratio d_{nb} / d_{bkr} | Near-Bank Stress (NBS) | | | | | | | | | | |
| | | 0.89 | 0.65 | 1.3692308 | Low | | | | | | | | | | |
| | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft^2) | Mean Depth d_{bkr} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkr} (lb/ft^2) | Ratio τ_{nb} / τ_{bkr} | Near-Bank Stress (NBS) | | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | | | Near-Bank Stress (NBS) | | | | | | | | | | |
| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | | | | | | | | | |
| Near-Bank Stress (NBS) ratings | Method number | | | | | | | | | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) | | | | | | | | |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 | | | | | | | | |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 | | | | | | | | |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 | | | | | | | | |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 | | | | | | | | |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 | | | | | | | | |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 | | | | | | | | |
| Overall Near-Bank Stress (NBS) rating | | | | | | Low | | | | | | | | | |

| Estimating Near-Bank Stress (NBS) | | | |
|--|--------------------------------|--------------|--|
| Stream: Eccleston | Location: Right Bank 17 | | |
| Station: 107+61.59 to 110+65.05 | Stream Type: | Valley Type: | |
| Observers: | Date: 5/4/2018 | | |

| Methods for Estimating Near-Bank Stress (NBS) | | | |
|---|-----------|---------------------|--|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance | |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | Level II | General prediction | |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction | |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction | |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | Level III | Detailed prediction | |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | Level III | Detailed prediction | |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation | |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | | | | | | | |
|------------------|---------------------------|-------------------------------------|-------------------------------|--|---------------------------|---|--|--------------------------------|------------------------|---|---------------------------|--|-----------|--|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | <table border="1"> <tr> <td>Method</td> <td>1</td> </tr> <tr> <td colspan="2">Dominant Near-Bank Stress</td> </tr> <tr> <td colspan="2">Very High</td> </tr> </table> | | | Method | 1 | Dominant Near-Bank Stress | | Very High | |
| | Method | 1 | | | | | | | | | | | | |
| | Dominant Near-Bank Stress | | | | | | | | | | | | | |
| Very High | | | | | | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | | | | | | | | | |
| | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} | Near-Bank Stress (NBS) | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | | Near-Bank Stress (NBS) | | | | | | | | | | |

| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | |
|--|---------------|-------------|-------------|-------------|-------------|------------------|-------------|
| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |
| Overall Near-Bank Stress (NBS) rating | | | | | | Very High | |

Estimating Near-Bank Stress (NBS)

Stream: **Eccleston** Location: **Left Bank 17**

Station: **102+41.73 to 106+23.76** Stream Type: Valley Type:

Observers: Date: **5/4/2018**

Methods for Estimating Near-Bank Stress (NBS)

| | | |
|---|-----------|---------------------|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | Level II | General prediction |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | Level III | Detailed prediction |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | Level III | Detailed prediction |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | | | | | | | |
|------------------|-----------------------------------|-------------------------------------|--|---------------------------|------------------------|---|--------------------------------|------------------------|--------|---|---------------------------|--|------|--|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | <table border="1" style="margin-left: auto; margin-right: auto;"> <tr> <td>Method</td> <td>5</td> </tr> <tr> <td colspan="2" style="text-align: center;">Dominant Near-Bank Stress</td> </tr> <tr> <td colspan="2" style="text-align: center;">High</td> </tr> </table> | | | Method | 5 | Dominant Near-Bank Stress | | High | |
| | Method | 5 | | | | | | | | | | | | |
| | Dominant Near-Bank Stress | | | | | | | | | | | | | |
| High | | | | | | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | | | | | | | | | |
| | | 2.08 | 1.11 | 1.8738739 | High | | | | | | | | | |
| (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} | Near-Bank Stress (NBS) | | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | Near-Bank Stress (NBS) | | | | | | | | | | | |

Converting Values to a Near-Bank Stress (NBS) Rating

| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
|--------------------------------|---------------|-------------|-------------|-------------|-------------|-------------|-------------|
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |

Overall Near-Bank Stress (NBS) rating **High**

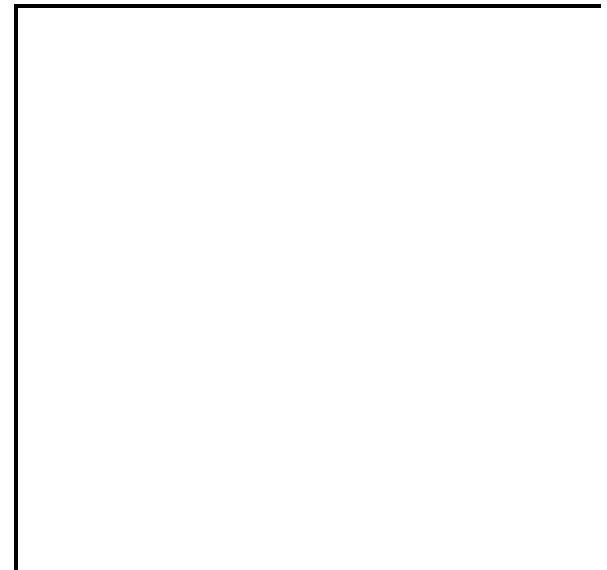
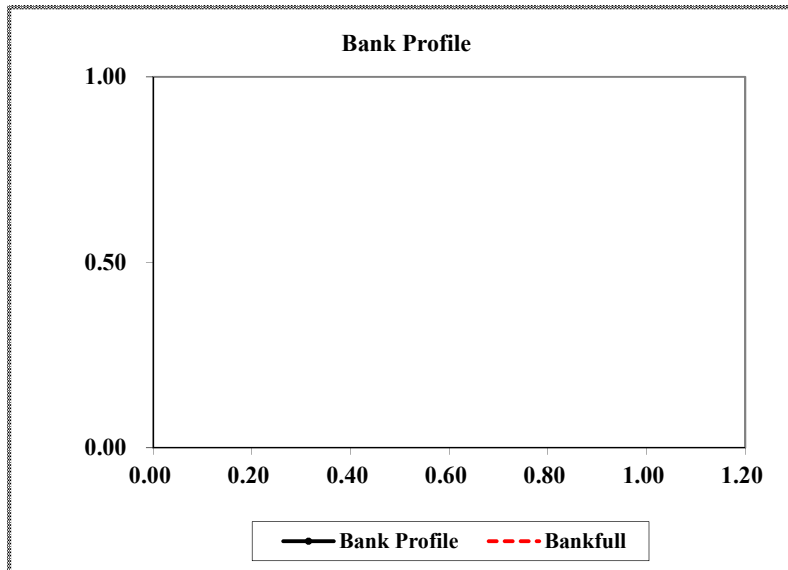
BANK EROSION HAZARD INDEX

| | | | | | | | | | | | | | | | |
|------------------|---------------------------|---------------------|-----|--------------|----|---------------|--|---------------------|----------------------------|-----------------|------------|-----------------|-------------|------------------|----------------|
| Stream: | Eccleston Mitigation Site | Observer(s): | PVC | Data: | SH | QA/QC: | | Total Score: | 38.06 | | | | | | |
| Reach: | 106+3.93 to 107+61.59 | Comments: | | | | | | High | | | | | | | |
| Location: | Right Bank 18 | Bank Length | | | | | | 157 | Total Score Values: | Very Low | Low | Moderate | High | Very High | Extreme |
| Date: | 5/4/2018 | | | | | | | | 5-10 | 10-20 | 20-30 | 30-40 | 40-45 | 45-50 | |

| Erodibility Variables | | | | | |
|--|--------------------------|-------|--------------|------------------------|-------|
| Bank Height / Bankfull Height Ratio | | | | | |
| Bank Height | Bankfull Height | Value | Index | Bank Erosion Potential | Notes |
| 2.50 | 1.00 | 2.50 | 8.57 | Very High | |
| Root Depth / Bank Height Ratio | | | | | |
| Root Depth | Bank Height | Value | Index | Bank Erosion Potential | Notes |
| 0.42 | 2.50 | 0.17 | 7.66 | High | |
| Weighted Root Density | | | | | |
| Root Density (%) | Root Depth / Bank Height | Value | Index | Bank Erosion Potential | Notes |
| 55.00 | 0.17 | 9.24 | 8.53 | Very High | |
| Bank Angle | | | | | |
| Bank Angle (°) | | | Index | Bank Erosion Potential | Notes |
| 65.00 | | | 4.40 | Moderate | |
| Surface Protection | | | | | |
| Surface Protection (%) | | | Index | Bank Erosion Potential | Notes |
| 55.00 | | | 3.90 | Low | |
| | | | Adjustment | | Notes |
| Bank Materials | | | | | |
| | | | 5.00 | | |
| | | | Adjustment | | Notes |
| Bank Stratification | | | | | |
| | | | 0.00 | | |
| TOTAL SCORE | | | 38.06 | | |

| Bank Erosion Potential | | | | | | | | | |
|---|--------------------------------------|--|--|-----------|-----------|-----------|-----------|-------|--|
| | | Very Low | Low | Moderate | High | Very High | Extreme | | |
| Erodibility Variables | Bank Height / Bankfull Height | Value | 1.00-1.10 | 1.11-1.19 | 1.20-1.50 | 1.60-2.00 | 2.10-2.80 | >2.80 | |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 | |
| | Root Depth / Bank Height | Value | 1.00-0.90 | 0.89-0.50 | 0.49-0.30 | 0.29-0.15 | 0.14-0.05 | <0.05 | |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 | |
| | Weighted Root Density | Value | 100-80 | 79-55 | 54-30 | 29-15 | 14-5 | <5 | |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 | |
| | Bank Angle | Value | 0-20 | 21-60 | 61-80 | 81-90 | 91-119 | >119 | |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 | |
| | Surface Protection | Value | 100-80 | 79-55 | 54-30 | 29-15 | 14-10 | <10 | |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 | |
| | Adjustments | | | | | | | | |
| | Bank Material | Bedrock | Bedrock banks have a very low erosion potential. | | | | | | |
| | | Boulders | Boulder banks have a low erosion potential. | | | | | | |
| | | Cobble | Subtract 10 points. No adjustment if sand/gravel compose greater than 50% of bank. | | | | | | |
| Clay/Silt Loam | | Add 5 points. | | | | | | | |
| Gravel | | Add 5-10 points depending on percentage of bank material composed of sand. | | | | | | | |
| Sand | | Add 10 points. | | | | | | | |
| Silt / Clay | No adjustment. | | | | | | | | |
| Stratification | | | | | | | | | |
| Add 5-10 points depending on position of unstable layers in relation to bankfull stage. | | | | | | | | | |

| Bank Profile | | |
|---------------------|-----------------|-------|
| Horizontal Distance | Vertical Height | Notes |
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| Bankfull | | |
| Horizontal Distance | Vertical Height | Notes |
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| Estimating Near-Bank Stress (NBS) | | | | | | | | | | | | | |
|--|---|---|-------------------------------|--|---------------------------|-------------------|---|--------------------------------|------------------------|---------------------------|--|-----|--|
| Stream: Eccleston | | Location: Right Bank 18 | | | | | | | | | | | |
| Station: 106+3.93 to 107+61.59 | | Stream Type: | | | Valley Type: | | | | | | | | |
| Observers: | | Date: 5/4/2018 | | | | | | | | | | | |
| Methods for Estimating Near-Bank Stress (NBS) | | | | | | | | | | | | | |
| (1) | Channel pattern, transverse bar or split channel/central bar creating NBS | | | Level I | Reconnaissance | | | | | | | | |
| (2) | Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | | | Level II | General prediction | | | | | | | | |
| (3) | Ratio of pool slope to average water surface slope (S_p / S) | | | Level II | General prediction | | | | | | | | |
| (4) | Ratio of pool slope to riffle slope (S_p / S_{rif}) | | | Level II | General prediction | | | | | | | | |
| (5) | Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | | | Level III | Detailed prediction | | | | | | | | |
| (6) | Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | | | Level III | Detailed prediction | | | | | | | | |
| (7) | Velocity profiles / Isovels / Velocity gradient | | | Level IV | Validation | | | | | | | | |
| Level I | (1) | Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High | | | | | | | | | | | |
| | | Extensive deposition (continuous, cross-channel).....NBS = Extreme | | | | | | | | | | | |
| | | Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme | | | | | | | | | | | |
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | | | | | | | | |
| | | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | |
| | | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | |
| | | <table border="1"> <tr> <td>Method</td> <td>5</td> </tr> <tr> <td colspan="2">Dominant Near-Bank Stress</td> </tr> <tr> <td colspan="2">Low</td> </tr> </table> | | | | | | Method | 5 | Dominant Near-Bank Stress | | Low | |
| Method | 5 | | | | | | | | | | | | |
| Dominant Near-Bank Stress | | | | | | | | | | | | | |
| Low | | | | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | | | | | | | | |
| | | 0.75 | 0.64 | 1.171875 | Low | | | | | | | | |
| Level III | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Near-Bank Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} | Near-Bank Stress (NBS) | | | | |
| | | | | | | | | | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | | Near-Bank Stress (NBS) | | | | | | | | | |
| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | | | | | | | |
| Near-Bank Stress (NBS) ratings | Method number | | | | | | | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) | | | | | | |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 | | | | | | |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 | | | | | | |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 | | | | | | |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 | | | | | | |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 | | | | | | |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 | | | | | | |
| Overall Near-Bank Stress (NBS) rating | | | | | | Low | | | | | | | |

| Estimating Near-Bank Stress (NBS) | | | | | | | | |
|--|---|---|-------------------------------|--|---------------------------|-------------------|--|--------------------------------|
| Stream: Eccleston | | Location: Left Bank 18 | | | | | | |
| Station: 202+64.02 to 205+15.89 | | Stream Type: | | Valley Type: | | | | |
| Observers: PVC & SH | | Date: 5/4/2018 | | | | | | |
| Methods for Estimating Near-Bank Stress (NBS) | | | | | | | | |
| (1) | Channel pattern, transverse bar or split channel/central bar creating NBS | | | Level I | Reconnaissance | | | |
| (2) | Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | | | Level II | General prediction | | | |
| (3) | Ratio of pool slope to average water surface slope (S_p / S) | | | Level II | General prediction | | | |
| (4) | Ratio of pool slope to riffle slope (S_p / S_{rif}) | | | Level II | General prediction | | | |
| (5) | Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | | | Level III | Detailed prediction | | | |
| (6) | Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | | | Level III | Detailed prediction | | | |
| (7) | Velocity profiles / Isovels / Velocity gradient | | | Level IV | Validation | | | |
| Level I | (1) | Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High Extensive deposition (continuous, cross-channel).....NBS = Extreme Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme | | | | | | |
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | | | |
| | (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | |
| | (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | | | |
| | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | | Near-Bank Stress (NBS) | | | | |
| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | | |
| Near-Bank Stress (NBS) ratings | Method number | | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) | |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 | |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 | |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 | |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 | |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 | |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 | |
| Overall Near-Bank Stress (NBS) rating | | | | | | Low | | |

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| Method | 5 |
| Dominant Near-Bank Stress | |
| Low | |

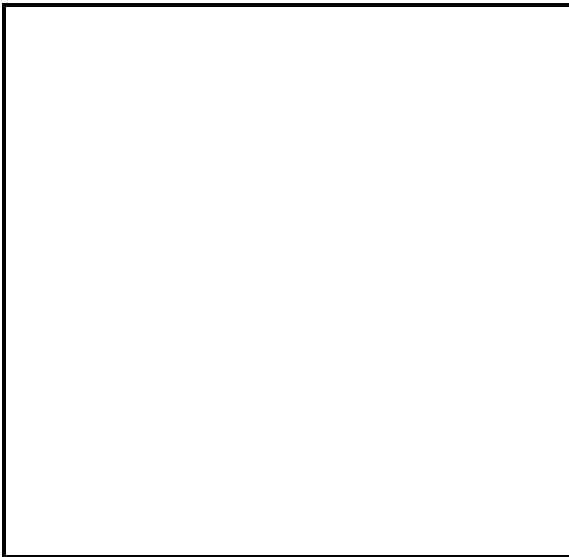
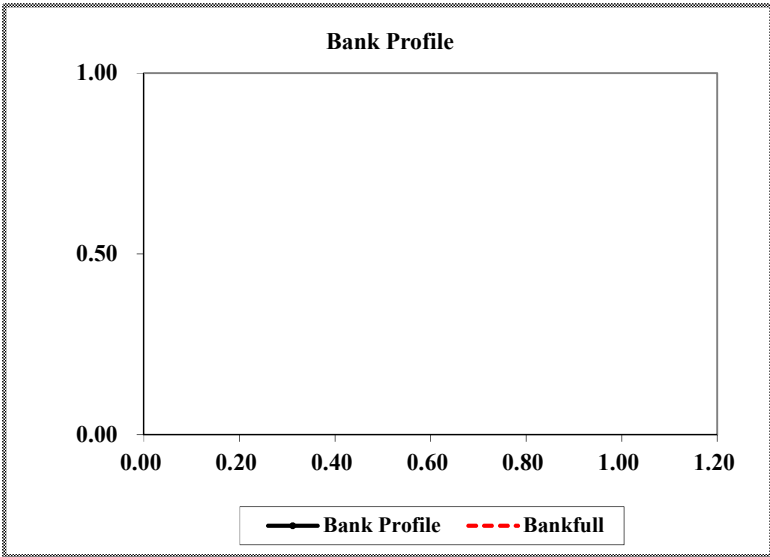
BANK EROSION HAZARD INDEX

| | | | | | | | | | | | | | |
|------------------|---------------------------|---------------------|-----|--------------|----|---------------|------|----------------------------|-----------|----------|-------|-----------|---------|
| Stream: | Eccleston Mitigation Site | Observer(s): | PVC | Data: | SH | QA/QC: | | Total Score: | 42.67 | | | | |
| Reach: | 102+40.18 to 106+3.93 | Comments: | | | | | | Total Score Values: | Very High | | | | |
| Location: | Right Bank 19 | Bank Length | 362 | | | | | Very Low | Low | Moderate | High | Very High | Extreme |
| Date: | 5/4/2018 | | | | | | 5-10 | 10-20 | 20-30 | 30-40 | 40-45 | 45-50 | |

| Erodibility Variables | | | | | |
|--|--------------------------|-------|--------------|------------------------|-------|
| Bank Height / Bankfull Height Ratio | | | | | |
| Bank Height | Bankfull Height | Value | Index | Bank Erosion Potential | Notes |
| 2.50 | 1.00 | 2.50 | 8.57 | Very High | |
| Root Depth / Bank Height Ratio | | | | | |
| Root Depth | Bank Height | Value | Index | Bank Erosion Potential | Notes |
| 0.17 | 2.50 | 0.07 | 8.80 | Very High | |
| Weighted Root Density | | | | | |
| Root Density (%) | Root Depth / Bank Height | Value | Index | Bank Erosion Potential | Notes |
| 30.00 | 0.07 | 2.04 | 10.00 | Extreme | |
| Bank Angle | | | | | |
| Bank Angle (°) | | | Index | Bank Erosion Potential | Notes |
| 65.00 | | | 4.40 | Moderate | |
| Surface Protection | | | | | |
| Surface Protection (%) | | | Index | Bank Erosion Potential | Notes |
| 30.00 | | | 5.90 | Moderate | |
| | | | Adjustment | | Notes |
| Bank Materials | | | 5.00 | | |
| | | | Adjustment | | Notes |
| Bank Stratification | | | 0.00 | | |
| TOTAL SCORE | | | 42.67 | | |

| Bank Erosion Potential | | | | | | | | |
|---|--------------------------------------|--|-----------|-----------|-----------|-----------|-----------|-------|
| | | Very Low | Low | Moderate | High | Very High | Extreme | |
| Erodibility Variables | Bank Height / Bankfull Height | Value | 1.00-1.10 | 1.11-1.19 | 1.20-1.50 | 1.60-2.00 | 2.10-2.80 | >2.80 |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| | Root Depth / Bank Height | Value | 1.00-0.90 | 0.89-0.50 | 0.49-0.30 | 0.29-0.15 | 0.14-0.05 | <0.05 |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| | Weighted Root Density | Value | 100-80 | 79-55 | 54-30 | 29-15 | 14-5 | <5 |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| | Bank Angle | Value | 0-20 | 21-60 | 61-80 | 81-90 | 91-119 | >119 |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| | Surface Protection | Value | 100-80 | 79-55 | 54-30 | 29-15 | 14-10 | <10 |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| Adjustments | | | | | | | | |
| Bank Material | Bedrock | Bedrock banks have a very low erosion potential. | | | | | | |
| | Boulders | Boulder banks have a low erosion potential. | | | | | | |
| | Cobble | Subtract 10 points. No adjustment if sand/gravel compose greater than 50% of bank. | | | | | | |
| | Clay/Silt Loam | Add 5 points. | | | | | | |
| | Gravel | Add 5-10 points depending on percentage of bank material composed of sand. | | | | | | |
| | Sand | Add 10 points. | | | | | | |
| | Silt / Clay | No adjustment. | | | | | | |
| Stratification | | | | | | | | |
| Add 5-10 points depending on position of unstable layers in relation to bankfull stage. | | | | | | | | |

| Bank Profile | | |
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| Horizontal Distance | Vertical Height | Notes |
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| Bankfull | | |
| Horizontal Distance | Vertical Height | Notes |
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| Estimating Near-Bank Stress (NBS) | | | | | | | | |
|--|---|---|-------------------------------|--|---------------------------|-------------------|--|--------------------------------|
| Stream: Eccleston | | Location: Right Bank 19 | | | | | | |
| Station: 102+40.18 to 106+3.93 | | Stream Type: | | | Valley Type: | | | |
| Observers: PVC & SH | | Date: 5/4/2018 | | | | | | |
| Methods for Estimating Near-Bank Stress (NBS) | | | | | | | | |
| (1) | Channel pattern, transverse bar or split channel/central bar creating NBS | | | Level I | Reconnaissance | | | |
| (2) | Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | | | Level II | General prediction | | | |
| (3) | Ratio of pool slope to average water surface slope (S_p / S) | | | Level II | General prediction | | | |
| (4) | Ratio of pool slope to riffle slope (S_p / S_{rif}) | | | Level II | General prediction | | | |
| (5) | Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | | | Level III | Detailed prediction | | | |
| (6) | Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | | | Level III | Detailed prediction | | | |
| (7) | Velocity profiles / Isovels / Velocity gradient | | | Level IV | Validation | | | |
| Level I | (1) | Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High Extensive deposition (continuous, cross-channel).....NBS = Extreme Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme | | | | | | |
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | | | |
| | (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | |
| | (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | | | |
| | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | | Near-Bank Stress (NBS) | | | | |
| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | | |
| Near-Bank Stress (NBS) ratings | Method number | | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) | |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 | |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 | |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 | |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 | |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 | |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 | |
| Overall Near-Bank Stress (NBS) rating | | | | | | Low | | |

| | |
|----------------------------------|----------|
| Method | 5 |
| Dominant Near-Bank Stress | |
| Low | |

| Estimating Near-Bank Stress (NBS) | | | |
|--|-------------------------------|--------------|--|
| Stream: Eccleston | Location: Left Bank 19 | | |
| Station: 205+15.89 to 205+62.34 | Stream Type: | Valley Type: | |
| Observers: PVC & SH | Date: 5/4/2018 | | |

| Methods for Estimating Near-Bank Stress (NBS) | | | |
|---|-----------|---------------------|--|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance | |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | Level II | General prediction | |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction | |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction | |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | Level III | Detailed prediction | |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | Level III | Detailed prediction | |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation | |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | | | | | | | |
|------------------|---------------------------|-------------------------------------|-------------------------------|--|---------------------------|--|--|--------------------------------|------------------------|---|---------------------------|--|-----|--|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | <table border="1"> <tr><td>Method</td><td>5</td></tr> <tr><td>Dominant Near-Bank Stress</td><td></td></tr> <tr><td>Low</td><td></td></tr> </table> | | | Method | 5 | Dominant Near-Bank Stress | | Low | |
| | Method | 5 | | | | | | | | | | | | |
| | Dominant Near-Bank Stress | | | | | | | | | | | | | |
| Low | | | | | | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | 0.72 | 0.55 | 1.3090909 | Low | | | | | |
| | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} | Near-Bank Stress (NBS) | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | | Near-Bank Stress (NBS) | | | | | | | | | | |

| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | |
|--|---------------|-------------|-------------|-------------|-------------|-------------|-------------|
| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |
| Overall Near-Bank Stress (NBS) rating | | | | | | Low | |

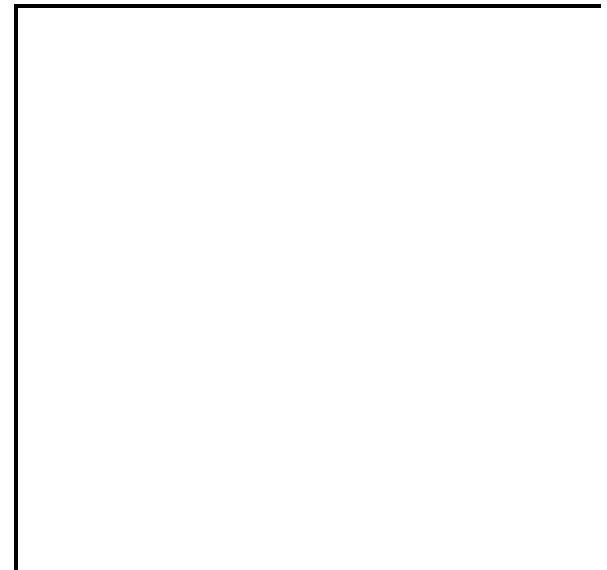
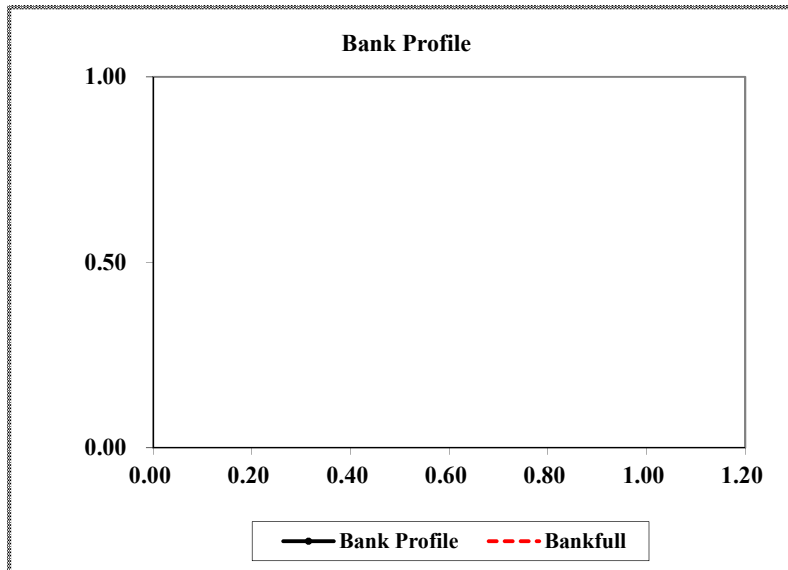
BANK EROSION HAZARD INDEX

| | | | | | | | | | | | | | | |
|------------------|---------------------------|---------------------|-----|--------------|----|---------------|------|----------------------------|----------|-------|----------|-------|-----------|---------|
| Stream: | Eccleston Mitigation Site | Observer(s): | PVC | Data: | SH | QA/QC: | | Total Score: | 41.36 | | | | | |
| Reach: | 202+64.58 to 205+11.94 | Comments: | | | | | | Very High | | | | | | |
| Location: | Right Bank 20 | Bank Length | 244 | | | | | Total Score Values: | Very Low | Low | Moderate | High | Very High | Extreme |
| Date: | 5/4/2018 | | | | | | 5-10 | 10-20 | 20-30 | 30-40 | 40-45 | 45-50 | | |

| Erodibility Variables | | | | | |
|--|--------------------------|-------|------------|------------------------|-------|
| Bank Height / Bankfull Height Ratio | | | | | |
| Bank Height | Bankfull Height | Value | Index | Bank Erosion Potential | Notes |
| 3.00 | 1.00 | 3.00 | 10.00 | Extreme | |
| Root Depth / Bank Height Ratio | | | | | |
| Root Depth | Bank Height | Value | Index | Bank Erosion Potential | Notes |
| 0.25 | 3.00 | 0.08 | 8.63 | Very High | |
| Weighted Root Density | | | | | |
| Root Density (%) | Root Depth / Bank Height | Value | Index | Bank Erosion Potential | Notes |
| 30.00 | 0.08 | 2.50 | 10.00 | Extreme | |
| Bank Angle | | | | | |
| Bank Angle (°) | | | Index | Bank Erosion Potential | Notes |
| 50.00 | | | 3.41 | Low | |
| Surface Protection | | | | | |
| Surface Protection (%) | | | Index | Bank Erosion Potential | Notes |
| 50.00 | | | 4.32 | Moderate | |
| | | | Adjustment | | Notes |
| Bank Materials | | | 5.00 | | |
| | | | Adjustment | | Notes |
| Bank Stratification | | | 0.00 | | |
| TOTAL SCORE | | | 41.36 | | |

| Bank Erosion Potential | | | | | | | | |
|---|--------------------------------------|--|--|-----------|-----------|-----------|-----------|-------|
| | | Very Low | Low | Moderate | High | Very High | Extreme | |
| Erodibility Variables | Bank Height / Bankfull Height | Value | 1.00-1.10 | 1.11-1.19 | 1.20-1.50 | 1.60-2.00 | 2.10-2.80 | >2.80 |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| | Root Depth / Bank Height | Value | 1.00-0.90 | 0.89-0.50 | 0.49-0.30 | 0.29-0.15 | 0.14-0.05 | <0.05 |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| | Weighted Root Density | Value | 100-80 | 79-55 | 54-30 | 29-15 | 14-5 | <5 |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| | Bank Angle | Value | 0-20 | 21-60 | 61-80 | 81-90 | 91-119 | >119 |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| | Surface Protection | Value | 100-80 | 79-55 | 54-30 | 29-15 | 14-10 | <10 |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| | Bank Material | Adjustments | | | | | | |
| | | Bedrock | Bedrock banks have a very low erosion potential. | | | | | |
| Boulders | | Boulder banks have a low erosion potential. | | | | | | |
| Cobble | | Subtract 10 points. No adjustment if sand/gravel compose greater than 50% of bank. | | | | | | |
| Clay/Silt Loam | | Add 5 points. | | | | | | |
| Gravel | | Add 5-10 points depending on percentage of bank material composed of sand. | | | | | | |
| Sand | | Add 10 points. | | | | | | |
| Silt / Clay | No adjustment. | | | | | | | |
| Stratification | | | | | | | | |
| Add 5-10 points depending on position of unstable layers in relation to bankfull stage. | | | | | | | | |

| Bank Profile | | |
|---------------------|-----------------|-------|
| Horizontal Distance | Vertical Height | Notes |
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| Bankfull | | |
| Horizontal Distance | Vertical Height | Notes |
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| Estimating Near-Bank Stress (NBS) | | | |
|--|--------------------------------|--------------|--|
| Stream: Eccleston | Location: Right Bank 20 | | |
| Station: 202+64.58 to 205+11.94 | Stream Type: | Valley Type: | |
| Observers: PVC & SH | Date: 5/4/2018 | | |

| Methods for Estimating Near-Bank Stress (NBS) | | | |
|---|-----------|---------------------|--|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance | |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | Level II | General prediction | |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction | |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction | |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | Level III | Detailed prediction | |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | Level III | Detailed prediction | |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation | |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | | | | | | | |
|------------------|---------------------------|-------------------------------------|-------------------------------|--|---------------------------|--|--|--------------------------------|------------------------|---|---------------------------|--|---------|--|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | <table border="1"> <tr><td>Method</td><td>5</td></tr> <tr><td>Dominant Near-Bank Stress</td><td></td></tr> <tr><td>Extreme</td><td></td></tr> </table> | | | Method | 5 | Dominant Near-Bank Stress | | Extreme | |
| | Method | 5 | | | | | | | | | | | | |
| | Dominant Near-Bank Stress | | | | | | | | | | | | | |
| Extreme | | | | | | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | 0.64 | 0.2 | 3.2 | Extreme | | | | | |
| | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} | Near-Bank Stress (NBS) | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | | Near-Bank Stress (NBS) | | | | | | | | | | |

| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | |
|--|---------------|-------------|-------------|-------------|-------------|----------------|-------------|
| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |
| Overall Near-Bank Stress (NBS) rating | | | | | | Extreme | |

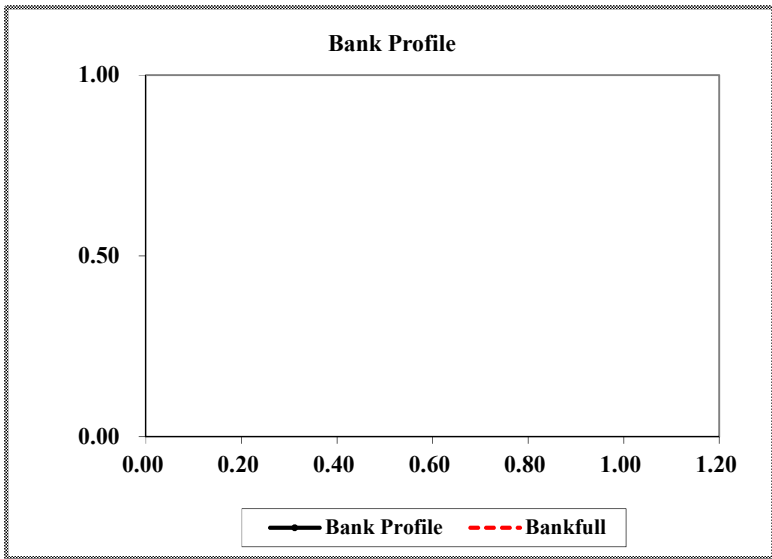
BANK EROSION HAZARD INDEX

| | | | | | | | | | | | | | | | |
|------------------|---------------------------|---------------------|-----|--------------|----|---------------|--|---------------------|----------------------------|-----------------|------------|-----------------|-------------|------------------|----------------|
| Stream: | Eccleston Mitigation Site | Observer(s): | PVC | Data: | SH | QA/QC: | | Total Score: | 37.77 | | | | | | |
| Reach: | 404+4.57 to 405+60.53 | Comments: | | | | | | | High | | | | | | |
| Location: | Left Bank 20 | Bank Length | 155 | | | | | | Total Score Values: | Very Low | Low | Moderate | High | Very High | Extreme |
| Date: | 5/4/2018 | | | | | | | 5-10 | 10-20 | 20-30 | 30-40 | 40-45 | 45-50 | | |

| Erodibility Variables | | | | | |
|--|--------------------------|-------|--------------|------------------------|-------|
| Bank Height / Bankfull Height Ratio | | | | | |
| Bank Height | Bankfull Height | Value | Index | Bank Erosion Potential | Notes |
| 0.50 | 0.50 | 1.00 | 1.00 | Very Low | |
| Root Depth / Bank Height Ratio | | | | | |
| Root Depth | Bank Height | Value | Index | Bank Erosion Potential | Notes |
| 0.42 | 0.50 | 0.84 | 2.24 | Low | |
| Weighted Root Density | | | | | |
| Root Density (%) | Root Depth / Bank Height | Value | Index | Bank Erosion Potential | Notes |
| 10.00 | 0.84 | 8.40 | 8.62 | Very High | |
| Bank Angle | | | | | |
| Bank Angle (°) | | | Index | Bank Erosion Potential | Notes |
| 90.00 | | | 7.90 | High | |
| Surface Protection | | | | | |
| Surface Protection (%) | | | Index | Bank Erosion Potential | Notes |
| 15.00 | | | 8.00 | Very High | |
| | | | | Adjustment | Notes |
| Bank Materials | | | | 10.00 | |
| | | | | Adjustment | Notes |
| Bank Stratification | | | | 0.00 | |
| TOTAL SCORE | | | 37.77 | | |

| Bank Erosion Potential | | | | | | | |
|---|--|-----------|-----------|-----------|-----------|-----------|---------|
| | | Very Low | Low | Moderate | High | Very High | Extreme |
| Bank Height / Bankfull Height | Value | 1.00-1.10 | 1.11-1.19 | 1.20-1.50 | 1.60-2.00 | 2.10-2.80 | >2.80 |
| | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| Root Depth / Bank Height | Value | 1.00-0.90 | 0.89-0.50 | 0.49-0.30 | 0.29-0.15 | 0.14-0.05 | <0.05 |
| | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| Weighted Root Density | Value | 100-80 | 79-55 | 54-30 | 29-15 | 14-5 | <5 |
| | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| Bank Angle | Value | 0-20 | 21-60 | 61-80 | 81-90 | 91-119 | >119 |
| | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| Surface Protection | Value | 100-80 | 79-55 | 54-30 | 29-15 | 14-10 | <10 |
| | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| Adjustments | | | | | | | |
| Bedrock | Bedrock banks have a very low erosion potential. | | | | | | |
| Boulders | Boulder banks have a low erosion potential. | | | | | | |
| Cobble | Subtract 10 points. No adjustment if sand/gravel compose greater than 50% of bank. | | | | | | |
| Clay/Silt Loam | Add 5 points. | | | | | | |
| Gravel | Add 5-10 points depending on percentage of bank material composed of sand. | | | | | | |
| Sand | Add 10 points. | | | | | | |
| Silt / Clay | No adjustment. | | | | | | |
| Stratification | | | | | | | |
| Add 5-10 points depending on position of unstable layers in relation to bankfull stage. | | | | | | | |

| Bank Profile | | |
|---------------------|-----------------|-------|
| Horizontal Distance | Vertical Height | Notes |
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| Bankfull | | |
| Horizontal Distance | Vertical Height | Notes |
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| Estimating Near-Bank Stress (NBS) | | | |
|---------------------------------------|-------------------------------|--------------|--|
| Stream: Eccleston | Location: Left Bank 20 | | |
| Station: 404+4.57 to 405+60.53 | Stream Type: | Valley Type: | |
| Observers: PVC & SH | Date: 5/4/2018 | | |

| Methods for Estimating Near-Bank Stress (NBS) | | |
|---|-----------|---------------------|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkr}) | Level II | General prediction |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkr}) | Level III | Detailed prediction |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkr}) | Level III | Detailed prediction |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation |

| | | | |
|---------|-----|--|--|
| Level I | (1) | Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High | |
| | | Extensive deposition (continuous, cross-channel).....NBS = Extreme | |
| | | Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme | |

| | | | | | | | | | | | | | | | |
|-----------|-----------------------------------|-------------------------------------|---|---------------------------|------------------------|---|--------------------------------|------------------------|--|--------|---|---------------------------|--|-----|--|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkr} (ft) | Ratio R_c / W_{bkr} | Near-Bank Stress (NBS) | <table border="1"> <tr> <td>Method</td> <td>5</td> </tr> <tr> <td colspan="2">Dominant Near-Bank Stress</td> </tr> <tr> <td colspan="2">Low</td> </tr> </table> | | | | Method | 5 | Dominant Near-Bank Stress | | Low | |
| | Method | 5 | | | | | | | | | | | | | |
| | Dominant Near-Bank Stress | | | | | | | | | | | | | | |
| Low | | | | | | | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkr} (ft) | Ratio d_{nb} / d_{bkr} | Near-Bank Stress (NBS) | | | | | | | | | | |
| | | 0.72 | 0.55 | 1.3090909 | Low | | | | | | | | | | |
| (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkr} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkr} (lb/ft ²) | Ratio τ_{nb} / τ_{bkr} | Near-Bank Stress (NBS) | | | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | | Near-Bank Stress (NBS) | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |

| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | |
|--|---------------|-------------|-------------|-------------|-------------|-------------|-------------|
| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |
| Overall Near-Bank Stress (NBS) rating | | | | | | Low | |

| Estimating Near-Bank Stress (NBS) | | | |
|--|--------------------------------|--------------|--|
| Stream: Eccleston | Location: Right Bank 21 | | |
| Station: 205+11.94 to 205+58.48 | Stream Type: | Valley Type: | |
| Observers: PVC & SH | Date: 5/4/2018 | | |

| Methods for Estimating Near-Bank Stress (NBS) | | |
|---|-----------|---------------------|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkr}) | Level II | General prediction |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkr}) | Level III | Detailed prediction |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkr}) | Level III | Detailed prediction |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | | | | | | | | |
|-----------|-----------------------------------|-------------------------------------|--|---------------------------|------------------------|--|--------------------------------|------------------------|--|--------|---|---------------------------|--|---------|--|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkr} (ft) | Ratio R_c / W_{bkr} | Near-Bank Stress (NBS) | <table border="1"> <tr><td>Method</td><td>5</td></tr> <tr><td colspan="2">Dominant Near-Bank Stress</td></tr> <tr><td colspan="2">Extreme</td></tr> </table> | | | | Method | 5 | Dominant Near-Bank Stress | | Extreme | |
| | Method | 5 | | | | | | | | | | | | | |
| | Dominant Near-Bank Stress | | | | | | | | | | | | | | |
| Extreme | | | | | | | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkr} (ft) | Ratio d_{nb} / d_{bkr} | Near-Bank Stress (NBS) | | | | | | | | | | |
| | | 0.64 | 0.2 | 3.2 | Extreme | | | | | | | | | | |
| (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft^2) | Mean Depth d_{bkr} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkr} (lb/ft^2) | Ratio τ_{nb} / τ_{bkr} | Near-Bank Stress (NBS) | | | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | | Near-Bank Stress (NBS) | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |

| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | |
|--|---------------|-------------|-------------|-------------|-------------|----------------|-------------|
| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |
| Overall Near-Bank Stress (NBS) rating | | | | | | Extreme | |

| Estimating Near-Bank Stress (NBS) | | | |
|--|-------------------------------|--------------|--|
| Stream: Eccleston | Location: Left Bank 21 | | |
| Station: 405+60.53 to 410+65.09 | Stream Type: | Valley Type: | |
| Observers: PVC & SH | Date: 5/4/2018 | | |

| Methods for Estimating Near-Bank Stress (NBS) | | |
|---|-----------|---------------------|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkr}) | Level II | General prediction |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkr}) | Level III | Detailed prediction |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkr}) | Level III | Detailed prediction |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | | | | | | | | |
|-----------|-----------------------------------|-------------------------------------|--|---------------------------|------------------------|---|--------------------------------|------------------------|--|--------|---|---------------------------|--|-----|--|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkr} (ft) | Ratio R_c / W_{bkr} | Near-Bank Stress (NBS) | <table border="1"> <tr> <td>Method</td> <td>5</td> </tr> <tr> <td colspan="2">Dominant Near-Bank Stress</td> </tr> <tr> <td colspan="2">Low</td> </tr> </table> | | | | Method | 5 | Dominant Near-Bank Stress | | Low | |
| | Method | 5 | | | | | | | | | | | | | |
| | Dominant Near-Bank Stress | | | | | | | | | | | | | | |
| Low | | | | | | | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkr} (ft) | Ratio d_{nb} / d_{bkr} | Near-Bank Stress (NBS) | | | | | | | | | | |
| | | 0.72 | 0.55 | 1.3090909 | Low | | | | | | | | | | |
| (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft^2) | Mean Depth d_{bkr} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkr} (lb/ft^2) | Ratio τ_{nb} / τ_{bkr} | Near-Bank Stress (NBS) | | | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | | Near-Bank Stress (NBS) | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |

| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | |
|--|---------------|-------------|-------------|-------------|-------------|-------------|-------------|
| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |
| Overall Near-Bank Stress (NBS) rating | | | | | | Low | |

| Estimating Near-Bank Stress (NBS) | | | |
|---------------------------------------|--------------------------------|--------------|--|
| Stream: Eccleston | Location: Right Bank 22 | | |
| Station: 404+7.41 to 405+56.34 | Stream Type: | Valley Type: | |
| Observers: PVC & SH | Date: 5/4/2018 | | |

| Methods for Estimating Near-Bank Stress (NBS) | | |
|---|-----------|---------------------|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkr}) | Level II | General prediction |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkr}) | Level III | Detailed prediction |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkr}) | Level III | Detailed prediction |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | | | | | | | | |
|-----------|-----------------------------------|-------------------------------------|--|---------------------------|------------------------|--|--------------------------------|------------------------|--|--------|---|---------------------------|--|---------|--|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkr} (ft) | Ratio R_c / W_{bkr} | Near-Bank Stress (NBS) | <table border="1"> <tr><td>Method</td><td>5</td></tr> <tr><td colspan="2">Dominant Near-Bank Stress</td></tr> <tr><td colspan="2">Extreme</td></tr> </table> | | | | Method | 5 | Dominant Near-Bank Stress | | Extreme | |
| | Method | 5 | | | | | | | | | | | | | |
| | Dominant Near-Bank Stress | | | | | | | | | | | | | | |
| Extreme | | | | | | | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkr} (ft) | Ratio d_{nb} / d_{bkr} | Near-Bank Stress (NBS) | | | | | | | | | | |
| | | 0.64 | 0.2 | 3.2 | Extreme | | | | | | | | | | |
| (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft^2) | Mean Depth d_{bkr} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkr} (lb/ft^2) | Ratio τ_{nb} / τ_{bkr} | Near-Bank Stress (NBS) | | | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | | Near-Bank Stress (NBS) | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |

| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | |
|--|---------------|-------------|-------------|-------------|-------------|----------------|-------------|
| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |
| Overall Near-Bank Stress (NBS) rating | | | | | | Extreme | |

| Estimating Near-Bank Stress (NBS) | | | | | | | | |
|--|---|---|-------------------------------|--|---------------------------|-------------------|--|--------------------------------|
| Stream: Eccleston | | Location: Left Bank 22 | | | | | | |
| Station: 309+20.39 to 311+1.38 | | Stream Type: | | Valley Type: | | | | |
| Observers: PVC & SH | | Date: 5/4/2018 | | | | | | |
| Methods for Estimating Near-Bank Stress (NBS) | | | | | | | | |
| (1) | Channel pattern, transverse bar or split channel/central bar creating NBS | | | Level I | Reconnaissance | | | |
| (2) | Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | | | Level II | General prediction | | | |
| (3) | Ratio of pool slope to average water surface slope (S_p / S) | | | Level II | General prediction | | | |
| (4) | Ratio of pool slope to riffle slope (S_p / S_{rif}) | | | Level II | General prediction | | | |
| (5) | Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | | | Level III | Detailed prediction | | | |
| (6) | Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | | | Level III | Detailed prediction | | | |
| (7) | Velocity profiles / Isovels / Velocity gradient | | | Level IV | Validation | | | |
| Level I | (1) | Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High Extensive deposition (continuous, cross-channel).....NBS = Extreme Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme | | | | | | |
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | | | |
| | (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | |
| | (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | | | |
| | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft^2) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft^2) | Ratio τ_{nb} / τ_{bkf} |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | | Near-Bank Stress (NBS) | | | | |
| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | | |
| Near-Bank Stress (NBS) ratings | Method number | | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) | |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 | |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 | |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 | |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 | |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 | |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 | |
| Overall Near-Bank Stress (NBS) rating | | | | | | Low | | |

| | |
|---------------------------|---|
| Method | 5 |
| Dominant Near-Bank Stress | |
| Low | |

| Estimating Near-Bank Stress (NBS) | | | |
|--|--------------------------------|--------------|--|
| Stream: Eccleston | Location: Right Bank 23 | | |
| Station: 405+56.34 to 410+65.81 | Stream Type: | Valley Type: | |
| Observers: PVC & SH | Date: 5/4/2018 | | |

| Methods for Estimating Near-Bank Stress (NBS) | | | |
|---|-----------|---------------------|--|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance | |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | Level II | General prediction | |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction | |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction | |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | Level III | Detailed prediction | |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | Level III | Detailed prediction | |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation | |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | | | | | | | |
|------------------|---------------------------|-------------------------------------|-------------------------------|--|---------------------------|--|--|--------------------------------|------------------------|---|---------------------------|--|---------|--|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | <table border="1"> <tr><td>Method</td><td>5</td></tr> <tr><td>Dominant Near-Bank Stress</td><td></td></tr> <tr><td>Extreme</td><td></td></tr> </table> | | | Method | 5 | Dominant Near-Bank Stress | | Extreme | |
| | Method | 5 | | | | | | | | | | | | |
| | Dominant Near-Bank Stress | | | | | | | | | | | | | |
| Extreme | | | | | | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | 0.64 | 0.2 | 3.2 | Extreme | | | | | |
| | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} | Near-Bank Stress (NBS) | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | Near-Bank Stress (NBS) | | | | | | | | | | | |

| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | |
|--|---------------|-------------|-------------|-------------|-------------|----------------|-------------|
| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |
| Overall Near-Bank Stress (NBS) rating | | | | | | Extreme | |

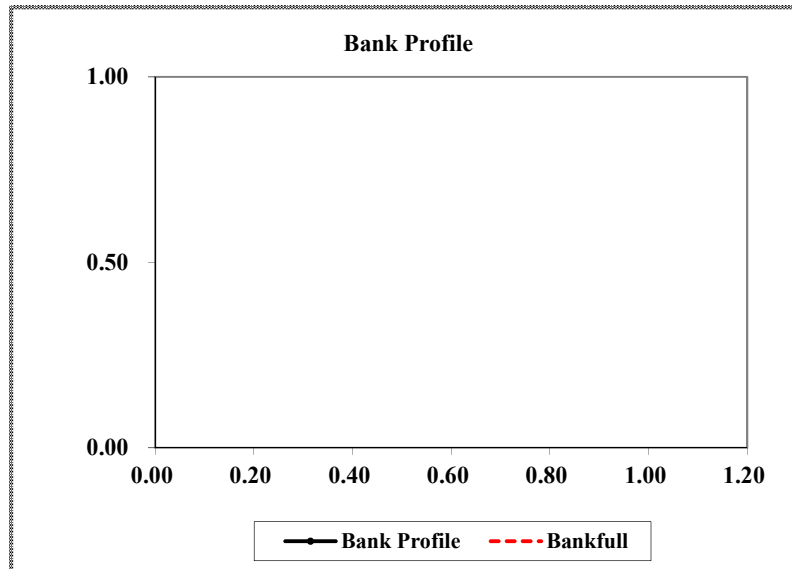
BANK EROSION HAZARD INDEX

| | | | | | | | | | | | |
|------------------|---------------------------|---------------------|-----|----------------------------|----|---------------|-------|---------------------|-------|--------------|---------|
| Stream: | Eccleston Mitigation Site | Observer(s): | PVC | Data: | SH | QA/QC: | | Total Score: | | 40.65 | |
| Reach: | 307+55.25 to 309+20.39 | Comments: | | | | | | | | | |
| Location: | Left Bank 23 | Bank Length | | 163 | | | | | | | |
| Date: | 5/4/2018 | | | Total Score Values: | | Very Low | Low | Moderate | High | Very High | Extreme |
| | | | | | | 5-10 | 10-20 | 20-30 | 30-40 | 40-45 | 45-50 |

| Erodibility Variables | | | | | |
|-------------------------------------|--------------------------|-------|--------------|------------------------|-------|
| Bank Height / Bankfull Height Ratio | | | | | |
| Bank Height | Bankfull Height | Value | Index | Bank Erosion Potential | Notes |
| 2.50 | 1.00 | 2.50 | 8.57 | Very High | |
| Root Depth / Bank Height Ratio | | | | | |
| Root Depth | Bank Height | Value | Index | Bank Erosion Potential | Notes |
| 0.17 | 2.50 | 0.07 | 8.80 | Very High | |
| Weighted Root Density | | | | | |
| Root Density (%) | Root Depth / Bank Height | Value | Index | Bank Erosion Potential | Notes |
| 40.00 | 0.07 | 2.72 | 10.00 | Extreme | |
| Bank Angle | | | | | |
| Bank Angle (°) | | | Index | Bank Erosion Potential | Notes |
| 45.00 | | | 3.17 | Low | |
| Surface Protection | | | | | |
| Surface Protection (%) | | | Index | Bank Erosion Potential | Notes |
| 40.00 | | | 5.11 | Moderate | |
| | | | Adjustment | | Notes |
| Bank Materials | | | 5.00 | | |
| | | | Adjustment | | Notes |
| Bank Stratification | | | 0.00 | | |
| TOTAL SCORE | | | 40.65 | | |

| Bank Erosion Potential | | | | | | | | |
|---|--------------------------------------|--|--|-----------|-----------|-----------|-----------|-------|
| | | Very Low | Low | Moderate | High | Very High | Extreme | |
| | | | | | | | | |
| Erodibility Variables | Bank Height / Bankfull Height | Value | 1.00-1.10 | 1.11-1.19 | 1.20-1.50 | 1.60-2.00 | 2.10-2.80 | >2.80 |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| | Root Depth / Bank Height | Value | 1.00-0.90 | 0.89-0.50 | 0.49-0.30 | 0.29-0.15 | 0.14-0.05 | <0.05 |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| | Weighted Root Density | Value | 100-80 | 79-55 | 54-30 | 29-15 | 14-5 | <5 |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| | Bank Angle | Value | 0-20 | 21-60 | 61-80 | 81-90 | 91-119 | >119 |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| | Surface Protection | Value | 100-80 | 79-55 | 54-30 | 29-15 | 14-10 | <10 |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| | Adjustments | | | | | | | |
| | Bank Material | Bedrock | Bedrock banks have a very low erosion potential. | | | | | |
| Boulders | | Boulder banks have a low erosion potential. | | | | | | |
| Cobble | | Subtract 10 points. No adjustment if sand/gravel compose greater than 50% of bank. | | | | | | |
| Clay/Silt Loam | | Add 5 points. | | | | | | |
| Gravel | | Add 5-10 points depending on percentage of bank material composed of sand. | | | | | | |
| Sand | | Add 10 points. | | | | | | |
| Silt / Clay | No adjustment. | | | | | | | |
| Stratification | | | | | | | | |
| Add 5-10 points depending on position of unstable layers in relation to bankfull stage. | | | | | | | | |

| Bank Profile | | |
|---------------------|-----------------|-------|
| Horizontal Distance | Vertical Height | Notes |
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| Bankfull | | |
| Horizontal Distance | Vertical Height | Notes |
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| Estimating Near-Bank Stress (NBS) | | | | | | | | |
|--|---|---|-------------------------------|--|---------------------------|---------------------|---|--------------------------------|
| Stream: Eccleston | | Location: Left Bank 23 | | | | | | |
| Station: 307+55.25 to 309+20.39 | | Stream Type: | | | Valley Type: | | | |
| Observers: PVC & SH | | Date: 5/4/2018 | | | | | | |
| Methods for Estimating Near-Bank Stress (NBS) | | | | | | | | |
| (1) | Channel pattern, transverse bar or split channel/central bar creating NBS | | | | Level I | Reconnaissance | | |
| (2) | Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | | | | Level II | General prediction | | |
| (3) | Ratio of pool slope to average water surface slope (S_p / S) | | | | Level II | General prediction | | |
| (4) | Ratio of pool slope to riffle slope (S_p / S_{rif}) | | | | Level II | General prediction | | |
| (5) | Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | | | | Level III | Detailed prediction | | |
| (6) | Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | | | | Level III | Detailed prediction | | |
| (7) | Velocity profiles / Isovels / Velocity gradient | | | | Level IV | Validation | | |
| Level I | (1) | Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High Extensive deposition (continuous, cross-channel).....NBS = Extreme Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme | | | | | | |
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | | | |
| | (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | |
| | (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | | | |
| | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Near-Bank Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | | Near-Bank Stress (NBS) | | | | |
| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | | |
| Near-Bank Stress (NBS) ratings | Method number | | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) | |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 | |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 | |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 | |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 | |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 | |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 | |
| Overall Near-Bank Stress (NBS) rating | | | | | | Low | | |

| | |
|----------------------------------|----------|
| Method | 5 |
| Dominant Near-Bank Stress | |
| Low | |

| Estimating Near-Bank Stress (NBS) | | | | | | | | | |
|--|---|--|-------------------------------|--|---------------------------|-------------------|--|--------------------------------|------------------------|
| Stream: Eccleston | | Location: Right Bank 24 | | | | | | | |
| Station: 306+16.05 to 310+97.33 | | Stream Type: | | Valley Type: | | | | | |
| Observers: PVC & SH | | Date: 5/4/2018 | | | | | | | |
| Methods for Estimating Near-Bank Stress (NBS) | | | | | | | | | |
| (1) | Channel pattern, transverse bar or split channel/central bar creating NBS | | | Level I | Reconnaissance | | | | |
| (2) | Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | | | Level II | General prediction | | | | |
| (3) | Ratio of pool slope to average water surface slope (S_p / S) | | | Level II | General prediction | | | | |
| (4) | Ratio of pool slope to riffle slope (S_p / S_{rif}) | | | Level II | General prediction | | | | |
| (5) | Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | | | Level III | Detailed prediction | | | | |
| (6) | Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | | | Level III | Detailed prediction | | | | |
| (7) | Velocity profiles / Isovels / Velocity gradient | | | Level IV | Validation | | | | |
| Level I | (1) | Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High | | | | | | | |
| | | Extensive deposition (continuous, cross-channel).....NBS = Extreme | | | | | | | |
| | | Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme | | | | | | | |
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| Level II | (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | |
| | | | | | | | | | |
| Level II | (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | |
| | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | | | | |
| | | 0.55 | 0.43 | 1.2790698 | Low | | | | |
| Level III | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft^2) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft^2) | Ratio τ_{nb} / τ_{bkf} | Near-Bank Stress (NBS) |
| | | | | | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | | Near-Bank Stress (NBS) | | | | | |
| | | | | | | | | | |
| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | | | |
| Near-Bank Stress (NBS) ratings | Method number | | | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) | | |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 | | |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 | | |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 | | |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 | | |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 | | |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 | | |
| Overall Near-Bank Stress (NBS) rating | | | | | | Low | | | |

| | |
|---------------------------|---|
| Method | 5 |
| Dominant Near-Bank Stress | |
| Low | |

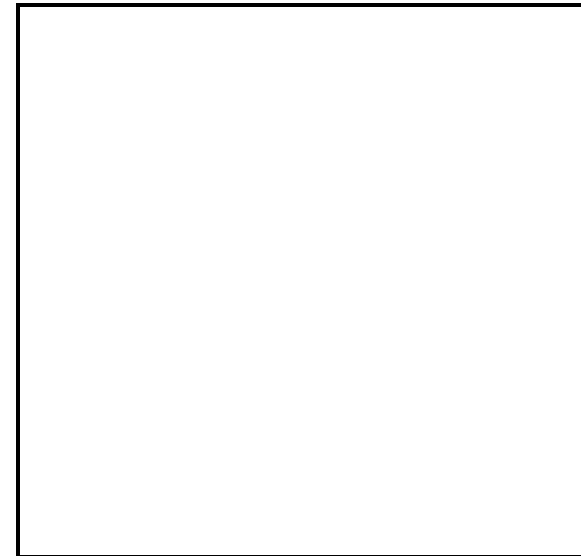
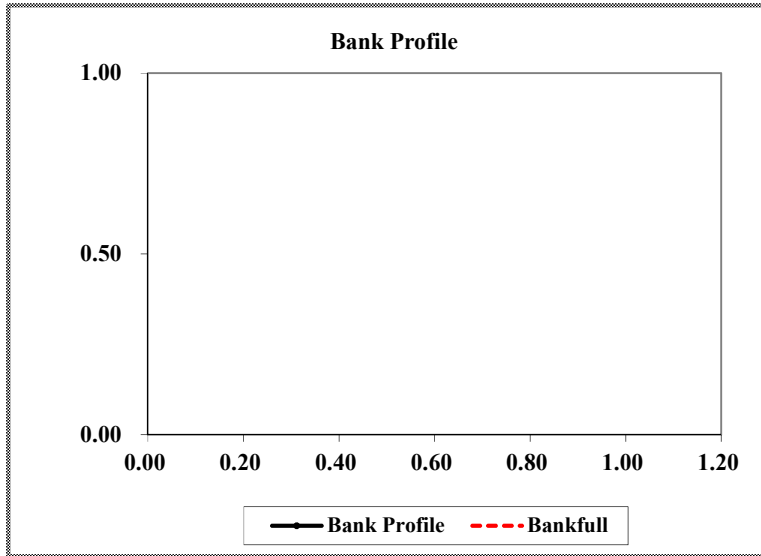
BANK EROSION HAZARD INDEX

| | | | | | | | | | | | | | | |
|-----------|---------------------------|--------------|-----|-------|----|--------|--|--------------|----------|-------|----------|-------|-----------|---------|
| Stream: | Eccleston Mitigation Site | Observer(s): | PVC | Data: | SH | QA/QC: | | Total Score: | 36.77 | | | | | |
| Reach: | 306+18.16 to 307+55.25 | Comments: | | | | | | Total Score | High | | | | | |
| Location: | Left Bank 24 | Bank Length | 137 | | | | | Values: | Very Low | Low | Moderate | High | Very High | Extreme |
| Date: | 5/4/2018 | | | | | | | | 5-10 | 10-20 | 20-30 | 30-40 | 40-45 | 45-50 |

| Erodibility Variables | | | | | |
|--|--------------------------|-------|------------|------------------------|-------|
| Bank Height / Bankfull Height Ratio | | | | | |
| Bank Height | Bankfull Height | Value | Index | Bank Erosion Potential | Notes |
| 2.50 | 1.00 | 2.50 | 8.57 | Very High | |
| Root Depth / Bank Height Ratio | | | | | |
| Root Depth | Bank Height | Value | Index | Bank Erosion Potential | Notes |
| 0.58 | 2.50 | 0.23 | 6.79 | High | |
| Weighted Root Density | | | | | |
| Root Density (%) | Root Depth / Bank Height | Value | Index | Bank Erosion Potential | Notes |
| 60.00 | 0.23 | 13.92 | 8.01 | Very High | |
| Bank Angle | | | | | |
| Bank Angle (°) | | | Index | Bank Erosion Potential | Notes |
| 70.00 | | | 4.90 | Moderate | |
| Surface Protection | | | | | |
| Surface Protection (%) | | | Index | Bank Erosion Potential | Notes |
| 60.00 | | | 3.50 | Low | |
| | | | Adjustment | | Notes |
| Bank Materials | | | 5.00 | | |
| | | | Adjustment | | Notes |
| Bank Stratification | | | 0.00 | | |
| TOTAL SCORE | | | 36.77 | | |

| Bank Erosion Potential | | | | | | | | |
|---|--------------------------------------|--|--|-----------|-----------|-----------|-----------|-------|
| | | Very Low | Low | Moderate | High | Very High | Extreme | |
| Erodibility Variables | Bank Height / Bankfull Height | Value | 1.00-1.10 | 1.11-1.19 | 1.20-1.50 | 1.60-2.00 | 2.10-2.80 | >2.80 |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| | Root Depth / Bank Height | Value | 1.00-0.90 | 0.89-0.50 | 0.49-0.30 | 0.29-0.15 | 0.14-0.05 | <0.05 |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| | Weighted Root Density | Value | 100-80 | 79-55 | 54-30 | 29-15 | 14-5 | <5 |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| | Bank Angle | Value | 0-20 | 21-60 | 61-80 | 81-90 | 91-119 | >119 |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| | Surface Protection | Value | 100-80 | 79-55 | 54-30 | 29-15 | 14-10 | <10 |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| | Adjustments | | | | | | | |
| | Bank Material | Bedrock | Bedrock banks have a very low erosion potential. | | | | | |
| Boulders | | Boulder banks have a low erosion potential. | | | | | | |
| Cobble | | Subtract 10 points. No adjustment if sand/gravel compose greater than 50% of bank. | | | | | | |
| Clay/Silt Loam | | Add 5 points. | | | | | | |
| Gravel | | Add 5-10 points depending on percentage of bank material composed of sand. | | | | | | |
| | Sand | Add 10 points. | | | | | | |
| | Silt / Clay | No adjustment. | | | | | | |
| Stratification | | | | | | | | |
| Add 5-10 points depending on position of unstable layers in relation to bankfull stage. | | | | | | | | |

| Bank Profile | | |
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| Horizontal Distance | Vertical Height | Notes |
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| Bankfull | | |
| Horizontal Distance | Vertical Height | Notes |
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| Estimating Near-Bank Stress (NBS) | | | | | | | | |
|--|---|---|-------------------------------|--|---------------------------|-------------------|---|--------------------------------|
| Stream: Eccleston | | Location: Left Bank 24 | | | | | | |
| Station: 306+18.16 to 307+55.25 | | Stream Type: | | Valley Type: | | | | |
| Observers: PVC & SH | | Date: 5/4/2018 | | | | | | |
| Methods for Estimating Near-Bank Stress (NBS) | | | | | | | | |
| (1) | Channel pattern, transverse bar or split channel/central bar creating NBS | | | Level I | Reconnaissance | | | |
| (2) | Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | | | Level II | General prediction | | | |
| (3) | Ratio of pool slope to average water surface slope (S_p / S) | | | Level II | General prediction | | | |
| (4) | Ratio of pool slope to riffle slope (S_p / S_{rif}) | | | Level II | General prediction | | | |
| (5) | Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | | | Level III | Detailed prediction | | | |
| (6) | Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | | | Level III | Detailed prediction | | | |
| (7) | Velocity profiles / Isovels / Velocity gradient | | | Level IV | Validation | | | |
| Level I | (1) | Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High Extensive deposition (continuous, cross-channel).....NBS = Extreme Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme | | | | | | |
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | | | |
| | (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | |
| | (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | | | |
| | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft^2) | Mean Depth d_{bkf} (ft) | Average Slope S | Near-Bank Shear Stress τ_{bkf} (lb/ft^2) | Ratio τ_{nb} / τ_{bkf} |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | | Near-Bank Stress (NBS) | | | | |
| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | | |
| Near-Bank Stress (NBS) ratings | Method number | | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) | |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 | |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 | |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 | |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 | |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 | |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 | |
| Overall Near-Bank Stress (NBS) rating | | | | | | Low | | |

| | |
|----------------------------------|----------|
| Method | 5 |
| Dominant Near-Bank Stress | |
| Low | |

| Estimating Near-Bank Stress (NBS) | | | | | | | | | |
|--|---|--|-------------------------------|--|---------------------------|-------------------|--|--------------------------------|------------------------|
| Stream: Eccleston | | Location: Right Bank 25 | | | | | | | |
| Station: 305+52.82 to 306+16.05 | | Stream Type: | | Valley Type: | | | | | |
| Observers: PVC & SH | | Date: 5/4/2018 | | | | | | | |
| Methods for Estimating Near-Bank Stress (NBS) | | | | | | | | | |
| (1) | Channel pattern, transverse bar or split channel/central bar creating NBS | | | Level I | Reconnaissance | | | | |
| (2) | Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | | | Level II | General prediction | | | | |
| (3) | Ratio of pool slope to average water surface slope (S_p / S) | | | Level II | General prediction | | | | |
| (4) | Ratio of pool slope to riffle slope (S_p / S_{rif}) | | | Level II | General prediction | | | | |
| (5) | Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | | | Level III | Detailed prediction | | | | |
| (6) | Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | | | Level III | Detailed prediction | | | | |
| (7) | Velocity profiles / Isovels / Velocity gradient | | | Level IV | Validation | | | | |
| Level I | (1) | Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High | | | | | | | |
| | | Extensive deposition (continuous, cross-channel).....NBS = Extreme | | | | | | | |
| | | Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme | | | | | | | |
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| Level II | (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | |
| | | | | | | | | | |
| Level II | (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | |
| | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | | | | |
| | | 0.55 | 0.43 | 1.2790698 | Low | | | | |
| Level III | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft^2) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft^2) | Ratio τ_{nb} / τ_{bkf} | Near-Bank Stress (NBS) |
| | | | | | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | | Near-Bank Stress (NBS) | | | | | |
| | | | | | | | | | |
| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | | | |
| Near-Bank Stress (NBS) ratings | Method number | | | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) | | |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 | | |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 | | |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 | | |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 | | |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 | | |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 | | |
| Overall Near-Bank Stress (NBS) rating | | | | | | Low | | | |

| | |
|----------------------------------|----------|
| Method | 5 |
| Dominant Near-Bank Stress | |
| Low | |

| Estimating Near-Bank Stress (NBS) | | | |
|--|-------------------------------|--------------|--|
| Stream: Eccleston | Location: Left Bank 25 | | |
| Station: 305+51.43 to 306+18.16 | Stream Type: | Valley Type: | |
| Observers: PVC & SH | Date: 5/4/2018 | | |

| Methods for Estimating Near-Bank Stress (NBS) | | |
|---|-----------|---------------------|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkr}) | Level II | General prediction |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkr}) | Level III | Detailed prediction |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkr}) | Level III | Detailed prediction |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | | | | | | | | |
|-----------|-----------------------------------|-------------------------------------|--|---------------------------|------------------------|---|--------------------------------|------------------------|--|--------|---|---------------------------|--|-----|--|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkr} (ft) | Ratio R_c / W_{bkr} | Near-Bank Stress (NBS) | <table border="1"> <tr> <td>Method</td> <td>5</td> </tr> <tr> <td colspan="2">Dominant Near-Bank Stress</td> </tr> <tr> <td colspan="2">Low</td> </tr> </table> | | | | Method | 5 | Dominant Near-Bank Stress | | Low | |
| | Method | 5 | | | | | | | | | | | | | |
| | Dominant Near-Bank Stress | | | | | | | | | | | | | | |
| Low | | | | | | | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkr} (ft) | Ratio d_{nb} / d_{bkr} | Near-Bank Stress (NBS) | | | | | | | | | | |
| | | 0.53 | 0.38 | 1.3947368 | Low | | | | | | | | | | |
| (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft^2) | Mean Depth d_{bkr} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkr} (lb/ft^2) | Ratio τ_{nb} / τ_{bkr} | Near-Bank Stress (NBS) | | | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | | Near-Bank Stress (NBS) | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |

| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | |
|--|---------------|-------------|-------------|-------------|-------------|-------------|-------------|
| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |
| Overall Near-Bank Stress (NBS) rating | | | | | | Low | |

| Estimating Near-Bank Stress (NBS) | | | |
|--|--------------------------------|--------------|--|
| Stream: Eccleston | Location: Right Bank 26 | | |
| Station: 302+31.22 to 305+52.82 | Stream Type: | Valley Type: | |
| Observers: PVC & SH | Date: 5/4/2018 | | |

| Methods for Estimating Near-Bank Stress (NBS) | | |
|---|-----------|---------------------|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | Level II | General prediction |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | Level III | Detailed prediction |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | Level III | Detailed prediction |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | | | | | | | |
|------------------|---------------------------|-------------------------------------|-------------------------------|--|---------------------------|--|--|--------------------------------|------------------------|---|---------------------------|--|-----|--|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | <table border="1"> <tr><td>Method</td><td>5</td></tr> <tr><td>Dominant Near-Bank Stress</td><td></td></tr> <tr><td>Low</td><td></td></tr> </table> | | | Method | 5 | Dominant Near-Bank Stress | | Low | |
| | Method | 5 | | | | | | | | | | | | |
| | Dominant Near-Bank Stress | | | | | | | | | | | | | |
| Low | | | | | | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | 0.55 | 0.43 | 1.2790698 | Low | | | | | |
| | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} | Near-Bank Stress (NBS) | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | Near-Bank Stress (NBS) | | | | | | | | | | | |

| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | |
|--|---------------|-------------|-------------|-------------|-------------|-------------|-------------|
| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |
| Overall Near-Bank Stress (NBS) rating | | | | | | Low | |

| Estimating Near-Bank Stress (NBS) | | | |
|--|-------------------------------|--------------|--|
| Stream: Eccleston | Location: Left Bank 26 | | |
| Station: 302+30.62 to 305+51.43 | Stream Type: | Valley Type: | |
| Observers: PVC & SH | Date: 5/4/2018 | | |

| Methods for Estimating Near-Bank Stress (NBS) | | |
|---|-----------|---------------------|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkr}) | Level II | General prediction |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkr}) | Level III | Detailed prediction |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkr}) | Level III | Detailed prediction |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | | | | | | | | |
|-----------|-----------------------------------|-------------------------------------|--|---------------------------|------------------------|---|--------------------------------|------------------------|--|--------|---|---------------------------|--|-----|--|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkr} (ft) | Ratio R_c / W_{bkr} | Near-Bank Stress (NBS) | <table border="1"> <tr> <td>Method</td> <td>5</td> </tr> <tr> <td colspan="2">Dominant Near-Bank Stress</td> </tr> <tr> <td colspan="2">Low</td> </tr> </table> | | | | Method | 5 | Dominant Near-Bank Stress | | Low | |
| | Method | 5 | | | | | | | | | | | | | |
| | Dominant Near-Bank Stress | | | | | | | | | | | | | | |
| Low | | | | | | | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkr} (ft) | Ratio d_{nb} / d_{bkr} | Near-Bank Stress (NBS) | | | | | | | | | | |
| | | 0.53 | 0.38 | 1.3947368 | Low | | | | | | | | | | |
| (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft^2) | Mean Depth d_{bkr} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkr} (lb/ft^2) | Ratio τ_{nb} / τ_{bkr} | Near-Bank Stress (NBS) | | | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | | Near-Bank Stress (NBS) | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |

| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | |
|--|---------------|-------------|-------------|-------------|-------------|-------------|-------------|
| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |
| Overall Near-Bank Stress (NBS) rating | | | | | | Low | |

| Estimating Near-Bank Stress (NBS) | | | | | | | | | | | | | |
|--|---|---|-------------------------------|--|---------------------------|-------------------|--|--------------------------------|------------------------|---------------------------|--|-----|--|
| Stream: Eccleston | | Location: Right Bank 27 | | | | | | | | | | | |
| Station: 301+33.97 to 302+31.22 | | Stream Type: | | Valley Type: | | | | | | | | | |
| Observers: PVC & SH | | Date: 5/4/2018 | | | | | | | | | | | |
| Methods for Estimating Near-Bank Stress (NBS) | | | | | | | | | | | | | |
| (1) | Channel pattern, transverse bar or split channel/central bar creating NBS | | | Level I | Reconnaissance | | | | | | | | |
| (2) | Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | | | Level II | General prediction | | | | | | | | |
| (3) | Ratio of pool slope to average water surface slope (S_p / S) | | | Level II | General prediction | | | | | | | | |
| (4) | Ratio of pool slope to riffle slope (S_p / S_{rif}) | | | Level II | General prediction | | | | | | | | |
| (5) | Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | | | Level III | Detailed prediction | | | | | | | | |
| (6) | Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | | | Level III | Detailed prediction | | | | | | | | |
| (7) | Velocity profiles / Isovels / Velocity gradient | | | Level IV | Validation | | | | | | | | |
| Level I | (1) | Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High | | | | | | | | | | | |
| | | Extensive deposition (continuous, cross-channel).....NBS = Extreme | | | | | | | | | | | |
| | | Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme | | | | | | | | | | | |
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | | | | | | | | |
| | | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | |
| | | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | |
| | | <table border="1"> <tr> <td>Method</td> <td>5</td> </tr> <tr> <td colspan="2">Dominant Near-Bank Stress</td> </tr> <tr> <td colspan="2">Low</td> </tr> </table> | | | | | | Method | 5 | Dominant Near-Bank Stress | | Low | |
| Method | 5 | | | | | | | | | | | | |
| Dominant Near-Bank Stress | | | | | | | | | | | | | |
| Low | | | | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | | | | | | | | |
| | | 0.55 | 0.43 | 1.2790698 | Low | | | | | | | | |
| Level III | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} | Near-Bank Stress (NBS) | | | | |
| | | | | | | | | | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | | Near-Bank Stress (NBS) | | | | | | | | | |
| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | | | | | | | |
| Near-Bank Stress (NBS) ratings | Method number | | | | | | | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) | | | | | | |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 | | | | | | |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 | | | | | | |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 | | | | | | |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 | | | | | | |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 | | | | | | |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 | | | | | | |
| Overall Near-Bank Stress (NBS) rating | | | | | | Low | | | | | | | |

| Estimating Near-Bank Stress (NBS) | | | |
|--|-------------------------------|--------------|--|
| Stream: Eccleston | Location: Left Bank 27 | | |
| Station: 301+25.14 to 302+30.62 | Stream Type: | Valley Type: | |
| Observers: PVC & SH | Date: 5/4/2018 | | |

| Methods for Estimating Near-Bank Stress (NBS) | | | |
|---|-----------|---------------------|--|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance | |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | Level II | General prediction | |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction | |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction | |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | Level III | Detailed prediction | |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | Level III | Detailed prediction | |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation | |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | | | | | | | |
|------------------|-----------------------------------|-------------------------------------|--|---------------------------|------------------------|--|--------------------------------|------------------------|--------|---|---------------------------|--|-----------|--|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | <table border="1"> <tr><td>Method</td><td>1</td></tr> <tr><td>Dominant Near-Bank Stress</td><td></td></tr> <tr><td>Very High</td><td></td></tr> </table> | | | Method | 1 | Dominant Near-Bank Stress | | Very High | |
| | Method | 1 | | | | | | | | | | | | |
| | Dominant Near-Bank Stress | | | | | | | | | | | | | |
| Very High | | | | | | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | | | | | | | | | |
| | | 0.53 | 0.38 | 1.3947368 | Low | | | | | | | | | |
| (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} | Near-Bank Stress (NBS) | | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | Near-Bank Stress (NBS) | | | | | | | | | | | |
| | | | | | | | | | | | | | | |

| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | |
|--|---------------|-------------|-------------|-------------|-------------|------------------|-------------|
| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |
| Overall Near-Bank Stress (NBS) rating | | | | | | Very High | |

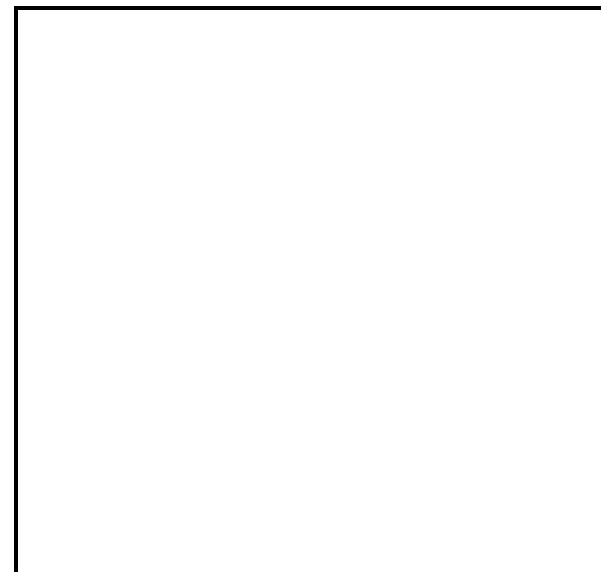
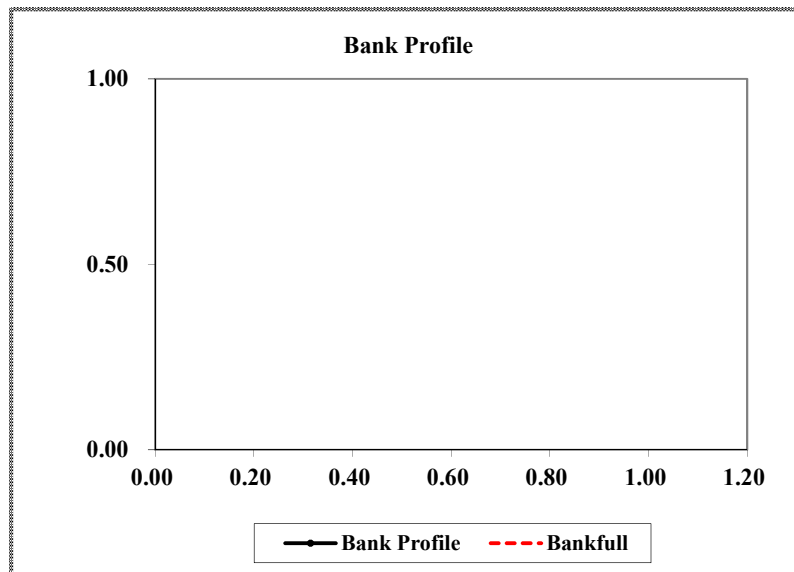
BANK EROSION HAZARD INDEX

| | | | | | | | | | | | | | | | |
|------------------|---------------------------|---------------------|-----|--------------|----|---------------|--|---------------------|----------------------------|------|-------|-------|-------|-------|-------|
| Stream: | Eccleston Mitigation Site | Observer(s): | PVC | Data: | SH | QA/QC: | | Total Score: | 45.43 | | | | | | |
| Reach: | 500+3.19 to 503+63.08 | Comments: | | | | | | | Very High | | | | | | |
| Location: | Right Bank 28 | Bank Length | 345 | | | | | | Total Score Values: | 5-10 | 10-20 | 20-30 | 30-40 | 40-45 | 45-50 |
| Date: | 5/4/2018 | | | | | | | | | | | | | | |

| Erodibility Variables | | | | | |
|-------------------------------------|--------------------------|-------|--------------|------------------------|-------|
| Bank Height / Bankfull Height Ratio | | | | | |
| Bank Height | Bankfull Height | Value | Index | Bank Erosion Potential | Notes |
| 6.00 | 1.50 | 4.00 | 10.00 | Extreme | |
| Root Depth / Bank Height Ratio | | | | | |
| Root Depth | Bank Height | Value | Index | Bank Erosion Potential | Notes |
| 0.50 | 6.00 | 0.08 | 8.63 | Very High | |
| Weighted Root Density | | | | | |
| Root Density (%) | Root Depth / Bank Height | Value | Index | Bank Erosion Potential | Notes |
| 20.00 | 0.08 | 1.67 | 10.00 | Extreme | |
| Bank Angle | | | | | |
| Bank Angle (°) | | | Index | Bank Erosion Potential | Notes |
| 80.00 | | | 5.90 | Moderate | |
| Surface Protection | | | | | |
| Surface Protection (%) | | | Index | Bank Erosion Potential | Notes |
| 30.00 | | | 5.90 | Moderate | |
| | | | Adjustment | | Notes |
| Bank Materials | | | | | |
| | | | 5.00 | | Notes |
| | | | Adjustment | | Notes |
| Bank Stratification | | | | | |
| | | | 0.00 | | |
| TOTAL SCORE | | | 45.43 | | |

| Bank Erosion Potential | | | | | | | | |
|---|--|-----------|-----------|-----------|-----------|-----------|-----------|---------|
| Erodibility Variables | | | Very Low | Low | Moderate | High | Very High | Extreme |
| | Bank Height / Bankfull Height | Value | 1.00-1.10 | 1.11-1.19 | 1.20-1.50 | 1.60-2.00 | 2.10-2.80 | >2.80 |
| | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 | |
| Root Depth / Bank Height | Value | 1.00-0.90 | 0.89-0.50 | 0.49-0.30 | 0.29-0.15 | 0.14-0.05 | <0.05 | |
| | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 | |
| Weighted Root Density | Value | 100-80 | 79-55 | 54-30 | 29-15 | 14-5 | <5 | |
| | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 | |
| Bank Angle | Value | 0-20 | 21-60 | 61-80 | 81-90 | 91-119 | >119 | |
| | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 | |
| Surface Protection | Value | 100-80 | 79-55 | 54-30 | 29-15 | 14-10 | <10 | |
| | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 | |
| Adjustments | | | | | | | | |
| Bedrock | Bedrock banks have a very low erosion potential. | | | | | | | |
| Boulders | Boulder banks have a low erosion potential. | | | | | | | |
| Cobble | Subtract 10 points. No adjustment if sand/gravel compose greater than 50% of bank. | | | | | | | |
| Clay/Silt Loam | Add 5 points. | | | | | | | |
| Gravel | Add 5-10 points depending on percentage of bank material composed of sand. | | | | | | | |
| Sand | Add 10 points. | | | | | | | |
| Silt / Clay | No adjustment. | | | | | | | |
| Stratification | | | | | | | | |
| Add 5-10 points depending on position of unstable layers in relation to bankfull stage. | | | | | | | | |

| Bank Profile | | |
|---------------------|-----------------|-------|
| Horizontal Distance | Vertical Height | Notes |
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| | | |
| Bankfull | | |
| Horizontal Distance | Vertical Height | Notes |
| | | |
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| Estimating Near-Bank Stress (NBS) | | | | | | | | | | | | | |
|---|---|--|-------------------------------|--|---------------------------|-------------------|--|--------------------------------|------------------------|---------------------------|--|-----------|--|
| Stream: Eccleston | | Location: Right Bank 28 | | | | | | | | | | | |
| Station: 500+3.19 to 503+63.08 | | Stream Type: | | Valley Type: | | | | | | | | | |
| Observers: PVC & SH | | Date: 5/4/2018 | | | | | | | | | | | |
| Methods for Estimating Near-Bank Stress (NBS) | | | | | | | | | | | | | |
| (1) | Channel pattern, transverse bar or split channel/central bar creating NBS | | | Level I | Reconnaissance | | | | | | | | |
| (2) | Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | | | Level II | General prediction | | | | | | | | |
| (3) | Ratio of pool slope to average water surface slope (S_p / S) | | | Level II | General prediction | | | | | | | | |
| (4) | Ratio of pool slope to riffle slope (S_p / S_{rif}) | | | Level II | General prediction | | | | | | | | |
| (5) | Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | | | Level III | Detailed prediction | | | | | | | | |
| (6) | Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | | | Level III | Detailed prediction | | | | | | | | |
| (7) | Velocity profiles / Isovels / Velocity gradient | | | Level IV | Validation | | | | | | | | |
| Level I | (1) | Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High | | | | | | | | | | | |
| | | Extensive deposition (continuous, cross-channel).....NBS = Extreme | | | | | | | | | | | |
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | | | | | | | | |
| | | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | |
| | | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | | | | | | | | |
| | | 0.83 | 0.62 | 1.3387097 | Low | | | | | | | | |
| Level IV | (7) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} | Near-Bank Stress (NBS) | | | | |
| | | | | | | | | | | | | | |
| <table border="1" style="margin-left: auto; margin-right: auto;"> <tr><td>Method</td><td>1</td></tr> <tr><td colspan="2">Dominant Near-Bank Stress</td></tr> <tr><td colspan="2">Very High</td></tr> </table> | | | | | | | | Method | 1 | Dominant Near-Bank Stress | | Very High | |
| Method | 1 | | | | | | | | | | | | |
| Dominant Near-Bank Stress | | | | | | | | | | | | | |
| Very High | | | | | | | | | | | | | |
| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | | | | | | | |
| Near-Bank Stress (NBS) ratings | Method number | | | | | | | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) | | | | | | |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 | | | | | | |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 | | | | | | |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 | | | | | | |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 | | | | | | |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 | | | | | | |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 | | | | | | |
| Overall Near-Bank Stress (NBS) rating | | | | | | Very High | | | | | | | |

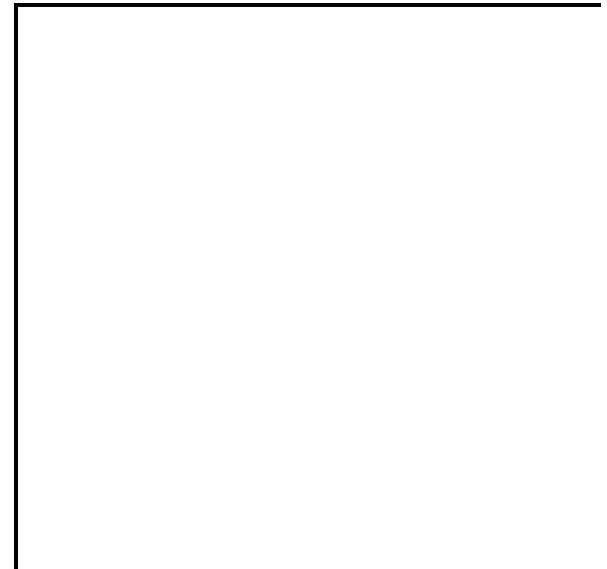
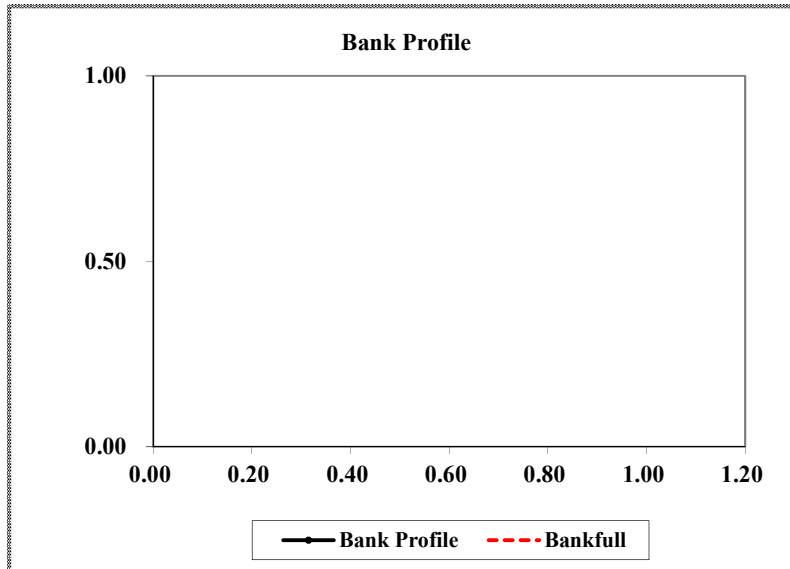
BANK EROSION HAZARD INDEX

| | | | | | | | | | | | | | | |
|-----------|---------------------------|--------------|-----|-------|----|--------|--|---------------------|----------|-------|----------|-------|-----------|---------|
| Stream: | Eccleston Mitigation Site | Observer(s): | PVC | Data: | SH | QA/QC: | | Total Score: | 44.64 | | | | | |
| Reach: | 500+2.38 to 503+65.54 | Comments: | | | | | | Very High | | | | | | |
| Location: | Left Bank 28 | Bank Length | 367 | | | | | Total Score Values: | Very Low | Low | Moderate | High | Very High | Extreme |
| Date: | 5/4/2018 | | | | | | | | 5-10 | 10-20 | 20-30 | 30-40 | 40-45 | 45-50 |

| Erodibility Variables | | | | | |
|-------------------------------------|--------------------------|-------|--------------|------------------------|-------|
| Bank Height / Bankfull Height Ratio | | | | | |
| Bank Height | Bankfull Height | Value | Index | Bank Erosion Potential | Notes |
| 6.00 | 1.50 | 4.00 | 10.00 | Extreme | |
| Root Depth / Bank Height Ratio | | | | | |
| Root Depth | Bank Height | Value | Index | Bank Erosion Potential | Notes |
| 0.50 | 6.00 | 0.08 | 8.63 | Very High | |
| Weighted Root Density | | | | | |
| Root Density (%) | Root Depth / Bank Height | Value | Index | Bank Erosion Potential | Notes |
| 30.00 | 0.08 | 2.50 | 10.00 | Extreme | |
| Bank Angle | | | | | |
| Bank Angle (°) | | | Index | Bank Erosion Potential | Notes |
| 80.00 | | | 5.90 | Moderate | |
| Surface Protection | | | | | |
| Surface Protection (%) | | | Index | Bank Erosion Potential | Notes |
| 40.00 | | | 5.11 | Moderate | |
| | | | Adjustment | | Notes |
| | | | 5.00 | | |
| Bank Materials | | | | | |
| | | | Adjustment | | Notes |
| | | | 0.00 | | |
| Bank Stratification | | | | | |
| | | | | | |
| TOTAL SCORE | | | 44.64 | | |

| Bank Erosion Potential | | | | | | | | |
|---|--------------------------------------|--|--|-----------|-----------|-----------|-----------|-------|
| | | Very Low | Low | Moderate | High | Very High | Extreme | |
| Erodibility Variables | Bank Height / Bankfull Height | Value | 1.00-1.10 | 1.11-1.19 | 1.20-1.50 | 1.60-2.00 | 2.10-2.80 | >2.80 |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| | Root Depth / Bank Height | Value | 1.00-0.90 | 0.89-0.50 | 0.49-0.30 | 0.29-0.15 | 0.14-0.05 | <0.05 |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| | Weighted Root Density | Value | 100-80 | 79-55 | 54-30 | 29-15 | 14-5 | <5 |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| | Bank Angle | Value | 0-20 | 21-60 | 61-80 | 81-90 | 91-119 | >119 |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| | Surface Protection | Value | 100-80 | 79-55 | 54-30 | 29-15 | 14-10 | <10 |
| | | Index | 1.0-1.9 | 2.0-3.9 | 4.0-5.9 | 6.0-7.9 | 8.0-9.0 | 10 |
| | Bank Material | Adjustments | | | | | | |
| | | Bedrock | Bedrock banks have a very low erosion potential. | | | | | |
| | | Boulders | Boulder banks have a low erosion potential. | | | | | |
| | | Cobble | Subtract 10 points. No adjustment if sand/gravel compose greater than 50% of bank. | | | | | |
| | | Clay/Silt Loam | Add 5 points. | | | | | |
| Gravel | | Add 5-10 points depending on percentage of bank material composed of sand. | | | | | | |
| Sand | | Add 10 points. | | | | | | |
| Silt / Clay | No adjustment. | | | | | | | |
| Stratification | | | | | | | | |
| Add 5-10 points depending on position of unstable layers in relation to bankfull stage. | | | | | | | | |

| Bank Profile | | |
|---------------------|-----------------|-------|
| Horizontal Distance | Vertical Height | Notes |
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| Bankfull | | |
| Horizontal Distance | Vertical Height | Notes |
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| Estimating Near-Bank Stress (NBS) | | | |
|---------------------------------------|-------------------------------|--------------|--|
| Stream: Eccleston | Location: Left Bank 28 | | |
| Station: 500+2.38 to 503+65.54 | Stream Type: | Valley Type: | |
| Observers: PVC & SH | Date: 5/4/2018 | | |

| Methods for Estimating Near-Bank Stress (NBS) | | |
|---|-----------|---------------------|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkr}) | Level II | General prediction |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkr}) | Level III | Detailed prediction |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkr}) | Level III | Detailed prediction |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | | | | | | | | |
|-----------|-----------------------------------|-------------------------------------|---|---------------------------|------------------------|---|--------------------------------|------------------------|--|--------|---|---------------------------|--|----------|--|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkr} (ft) | Ratio R_c / W_{bkr} | Near-Bank Stress (NBS) | <table border="1"> <tr><td>Method</td><td>5</td></tr> <tr><td colspan="2">Dominant Near-Bank Stress</td></tr> <tr><td colspan="2">Moderate</td></tr> </table> | | | | Method | 5 | Dominant Near-Bank Stress | | Moderate | |
| | Method | 5 | | | | | | | | | | | | | |
| | Dominant Near-Bank Stress | | | | | | | | | | | | | | |
| Moderate | | | | | | | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkr} (ft) | Ratio d_{nb} / d_{bkr} | Near-Bank Stress (NBS) | | | | | | | | | | |
| | | 0.77 | 0.49 | 1.5714286 | Moderate | | | | | | | | | | |
| (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkr} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkr} (lb/ft ²) | Ratio τ_{nb} / τ_{bkr} | Near-Bank Stress (NBS) | | | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | | Near-Bank Stress (NBS) | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |

| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | |
|--|---------------|-------------|-------------|-------------|-------------|-----------------|-------------|
| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |
| Overall Near-Bank Stress (NBS) rating | | | | | | Moderate | |

| Estimating Near-Bank Stress (NBS) | | | | | | | | | | | | | |
|---|---|--|-------------------------------|--|---------------------------|-------------------|--|--------------------------------|------------------------|---------------------------|--|-----|--|
| Stream: Eccleston | | Location: Right Bank 29 | | | | | | | | | | | |
| Station: 503+63.08 to 507+15.6 | | Stream Type: | | Valley Type: | | | | | | | | | |
| Observers: PVC & SH | | Date: 5/4/2018 | | | | | | | | | | | |
| Methods for Estimating Near-Bank Stress (NBS) | | | | | | | | | | | | | |
| (1) | Channel pattern, transverse bar or split channel/central bar creating NBS | | | Level I | Reconnaissance | | | | | | | | |
| (2) | Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | | | Level II | General prediction | | | | | | | | |
| (3) | Ratio of pool slope to average water surface slope (S_p / S) | | | Level II | General prediction | | | | | | | | |
| (4) | Ratio of pool slope to riffle slope (S_p / S_{rif}) | | | Level II | General prediction | | | | | | | | |
| (5) | Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | | | Level III | Detailed prediction | | | | | | | | |
| (6) | Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | | | Level III | Detailed prediction | | | | | | | | |
| (7) | Velocity profiles / Isovels / Velocity gradient | | | Level IV | Validation | | | | | | | | |
| Level I | (1) | Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High | | | | | | | | | | | |
| | | Extensive deposition (continuous, cross-channel).....NBS = Extreme | | | | | | | | | | | |
| Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme | | | | | | | | | | | | | |
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | | | | | | | | |
| | | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | |
| | | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | |
| <table border="1"> <tr> <td>Method</td> <td>5</td> </tr> <tr> <td colspan="2">Dominant Near-Bank Stress</td> </tr> <tr> <td colspan="2">Low</td> </tr> </table> | | | | | | | | Method | 5 | Dominant Near-Bank Stress | | Low | |
| Method | 5 | | | | | | | | | | | | |
| Dominant Near-Bank Stress | | | | | | | | | | | | | |
| Low | | | | | | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | | | | | | | | |
| | | 0.83 | 0.62 | 1.3387097 | Low | | | | | | | | |
| Level III | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft^2) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft^2) | Ratio τ_{nb} / τ_{bkf} | Near-Bank Stress (NBS) | | | | |
| | | | | | | | | | | | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | | Near-Bank Stress (NBS) | | | | | | | | | |
| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | | | | | | | |
| Near-Bank Stress (NBS) ratings | Method number | | | | | | | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) | | | | | | |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 | | | | | | |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 | | | | | | |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 | | | | | | |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 | | | | | | |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 | | | | | | |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 | | | | | | |
| Overall Near-Bank Stress (NBS) rating | | | | | | Low | | | | | | | |

| Estimating Near-Bank Stress (NBS) | | | |
|--|-------------------------------|--------------|--|
| Stream: Eccleston | Location: Left Bank 29 | | |
| Station: 503+65.54 to 507+20.72 | Stream Type: | Valley Type: | |
| Observers: PVC & SH | Date: 5/4/2018 | | |

| Methods for Estimating Near-Bank Stress (NBS) | | | |
|---|-----------|---------------------|--|
| (1) Channel pattern, transverse bar or split channel/central bar creating NBS | Level I | Reconnaissance | |
| (2) Ratio of radius of curvature to bankfull width (R_c / W_{bkf}) | Level II | General prediction | |
| (3) Ratio of pool slope to average water surface slope (S_p / S) | Level II | General prediction | |
| (4) Ratio of pool slope to riffle slope (S_p / S_{rif}) | Level II | General prediction | |
| (5) Ratio of near-bank maximum depth to bankfull mean depth (d_{nb} / d_{bkf}) | Level III | Detailed prediction | |
| (6) Ratio of near-bank shear stress to bankfull shear stress (τ_{nb} / τ_{bkf}) | Level III | Detailed prediction | |
| (7) Velocity profiles / Isovels / Velocity gradient | Level IV | Validation | |

Level I (1) Transverse and/or central bars-short and/or discontinuous.....NBS = High / Very High
 Extensive deposition (continuous, cross-channel).....NBS = Extreme
 Chute cutoffs, down-valley meander migration, converging flow.....NBS = Extreme

| | | | | | | | | | | | | |
|------------------|---------------------------|-------------------------------------|-------------------------------|--|---------------------------|---|--|--------------------------------|------------------------|---|---------------------------|----------|
| Level II | (2) | Radius of Curvature R_c (ft) | Bankfull Width W_{bkf} (ft) | Ratio R_c / W_{bkf} | Near-Bank Stress (NBS) | <table border="1"> <tr><td>Method</td><td>5</td></tr> <tr><td>Dominant Near-Bank Stress</td></tr> <tr><td>Moderate</td></tr> </table> | | | Method | 5 | Dominant Near-Bank Stress | Moderate |
| | Method | 5 | | | | | | | | | | |
| | Dominant Near-Bank Stress | | | | | | | | | | | |
| Moderate | | | | | | | | | | | | |
| (3) | Pool Slope S_p | Average Slope S | Ratio S_p / S | Near-Bank Stress (NBS) | | | | | | | | |
| (4) | Pool Slope S_p | Riffle Slope S_{rif} | Ratio S_p / S_{rif} | Near-Bank Stress (NBS) | | | | | | | | |
| Level III | (5) | Near-Bank Max Depth d_{nb} (ft) | Mean Depth d_{bkf} (ft) | Ratio d_{nb} / d_{bkf} | Near-Bank Stress (NBS) | 0.77 | 0.49 | 1.5714286 | Moderate | | | |
| | (6) | Near-Bank Max Depth d_{nb} (ft) | Near-Bank Slope S_{nb} | Near-Bank Shear Stress τ_{nb} (lb/ft ²) | Mean Depth d_{bkf} (ft) | Average Slope S | Bankfull Shear Stress τ_{bkf} (lb/ft ²) | Ratio τ_{nb} / τ_{bkf} | Near-Bank Stress (NBS) | | | |
| Level IV | (7) | Velocity Gradient (ft / sec / ft) | Near-Bank Stress (NBS) | | | | | | | | | |

| Converting Values to a Near-Bank Stress (NBS) Rating | | | | | | | |
|--|---------------|-------------|-------------|-------------|-------------|-----------------|-------------|
| Near-Bank Stress (NBS) ratings | Method number | | | | | | |
| | (1) | (2) | (3) | (4) | (5) | (6) | (7) |
| Very Low | N/A | > 3.00 | < 0.20 | < 0.40 | < 1.00 | < 0.80 | < 0.50 |
| Low | N/A | 2.21 – 3.00 | 0.20 – 0.40 | 0.41 – 0.60 | 1.00 – 1.50 | 0.80 – 1.05 | 0.50 – 1.00 |
| Moderate | N/A | 2.01 – 2.20 | 0.41 – 0.60 | 0.61 – 0.80 | 1.51 – 1.80 | 1.06 – 1.14 | 1.01 – 1.60 |
| High | See | 1.81 – 2.00 | 0.61 – 0.80 | 0.81 – 1.00 | 1.81 – 2.50 | 1.15 – 1.19 | 1.61 – 2.00 |
| Very High | (1) | 1.50 – 1.80 | 0.81 – 1.00 | 1.01 – 1.20 | 2.51 – 3.00 | 1.20 – 1.60 | 2.01 – 2.40 |
| Extreme | Above | < 1.50 | > 1.00 | > 1.20 | > 3.00 | > 1.60 | > 2.40 |
| Overall Near-Bank Stress (NBS) rating | | | | | | Moderate | |

indicates results to be Reported to the State (per Section 7.1.3)

Protocol 1

Credit for Prevented Sediment during Storm Flow

Step 1: Estimate stream sediment erosion rate

| | | |
|---------------------|---------------------|---|
| Erosion Rate = | 2024.8 tons/yr* | -from Eccleston stream bank erosion rate (BEHI-NBS data) |
| Study Length = | 12754 LF | -Combined right and left bank lengths |
| <hr/> | | |
| Unit Erosion Rate = | 0.158758 tons/ft/yr | * Unit Density of soil = 2286.74 lb/CY (per Bulk Density testing) |

| | |
|---|---------------------|
| Existing Stream length to be restored = | 5564 LF |
| x | 0.158758 tons/ft/yr |
| <hr/> | |
| Total Erosion = | 883.3 tons/yr |

Step 2: Convert stream bank erosion to nutrient loading

| | | |
|----------------------------|---------------|--|
| Nitrogen Concentration = | 1.35 lbs/ton | - from recommendations of the Expert Panel to Define Removal Rates for individual Stream |
| Phosphorus Concentration = | 0.445 lbs/ton | Restoration Projects prepared by Tom Schueler and Bill Stack |

Step 3: Estimate stream restoration efficiency

| | |
|----------------------------------|----------------|
| Load Reductions (50% efficiency) | |
| Sediment (TSS) = | 883,330 lbs/yr |
| Nitrogen (TN) = | 596.2 lbs/yr |
| Phosphorus (TP) = | 196.5 lbs/yr |

Protocol 2

Credit for in-stream and riparian nutrient processing within the hyporheic zone during base

Step 1: Determine the total post construction stream length that has been reconnected using the bank height ratio of 1.0 or less:

| | | |
|-------------------------------------|---------|---|
| Restored (proposed) Stream Length = | 6796 LF | length of restored stream where BHR = 1.0 or less |
|-------------------------------------|---------|---|

Step 2: Determine the dimensions of the hyporheic box

| | | | |
|--------------------------|-------|-------------------------|---|
| Channel Width = | 9 ft | where BHR = 1.0 or less | Channel Width = average of all stream reaches |
| Left Floodplain Width = | 5 ft | (max. credit = 5 ft) | |
| Right Floodplain Width = | 5 ft | (max. credit = 5 ft) | |
| <hr/> | | | |
| Width Hyporheic Box = | 19 ft | | |

| | | |
|-----------------------|---------|---------------|
| Depth Hyporheic Box = | 5 ft | from guidance |
| x | 6796 LF | |

| | |
|-----------------------------|-------------------------|
| Total Vol. Hyporheic Zone = | 645,620 ft ³ |
|-----------------------------|-------------------------|

| | | |
|-------------------------|---------------|-------------------------------------|
| Mass of hyporheic box = | 31085.4 tons* | * Unit Density of soil = 2600 lb/CY |
|-------------------------|---------------|-------------------------------------|

Step 3: Multiply the hyporheic box mass by the unit denitrification rate

| | |
|-----------------------------|----------------------|
| Unit Denitrification Rate = | 1.06E-04 lbs/ton/day |
|-----------------------------|----------------------|

| | |
|-----------------|----------------|
| Load Reduction | |
| Nitrogen (TN) = | 1202.7 lbs/yr* |

Watershed Area at Downstream POI = 1,728 acres

Impervious Area = 22.7%

* <40% of watershed annual N load (full credit is applicable)

Protocol 3

Credit for Floodplain Reconnection Volume

**Not performed for this project*



APPENDIX F Ecological Uplift

HABITAT ASSESSMENT FIELD DATA SHEET—LOW GRADIENT STREAMS (FRONT)

| | | |
|---------------------------------|--|-------------------|
| STREAM NAME | LOCATION <u>Intersection Tr.b</u> | |
| STATION # _____ RIVERMILE _____ | STREAM CLASS | |
| LAT _____ LONG _____ | RIVER BASIN | |
| STORET # | AGENCY | |
| INVESTIGATORS | | |
| FORM COMPLETED BY | DATE <u>5/4/18</u> TIME _____ AM PM | REASON FOR SURVEY |



| | Habitat Parameter | Condition Category | | | |
|--|---|--|--|--|--|
| | | Optimal | Suboptimal | Marginal | Poor |
| Parameters to be evaluated in sampling reach | 1. Epifaunal Substrate/ Available Cover | Greater than 50% of substrate favorable for epifaunal colonization and fish cover; mix of snags, submerged logs, undercut banks, cobble or other stable habitat and at stage to allow full colonization potential (i.e., logs/snags that are <u>not</u> new fall and not transient). | 30-50% mix of stable habitat; well-suited for full colonization potential; adequate habitat for maintenance of populations; presence of additional substrate in the form of new fall, but not yet prepared for colonization (may rate at high end of scale). | 10-30% mix of stable habitat; habitat availability less than desirable; substrate frequently disturbed or removed. | Less than 10% stable habitat; lack of habitat is obvious; substrate unstable or lacking. |
| | SCORE | 20 19 18 17 16 | 15 14 13 12 11 | 10 9 8 <u>7</u> 6 | 5 4 3 2 1 0 |
| | 2. Pool Substrate Characterization | Mixture of substrate materials, with gravel and firm sand prevalent; root mats and submerged vegetation common. | Mixture of soft sand, mud, or clay; mud may be dominant; some root mats and submerged vegetation present. | All mud or clay or sand bottom; little or no root mat; no submerged vegetation. | Hard-pan clay or bedrock; no root mat or vegetation. |
| | SCORE | 20 19 18 17 16 | 15 14 13 12 11 | 10 9 <u>8</u> 7 6 | 5 4 3 2 1 0 |
| | 3. Pool Variability | Even mix of large-shallow, large-deep, small-shallow, small-deep pools present. | Majority of pools large-deep; very few shallow. | Shallow pools much more prevalent than deep pools. | Majority of pools small-shallow or pools absent. |
| | SCORE | 20 19 18 17 16 | 15 14 13 12 11 | 10 9 8 7 6 | 5 4 3 2 <u>1</u> 0 |
| 4. Sediment Deposition | Little or no enlargement of islands or point bars and less than <20% of the bottom affected by sediment deposition. | Some new increase in bar formation, mostly from gravel, sand or fine sediment; 20-50% of the bottom affected; slight deposition in pools. | Moderate deposition of new gravel, sand or fine sediment on old and new bars; 50-80% of the bottom affected; sediment deposits at obstructions, constrictions, and bends; moderate deposition of pools prevalent. | Heavy deposits of fine material, increased bar development; more than 80% of the bottom changing frequently; pools almost absent due to substantial sediment deposition. | |
| SCORE | 20 19 18 17 16 | <u>15</u> 14 13 12 11 | 10 9 8 7 6 | 5 4 3 2 1 0 | |
| 5. Channel Flow Status | Water reaches base of both lower banks, and minimal amount of channel substrate is exposed. | Water fills >75% of the available channel; or <25% of channel substrate is exposed. | Water fills 25-75% of the available channel, and/or riffle substrates are mostly exposed. | Very little water in channel and mostly present as standing pools. | |
| SCORE | 20 19 18 17 16 | 15 14 13 12 11 | 10 9 8 7 6 | 5 4 3 <u>2</u> 1 0 | |

HABITAT ASSESSMENT FIELD DATA SHEET—LOW GRADIENT STREAMS (BACK)

| Habitat Parameter | Condition Category | | | | | | | | | | | | | | | | | | | | |
|---|--|----|----|----|----|---|----|----|----|----|---|---|---|---|---|------|---|---|---|---|---|
| | Optimal | | | | | Suboptimal | | | | | Marginal | | | | | Poor | | | | | |
| 6. Channel Alteration | Channelization or dredging absent or minimal; stream with normal pattern. | | | | | | | | | | | | | | | | | | | | |
| | Some channelization present, usually in areas of bridge abutments; evidence of past channelization, i.e., dredging, (greater than past 20 yr) may be present, but recent channelization is not present. | | | | | Channelization may be extensive; embankments or shoring structures present on both banks; and 40 to 80% of stream reach channelized and disrupted. | | | | | Banks shored with gabion or cement; over 80% of the stream reach channelized and disrupted. Instream habitat greatly altered or removed entirely. | | | | | | | | | | |
| SCORE | 20 | 19 | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |
| 7. Channel Sinuosity | The bends in the stream increase the stream length 3 to 4 times longer than if it was in a straight line. (Note - channel braiding is considered normal in coastal plains and other low-lying areas. This parameter is not easily rated in these areas.) | | | | | | | | | | | | | | | | | | | | |
| | The bends in the stream increase the stream length 1 to 2 times longer than if it was in a straight line. | | | | | The bends in the stream increase the stream length 1 to 2 times longer than if it was in a straight line. | | | | | Channel straight; waterway has been channelized for a long distance. | | | | | | | | | | |
| SCORE | 20 | 19 | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |
| 8. Bank Stability (score each bank) | Banks stable; evidence of erosion or bank failure absent or minimal; little potential for future problems. <5% of bank affected. | | | | | | | | | | | | | | | | | | | | |
| | Moderately stable; infrequent, small areas of erosion mostly healed over. 5-30% of bank in reach has areas of erosion. | | | | | Moderately unstable; 30-60% of bank in reach has areas of erosion; high erosion potential during floods. | | | | | Unstable; many eroded areas; "raw" areas frequent along straight sections and bends; obvious bank sloughing; 60-100% of bank has erosional scars. | | | | | | | | | | |
| SCORE ___ (LB) | Left Bank | 10 | 9 | | | 8 | 7 | 6 | | | 5 | 4 | 3 | | | 2 | 1 | 0 | | | |
| SCORE ___ (RB) | Right Bank | 10 | 9 | | | 8 | 7 | 6 | | | 5 | 4 | 3 | | | 2 | 1 | 0 | | | |
| 9. Vegetative Protection (score each bank) | More than 90% of the streambank surfaces and immediate riparian zone covered by native vegetation, including trees, understory shrubs, or nonwoody macrophytes; vegetative disruption through grazing or mowing minimal or not evident; almost all plants allowed to grow naturally. | | | | | | | | | | | | | | | | | | | | |
| | 70-90% of the streambank surfaces covered by native vegetation, but one class of plants is not well-represented; disruption evident but not affecting full plant growth potential to any great extent; more than one-half of the potential plant stubble height remaining. | | | | | 50-70% of the streambank surfaces covered by vegetation; disruption obvious; patches of bare soil or closely cropped vegetation common; less than one-half of the potential plant stubble height remaining. | | | | | Less than 50% of the streambank surfaces covered by vegetation; disruption of streambank vegetation is very high; vegetation has been removed to 5 centimeters or less in average stubble height. | | | | | | | | | | |
| SCORE ___ (LB) | Left Bank | 10 | 9 | | | 8 | 7 | 6 | | | 5 | 4 | 3 | | | 2 | 1 | 0 | | | |
| SCORE ___ (RB) | Right Bank | 10 | 9 | | | 8 | 7 | 6 | | | 5 | 4 | 3 | | | 2 | 1 | 0 | | | |
| 10. Riparian Vegetative Zone Width (score each bank riparian zone) | Width of riparian zone >18 meters; human activities (i.e., parking lots, roadbeds, clear-cuts, lawns, or crops) have not impacted zone. | | | | | | | | | | | | | | | | | | | | |
| | Width of riparian zone 12-18 meters; human activities have impacted zone only minimally. | | | | | Width of riparian zone 6-12 meters; human activities have impacted zone a great deal. | | | | | Width of riparian zone <6 meters; little or no riparian vegetation due to human activities. | | | | | | | | | | |
| SCORE ___ (LB) | Left Bank | 10 | 9 | | | 8 | 7 | 6 | | | 5 | 4 | 3 | | | 2 | 1 | 0 | | | |
| SCORE ___ (RB) | Right Bank | 10 | 9 | | | 8 | 7 | 6 | | | 5 | 4 | 3 | | | 2 | 1 | 0 | | | |

Total Score _____

HABITAT ASSESSMENT FIELD DATA SHEET—LOW GRADIENT STREAMS (FRONT)

| | | | |
|-------------------|-----------------|--|-------------------|
| STREAM NAME | | LOCATION <u>Below Cypress</u> | |
| STATION # _____ | RIVERMILE _____ | STREAM CLASS | |
| LAT _____ | LONG _____ | RIVER BASIN | |
| STORET # _____ | | AGENCY | |
| INVESTIGATORS | | | |
| FORM COMPLETED BY | | DATE <u>5/18/8</u> TIME _____ AM PM | REASON FOR SURVEY |

| Habitat Parameter | Condition Category | | | |
|---|--|---|---|--|
| | Optimal | Suboptimal | Marginal | Poor |
| 1. Epifaunal Substrate/ Available Cover | Greater than 50% of substrate favorable for epifaunal colonization and fish cover; mix of snags, submerged logs, undercut banks, cobble or other stable habitat and at stage to allow full colonization potential (i.e., logs/snags that are <u>not</u> new fall and not transient). | 30-50% mix of stable habitat; well-suited for full colonization potential; adequate habitat for maintenance of populations; presence of additional substrate in the form of newfall, but not yet prepared for colonization (may rate at high end of scale). | 10-30% mix of stable habitat; habitat availability less than desirable; substrate frequently disturbed or removed. | Less than 10% stable habitat; lack of habitat is obvious; substrate unstable or lacking. |
| | SCORE | 20 19 18 17 16 | 15 (14) 13 12 11 | 10 9 8 7 6 |
| 2. Pool Substrate Characterization | Mixture of substrate materials, with gravel and firm sand prevalent; root mats and submerged vegetation common. | Mixture of soft sand, mud, or clay; mud may be dominant; some root mats and submerged vegetation present. | All mud or clay or sand bottom; little or no root mat; no submerged vegetation. | Hard-pan clay or bedrock; no root mat or vegetation. |
| | SCORE | 20 19 18 17 (16) | 15 14 13 12 11 | 10 9 8 7 6 |
| 3. Pool Variability | Even mix of large-shallow, large-deep, small-shallow, small-deep pools present. | Majority of pools large-deep; very few shallow. | Shallow pools much more prevalent than deep pools. | Majority of pools small-shallow or pools absent. |
| | SCORE | 20 19 18 17 16 | 15 (14) 13 12 11 | 10 9 8 7 6 |
| 4. Sediment Deposition | Little or no enlargement of islands or point bars and less than <20% of the bottom affected by sediment deposition. | Some new increase in bar formation, mostly from gravel, sand or fine sediment; 20-50% of the bottom affected; slight deposition in pools. | Moderate deposition of new gravel, sand or fine sediment on old and new bars; 50-80% of the bottom affected; sediment deposits at obstructions, constrictions, and bends; moderate deposition of pools prevalent. | Heavy deposits of fine material, increased bar development; more than 80% of the bottom changing frequently; pools almost absent due to substantial sediment deposition. |
| | SCORE | 20 19 18 17 16 | 15 14 13 (12) 11 | 10 9 8 7 6 |
| 5. Channel Flow Status | Water reaches base of both lower banks, and minimal amount of channel substrate is exposed. | Water fills >75% of the available channel; or <25% of channel substrate is exposed. | Water fills 25-75% of the available channel, and/or riffle substrates are mostly exposed. | Very little water in channel and mostly present as standing pools. |
| | SCORE | 20 19 18 17 16 | 15 14 (13) 12 11 | 10 9 8 7 6 |

Parameters to be evaluated in sampling reach

Below Cypress

HABITAT ASSESSMENT FIELD DATA SHEET—LOW GRADIENT STREAMS (BACK)

| Habitat Parameter | Condition Category | | | | | | | | | | | | | | | | | | | | |
|--|--|-----------|----|----|----|---|----|----|----|----|---|---|---|---|---|------|---|---|---|---|---|
| | Optimal | | | | | Suboptimal | | | | | Marginal | | | | | Poor | | | | | |
| 6. Channel Alteration | Channelization or dredging absent or minimal; stream with normal pattern. | | | | | | | | | | | | | | | | | | | | |
| | Some channelization present, usually in areas of bridge abutments; evidence of past channelization, i.e., dredging, (greater than past 20 yr) may be present, but recent channelization is not present. | | | | | Channelization may be extensive; embankments or shoring structures present on both banks; and 40 to 80% of stream reach channelized and disrupted. | | | | | Banks shored with gabion or cement; over 80% of the stream reach channelized and disrupted. Instream habitat greatly altered or removed entirely. | | | | | | | | | | |
| SCORE | 20 | 19 | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |
| 7. Channel Sinuosity | The bends in the stream increase the stream length 3 to 4 times longer than if it was in a straight line. (Note - channel braiding is considered normal in coastal plains and other low-lying areas. This parameter is not easily rated in these areas.) | | | | | | | | | | | | | | | | | | | | |
| | The bends in the stream increase the stream length 1 to 2 times longer than if it was in a straight line. | | | | | The bends in the stream increase the stream length 1 to 2 times longer than if it was in a straight line. | | | | | Channel straight; waterway has been channelized for a long distance. | | | | | | | | | | |
| SCORE | 20 | 19 | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |
| 8. Bank Stability (score each bank) | Banks stable; evidence of erosion or bank failure absent or minimal; little potential for future problems. <5% of bank affected. | | | | | | | | | | | | | | | | | | | | |
| | Moderately stable; infrequent, small areas of erosion mostly healed over. 5-30% of bank in reach has areas of erosion. | | | | | Moderately unstable; 30-60% of bank in reach has areas of erosion; high erosion potential during floods. | | | | | Unstable; many eroded areas; "raw" areas frequent along straight sections and bends; obvious bank sloughing; 60-100% of bank has erosional scars. | | | | | | | | | | |
| | SCORE ___ (LB) | Left Bank | 10 | 9 | | | 8 | 7 | 6 | | | 5 | 4 | 3 | | | 2 | 1 | 0 | | |
| SCORE ___ (RB) | Right Bank | 10 | 9 | | | 8 | 7 | 6 | | | 5 | 4 | 3 | | | 2 | 1 | 0 | | | |
| 9. Vegetative Protection (score each bank) | More than 90% of the streambank surfaces and immediate riparian zone covered by native vegetation, including trees, understory shrubs, or nonwoody macrophytes; vegetative disruption through grazing or mowing minimal or not evident; almost all plants allowed to grow naturally. | | | | | | | | | | | | | | | | | | | | |
| | 70-90% of the streambank surfaces covered by native vegetation, but one class of plants is not well-represented; disruption evident but not affecting full plant growth potential to any great extent; more than one-half of the potential plant stubble height remaining. | | | | | 50-70% of the streambank surfaces covered by vegetation; disruption obvious; patches of bare soil or closely cropped vegetation common; less than one-half of the potential plant stubble height remaining. | | | | | Less than 50% of the streambank surfaces covered by vegetation; disruption of streambank vegetation is very high; vegetation has been removed to 5 centimeters or less in average stubble height. | | | | | | | | | | |
| | SCORE ___ (LB) | Left Bank | 10 | 9 | | | 8 | 7 | 6 | | | 5 | 4 | 3 | | | 2 | 1 | 0 | | |
| SCORE ___ (RB) | Right Bank | 10 | 9 | | | 8 | 7 | 6 | | | 5 | 4 | 3 | | | 2 | 1 | 0 | | | |
| 10. Riparian Vegetative Zone Width (score each bank riparian zone) | Width of riparian zone >18 meters; human activities (i.e., parking lots, roadbeds, clear-cuts, lawns, or crops) have not impacted zone. | | | | | | | | | | | | | | | | | | | | |
| | Width of riparian zone 12-18 meters; human activities have impacted zone only minimally. | | | | | Width of riparian zone 6-12 meters; human activities have impacted zone a great deal. | | | | | Width of riparian zone <6 meters; little or no riparian vegetation due to human activities. | | | | | | | | | | |
| | SCORE ___ (LB) | Left Bank | 10 | 9 | | | 8 | 7 | 6 | | | 5 | 4 | 3 | | | 2 | 1 | 0 | | |
| SCORE ___ (RB) | Right Bank | 10 | 9 | | | 8 | 7 | 6 | | | 5 | 4 | 3 | | | 2 | 1 | 0 | | | |

Total Score _____

HABITAT ASSESSMENT FIELD DATA SHEET—LOW GRADIENT STREAMS (FRONT)

| | | | |
|-------------------------|-----------------|---|-------------------------|
| STREAM NAME | | LOCATION <u>Downstream Forested Jones</u> | |
| STATION # _____ | RIVERMILE _____ | STREAM CLASS _____ | |
| LAT _____ | LONG _____ | RIVER BASIN _____ | |
| STORET # _____ | | AGENCY _____ | |
| INVESTIGATORS _____ | | | |
| FORM COMPLETED BY _____ | | DATE <u>5/4/18</u> TIME _____ AM PM | REASON FOR SURVEY _____ |

| Habitat Parameter | Condition Category | | | |
|--|--|---|---|--|
| | Optimal | Suboptimal | Marginal | Poor |
| 1. Epifaunal Substrate/ Available Cover | Greater than 50% of substrate favorable for epifaunal colonization and fish cover; mix of snags, submerged logs, undercut banks, cobble or other stable habitat and at stage to allow full colonization potential (i.e., logs/snags that are <u>not</u> new fall and not transient). | 30-50% mix of stable habitat; well-suited for full colonization potential; adequate habitat for maintenance of populations; presence of additional substrate in the form of newfall, but not yet prepared for colonization (may rate at high end of scale). | 10-30% mix of stable habitat; habitat availability less than desirable; substrate frequently disturbed or removed. | Less than 10% stable habitat; lack of habitat is obvious; substrate unstable or lacking. |
| | SCORE | 20 19 18 17 16 | 15 14 13 12 11 | 10 9 8 (7) 6 |
| 2. Pool Substrate Characterization | Mixture of substrate materials, with gravel and firm sand prevalent; root mats and submerged vegetation common. | Mixture of soft sand, mud, or clay; mud may be dominant; some root mats and submerged vegetation present. | All mud or clay or sand bottom; little or no root mat; no submerged vegetation. | Hard-pan clay or bedrock; no root mat or vegetation. |
| | SCORE | 20 19 18 17 16 | 15 (14) 13 12 11 | 10 9 8 7 6 |
| 3. Pool Variability | Even mix of large-shallow, large-deep, small-shallow, small-deep pools present. | Majority of pools large-deep; very few shallow. | Shallow pools much more prevalent than deep pools. | Majority of pools small-shallow or pools absent. |
| | SCORE | 20 19 18 17 16 | 15 14 13 12 (11) | 10 9 8 7 6 |
| 4. Sediment Deposition | Little or no enlargement of islands or point bars and less than <20% of the bottom affected by sediment deposition. | Some new increase in bar formation, mostly from gravel, sand or fine sediment; 20-50% of the bottom affected; slight deposition in pools. | Moderate deposition of new gravel, sand or fine sediment on old and new bars; 50-80% of the bottom affected; sediment deposits at obstructions, constrictions, and bends; moderate deposition of pools prevalent. | Heavy deposits of fine material, increased bar development; more than 80% of the bottom changing frequently; pools almost absent due to substantial sediment deposition. |
| | SCORE | 20 19 18 17 16 | 15 14 13 12 11 | 10 9 (8) 7 6 |
| 5. Channel Flow Status | Water reaches base of both lower banks, and minimal amount of channel substrate is exposed. | Water fills >75% of the available channel; or <25% of channel substrate is exposed. | Water fills 25-75% of the available channel, and/or riffle substrates are mostly exposed. | Very little water in channel and mostly present as standing pools. |
| | SCORE | 20 19 18 17 16 | 15 14 13 12 11 | 10 9 (8) 7 6 |

Downstream Forested Jones

HABITAT ASSESSMENT FIELD DATA SHEET—LOW GRADIENT STREAMS (BACK)

| Habitat Parameter | Condition Category | | | | | | | | | | | | | | | | | | | | |
|---|--|----|----|----|----|--|----|----|----|----|---|---|---|---|---|---|---|---|---|---|---|
| | Optimal | | | | | Suboptimal | | | | | Marginal | | | | | Poor | | | | | |
| 6. Channel Alteration | Channelization or dredging absent or minimal; stream with normal pattern. | | | | | Some channelization present, usually in areas of bridge abutments; evidence of past channelization, i.e., dredging, (greater than past 20 yr) may be present, but recent channelization is not present. | | | | | Channelization may be extensive; embankments or shoring structures present on both banks; and 40 to 80% of stream reach channelized and disrupted. | | | | | Banks shored with gabion or cement; over 80% of the stream reach channelized and disrupted. Instream habitat greatly altered or removed entirely. | | | | | |
| SCORE | 20 | 19 | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |
| 7. Channel Sinuosity | The bends in the stream increase the stream length 3 to 4 times longer than if it was in a straight line. (Note - channel braiding is considered normal in coastal plains and other low-lying areas. This parameter is not easily rated in these areas.) | | | | | The bends in the stream increase the stream length 1 to 2 times longer than if it was in a straight line. | | | | | The bends in the stream increase the stream length 1 to 2 times longer than if it was in a straight line. | | | | | Channel straight; waterway has been channelized for a long distance. | | | | | |
| SCORE | 20 | 19 | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |
| 8. Bank Stability (score each bank) | Banks stable; evidence of erosion or bank failure absent or minimal; little potential for future problems. <5% of bank affected. | | | | | Moderately stable; infrequent, small areas of erosion mostly healed over. 5-30% of bank in reach has areas of erosion. | | | | | Moderately unstable; 30-60% of bank in reach has areas of erosion; high erosion potential during floods. | | | | | Unstable; many eroded areas; "raw" areas frequent along straight sections and bends; obvious bank sloughing; 60-100% of bank has erosional scars. | | | | | |
| SCORE ___ (LB) | Left Bank | | 10 | 9 | | 8 | 7 | 6 | | | 5 | 4 | 3 | | | 2 | 1 | 0 | | | |
| SCORE ___ (RB) | Right Bank | | 10 | 9 | | 8 | 7 | 6 | | | 5 | 4 | 3 | | | 2 | 1 | 0 | | | |
| 9. Vegetative Protection (score each bank) | More than 90% of the streambank surfaces and immediate riparian zone covered by native vegetation, including trees, understory shrubs, or nonwoody macrophytes; vegetative disruption through grazing or mowing minimal or not evident; almost all plants allowed to grow naturally. | | | | | 70-90% of the streambank surfaces covered by native vegetation, but one class of plants is not well-represented; disruption evident but not affecting full plant growth potential to any great extent; more than one-half of the potential plant stubble height remaining. | | | | | 50-70% of the streambank surfaces covered by vegetation; disruption obvious; patches of bare soil or closely cropped vegetation common; less than one-half of the potential plant stubble height remaining. | | | | | Less than 50% of the streambank surfaces covered by vegetation; disruption of streambank vegetation is very high; vegetation has been removed to 5 centimeters or less in average stubble height. | | | | | |
| SCORE ___ (LB) | Left Bank | | 10 | 9 | | 8 | 7 | 6 | | | 5 | 4 | 3 | | | 2 | 1 | 0 | | | |
| SCORE ___ (RB) | Right Bank | | 10 | 9 | | 8 | 7 | 6 | | | 5 | 4 | 3 | | | 2 | 1 | 0 | | | |
| 10. Riparian Vegetative Zone Width (score each bank riparian zone) | Width of riparian zone >18 meters; human activities (i.e., parking lots, roadbeds, clear-cuts, lawns, or crops) have not impacted zone. | | | | | Width of riparian zone 12-18 meters; human activities have impacted zone only minimally. | | | | | Width of riparian zone 6-12 meters; human activities have impacted zone a great deal. | | | | | Width of riparian zone <6 meters; little or no riparian vegetation due to human activities. | | | | | |
| SCORE ___ (LB) | Left Bank | | 10 | 9 | | 8 | 7 | 6 | | | 5 | 4 | 3 | | | 2 | 1 | 0 | | | |
| SCORE ___ (RB) | Right Bank | | 10 | 9 | | 8 | 7 | 6 | | | 5 | 4 | 3 | | | 2 | 1 | 0 | | | |

Parameters to be evaluated broader than sampling reach

Total Score _____

HABITAT ASSESSMENT FIELD DATA SHEET—LOW GRADIENT STREAMS (FRONT)

| | | | |
|---------------------------------|--|--|-------------------|
| STREAM NAME | | LOCATION <u>Walnut</u> | |
| STATION # _____ RIVERMILE _____ | | STREAM CLASS | |
| LAT _____ LONG _____ | | RIVER BASIN | |
| STORET # | | AGENCY | |
| INVESTIGATORS | | | |
| FORM COMPLETED BY | | DATE <u>5/4/18</u> TIME _____ AM PM | REASON FOR SURVEY |

| | Habitat Parameter | Condition Category | | | |
|--|---|--|---|--|--|
| | | Optimal | Suboptimal | Marginal | Poor |
| Parameters to be evaluated in sampling reach | 1. Epifaunal Substrate/ Available Cover | Greater than 50% of substrate favorable for epifaunal colonization and fish cover; mix of snags, submerged logs, undercut banks, cobble or other stable habitat and at stage to allow full colonization potential (i.e., logs/snags that are <u>not</u> new fall and not transient). | 30-50% mix of stable habitat; well-suited for full colonization potential; adequate habitat for maintenance of populations; presence of additional substrate in the form of newfall, but not yet prepared for colonization (may rate at high end of scale). | 10-30% mix of stable habitat; habitat availability less than desirable; substrate frequently disturbed or removed. | Less than 10% stable habitat; lack of habitat is obvious; substrate unstable or lacking. |
| | SCORE | 20 19 18 17 16 | 15 14 13 12 11 | 10 9 8 7 6 | 5 4 3 2 1 0 |
| | 2. Pool Substrate Characterization | Mixture of substrate materials, with gravel and firm sand prevalent; root mats and submerged vegetation common. | Mixture of soft sand, mud, or clay; mud may be dominant; some root mats and submerged vegetation present. | All mud or clay or sand bottom; little or no root mat; no submerged vegetation. | Hard-pan clay or bedrock; no root mat or vegetation. |
| | SCORE | 20 19 18 17 16 | 15 14 13 12 11 | 10 9 8 7 6 | 5 4 3 2 1 0 |
| | 3. Pool Variability | Even mix of large-shallow, large-deep, small-shallow, small-deep pools present. | Majority of pools large-deep; very few shallow. | Shallow pools much more prevalent than deep pools. | Majority of pools small-shallow or pools absent. |
| | SCORE | 20 19 18 17 16 | 15 14 13 12 11 | 10 9 8 7 6 | 5 4 3 2 1 0 |
| 4. Sediment Deposition | Little or no enlargement of islands or point bars and less than <20% of the bottom affected by sediment deposition. | Some new increase in bar formation, mostly from gravel, sand or fine sediment; 20-50% of the bottom affected; slight deposition in pools. | Moderate deposition of new gravel, sand or fine sediment on old and new bars; 50-80% of the bottom affected; sediment deposits at obstructions, constrictions, and bends; moderate deposition of pools prevalent. | Heavy deposits of fine material, increased bar development; more than 80% of the bottom changing frequently; pools almost absent due to substantial sediment deposition. | |
| SCORE | 20 19 18 17 16 | 15 14 13 12 11 | 10 9 8 7 6 | 5 4 3 2 1 0 | |
| 5. Channel Flow Status | Water reaches base of both lower banks, and minimal amount of channel substrate is exposed. | Water fills >75% of the available channel; or <25% of channel substrate is exposed. | Water fills 25-75% of the available channel, and/or riffle substrates are mostly exposed. | Very little water in channel and mostly present as standing pools. | |
| SCORE | 20 19 18 17 16 | 15 14 13 12 11 | 10 9 8 7 6 | 5 4 3 2 1 0 | |

Walnut

HABITAT ASSESSMENT FIELD DATA SHEET—LOW GRADIENT STREAMS (BACK)

| Habitat Parameter | Condition Category | | | | | | | | | | | | | | | | | | | | |
|---|--|----|----|----|----|--|----|----|----|----|---|---|---|---|---|---|---|---|---|---|---|
| | Optimal | | | | | Suboptimal | | | | | Marginal | | | | | Poor | | | | | |
| 6. Channel Alteration | Channelization or dredging absent or minimal; stream with normal pattern. | | | | | Some channelization present, usually in areas of bridge abutments; evidence of past channelization, i.e., dredging, (greater than past 20 yr) may be present, but recent channelization is not present. | | | | | Channelization may be extensive; embankments or shoring structures present on both banks; and 40 to 80% of stream reach channelized and disrupted. | | | | | Banks shored with gabion or cement; over 80% of the stream reach channelized and disrupted. Instream habitat greatly altered or removed entirely. | | | | | |
| SCORE | 20 | 19 | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |
| 7. Channel Sinuosity | The bends in the stream increase the stream length 3 to 4 times longer than if it was in a straight line. (Note - channel braiding is considered normal in coastal plains and other low-lying areas. This parameter is not easily rated in these areas.) | | | | | The bends in the stream increase the stream length 1 to 2 times longer than if it was in a straight line. | | | | | The bends in the stream increase the stream length 1 to 2 times longer than if it was in a straight line. | | | | | Channel straight; waterway has been channelized for a long distance. | | | | | |
| SCORE | 20 | 19 | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |
| 8. Bank Stability (score each bank) | Banks stable; evidence of erosion or bank failure absent or minimal; little potential for future problems. <5% of bank affected. | | | | | Moderately stable; infrequent, small areas of erosion mostly healed over. 5-30% of bank in reach has areas of erosion. | | | | | Moderately unstable; 30-60% of bank in reach has areas of erosion; high erosion potential during floods. | | | | | Unstable; many eroded areas; "raw" areas frequent along straight sections and bends; obvious bank sloughing; 60-100% of bank has erosional scars. | | | | | |
| SCORE ___ (LB) | Left Bank | | 10 | 9 | | 8 | 7 | 6 | | | 5 | 4 | 3 | | | 2 | 1 | 0 | | | |
| SCORE ___ (RB) | Right Bank | | 10 | 9 | | 8 | 7 | 6 | | | 5 | 4 | 3 | | | 2 | 1 | 0 | | | |
| 9. Vegetative Protection (score each bank) | More than 90% of the streambank surfaces and immediate riparian zone covered by native vegetation, including trees, understory shrubs, or nonwoody macrophytes; vegetative disruption through grazing or mowing minimal or not evident; almost all plants allowed to grow naturally. | | | | | 70-90% of the streambank surfaces covered by native vegetation, but one class of plants is not well-represented; disruption evident but not affecting full plant growth potential to any great extent; more than one-half of the potential plant stubble height remaining. | | | | | 50-70% of the streambank surfaces covered by vegetation; disruption obvious; patches of bare soil or closely cropped vegetation common; less than one-half of the potential plant stubble height remaining. | | | | | Less than 50% of the streambank surfaces covered by vegetation; disruption of streambank vegetation is very high; vegetation has been removed to 5 centimeters or less in average stubble height. | | | | | |
| SCORE ___ (LB) | Left Bank | | 10 | 9 | | 8 | 7 | 6 | | | 5 | 4 | 3 | | | 2 | 1 | 0 | | | |
| SCORE ___ (RB) | Right Bank | | 10 | 9 | | 8 | 7 | 6 | | | 5 | 4 | 3 | | | 2 | 1 | 0 | | | |
| 10. Riparian Vegetative Zone Width (score each bank riparian zone) | Width of riparian zone >18 meters; human activities (i.e., parking lots, roadbeds, clear-cuts, lawns, or crops) have not impacted zone. | | | | | Width of riparian zone 12-18 meters; human activities have impacted zone only minimally. | | | | | Width of riparian zone 6-12 meters; human activities have impacted zone a great deal. | | | | | Width of riparian zone <6 meters: little or no riparian vegetation due to human activities. | | | | | |
| SCORE ___ (LB) | Left Bank | | 10 | 9 | | 8 | 7 | 6 | | | 5 | 4 | 3 | | | 2 | 1 | 0 | | | |
| SCORE ___ (RB) | Right Bank | | 10 | 9 | | 8 | 7 | 6 | | | 5 | 4 | 3 | | | 2 | 1 | 0 | | | |

Total Score _____

HABITAT ASSESSMENT FIELD DATA SHEET—LOW GRADIENT STREAMS (FRONT)

| | | | |
|-------------------|-----------------|--|-------------------|
| STREAM NAME | | LOCATION <u>Middle Jones</u> | |
| STATION # _____ | RIVERMILE _____ | STREAM CLASS | |
| LAT _____ | LONG _____ | RIVER BASIN | |
| STORET # | | AGENCY | |
| INVESTIGATORS | | | |
| FORM COMPLETED BY | | DATE <u>5/4/18</u> TIME _____ AM PM | REASON FOR SURVEY |

| Habitat Parameter | Condition Category | | | |
|---|--------------------|--|---|---|
| | Optimal | Suboptimal | Marginal | Poor |
| 1. Epifaunal Substrate/ Available Cover Greater than 50% of substrate favorable for epifaunal colonization and fish cover; mix of snags, submerged logs, undercut banks, cobble or other stable habitat and at stage to allow full colonization potential (i.e., logs/snags that are <u>not</u> new fall and not transient). SCORE | 20 19 18 17 16 | 30-50% mix of stable habitat; well-suited for full colonization potential; adequate habitat for maintenance of populations; presence of additional substrate in the form of new fall, but not yet prepared for colonization (may rate at high end of scale). 15 14 13 12 11 | 10-30% mix of stable habitat; habitat availability less than desirable; substrate frequently disturbed or removed. 10 9 8 7 6 | Less than 10% stable habitat; lack of habitat is obvious; substrate unstable or lacking. 5 4 3 2 1 0 |
| | 20 19 18 17 16 | 15 14 13 12 11 | 10 9 8 7 6 | 5 4 3 2 1 0 |
| 2. Pool Substrate Characterization Mixture of substrate materials, with gravel and firm sand prevalent; root mats and submerged vegetation common. SCORE | 20 19 18 17 16 | Mixture of soft sand, mud, or clay; mud may be dominant; some root mats and submerged vegetation present. 15 14 13 12 11 | All mud or clay or sand bottom; little or no root mat; no submerged vegetation. 10 9 8 7 6 | Hard-pan clay or bedrock; no root mat or vegetation. 5 4 3 2 1 0 |
| | 20 19 18 17 16 | 15 14 13 12 11 | 10 9 8 7 6 | 5 4 3 2 1 0 |
| 3. Pool Variability Even mix of large-shallow, large-deep, small-shallow, small-deep pools present. SCORE | 20 19 18 17 16 | Majority of pools large-deep; very few shallow. 15 14 13 12 11 | Shallow pools much more prevalent than deep pools. 10 9 8 7 6 | Majority of pools small-shallow or pools absent. 5 4 3 2 1 0 |
| | 20 19 18 17 16 | 15 14 13 12 11 | 10 9 8 7 6 | 5 4 3 2 1 0 |
| 4. Sediment Deposition Little or no enlargement of islands or point bars and less than <20% of the bottom affected by sediment deposition. SCORE | 20 19 18 17 16 | Some new increase in bar formation, mostly from gravel, sand or fine sediment; 20-50% of the bottom affected; slight deposition in pools. 15 14 13 12 11 | Moderate deposition of new gravel, sand or fine sediment on old and new bars; 50-80% of the bottom affected; sediment deposits at obstructions, constrictions, and bends; moderate deposition of pools prevalent. 10 9 8 7 6 | Heavy deposits of fine material, increased bar development; more than 80% of the bottom changing frequently; pools almost absent due to substantial sediment deposition. 5 4 3 2 1 0 |
| | 20 19 18 17 16 | 15 14 13 12 11 | 10 9 8 7 6 | 5 4 3 2 1 0 |
| 5. Channel Flow Status Water reaches base of both lower banks, and minimal amount of channel substrate is exposed. SCORE | 20 19 18 17 16 | Water fills >75% of the available channel; or <25% of channel substrate is exposed. 15 14 13 12 11 | Water fills 25-75% of the available channel, and/or riffle substrates are mostly exposed. 10 9 8 7 6 | Very little water in channel and mostly present as standing pools. 5 4 3 2 1 0 |
| | 20 19 18 17 16 | 15 14 13 12 11 | 10 9 8 7 6 | 5 4 3 2 1 0 |

HABITAT ASSESSMENT FIELD DATA SHEET—LOW GRADIENT STREAMS (BACK)

| Habitat Parameter | Condition Category | | | | | | | | | | | | | | | | | | | | | | | |
|---|--|----|----|----|----|------------|----|----|----|----|----------|---|------------|----|---|------|---|---|---|---|---|---|---|---|
| | Optimal | | | | | Suboptimal | | | | | Marginal | | | | | Poor | | | | | | | | |
| 6. Channel Alteration | Channelization or dredging absent or minimal; stream with normal pattern. | | | | | | | | | | | | | | | | | | | | | | | |
| SCORE | 20 | 19 | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | | | |
| 7. Channel Sinuosity | The bends in the stream increase the stream length 3 to 4 times longer than if it was in a straight line. (Note - channel braiding is considered normal in coastal plains and other low-lying areas. This parameter is not easily rated in these areas.) | | | | | | | | | | | | | | | | | | | | | | | |
| SCORE | 20 | 19 | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | | | |
| 8. Bank Stability (score each bank) | Banks stable; evidence of erosion or bank failure absent or minimal; little potential for future problems. <5% of bank affected. | | | | | | | | | | | | | | | | | | | | | | | |
| SCORE ___ (LB) | Left Bank | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | Right Bank | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |
| SCORE ___ (RB) | Left Bank | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | Right Bank | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |
| 9. Vegetative Protection (score each bank) | More than 90% of the streambank surfaces and immediate riparian zone covered by native vegetation, including trees, understory shrubs, or nonwoody macrophytes; vegetative disruption through grazing or mowing minimal or not evident; almost all plants allowed to grow naturally. | | | | | | | | | | | | | | | | | | | | | | | |
| SCORE ___ (LB) | Left Bank | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | Right Bank | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |
| SCORE ___ (RB) | Left Bank | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | Right Bank | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |
| 10. Riparian Vegetative Zone Width (score each bank riparian zone) | Width of riparian zone >18 meters; human activities (i.e., parking lots, roadbeds, clear-cuts, lawns, or crops) have not impacted zone. | | | | | | | | | | | | | | | | | | | | | | | |
| SCORE ___ (LB) | Left Bank | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | Right Bank | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |
| SCORE ___ (RB) | Left Bank | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | Right Bank | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |

Total Score _____

HABITAT ASSESSMENT FIELD DATA SHEET—LOW GRADIENT STREAMS (FRONT)

| | | |
|---------------------------------|--|-------------------|
| STREAM NAME | LOCATION <u>Braided Trib</u> | |
| STATION # _____ RIVERMILE _____ | STREAM CLASS | |
| LAT _____ LONG _____ | RIVER BASIN | |
| STORET # | AGENCY | |
| INVESTIGATORS | | |
| FORM COMPLETED BY | DATE <u>5/4/18</u> TIME _____ AM PM | REASON FOR SURVEY |

| | Habitat Parameter | Condition Category | | | |
|--|--|--|--|--|-------------|
| | Optimal | Suboptimal | Marginal | Poor | |
| Parameters to be evaluated in sampling reach | 1. Epifaunal Substrate/ Available Cover Greater than 50% of substrate favorable for epifaunal colonization and fish cover; mix of snags, submerged logs, undercut banks, cobble or other stable habitat and at stage to allow full colonization potential (i.e., logs/snags that are <u>not</u> new fall and not transient). | 30-50% mix of stable habitat; well-suited for full colonization potential; adequate habitat for maintenance of populations; presence of additional substrate in the form of new fall, but not yet prepared for colonization (may rate at high end of scale). | 10-30% mix of stable habitat; habitat availability less than desirable; substrate frequently disturbed or removed. | Less than 10% stable habitat; lack of habitat is obvious; substrate unstable or lacking. | |
| | SCORE | 20 19 18 17 16 | 15 14 13 12 11 | 10 9 8 7 6 | 5 4 3 2 1 0 |
| | 2. Pool Substrate Characterization Mixture of substrate materials, with gravel and firm sand prevalent; root mats and submerged vegetation common. | Mixture of soft sand, mud, or clay; mud may be dominant; some root mats and submerged vegetation present. | All mud or clay or sand bottom; little or no root mat; no submerged vegetation. | Hard-pan clay or bedrock; no root mat or vegetation. | |
| | SCORE | 20 19 18 17 16 | 15 14 13 12 11 | 10 9 8 7 6 | 5 4 3 2 1 0 |
| | 3. Pool Variability Even mix of large-shallow, large-deep, small-shallow, small-deep pools present. | Majority of pools large-deep; very few shallow. | Shallow pools much more prevalent than deep pools. | Majority of pools small-shallow or pools absent. | |
| SCORE | 20 19 18 17 16 | 15 14 13 12 11 | 10 9 8 7 6 | 5 4 3 2 1 0 | |
| 4. Sediment Deposition Little or no enlargement of islands or point bars and less than <20% of the bottom affected by sediment deposition. | Some new increase in bar formation, mostly from gravel, sand or fine sediment; 20-50% of the bottom affected; slight deposition in pools. | Moderate deposition of new gravel, sand or fine sediment on old and new bars; 50-80% of the bottom affected; sediment deposits at obstructions, constrictions, and bends; moderate deposition of pools prevalent. | Heavy deposits of fine material, increased bar development; more than 80% of the bottom changing frequently; pools almost absent due to substantial sediment deposition. | | |
| SCORE | 20 19 18 17 16 | 15 14 13 12 11 | 10 9 8 7 6 | 5 4 3 2 1 0 | |
| 5. Channel Flow Status Water reaches base of both lower banks, and minimal amount of channel substrate is exposed. | Water fills >75% of the available channel; or <25% of channel substrate is exposed. | Water fills 25-75% of the available channel, and/or riffle substrates are mostly exposed. | Very little water in channel and mostly present as standing pools. | | |
| SCORE | 20 19 18 17 16 | 15 14 13 12 11 | 10 9 8 7 6 | 5 4 3 2 1 0 | |

Braided Trib

HABITAT ASSESSMENT FIELD DATA SHEET—LOW GRADIENT STREAMS (BACK)

| Habitat Parameter | Condition Category | | | |
|--|--|--|---|---|
| | Optimal | Suboptimal | Marginal | Poor |
| 6. Channel Alteration | Channelization or dredging absent or minimal; stream with normal pattern. | Some channelization present, usually in areas of bridge abutments; evidence of past channelization, i.e., dredging, (greater than past 20 yr) may be present, but recent channelization is not present. | Channelization may be extensive; embankments or shoring structures present on both banks; and 40 to 80% of stream reach channelized and disrupted. | Banks shored with gabion or cement; over 80% of the stream reach channelized and disrupted. Instream habitat greatly altered or removed entirely. |
| SCORE | 20 19 18 17 16 | 15 14 13 12 11 | 10 9 8 7 6 | 5 4 3 2 1 0 |
| 7. Channel Sinuosity | The bends in the stream increase the stream length 3 to 4 times longer than if it was in a straight line. (Note - channel braiding is considered normal in coastal plains and other low-lying areas. This parameter is not easily rated in these areas.) | The bends in the stream increase the stream length 1 to 2 times longer than if it was in a straight line. <i>Braided</i> | The bends in the stream increase the stream length 1 to 2 times longer than if it was in a straight line. | Channel straight; waterway has been channelized for a long distance. |
| SCORE | 20 19 18 17 16 | 15 14 13 12 11 | 10 9 8 7 6 | 5 4 3 2 1 0 |
| 8. Bank Stability (score each bank) | Banks stable; evidence of erosion or bank failure absent or minimal; little potential for future problems. <5% of bank affected. | Moderately stable; infrequent, small areas of erosion mostly healed over. 5-30% of bank in reach has areas of erosion. | Moderately unstable; 30-60% of bank in reach has areas of erosion; high erosion potential during floods. | Unstable; many eroded areas; "raw" areas frequent along straight sections and bends; obvious bank sloughing; 60-100% of bank has erosional scars. |
| SCORE ___ (LB) | Left Bank 10 9 | 8 7 6 | 5 4 3 | 2 1 0 |
| SCORE ___ (RB) | Right Bank 10 9 | 8 7 6 | 5 4 3 | 2 1 0 |
| 9. Vegetative Protection (score each bank) Note: determine left or right side by facing downstream. | More than 90% of the streambank surfaces and immediate riparian zone covered by native vegetation, including trees, understory shrubs, or nonwoody macrophytes; vegetative disruption through grazing or mowing minimal or not evident; almost all plants allowed to grow naturally. | 70-90% of the streambank surfaces covered by native vegetation, but one class of plants is not well-represented; disruption evident but not affecting full plant growth potential to any great extent; more than one-half of the potential plant stubble height remaining. | 50-70% of the streambank surfaces covered by vegetation; disruption obvious; patches of bare soil or closely cropped vegetation common; less than one-half of the potential plant stubble height remaining. | Less than 50% of the streambank surfaces covered by vegetation; disruption of streambank vegetation is very high; vegetation has been removed to 5 centimeters or less in average stubble height. |
| SCORE ___ (LB) | Left Bank 10 9 | 8 7 6 | 5 4 3 | 2 1 0 |
| SCORE ___ (RB) | Right Bank 10 9 | 8 7 6 | 5 4 3 | 2 1 0 |
| 10. Riparian Vegetative Zone Width (score each bank riparian zone) | Width of riparian zone >18 meters; human activities (i.e., parking lots, roadbeds, clear-cuts, lawns, or crops) have not impacted zone. | Width of riparian zone 12-18 meters; human activities have impacted zone only minimally. | Width of riparian zone 6-12 meters; human activities have impacted zone a great deal. | Width of riparian zone <6 meters; little or no riparian vegetation due to human activities. |
| SCORE ___ (LB) | Left Bank 10 9 | 8 7 6 | 5 4 3 | 2 1 0 |
| SCORE ___ (RB) | Right Bank 10 9 | 8 7 6 | 5 4 3 | 2 1 0 |

Parameters to be evaluated broader than sampling reach

Total Score _____

HABITAT ASSESSMENT FIELD DATA SHEET—LOW GRADIENT STREAMS (FRONT)

| | | |
|---------------------------------|--------------------------------|-------------------|
| STREAM NAME | LOCATION <u>Railroad Trib</u> | |
| STATION # _____ RIVERMILE _____ | STREAM CLASS | |
| LAT _____ LONG _____ | RIVER BASIN | |
| STORET # | AGENCY | |
| INVESTIGATORS | | |
| FORM COMPLETED BY | DATE _____ TIME _____ AM PM | REASON FOR SURVEY |

| | Habitat Parameter | Condition Category | | | |
|--|--|--|---|---|--|
| | | Optimal | Suboptimal | Marginal | Poor |
| Parameters to be evaluated in sampling reach | 1. Epifaunal Substrate/ Available Cover | Greater than 50% of substrate favorable for epifaunal colonization and fish cover; mix of snags, submerged logs, undercut banks, cobble or other stable habitat and at stage to allow full colonization potential (i.e., logs/snags that are <u>not</u> new fall and not transient). | 30-50% mix of stable habitat; well-suited for full colonization potential; adequate habitat for maintenance of populations; presence of additional substrate in the form of newfall, but not yet prepared for colonization (may rate at high end of scale). | 10-30% mix of stable habitat; habitat availability less than desirable; substrate frequently disturbed or removed. | Less than 10% stable habitat; lack of habitat is obvious; substrate unstable or lacking. |
| | SCORE | 20 19 18 17 16 | 15 14 13 12 11 | 10 9 8 7 6 | 5 4 3 2 1 0 |
| | 2. Pool Substrate Characterization | Mixture of substrate materials, with gravel and firm sand prevalent; root mats and submerged vegetation common. | Mixture of soft sand, mud, or clay; mud may be dominant; some root mats and submerged vegetation present. | All mud or clay or sand bottom; little or no root mat; no submerged vegetation. | Hard-pan clay or bedrock; no root mat or vegetation. |
| | SCORE | 20 19 18 17 16 | 15 14 13 12 11 | 10 9 8 7 6 | 5 4 3 2 1 0 |
| | 3. Pool Variability | Even mix of large-shallow, large-deep, small-shallow, small-deep pools present. | Majority of pools large-deep; very few shallow. | Shallow pools much more prevalent than deep pools. | Majority of pools small-shallow or pools absent. |
| | SCORE | 20 19 18 17 16 | 15 14 13 12 11 | 10 9 8 7 6 | 5 4 3 2 1 0 |
| | 4. Sediment Deposition | Little or no enlargement of islands or point bars and less than <20% of the bottom affected by sediment deposition. | Some new increase in bar formation, mostly from gravel, sand or fine sediment; 20-50% of the bottom affected; slight deposition in pools. | Moderate deposition of new gravel, sand or fine sediment on old and new bars; 50-80% of the bottom affected; sediment deposits at obstructions, constrictions, and bends; moderate deposition of pools prevalent. | Heavy deposits of fine material, increased bar development; more than 80% of the bottom changing frequently; pools almost absent due to substantial sediment deposition. |
| | SCORE | 20 19 18 17 16 | 15 14 13 12 11 | 10 9 8 7 6 | 5 4 3 2 1 0 |
| | 5. Channel Flow Status | Water reaches base of both lower banks, and minimal amount of channel substrate is exposed. | Water fills >75% of the available channel; or <25% of channel substrate is exposed. | Water fills 25-75% of the available channel, and/or riffle substrates are mostly exposed. | Very little water in channel and mostly present as standing pools. |
| | SCORE | 20 19 18 17 16 | 15 14 13 12 11 | 10 9 8 7 6 | 5 4 3 2 1 0 |

Railroad Trib

HABITAT ASSESSMENT FIELD DATA SHEET—LOW GRADIENT STREAMS (BACK)

| Habitat Parameter | Condition Category | | | | | | | | | | | | | | | | | | | | |
|---|--|----|----|----|----|------------|----|----|----|----|----------|---|---|---|---|------|---|---|---|---|---|
| | Optimal | | | | | Suboptimal | | | | | Marginal | | | | | Poor | | | | | |
| 6. Channel Alteration | Channelization or dredging absent or minimal; stream with normal pattern. | | | | | | | | | | | | | | | | | | | | |
| | Some channelization present, usually in areas of bridge abutments; evidence of past channelization, i.e., dredging, (greater than past 20 yr) may be present, but recent channelization is not present. | | | | | | | | | | | | | | | | | | | | |
| Channelization may be extensive; embankments or shoring structures present on both banks; and 40 to 80% of stream reach channelized and disrupted. | | | | | | | | | | | | | | | | | | | | | |
| Banks shored with gabion or cement; over 80% of the stream reach channelized and disrupted. Instream habitat greatly altered or removed entirely. | | | | | | | | | | | | | | | | | | | | | |
| SCORE | 20 | 19 | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |
| 7. Channel Sinuosity | The bends in the stream increase the stream length 3 to 4 times longer than if it was in a straight line. (Note - channel braiding is considered normal in coastal plains and other low-lying areas. This parameter is not easily rated in these areas.) | | | | | | | | | | | | | | | | | | | | |
| | The bends in the stream increase the stream length 1 to 2 times longer than if it was in a straight line. | | | | | | | | | | | | | | | | | | | | |
| The bends in the stream increase the stream length 1 to 2 times longer than if it was in a straight line. | | | | | | | | | | | | | | | | | | | | | |
| Channel straight; waterway has been channelized for a long distance. | | | | | | | | | | | | | | | | | | | | | |
| SCORE | 20 | 19 | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |
| 8. Bank Stability (score each bank) | Banks stable; evidence of erosion or bank failure absent or minimal; little potential for future problems. <5% of bank affected. | | | | | | | | | | | | | | | | | | | | |
| | Moderately stable; infrequent, small areas of erosion mostly healed over. 5-30% of bank in reach has areas of erosion. | | | | | | | | | | | | | | | | | | | | |
| Moderately unstable; 30-60% of bank in reach has areas of erosion; high erosion potential during floods. | | | | | | | | | | | | | | | | | | | | | |
| Unstable; many eroded areas; "raw" areas frequent along straight sections and bends; obvious bank sloughing; 60-100% of bank has erosional scars. | | | | | | | | | | | | | | | | | | | | | |
| SCORE ___ (LB) | Left Bank | 10 | 9 | | | 8 | 7 | 6 | | | 5 | 4 | 3 | | | 2 | 1 | 0 | | | |
| SCORE ___ (RB) | Right Bank | 10 | 9 | | | 8 | 7 | 6 | | | 5 | 4 | 3 | | | 2 | 1 | 0 | | | |
| 9. Vegetative Protection (score each bank) | More than 90% of the streambank surfaces and immediate riparian zone covered by native vegetation, including trees, understory shrubs, or nonwoody macrophytes; vegetative disruption through grazing or mowing minimal or not evident; almost all plants allowed to grow naturally. | | | | | | | | | | | | | | | | | | | | |
| | 70-90% of the streambank surfaces covered by native vegetation, but one class of plants is not well-represented; disruption evident but not affecting full plant growth potential to any great extent; more than one-half of the potential plant stubble height remaining. | | | | | | | | | | | | | | | | | | | | |
| 50-70% of the streambank surfaces covered by vegetation; disruption obvious; patches of bare soil or closely cropped vegetation common; less than one-half of the potential plant stubble height remaining. | | | | | | | | | | | | | | | | | | | | | |
| Less than 50% of the streambank surfaces covered by vegetation; disruption of streambank vegetation is very high; vegetation has been removed to 5 centimeters or less in average stubble height. | | | | | | | | | | | | | | | | | | | | | |
| SCORE ___ (LB) | Left Bank | 10 | 9 | | | 8 | 7 | 6 | | | 5 | 4 | 3 | | | 2 | 1 | 0 | | | |
| SCORE ___ (RB) | Right Bank | 10 | 9 | | | 8 | 7 | 6 | | | 5 | 4 | 3 | | | 2 | 1 | 0 | | | |
| 10. Riparian Vegetative Zone Width (score each bank riparian zone) | Width of riparian zone >18 meters; human activities (i.e., parking lots, roadbeds, clear-cuts, lawns, or crops) have not impacted zone. | | | | | | | | | | | | | | | | | | | | |
| | Width of riparian zone 12-18 meters; human activities have impacted zone only minimally. | | | | | | | | | | | | | | | | | | | | |
| Width of riparian zone 6-12 meters; human activities have impacted zone a great deal. | | | | | | | | | | | | | | | | | | | | | |
| Width of riparian zone <6 meters; little or no riparian vegetation due to human activities. | | | | | | | | | | | | | | | | | | | | | |
| SCORE ___ (LB) | Left Bank | 10 | 9 | | | 8 | 7 | 6 | | | 5 | 4 | 3 | | | 2 | 1 | 0 | | | |
| SCORE ___ (RB) | Right Bank | 10 | 9 | | | 8 | 7 | 6 | | | 5 | 4 | 3 | | | 2 | 1 | 0 | | | |

Total Score _____

HABITAT ASSESSMENT FIELD DATA SHEET—LOW GRADIENT STREAMS (FRONT)

| | | |
|---------------------------------|--|-------------------|
| STREAM NAME | LOCATION <u>Cypress</u> | |
| STATION # _____ RIVERMILE _____ | STREAM CLASS | |
| LAT _____ LONG _____ | RIVER BASIN | |
| STORET # | AGENCY | |
| INVESTIGATORS | | |
| FORM COMPLETED BY | DATE <u>5/4/18</u> TIME _____ AM PM | REASON FOR SURVEY |

| Parameters to be evaluated in sampling reach | Habitat Parameter | Condition Category | | | |
|--|--|---|---|--|-------------|
| | | Optimal | Suboptimal | Marginal | Poor |
| | 1. Epifaunal Substrate/ Available Cover Greater than 50% of substrate favorable for epifaunal colonization and fish cover; mix of snags, submerged logs, undercut banks, cobble or other stable habitat and at stage to allow full colonization potential (i.e., logs/snags that are <u>not</u> new fall and not transient). | 30-50% mix of stable habitat; well-suited for full colonization potential; adequate habitat for maintenance of populations; presence of additional substrate in the form of newfall, but not yet prepared for colonization (may rate at high end of scale). | 10-30% mix of stable habitat; habitat availability less than desirable; substrate frequently disturbed or removed. | Less than 10% stable habitat; lack of habitat is obvious; substrate unstable or lacking. | |
| | SCORE | 20 19 18 17 16 | 15 14 13 12 11 | 10 9 8 7 6 | 5 4 3 2 1 0 |
| | 2. Pool Substrate Characterization Mixture of substrate materials, with gravel and firm sand prevalent; root mats and submerged vegetation common. | Mixture of soft sand, mud, or clay; mud may be dominant; some root mats and submerged vegetation present. | All mud or clay or sand bottom; little or no root mat; no submerged vegetation. | Hard-pan clay or bedrock; no root mat or vegetation. | |
| | SCORE | 20 19 18 17 16 | 15 14 13 12 11 | 10 9 8 7 6 | 5 4 3 2 1 0 |
| | 3. Pool Variability Even mix of large-shallow, large-deep, small-shallow, small-deep pools present. | Majority of pools large-deep; very few shallow. | Shallow pools much more prevalent than deep pools. | Majority of pools small-shallow or pools absent. | |
| | SCORE | 20 19 18 17 16 | 15 14 13 12 11 | 10 9 8 7 6 | 5 4 3 2 1 0 |
| | 4. Sediment Deposition Little or no enlargement of islands or point bars and less than <20% of the bottom affected by sediment deposition. | Some new increase in bar formation, mostly from gravel, sand or fine sediment; 20-50% of the bottom affected; slight deposition in pools. | Moderate deposition of new gravel, sand or fine sediment on old and new bars; 50-80% of the bottom affected; sediment deposits at obstructions, constrictions, and bends; moderate deposition of pools prevalent. | Heavy deposits of fine material, increased bar development; more than 80% of the bottom changing frequently; pools almost absent due to substantial sediment deposition. | |
| | SCORE | 20 19 18 17 16 | 15 14 13 12 11 | 10 9 8 7 6 | 5 4 3 2 1 0 |
| | 5. Channel Flow Status Water reaches base of both lower banks, and minimal amount of channel substrate is exposed. | Water fills >75% of the available channel; or <25% of channel substrate is exposed. | Water fills 25-75% of the available channel, and/or riffle substrates are mostly exposed. | Very little water in channel and mostly present as standing pools. | |
| | SCORE | 20 19 18 17 16 | 15 14 13 12 11 | 10 9 8 7 6 | 5 4 3 2 1 0 |

Cypress

HABITAT ASSESSMENT FIELD DATA SHEET—LOW GRADIENT STREAMS (BACK)

| Habitat Parameter | Condition Category | | | | | | | | | | | | | | | | | | | | |
|---|--|----|----|----|----|--|----|----|----|----|---|---|---|---|---|---|---|---|---|---|---|
| | Optimal | | | | | Suboptimal | | | | | Marginal | | | | | Poor | | | | | |
| 6. Channel Alteration | Channelization or dredging absent or minimal; stream with normal pattern. | | | | | Some channelization present, usually in areas of bridge abutments; evidence of past channelization, i.e., dredging, (greater than past 20 yr) may be present, but recent channelization is not present. | | | | | Channelization may be extensive; embankments or shoring structures present on both banks; and 40 to 80% of stream reach channelized and disrupted. | | | | | Banks shored with gabion or cement; over 80% of the stream reach channelized and disrupted. Instream habitat greatly altered or removed entirely. | | | | | |
| SCORE | 20 | 19 | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |
| 7. Channel Sinuosity | The bends in the stream increase the stream length 3 to 4 times longer than if it was in a straight line. (Note - channel braiding is considered normal in coastal plains and other low-lying areas. This parameter is not easily rated in these areas.) | | | | | The bends in the stream increase the stream length 1 to 2 times longer than if it was in a straight line. | | | | | The bends in the stream increase the stream length 1 to 2 times longer than if it was in a straight line. | | | | | Channel straight; waterway has been channelized for a long distance. | | | | | |
| SCORE | 20 | 19 | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |
| 8. Bank Stability (score each bank) | Banks stable; evidence of erosion or bank failure absent or minimal; little potential for future problems. <5% of bank affected. | | | | | Moderately stable; infrequent, small areas of erosion mostly healed over. 5-30% of bank in reach has areas of erosion. | | | | | Moderately unstable; 30-60% of bank in reach has areas of erosion; high erosion potential during floods. | | | | | Unstable; many eroded areas; "raw" areas frequent along straight sections and bends; obvious bank sloughing; 60-100% of bank has erosional scars. | | | | | |
| SCORE ___ (LB) | Left Bank 10 9 | | | | | 8 7 6 | | | | | 5 4 3 | | | | | 2 1 0 | | | | | |
| SCORE ___ (RB) | Right Bank 10 9 | | | | | 8 7 6 | | | | | 5 4 3 | | | | | 2 1 0 | | | | | |
| 9. Vegetative Protection (score each bank) | More than 90% of the streambank surfaces and immediate riparian zone covered by native vegetation, including trees, understory shrubs, or nonwoody macrophytes; vegetative disruption through grazing or mowing minimal or not evident; almost all plants allowed to grow naturally. | | | | | 70-90% of the streambank surfaces covered by native vegetation, but one class of plants is not well-represented; disruption evident but not affecting full plant growth potential to any great extent; more than one-half of the potential plant stubble height remaining. | | | | | 50-70% of the streambank surfaces covered by vegetation; disruption obvious; patches of bare soil or closely cropped vegetation common; less than one-half of the potential plant stubble height remaining. | | | | | Less than 50% of the streambank surfaces covered by vegetation; disruption of streambank vegetation is very high; vegetation has been removed to 5 centimeters or less in average stubble height. | | | | | |
| SCORE ___ (LB) | Left Bank 10 9 | | | | | 8 7 6 | | | | | 5 4 3 | | | | | 2 1 0 | | | | | |
| SCORE ___ (RB) | Right Bank 10 9 | | | | | 8 7 6 | | | | | 5 4 3 | | | | | 2 1 0 | | | | | |
| 10. Riparian Vegetative Zone Width (score each bank riparian zone) | Width of riparian zone >18 meters; human activities (i.e., parking lots, roadbeds, clear-cuts, lawns, or crops) have not impacted zone. | | | | | Width of riparian zone 12-18 meters; human activities have impacted zone only minimally. | | | | | Width of riparian zone 6-12 meters; human activities have impacted zone a great deal. | | | | | Width of riparian zone <6 meters; little or no riparian vegetation due to human activities. | | | | | |
| SCORE ___ (LB) | Left Bank 10 9 | | | | | 8 7 6 | | | | | 5 4 3 | | | | | 2 1 0 | | | | | |
| SCORE ___ (RB) | Right Bank 10 9 | | | | | 8 7 6 | | | | | 5 4 3 | | | | | 2 1 0 | | | | | |

Total Score _____



APPENDIX G

Design Computations

RIVERMORPH CROSS SECTION SUMMARY

 River Name: Proposed Design
 Reach Name: Main Stem
 Cross Section Name: Typical Section - B stream
 Survey Date: 09/27/2018

Cross Section Data Entry

BM Elevation: 0 ft
 Backsight Rod Reading: 0 ft

| TAPE | FS | ELEV | NOTE |
|-------|----|------|------|
| 0 | 0 | 2 | |
| 10 | 0 | 2 | BKF |
| 11.75 | 0 | 1.3 | |
| 16.25 | 0 | 1 | |
| 20.75 | 0 | 1.3 | |
| 22.5 | 0 | 2 | |
| 32 | 0 | 2 | |

 Cross Sectional Geometry

| | Channel | Left | Right |
|---------------------------|---------|-------|-------|
| Floodprone Elevation (ft) | 3 | 3 | 3 |
| Bankfull Elevation (ft) | 2 | 2 | 2 |
| Floodprone width (ft) | 32 | ----- | ----- |
| Bankfull width (ft) | 12.5 | 6.25 | 6.25 |
| Entrenchment Ratio | 2.56 | ----- | ----- |
| Mean Depth (ft) | 0.71 | 0.71 | 0.71 |
| Maximum Depth (ft) | 1 | 1 | 1 |
| width/Depth Ratio | 17.61 | 8.8 | 8.8 |
| Bankfull Area (sq ft) | 8.88 | 4.44 | 4.44 |
| wetted Perimeter (ft) | 12.79 | 7.39 | 7.39 |
| Hydraulic Radius (ft) | 0.69 | 0.6 | 0.6 |
| Begin BKF Station | 10 | 10 | 16.25 |
| End BKF Station | 22.5 | 16.25 | 22.5 |

 Entrainment Calculations

Entrainment Formula: Rosgen Modified Shields Curve

| | Channel | Left Side | Right Side |
|-------------------------|---------|-----------|------------|
| Slope | 0 | 0 | 0 |
| Shear Stress (lb/sq ft) | | | |
| Movable Particle (mm) | | | |

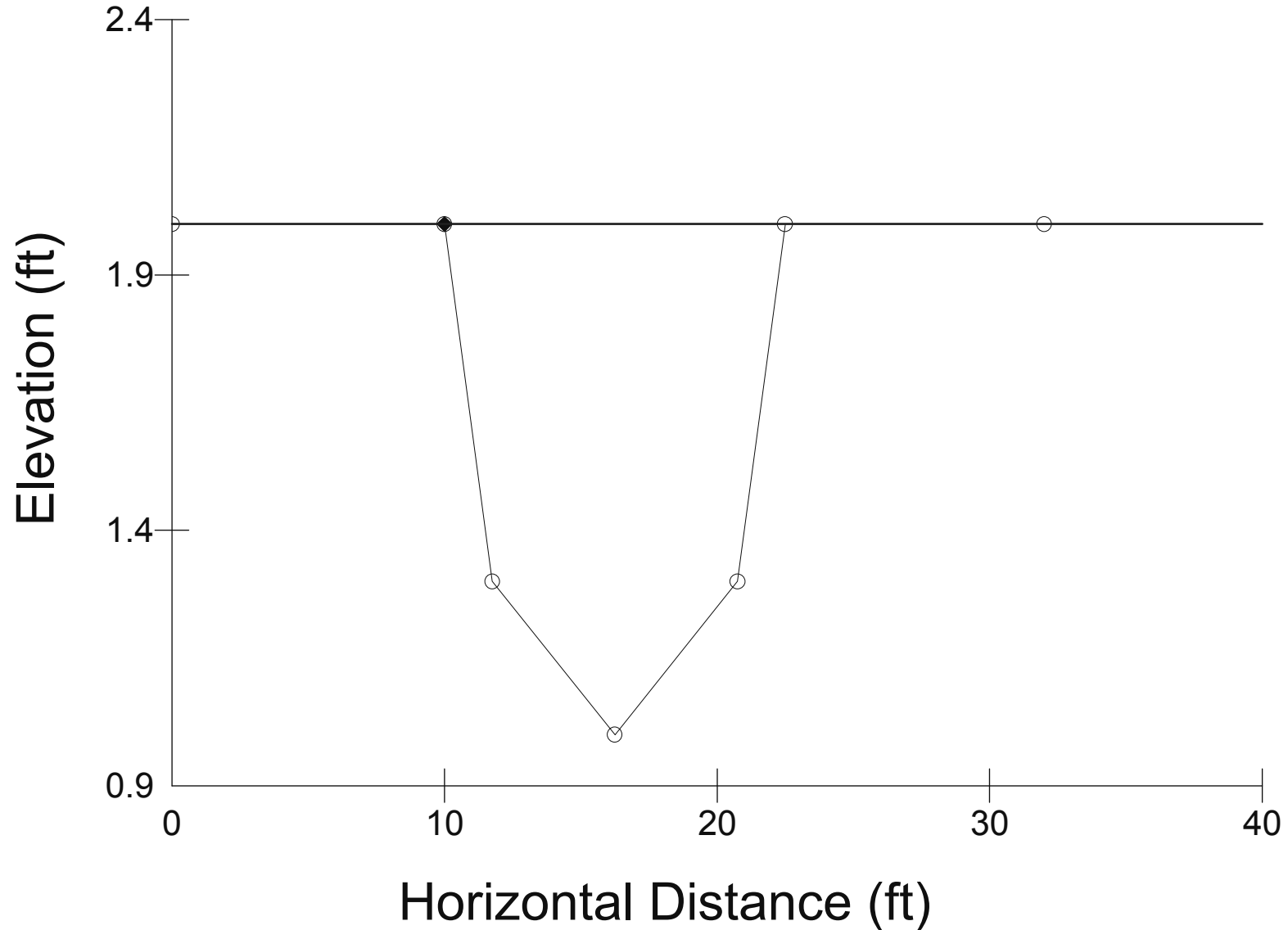
Typical Section - B stream

○ Ground Points ◆ Bankfull Indicators ▼ Water Surface Points

Wbkf = 12.5

Dbkf = .71

Abkf = 8.88



RIVERMORPH CROSS SECTION SUMMARY

 River Name: Proposed Design
 Reach Name: Main Stem
 Cross Section Name: Typical Section - C stream
 Survey Date: 09/13/2018

Cross Section Data Entry

BM Elevation: 0 ft
 Backsight Rod Reading: 0 ft

| TAPE | FS | ELEV | NOTE |
|------|----|------|------|
| 0 | 0 | 2 | |
| 10 | 0 | 2 | BKF |
| 11.5 | 0 | 1.4 | |
| 14.5 | 0 | 1.2 | |
| 17.5 | 0 | 1.4 | |
| 19 | 0 | 2 | |
| 29 | 0 | 2 | |

 Cross Sectional Geometry

| | Channel | Left | Right |
|---------------------------|---------|-------|-------|
| Floodprone Elevation (ft) | 2.8 | 2.8 | 2.8 |
| Bankfull Elevation (ft) | 2 | 2 | 2 |
| Floodprone width (ft) | 29 | ----- | ----- |
| Bankfull width (ft) | 9 | 4.5 | 4.5 |
| Entrenchment Ratio | 3.22 | ----- | ----- |
| Mean Depth (ft) | 0.57 | 0.57 | 0.57 |
| Maximum Depth (ft) | 0.8 | 0.8 | 0.8 |
| width/Depth Ratio | 15.79 | 7.94 | 7.89 |
| Bankfull Area (sq ft) | 5.1 | 2.55 | 2.55 |
| wetted Perimeter (ft) | 9.24 | 5.42 | 5.42 |
| Hydraulic Radius (ft) | 0.55 | 0.47 | 0.47 |
| Begin BKF Station | 10 | 10 | 14.5 |
| End BKF Station | 19 | 14.5 | 19 |

 Entrainment Calculations

Entrainment Formula: Rosgen Modified Shields Curve

| | Channel | Left Side | Right Side |
|-------------------------|---------|-----------|------------|
| Slope | 0 | 0 | 0 |
| Shear Stress (lb/sq ft) | | | |
| Movable Particle (mm) | | | |

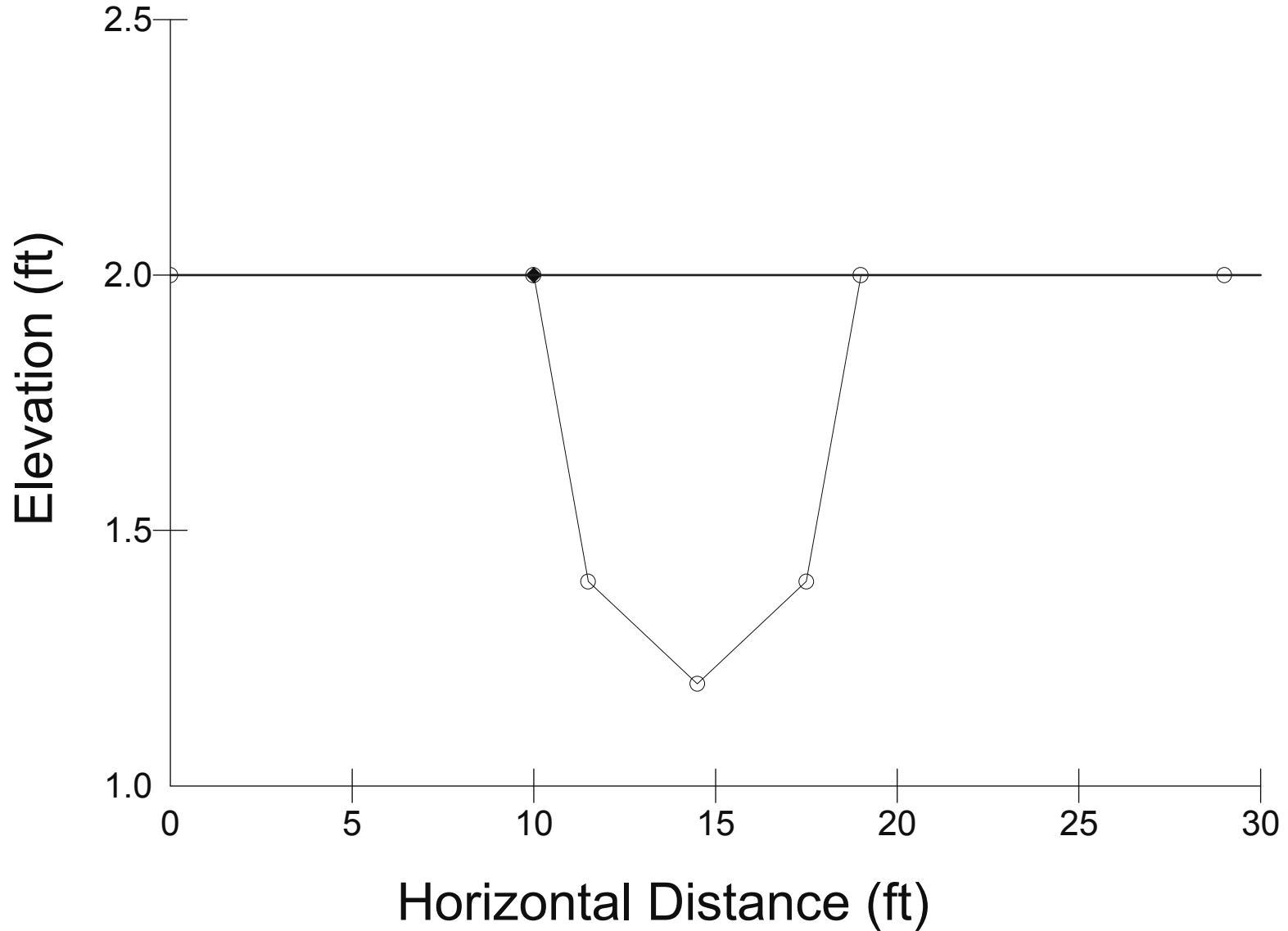
Typ Section - 9 ft

○ Ground Points ◆ Bankfull Indicators ▼ Water Surface Points

Wbkf = 9

Dbkf = .57

Abkf = 5.1



RIVERMORPH CROSS SECTION SUMMARY

 River Name: Proposed Design
 Reach Name: South Tributary
 Cross Section Name: Typical Section - B stream
 Survey Date: 09/18/2018

Cross Section Data Entry

BM Elevation: 0 ft
 Backsight Rod Reading: 0 ft

| TAPE | FS | ELEV | NOTE |
|-------|----|------|------|
| 0 | 0 | 2 | |
| 10 | 0 | 2 | BKF |
| 10.75 | 0 | 1.7 | |
| 12 | 0 | 1.7 | |
| 13 | 0 | 1.3 | |
| 14 | 0 | 1.3 | |
| 15 | 0 | 1.7 | |
| 16.25 | 0 | 1.7 | |
| 17 | 0 | 2 | |
| 26 | 0 | 2 | |

 Cross Sectional Geometry

| | Channel | Left | Right |
|---------------------------|---------|-------|-------|
| Floodprone Elevation (ft) | 2.7 | 2.7 | 2.7 |
| Bankfull Elevation (ft) | 2 | 2 | 2 |
| Floodprone width (ft) | 26 | ----- | ----- |
| Bankfull width (ft) | 7 | 3 | 4 |
| Entrenchment Ratio | 3.71 | ----- | ----- |
| Mean Depth (ft) | 0.38 | 0.33 | 0.42 |
| Maximum Depth (ft) | 0.7 | 0.7 | 0.7 |
| width/Depth Ratio | 18.42 | 9.11 | 9.52 |
| Bankfull Area (sq ft) | 2.67 | 0.99 | 1.69 |
| wetted Perimeter (ft) | 7.27 | 3.83 | 4.83 |
| Hydraulic Radius (ft) | 0.37 | 0.26 | 0.35 |
| Begin BKF Station | 10 | 10 | 13 |
| End BKF Station | 17 | 13 | 17 |

 Entrainment Calculations

Entrainment Formula: Rosgen Modified Shields Curve

| | Channel | Left Side | Right Side |
|-------------------------|---------|-----------|------------|
| Slope | 0 | 0 | 0 |
| Shear Stress (lb/sq ft) | | | |
| Movable Particle (mm) | | | |

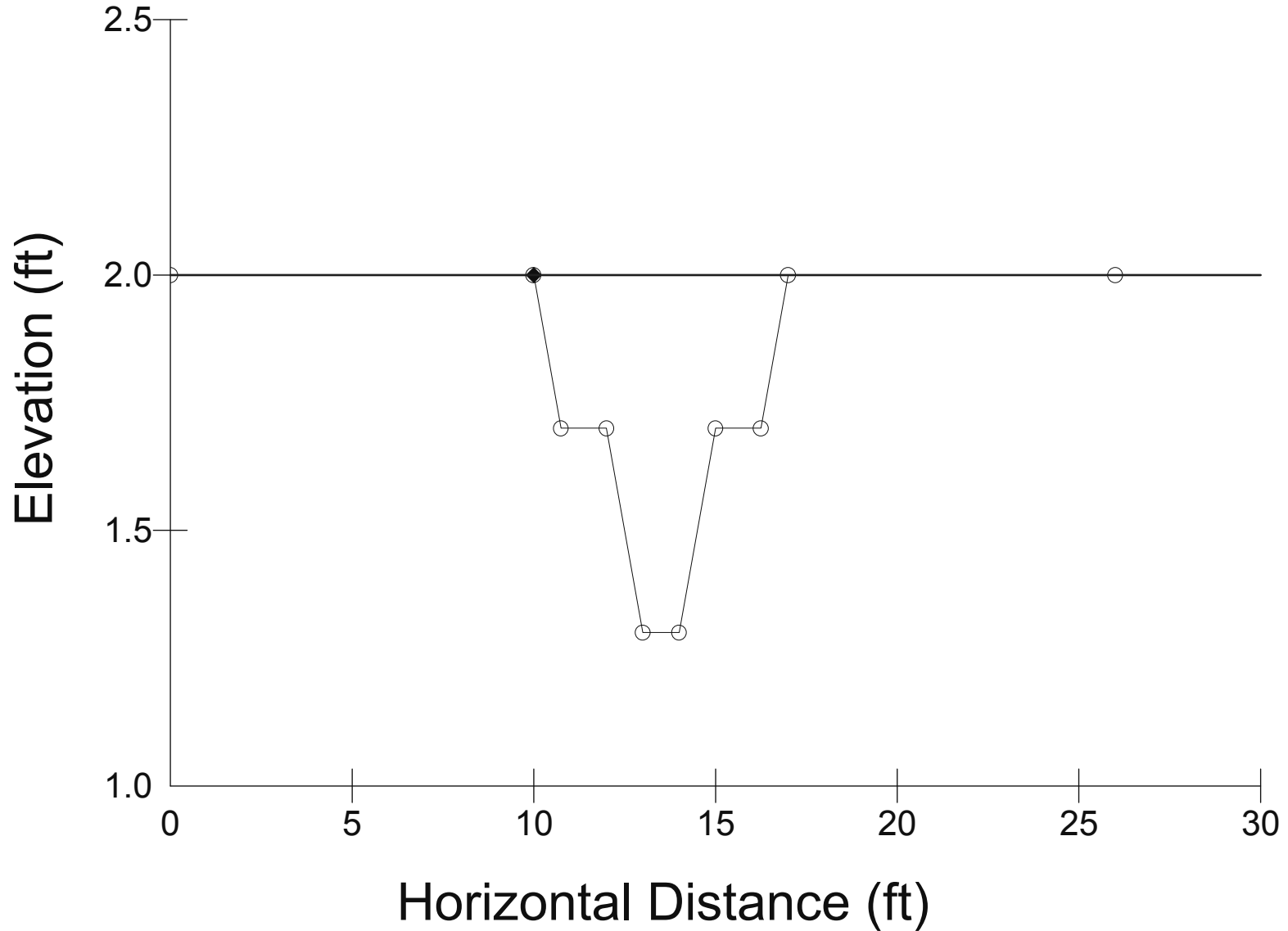
Typical Section - B stream

○ Ground Points ◆ Bankfull Indicators ▼ Water Surface Points

Wbkf = 7

Dbkf = .38

Abkf = 2.68



RIVERMORPH CROSS SECTION SUMMARY

 River Name: Proposed Design
 Reach Name: South Tributary
 Cross Section Name: Typical Section - C Stream
 Survey Date: 09/19/2018

Cross Section Data Entry

BM Elevation: 0 ft
 Backsight Rod Reading: 0 ft

| TAPE | FS | ELEV | NOTE |
|-------|----|------|------|
| 0 | 0 | 2 | |
| 10 | 0 | 2 | BKF |
| 11.05 | 0 | 1.58 | |
| 12.25 | 0 | 1.5 | |
| 13.45 | 0 | 1.58 | |
| 14.5 | 0 | 2 | |
| 24.5 | 0 | 2 | |

 Cross Sectional Geometry

| | Channel | Left | Right |
|---------------------------|---------|-------|-------|
| Floodprone Elevation (ft) | 2.5 | 2.5 | 2.5 |
| Bankfull Elevation (ft) | 2 | 2 | 2 |
| Floodprone width (ft) | 24.5 | ----- | ----- |
| Bankfull width (ft) | 4.5 | 2.25 | 2.25 |
| Entrenchment Ratio | 5.44 | ----- | ----- |
| Mean Depth (ft) | 0.34 | 0.34 | 0.34 |
| Maximum Depth (ft) | 0.5 | 0.5 | 0.5 |
| width/Depth Ratio | 13.24 | 6.55 | 6.62 |
| Bankfull Area (sq ft) | 1.54 | 0.77 | 0.77 |
| wetted Perimeter (ft) | 4.67 | 2.83 | 2.83 |
| Hydraulic Radius (ft) | 0.33 | 0.27 | 0.27 |
| Begin BKF Station | 10 | 10 | 12.25 |
| End BKF Station | 14.5 | 12.25 | 14.5 |

 Entrainment Calculations

Entrainment Formula: Rosgen Modified Shields Curve

| | Channel | Left Side | Right Side |
|-------------------------|---------|-----------|------------|
| Slope | 0 | 0 | 0 |
| Shear Stress (lb/sq ft) | | | |
| Movable Particle (mm) | | | |

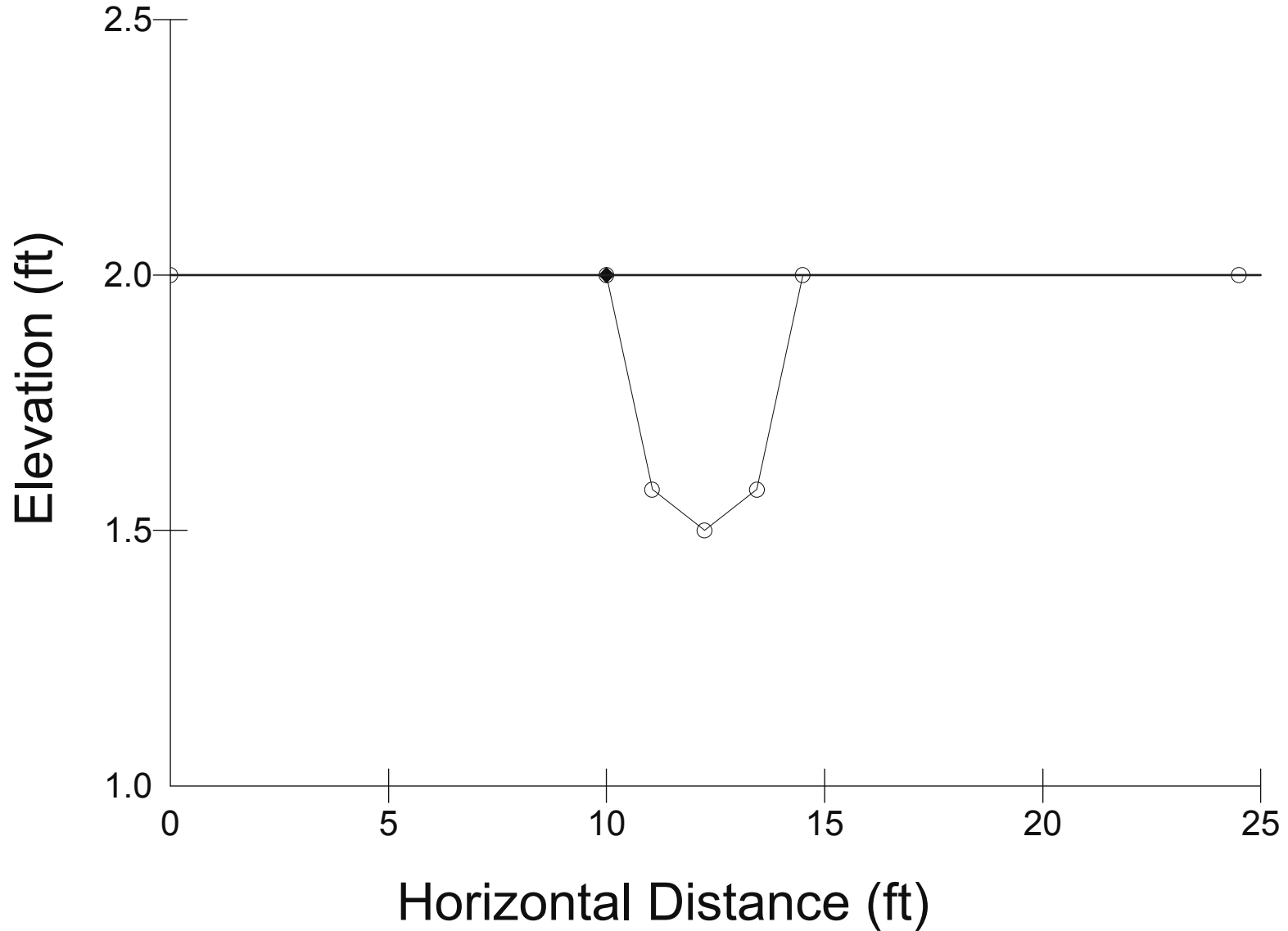
Typical Section - C Stream

○ Ground Points ◆ Bankfull Indicators ▼ Water Surface Points

Wbkf = 4.5

Dbkf = .34

Abkf = 1.55



RIVERMORPH CROSS SECTION SUMMARY

 River Name: Proposed Design
 Reach Name: North Tributary
 Cross Section Name: Typical Section - B Stream 10ft
 Survey Date: 09/18/2018

Cross Section Data Entry

BM Elevation: 0 ft
 Backsight Rod Reading: 0 ft

| TAPE | FS | ELEV | NOTE |
|-------|----|------|------|
| 0 | 0 | 2 | |
| 10 | 0 | 2 | BKF |
| 11.25 | 0 | 1.5 | |
| 12.75 | 0 | 1.5 | |
| 14 | 0 | 1.2 | |
| 16 | 0 | 1.2 | |
| 17.25 | 0 | 1.5 | |
| 18.75 | 0 | 1.5 | |
| 20 | 0 | 2 | |
| 30 | 0 | 2 | |

 Cross Sectional Geometry

| | Channel | Left | Right |
|---------------------------|---------|-------|-------|
| Floodprone Elevation (ft) | 2.8 | 2.8 | 2.8 |
| Bankfull Elevation (ft) | 2 | 2 | 2 |
| Floodprone width (ft) | 30 | ----- | ----- |
| Bankfull width (ft) | 10 | 5 | 5 |
| Entrenchment Ratio | 3 | ----- | ----- |
| Mean Depth (ft) | 0.53 | 0.53 | 0.54 |
| Maximum Depth (ft) | 0.8 | 0.8 | 0.8 |
| width/Depth Ratio | 18.87 | 9.35 | 9.26 |
| Bankfull Area (sq ft) | 5.35 | 2.67 | 2.68 |
| wetted Perimeter (ft) | 10.26 | 5.93 | 5.93 |
| Hydraulic Radius (ft) | 0.52 | 0.45 | 0.45 |
| Begin BKF Station | 10 | 10 | 15 |
| End BKF Station | 20 | 15 | 20 |

 Entrainment Calculations

Entrainment Formula: Rosgen Modified Shields Curve

| | Channel | Left Side | Right Side |
|-------------------------|---------|-----------|------------|
| Slope | 0 | 0 | 0 |
| Shear Stress (lb/sq ft) | | | |
| Movable Particle (mm) | | | |

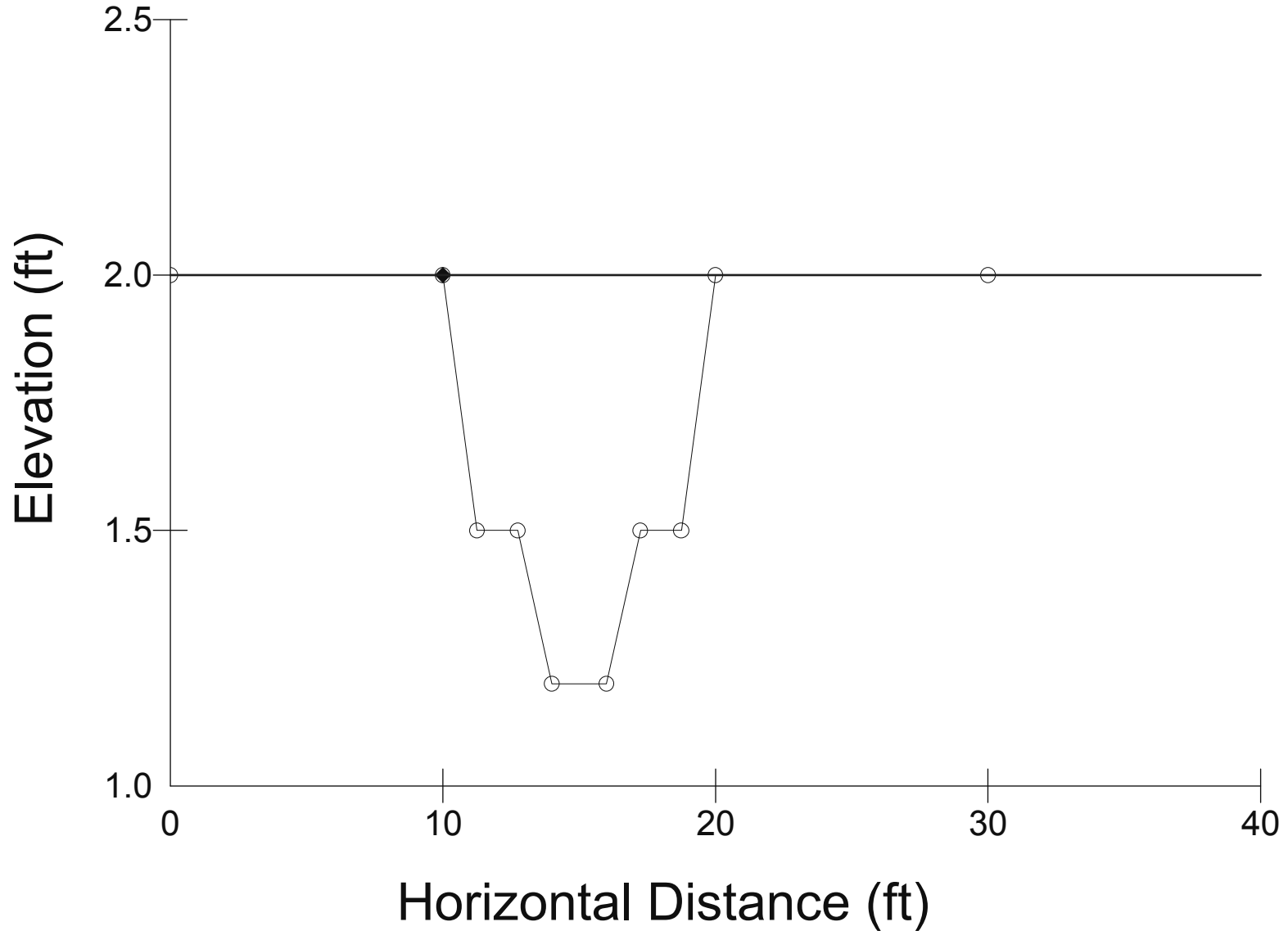
Typical Section 10ft

○ Ground Points ◆ Bankfull Indicators ▼ Water Surface Points

Wbkf = 10

Dbkf = .54

Abkf = 5.35



RIVERMORPH CROSS SECTION SUMMARY

 River Name: Proposed Design
 Reach Name: North Tributary
 Cross Section Name: Typical Section - C Stream
 Survey Date: 09/18/2018

Cross Section Data Entry

BM Elevation: 0 ft
 Backsight Rod Reading: 0 ft

| TAPE | FS | ELEV | NOTE |
|-------|----|------|------|
| 0 | 0 | 2 | |
| 10 | 0 | 2 | BKF |
| 11.15 | 0 | 1.54 | |
| 13.25 | 0 | 1.4 | |
| 15.35 | 0 | 1.54 | |
| 16.5 | 0 | 2 | |
| 28 | 0 | 2 | |

 Cross Sectional Geometry

| | Channel | Left | Right |
|---------------------------|---------|-------|-------|
| Floodprone Elevation (ft) | 2.6 | 2.6 | 2.6 |
| Bankfull Elevation (ft) | 2 | 2 | 2 |
| Floodprone width (ft) | 28 | ----- | ----- |
| Bankfull width (ft) | 6.5 | 4 | 2.5 |
| Entrenchment Ratio | 4.31 | ----- | ----- |
| Mean Depth (ft) | 0.42 | 0.45 | 0.38 |
| Maximum Depth (ft) | 0.6 | 0.6 | 0.55 |
| width/Depth Ratio | 15.48 | 8.85 | 6.58 |
| Bankfull Area (sq ft) | 2.75 | 1.81 | 0.95 |
| wetted Perimeter (ft) | 6.69 | 4.64 | 3.14 |
| Hydraulic Radius (ft) | 0.41 | 0.39 | 0.3 |
| Begin BKF Station | 10 | 10 | 14 |
| End BKF Station | 16.5 | 14 | 16.5 |

 Entrainment Calculations

Entrainment Formula: Rosgen Modified Shields Curve

| | Channel | Left Side | Right Side |
|-------------------------|---------|-----------|------------|
| Slope | 0 | 0 | 0 |
| Shear Stress (lb/sq ft) | | | |
| Movable Particle (mm) | | | |

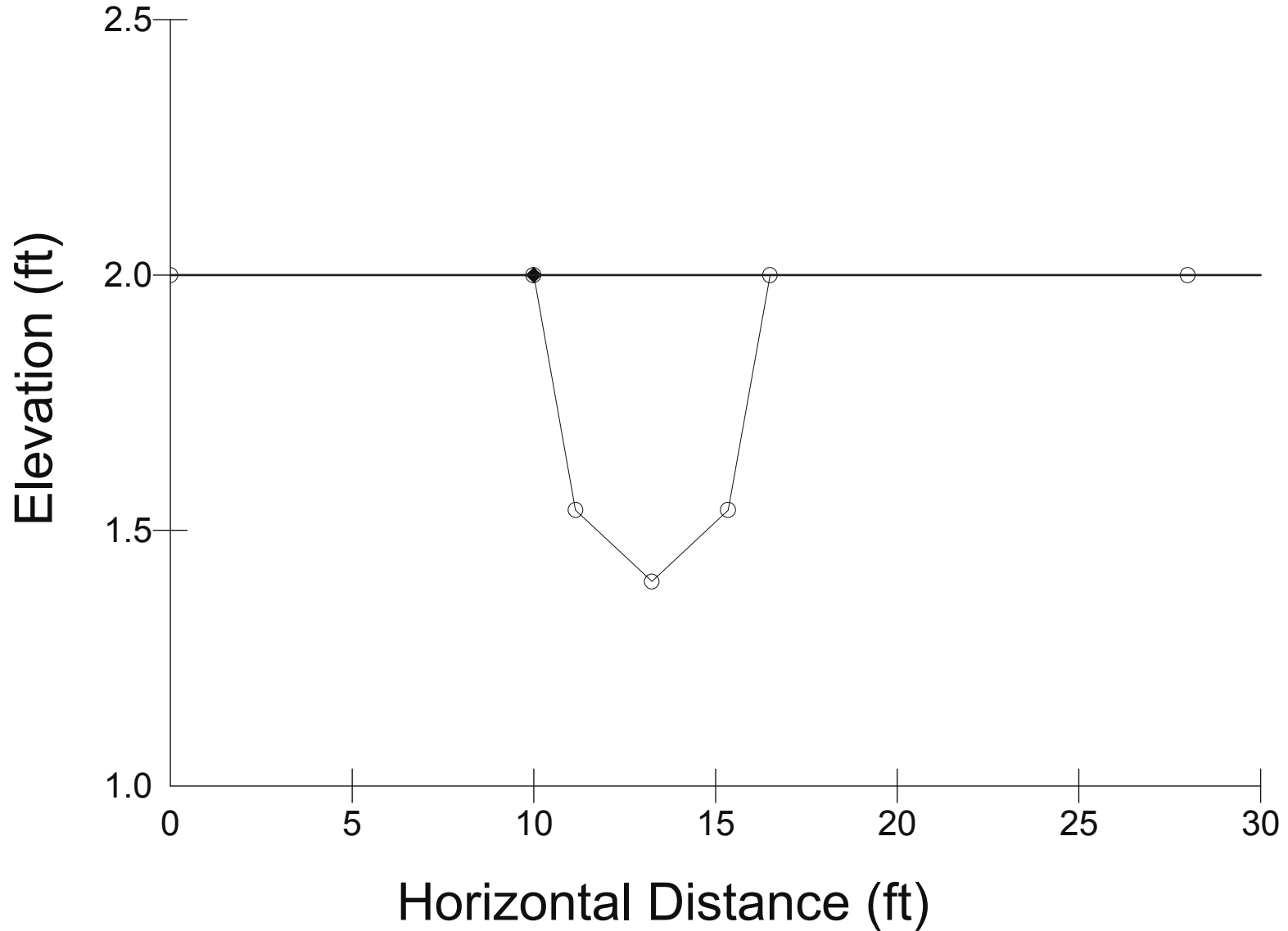
Typical C Stream Section

○ Ground Points ◆ Bankfull Indicators ▼ Water Surface Points

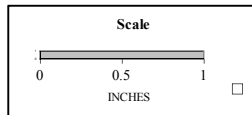
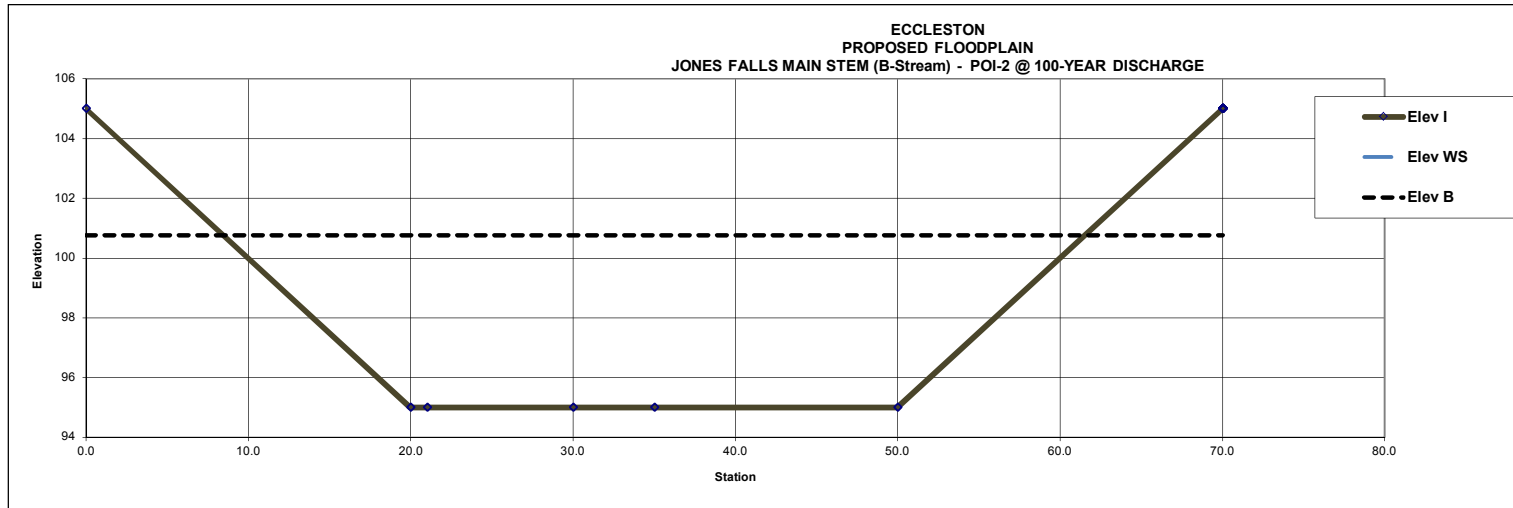
Wbkf = 6.5

Dbkf = .42

Abkf = 2.76



Proposed Floodplain - Jones Falls Sta. 100+00 to 101+43.02



Note: Scale set for print and view magnification at 65%

| Plot Scale | | |
|------------|--|-------------|
| 1 inch = | | feet horiz. |
| 1 inch = | | feet vert. |

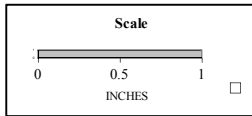
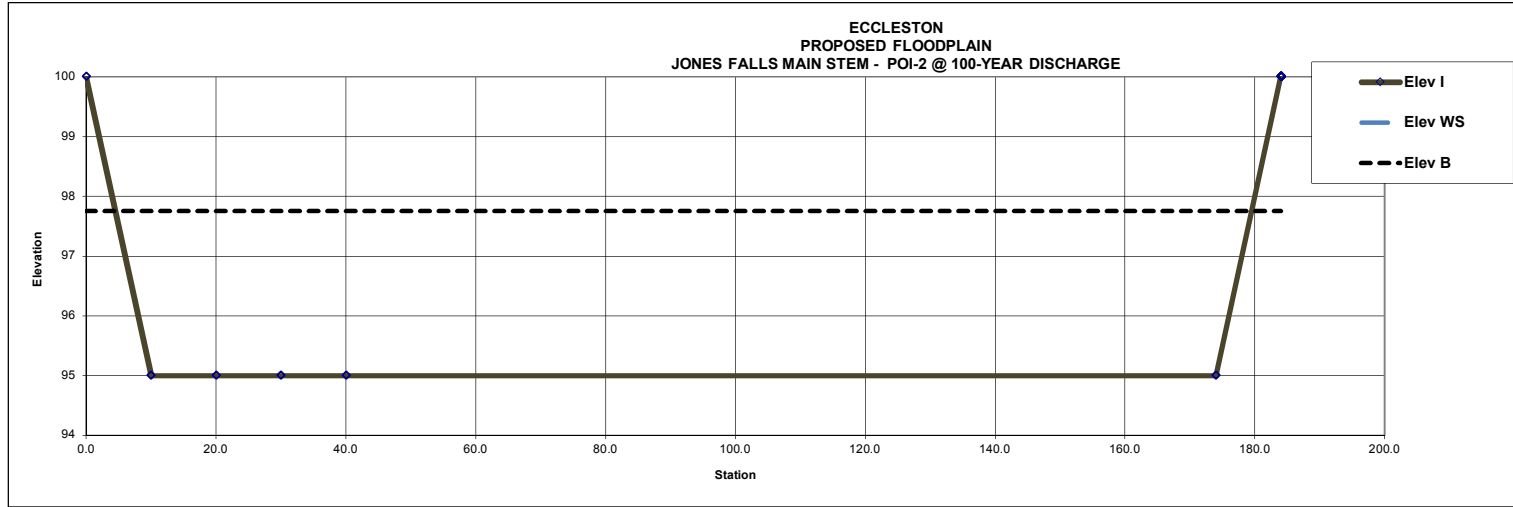
English Units

| GEOMETRY | |
|---------------------|--------|
| Bank Full Elevation | 100.77 |
| Bank Full Width | 53.06 |
| Bank Full Depth | 4.51 |
| Maximum Depth | 5.77 |
| Bank Full Area | 239.4 |
| Hydraulic Radius | 3.96 |
| Wetted Perimeter | 60.5 |
| Width/Depth Ratio | 11.8 |
| Flood Prone Width | 70.0 |
| Entrenchment | |
| Stream Type | C4/E4 |
| Rc | |

English Units

| HYDRAULICS | |
|-------------------------|------------------|
| Slope (ft/ft) | 0.0205 |
| Manning's n | 0.08 |
| Velocity (ft./s) | 6.66 |
| Froud # | 0.59 |
| Discharge (cu ft/s) | 1593.4 |
| Shear Stress (lb/sq ft) | 5.06 |
| CX Power (ft lb/s) | 2038.2 |
| Critical Size (mm) | 497.1 |
| Flow Type | Subcritical Flow |
| Rec. Interval | |

Proposed Floodplain - Jones Falls Sta. 101+43.02 to 107+52.45



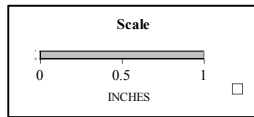
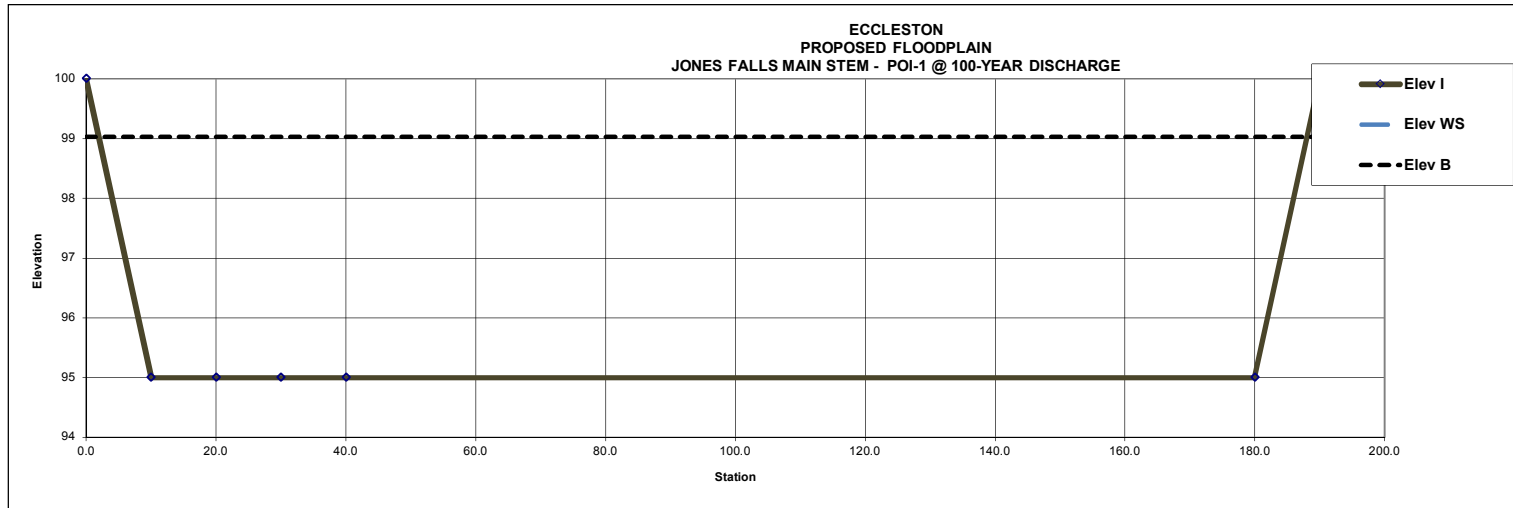
Note: Scale set for print and view magnification at 65%

| Plot Scale | |
|------------|-------------|
| 1 inch = | feet horiz. |
| 1 inch = | feet vert. |

| English Units | |
|---------------------|--------|
| GEOMETRY | |
| Bank Full Elevation | 97.75 |
| Bank Full Width | 175.01 |
| Bank Full Depth | 2.67 |
| Maximum Depth | 2.75 |
| Bank Full Area | 466.7 |
| Hydraulic Radius | 2.61 |
| Wetted Perimeter | 178.9 |
| Width/Depth Ratio | 65.6 |
| Flood Prone Width | 184.0 |
| Entrenchment | |
| Stream Type | C4/E4 |
| Rc | |

| English Units | |
|-------------------------|------------------|
| HYDRAULICS | |
| Slope (ft/ft) | 0.0094 |
| Manning's n | 0.08 |
| Velocity (ft./s) | 3.41 |
| Froud # | 0.37 |
| Discharge (cu ft/s) | 1593.1 |
| Shear Stress (lb/sq ft) | 1.53 |
| CX Power (ft lb/s) | 934.5 |
| Critical Size (mm) | 136.7 |
| Flow Type | Subcritical Flow |
| Rec. Interval | |

Proposed Floodplain - Jones Falls Sta. 107+52.45 to 126+76.91
 *Minimum width of the proposed floodplain to calculate the maximum shear stress.



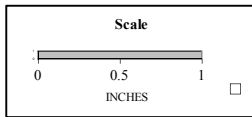
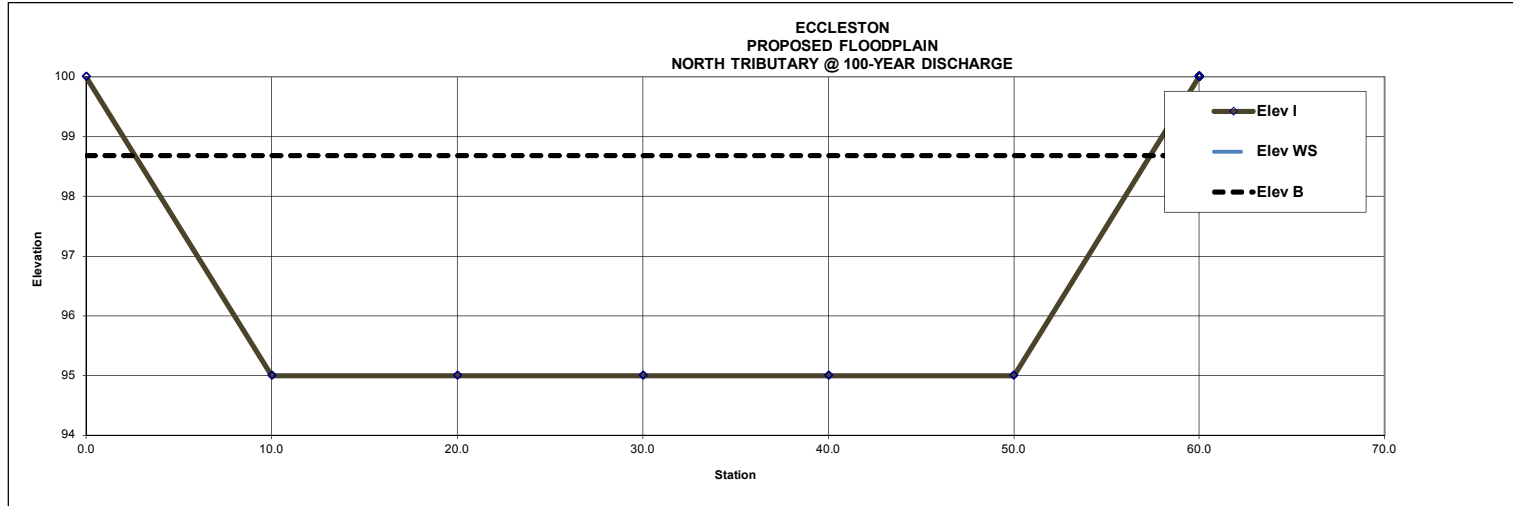
Note: Scale set for print and view magnification at 65%

| Plot Scale | |
|------------|-------------|
| 1 inch = | feet horiz. |
| 1 inch = | feet vert. |

| English Units | |
|---------------------|--------|
| GEOMETRY | |
| Bank Full Elevation | 99.03 |
| Bank Full Width | 186.11 |
| Bank Full Depth | 3.85 |
| Maximum Depth | 4.03 |
| Bank Full Area | 717.2 |
| Hydraulic Radius | 3.80 |
| Wetted Perimeter | 189.0 |
| Width/Depth Ratio | 48.3 |
| Flood Prone Width | 190.0 |
| Entrenchment | |
| Stream Type | C4/E4 |
| Rc | |

| English Units | |
|-------------------------|------------------|
| HYDRAULICS | |
| Slope (ft/ft) | 0.0094 |
| Manning's n | 0.08 |
| Velocity (ft./s) | 4.38 |
| Froud # | 0.40 |
| Discharge (cu ft/s) | 3144.2 |
| Shear Stress (lb/sq ft) | 2.23 |
| CX Power (ft lb/s) | 1844.3 |
| Critical Size (mm) | 204.9 |
| Flow Type | Subcritical Flow |
| Rec. Interval | |

Proposed Floodplain - North Tributary 600+00 to 601+35.58



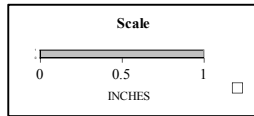
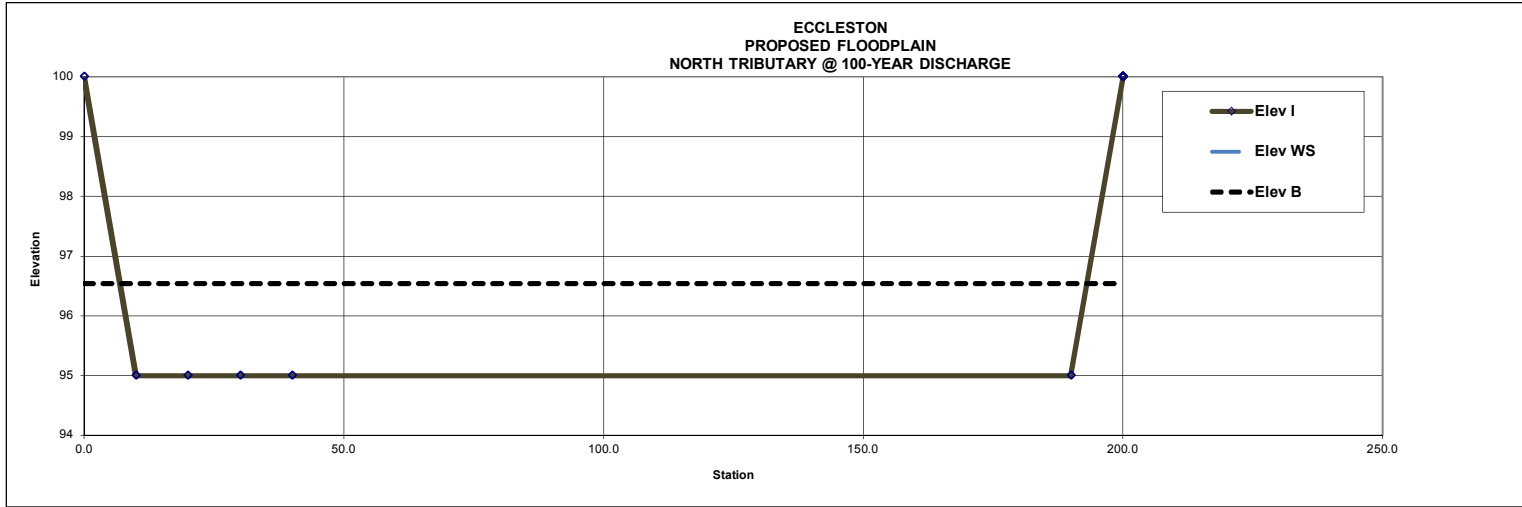
Note: Scale set for print and view magnification at 65%

| Plot Scale | | |
|------------|--|-------------|
| 1 inch = | | feet horiz. |
| 1 inch = | | feet vert. |

| English Units | |
|---------------------|-------|
| GEOMETRY | |
| Bank Full Elevation | 98.68 |
| Bank Full Width | 54.72 |
| Bank Full Depth | 3.19 |
| Maximum Depth | 3.68 |
| Bank Full Area | 174.3 |
| Hydraulic Radius | 3.02 |
| Wetted Perimeter | 57.8 |
| Width/Depth Ratio | 17.2 |
| Flood Prone Width | 60.0 |
| Entrenchment | |
| Stream Type | C4/E4 |
| Rc | |

| English Units | |
|-------------------------|------------------|
| HYDRAULICS | |
| Slope (ft/ft) | 0.0230 |
| Manning's n | 0.08 |
| Velocity (ft./s) | 5.88 |
| Froud # | 0.60 |
| Discharge (cu ft/s) | 1025.7 |
| Shear Stress (lb/sq ft) | 4.33 |
| CX Power (ft lb/s) | 1472.0 |
| Critical Size (mm) | 420.0 |
| Flow Type | Subcritical Flow |
| Rec. Interval | |

Proposed Floodplain - North Tributary 601+35.58 to 607+66.51



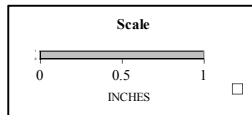
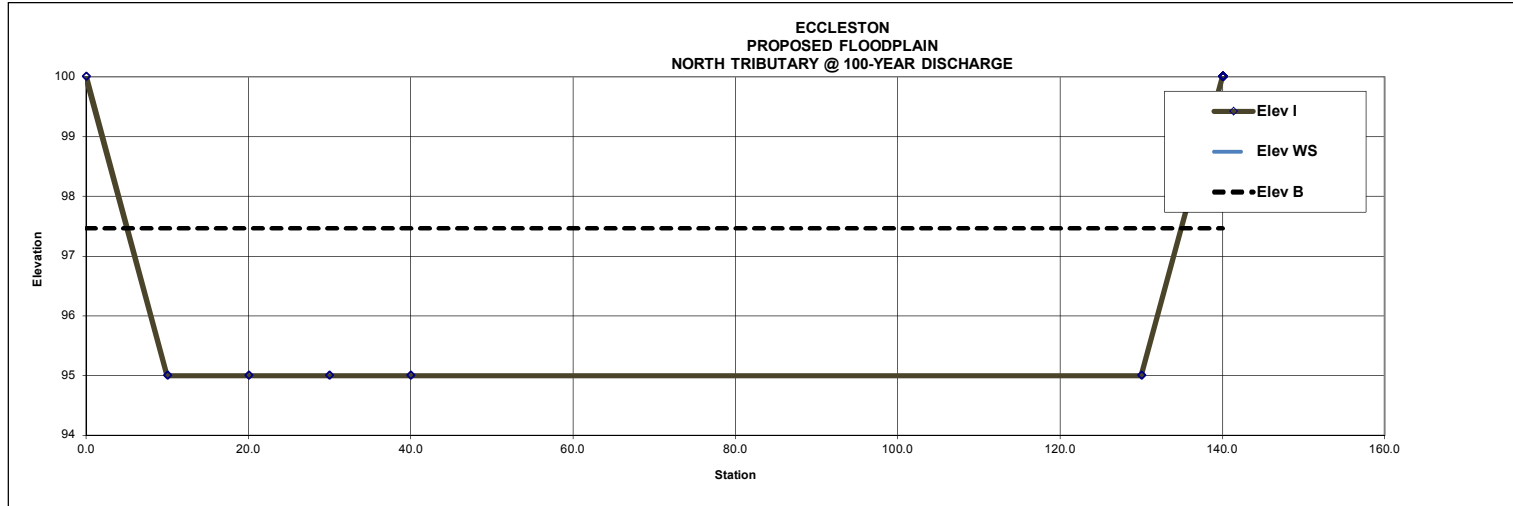
Note: Scale set for print and view magnification at 65%

| Plot Scale | | |
|------------|--|-------------|
| 1 inch = | | feet horiz. |
| 1 inch = | | feet vert. |

| English Units | |
|---------------------|--------|
| GEOMETRY | |
| Bank Full Elevation | 96.54 |
| Bank Full Width | 186.16 |
| Bank Full Depth | 1.51 |
| Maximum Depth | 1.54 |
| Bank Full Area | 281.9 |
| Hydraulic Radius | 1.47 |
| Wetted Perimeter | 191.7 |
| Width/Depth Ratio | 122.9 |
| Flood Prone Width | 192.3 |
| Entrenchment | 1.03 |
| Stream Type | C4/E4 |
| Rc | |

| English Units | |
|-------------------------|------------------|
| HYDRAULICS | |
| Slope (ft/ft) | 0.0230 |
| Manning's n | 0.08 |
| Velocity (ft./s) | 3.64 |
| Froud # | 0.53 |
| Discharge (cu ft/s) | 1027.2 |
| Shear Stress (lb/sq ft) | 2.11 |
| CX Power (ft lb/s) | 1474.2 |
| Critical Size (mm) | 193.4 |
| Flow Type | Subcritical Flow |
| Rec. Interval | |

Proposed Floodplain - North Tributary 607+66.51 to 614+42.09



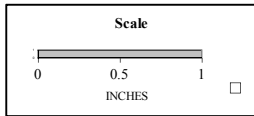
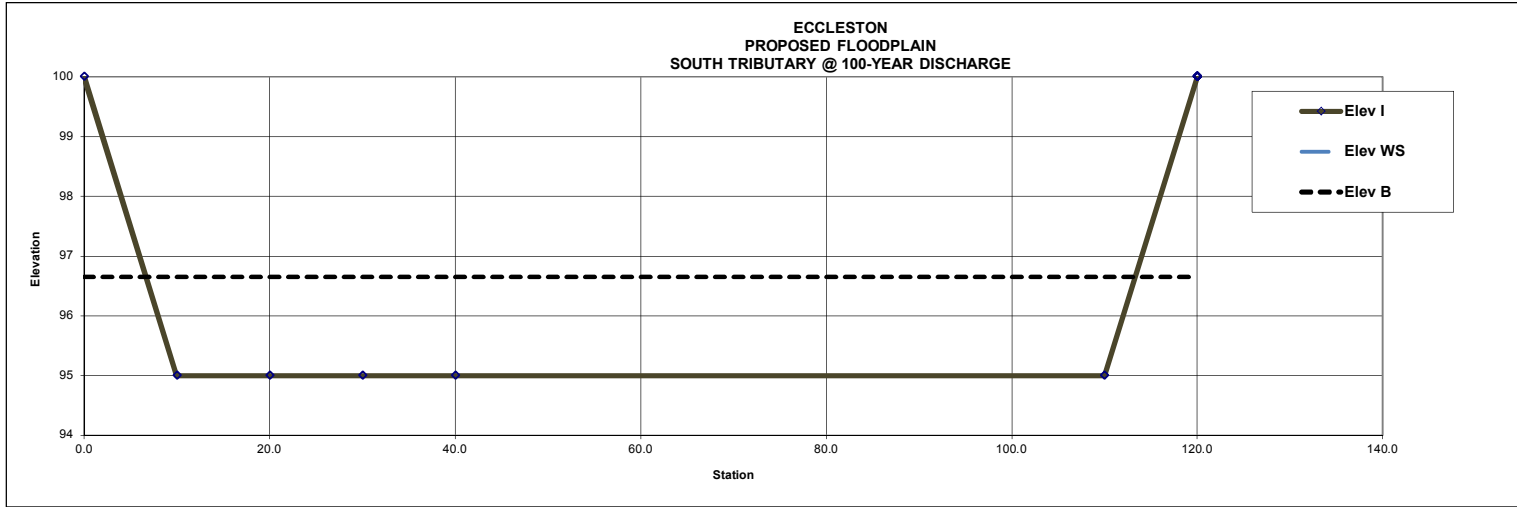
Note: Scale set for print and view magnification at 65%

| Plot Scale | |
|------------|-------------|
| 1 inch = | feet horiz. |
| 1 inch = | feet vert. |

| English Units | |
|---------------------|--------|
| GEOMETRY | |
| Bank Full Elevation | 97.47 |
| Bank Full Width | 129.86 |
| Bank Full Depth | 2.37 |
| Maximum Depth | 2.47 |
| Bank Full Area | 308.0 |
| Hydraulic Radius | 2.30 |
| Wetted Perimeter | 134.0 |
| Width/Depth Ratio | 54.8 |
| Flood Prone Width | 139.7 |
| Entrenchment | 1.08 |
| Stream Type | C4/E4 |
| Rc | |

| English Units | |
|-------------------------|------------------|
| HYDRAULICS | |
| Slope (ft/ft) | 0.0106 |
| Manning's n | 0.08 |
| Velocity (ft./s) | 3.33 |
| Froud # | 0.39 |
| Discharge (cu ft/s) | 1025.7 |
| Shear Stress (lb/sq ft) | 1.52 |
| CX Power (ft lb/s) | 678.4 |
| Critical Size (mm) | 135.7 |
| Flow Type | Subcritical Flow |
| Rec. Interval | |

Proposed Floodplain - South Tributary 200+00 to 207+62.80 and 300+00 to 304+16.88



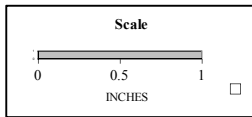
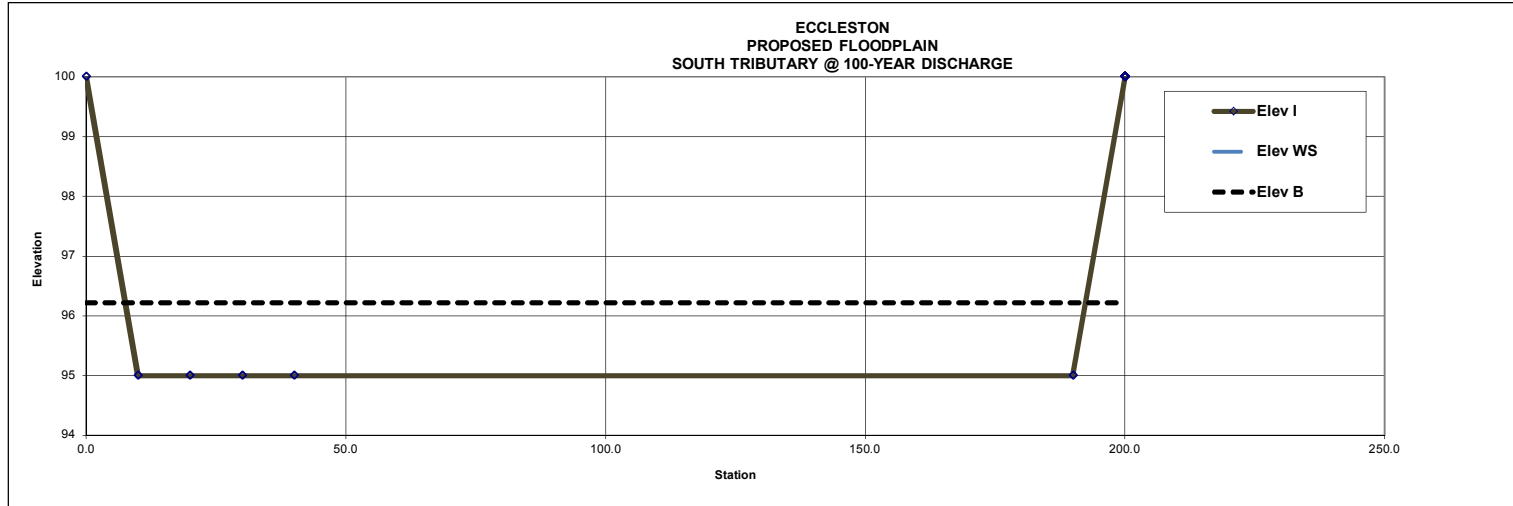
Note: Scale set for print and view magnification at 65%

| Plot Scale | | |
|------------|--|-------------|
| 1 inch = | | feet horiz. |
| 1 inch = | | feet vert. |

| English Units | |
|---------------------|--------|
| GEOMETRY | |
| Bank Full Elevation | 96.65 |
| Bank Full Width | 106.60 |
| Bank Full Depth | 1.60 |
| Maximum Depth | 1.65 |
| Bank Full Area | 170.6 |
| Hydraulic Radius | 1.52 |
| Wetted Perimeter | 112.0 |
| Width/Depth Ratio | 66.6 |
| Flood Prone Width | 113.2 |
| Entrenchment | 1.06 |
| Stream Type | C4/E4 |
| Rc | |

| English Units | |
|-------------------------|------------------|
| HYDRAULICS | |
| Slope (ft/ft) | 0.0220 |
| Manning's n | 0.08 |
| Velocity (ft./s) | 3.65 |
| Froud # | 0.52 |
| Discharge (cu ft/s) | 622.1 |
| Shear Stress (lb/sq ft) | 2.09 |
| CX Power (ft lb/s) | 854.0 |
| Critical Size (mm) | 191.5 |
| Flow Type | Subcritical Flow |
| Rec. Interval | |

Proposed Floodplain - South Tributary 207+62.80 to 211+52.03 and 304+16.88 to 309+72.59



Note: Scale set for print and view magnification at 65%

| Plot Scale | | |
|------------|--|-------------|
| 1 inch = | | feet horiz. |
| 1 inch = | | feet vert. |

| English Units | |
|---------------------|--------|
| GEOMETRY | |
| Bank Full Elevation | 96.22 |
| Bank Full Width | 184.88 |
| Bank Full Depth | 1.20 |
| Maximum Depth | 1.22 |
| Bank Full Area | 222.6 |
| Hydraulic Radius | 1.16 |
| Wetted Perimeter | 191.1 |
| Width/Depth Ratio | 153.6 |
| Flood Prone Width | 189.8 |
| Entrenchment | 1.03 |
| Stream Type | C4/E4 |
| Rc | |

| English Units | |
|-------------------------|------------------|
| HYDRAULICS | |
| Slope (ft/ft) | 0.0186 |
| Manning's n | 0.08 |
| Velocity (ft./s) | 2.80 |
| Froud # | 0.46 |
| Discharge (cu ft/s) | 624.2 |
| Shear Stress (lb/sq ft) | 1.35 |
| CX Power (ft lb/s) | 724.4 |
| Critical Size (mm) | 119.6 |
| Flow Type | Subcritical Flow |
| Rec. Interval | |



APPENDIX H

Hydraulics Analysis Data

Stream and Location: Eccleston

Reach: Intersection Tributary

Event for which n is assigned: Bankfull flow condition

1. Is roughness uniform throughout the reach being considered? Yes

If not, should n be assigned for the average condition of the reach? N/A

2. Is roughness uniformly distributed along the cross section? Yes

Is a division between channel and floodplain necessary? Yes

(Channel Roughness uses steps 3-13, Floodplain roughness uses steps 14-23.)

Is roughness uniformly distributed across the channel? Yes

If not, what basis should n for the individual segments be weighted? N/A

3. Describe the channel. Are present conditions representative of those during the flood?

A silt/sand bed stream with coarse gravel exhibiting a riffle / pool system.

If not, describe the probable conditions during the flood. Assume that channel conditions are representative of channel flowing full (to elevation of the floodplain/bankfull condition)

4. How will the roughness-producing effects of the following on the channel be accounted for?

Bank roughness: _____

Bedrock outcrops: No bedrock present.

Isolated boulders: No boulders present.

Vegetation: Mostly herbaceous near channel. Mix of woody and herbaceous vegetation in floodplain.

Obstructions: Woody debris jams.

Meander: Little to No sinuosity

5-10. Computation n for the channel

| Segment Number and Material | Approximate Dimensions | | Wetted perimeter | Area (sf) | Grain Size (mm) | Base n for segment | Adjustments | Adjusted n | Weight Factors | times weight factors |
|-----------------------------|------------------------|------------|------------------|-----------|-----------------|--------------------|-------------|------------|----------------|----------------------|
| | width (ft) | depth (ft) | | | | | | | | |
| 1 | | | | | 10.75 | 0.029 | None | N/A | N/A | 0.029 |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| SUM | | | | | | | | | | 0.029 |
| Weighted n = | | | | | | | | | | 0.029 |

**11-13. Computation n for the channel
Adjustment factors for the channel**

| Factor | Describe conditions briefly | Adjustment |
|--|--|--------------|
| Irregularity, n₁ | Minor - Compares to carefully degraded channels in good condition but having slightly eroded or scoured side slopes. | 0.005 |
| Alignment, n₂ | Alternating occasionally- Large and small cross sections alternate occasionally, or the main flow occasionally shifts from side to side owing to changes in cross-sectional shape. | 0.003 |
| Obstructions, n₃ | Negligible- Few scattered obstructions, which include debris deposits, stumps, exposed roots, logs, piers, or isolated boulders that occupy less than 5% of the cross-sectional area | 0.004 |
| Vegetation, n₄ | Small- the average depth of flow is atleast two times the height of the vegetation | 0.005 |
| Meander, m | Minor- Ratio of the channel length to valley length is 1.0 to 1.2 | 1.00 |
| Weighted n plus n_x adjustments | | 0.046 |
| Computed n times m factor = | | 0.046 |

Stream and Location: Eccleston

Reach: South Tributary

Event for which n is assigned: Bankfull flow condition

1. Is roughness uniform throughout the reach being considered? Yes

If not, should n be assigned for the average condition of the reach? N/A

2. Is roughness uniformly distributed along the cross section? Yes

Is a division between channel and floodplain necessary? Yes

(Channel Roughness uses steps 3-13, Floodplain roughness uses steps 14-23.)

Is roughness uniformly distributed across the channel? Yes

If not, what basis should n for the individual segments be weighted? N/A

3. Describe the channel. Are present conditions representative of those during the flood?

A silt/sand bed stream with coarse gravel exhibiting a riffle / pool system.

If not, describe the probable conditions during the flood. Assume that channel conditions are representative of channel flowing full (to elevation of the floodplain/bankfull condition)

4. How will the roughness-producing effects of the following on the channel be accounted for?

Bank roughness: _____

Bedrock outcrops: No bedrock present.

Isolated boulders: No boulders present.

Vegetation: Mostly herbaceous near channel. Mix of woody and herbaceous vegetation in floodplain.

Obstructions: Woody debris jams.

Meander: Little to No sinuosity

5-10. Computation n for the channel

| Segment Number and Material | Approximate Dimensions | | Wetted perimeter | Area (sf) | Grain Size (mm) | Base n for segment | Adjustments | Adjusted n | Weight Factors | times weight factors |
|-----------------------------|------------------------|------------|------------------|-----------|-----------------|--------------------|-------------|------------|----------------|----------------------|
| | width (ft) | depth (ft) | | | | | | | | |
| 1 | | | | | 37.42 | 0.032 | None | N/A | N/A | 0.032 |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| SUM | | | | | | | | | | 0.032 |
| Weighted n = | | | | | | | | | | 0.032 |

**11-13. Computation n for the channel
Adjustment factors for the channel**

| Factor | Describe conditions briefly | Adjustment |
|--|---|--------------|
| Irregularity, n₁ | Minor - Compares to carefully degraded channels in good condition but having slightly eroded or scoured side slopes. | 0.005 |
| Alignment, n₂ | Alternating occasionally- Large and small cross sections alternate occasionally, or the main flow occasionally shifts from side to side owing to changes in cross-sectional shape. | 0.003 |
| Obstructions, n₃ | Minor- Obstructions less than 15 percent of the cross-sectional area, and the spacing between obstructions is such that the sphere of influence around one obstruction does not extend to the sphere of influence around another obstruction. | 0.007 |
| Vegetation, n₄ | Medium- Brushy, moderately dense vegetation, similar to 1-to-2-year-old willow trees in the dormant season, growing along the banks, and no significant vegetation is evident along the channel bottoms | 0.010 |
| Meander, m | Minor- Ratio of the channel length to valley length is 1.0 to 1.2 | 1.00 |
| Weighted n plus n_x adjustments | | 0.057 |
| Computed n times m factor = | | 0.057 |

Stream and Location: Eccleston

Reach: North Tributary

Event for which n is assigned: Bankfull flow condition

1. Is roughness uniform throughout the reach being considered? Yes

If not, should n be assigned for the average condition of the reach? N/A

2. Is roughness uniformly distributed along the cross section? Yes

Is a division between channel and floodplain necessary? Yes

(Channel Roughness uses steps 3-13, Floodplain roughness uses steps 14-23.)

Is roughness uniformly distributed across the channel? Yes

If not, what basis should n for the individual segments be weighted? N/A

3. Describe the channel. Are present conditions representative of those during the flood?

A silt/sand bed stream with coarse gravel exhibiting a riffle / pool system

If not, describe the probable conditions during the flood. Assume that channel conditions are representative of channel flowing full (to elevation of the floodplain/bankfull condition)

4. How will the roughness-producing effects of the following on the channel be accounted for?

Bank roughness: _____

Bedrock outcrops: No bedrock present.

Isolated boulders: No boulders present.

Vegetation: Mostly herbaceous near channel. Mix of woody and herbaceous vegetation in floodplain.

Obstructions: Woody debris jams.

Meander: Little to No sinuosity

5-10. Computation n for the channel

| Segment Number and Material | Approximate Dimensions | | Wetted perimeter | Area (sf) | Grain Size (mm) | Base n for segment | Adjustments | Adjusted n | Weight Factors | times weight factors |
|-----------------------------|------------------------|------------|------------------|-----------|-----------------|--------------------|-------------|------------|---------------------|----------------------|
| | width (ft) | depth (ft) | | | | | | | | |
| 1 | | | | | 26.67 | 0.031 | None | N/A | N/A | 0.031 |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | SUM | 0.031 |
| | | | | | | | | | Weighted n = | 0.031 |

**11-13. Computation n for the channel
Adjustment factors for the channel**

| Factor | Describe conditions briefly | Adjustment |
|------------------------------------|---|--|
| Irregularity, n₁ | Minor - Compares to carefully degraded channels in good condition but having slightly eroded or scoured side slopes. | 0.005 |
| Alignment, n₂ | Alternating occasionally- Large and small cross sections alternate occasionally, or the main flow occasionally shifts from side to side owing to changes in cross-sectional shape. | 0.003 |
| Obstructions, n₃ | Minor- Obstructions less than 15 percent of the cross-sectional area, and the spacing between obstructions is such that the sphere of influence around one obstruction does not extend to the sphere of influence around another obstruction. | 0.007 |
| Vegetation, n₄ | Medium- Brushy, moderately dense vegetation, similar to 1-to-2-year-old willow trees in the dormant season, growing along the banks, and no significant vegetation is evident along the channel bottoms | 0.015 |
| Meander, m | Minor- Ratio of the channel length to valley length is 1.0 to 1.2 | 1.00 |
| | | Weighted n plus n_x adjustments |
| | | 0.061 |
| | | Computed n times m factor = |
| | | 0.061 |

Stream and Location: Eccleston

Reach: Main Stem

Event for which n is assigned: Bankfull flow condition

1. Is roughness uniform throughout the reach being considered? Yes

If not, should n be assigned for the average condition of the reach? N/A

2. Is roughness uniformly distributed along the cross section? Yes

Is a division between channel and floodplain necessary? Yes

(Channel Roughness uses steps 3-13, Floodplain roughness uses steps 14-23.)

Is roughness uniformly distributed across the channel? Yes

If not, what basis should n for the individual segments be weighted? N/A

3. Describe the channel. Are present conditions representative of those during the flood?

A silt/sand bed stream with coarse gravel exhibiting a riffle / pool system.

If not, describe the probable conditions during the flood. Assume that channel conditions are representative of channel flowing full (to elevation of the floodplain/bankfull condition)

4. How will the roughness-producing effects of the following on the channel be accounted for?

Bank roughness: _____

Bedrock outcrops: No bedrock present.

Isolated boulders: No boulders present.

Vegetation: Mostly herbaceous near channel. Mix of woody and herbaceous vegetation in floodplain.

Obstructions: Woody debris jams.

Meander: Little to No sinuosity

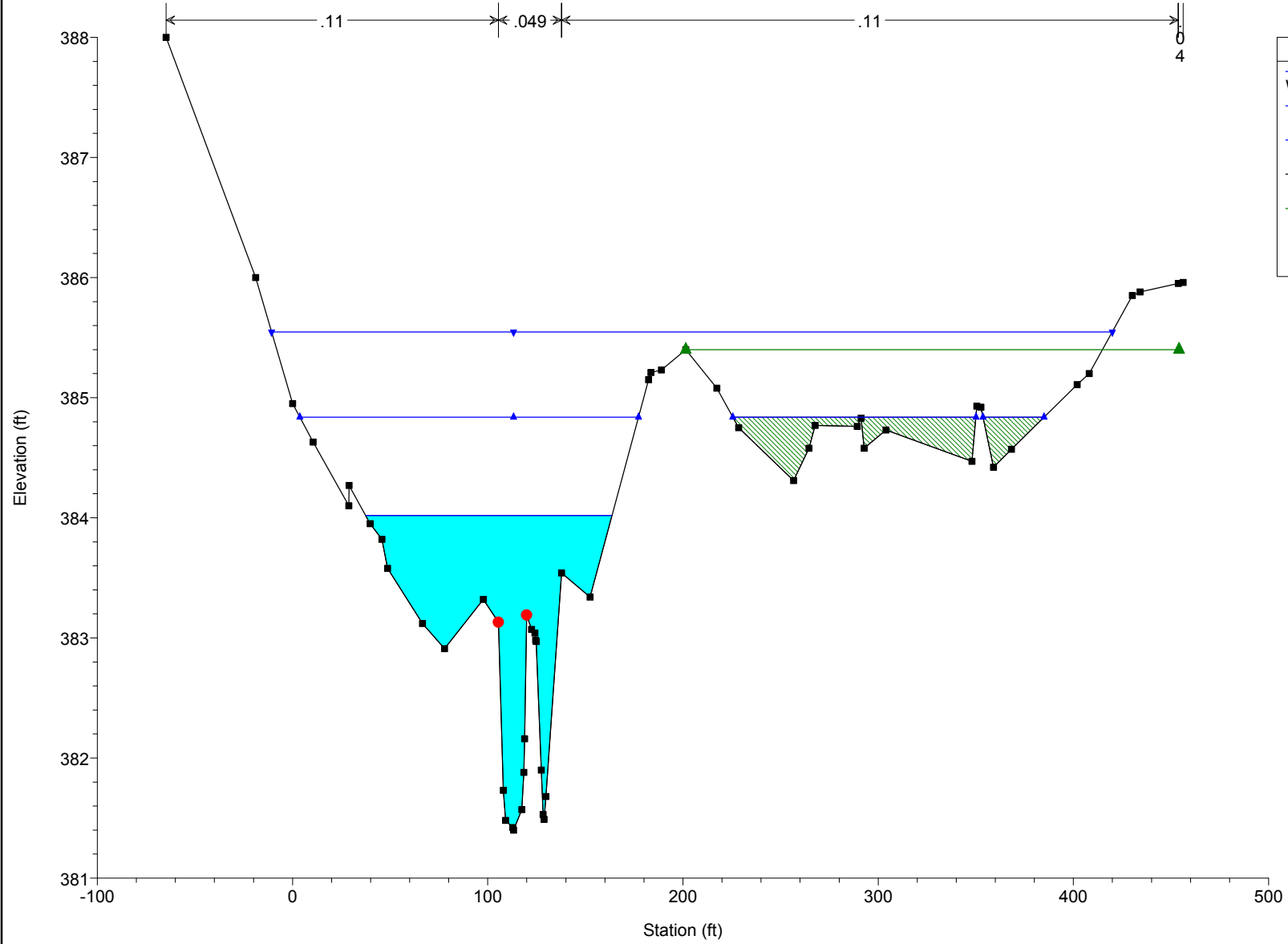
5-10. Computation n for the channel

| Segment Number and Material | Approximate Dimensions | | Wetted perimeter | Area (sf) | Grain Size (mm) | Base n for segment | Adjustments | Adjusted n | Weight Factors | times weight factors |
|-----------------------------|------------------------|------------|------------------|-----------|-----------------|--------------------|-------------|------------|----------------|----------------------|
| | width (ft) | depth (ft) | | | | | | | | |
| 1 | | | | | 36.892 | 0.032 | None | N/A | N/A | 0.032 |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| SUM | | | | | | | | | | 0.032 |
| Weighted n = | | | | | | | | | | 0.032 |

**11-13. Computation n for the channel
Adjustment factors for the channel**

| Factor | Describe conditions briefly | Adjustment |
|--|---|--------------|
| Irregularity, n₁ | Minor - Compares to carefully degraded channels in good condition but having slightly eroded or scoured side slopes. | 0.005 |
| Alignment, n₂ | Alternating occasionally- Large and small cross sections alternate occasionally, or the main flow occasionally shifts from side to side owing to changes in cross-sectional shape. | 0.003 |
| Obstructions, n₃ | Minor- Obstructions less than 15 percent of the cross-sectional area, and the spacing between obstructions is such that the sphere of influence around one obstruction does not extend to the sphere of influence around another obstruction. | 0.004 |
| Vegetation, n₄ | Small- the average depth of flow is atleast two times the height of the vegetation | 0.005 |
| Meander, m | Minor- Ratio of the channel length to valley length is 1.0 to 1.2 | 1.00 |
| Weighted n plus n_x adjustments | | 0.049 |
| Computed n times m factor = | | 0.049 |

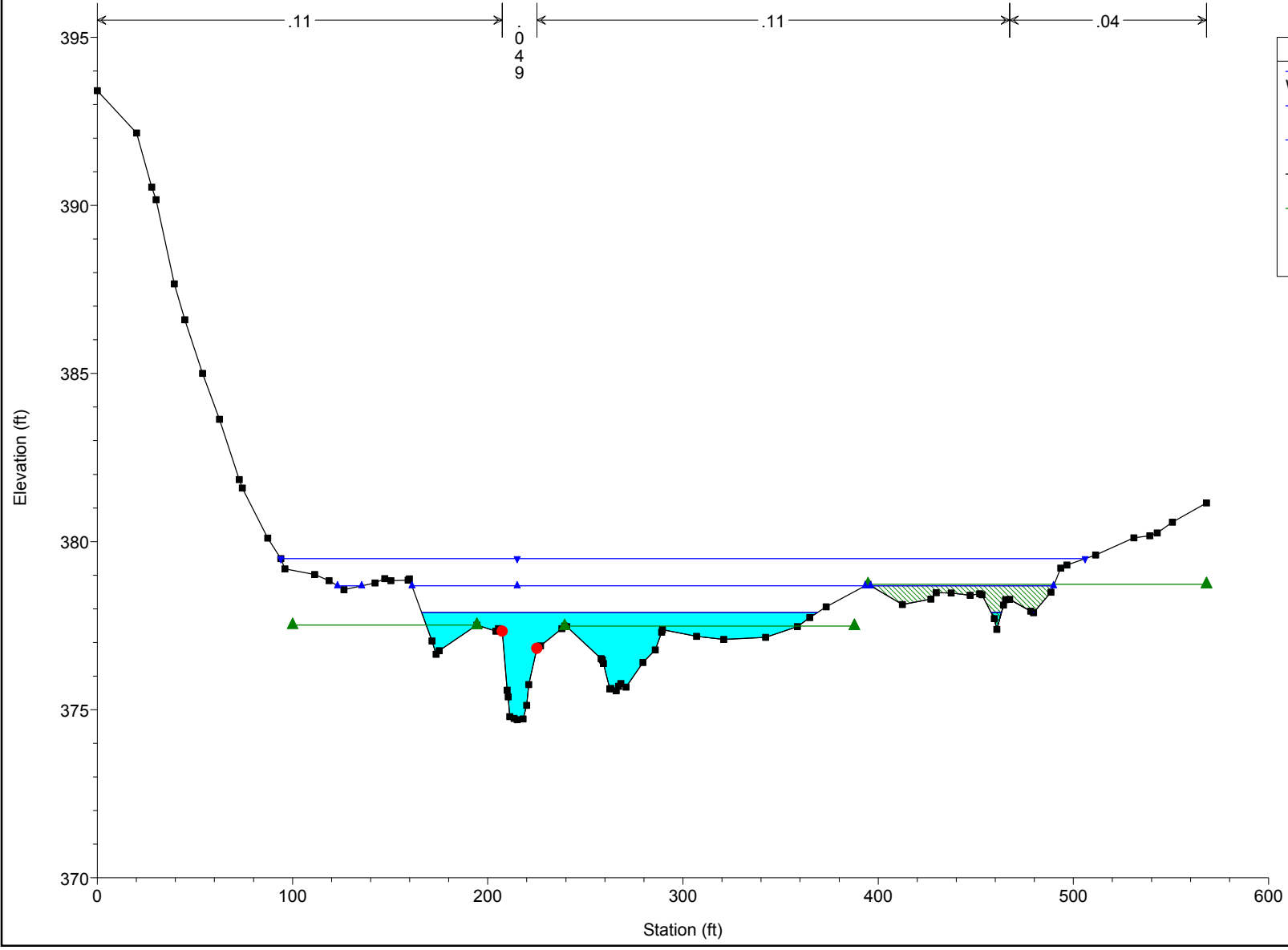
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River = JonesFalls Reach = JonesFalls RS = 15



Legend

- WS 100 Yr
- WS 10 Yr
- WS 2 Yr
- Ground
- Ineff
- Bank Sta

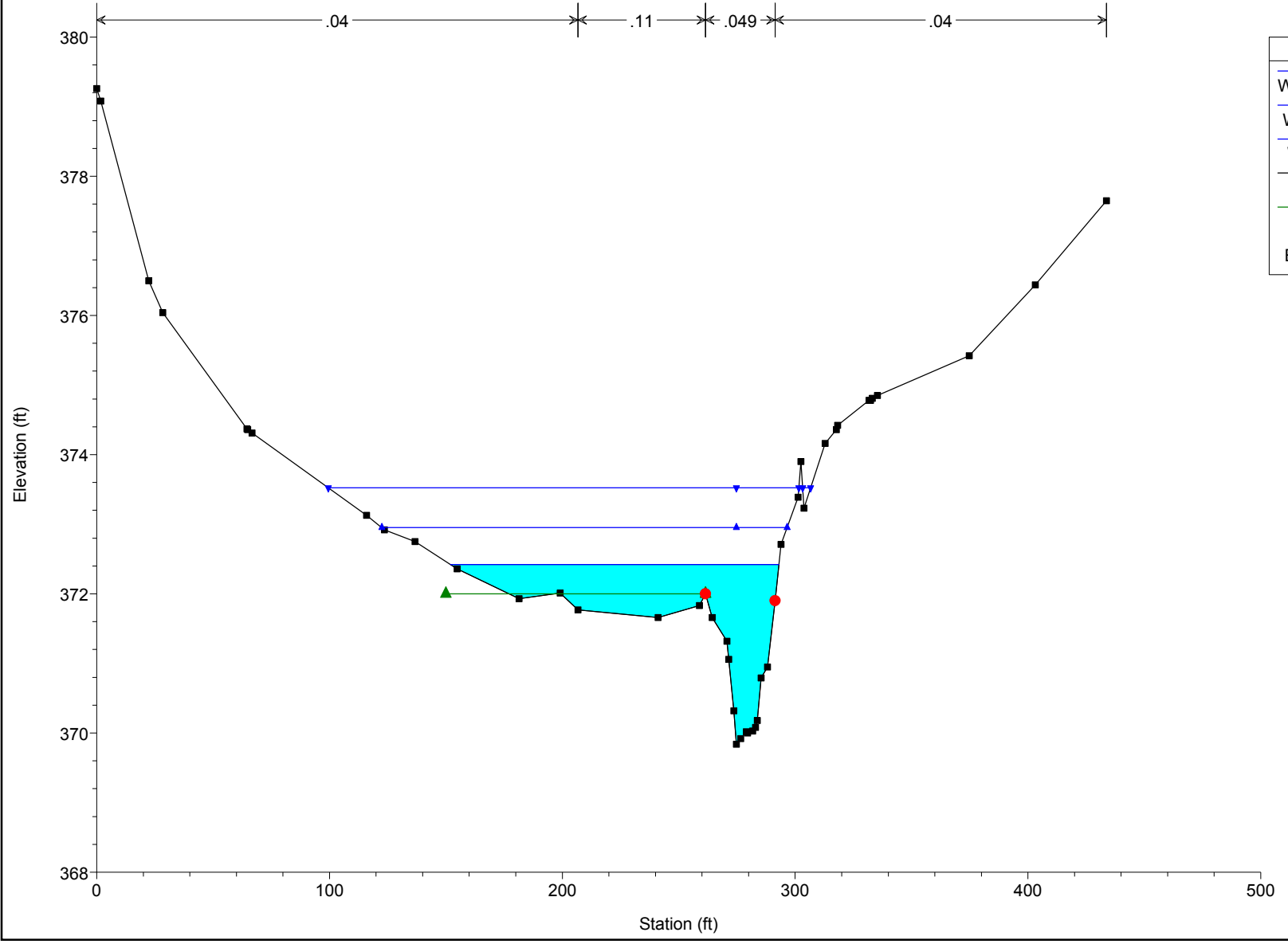
EcclestonMod Plan: existing 11/5/2018
River = JonesFalls Reach = JonesFalls RS = 14



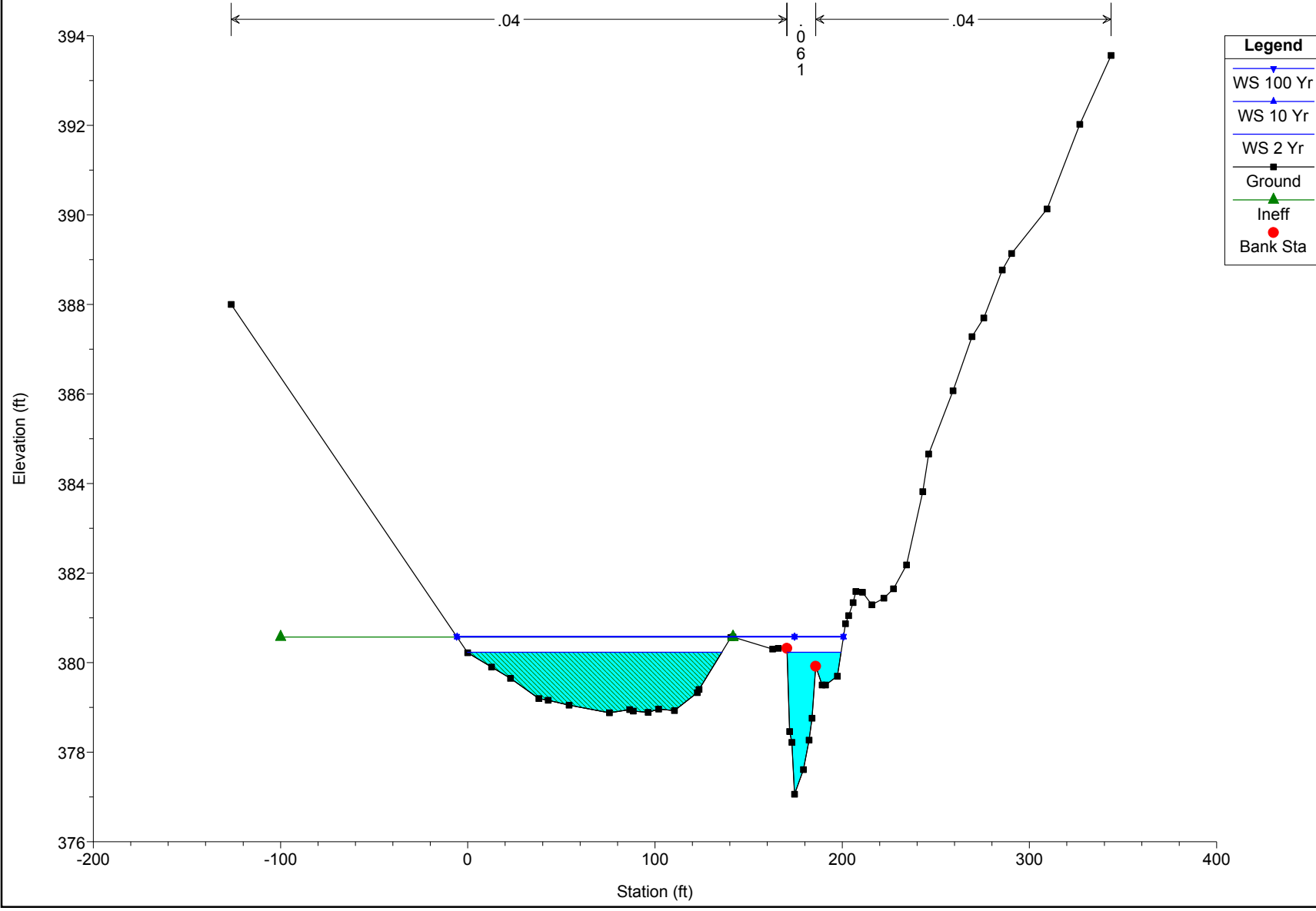
Legend

- WS 100 Yr
- WS 10 Yr
- WS 2 Yr
- Ground
- Ineff
- Bank Sta

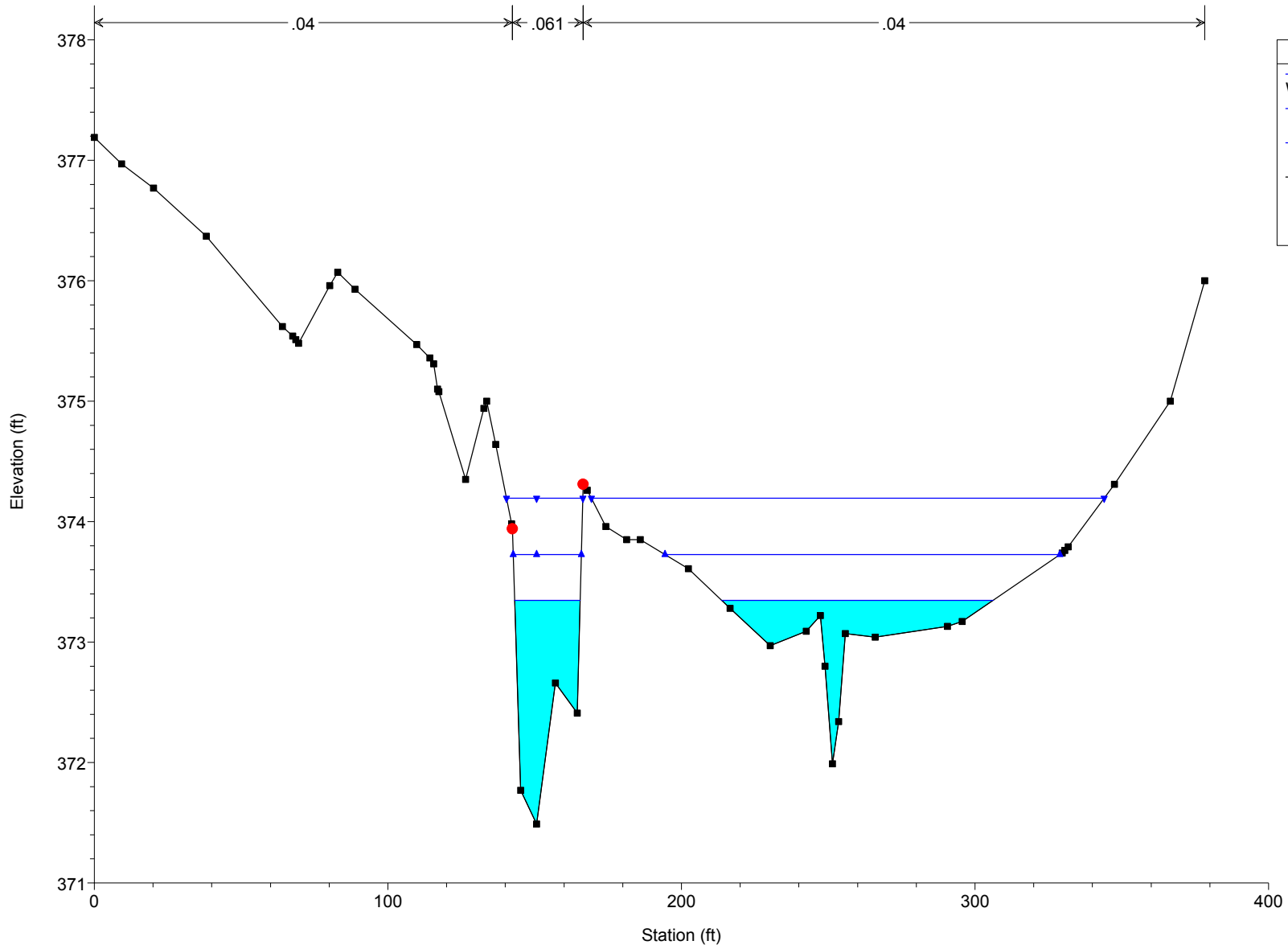
EcclestonMod Plan: existing 11/5/2018
River = JonesFalls Reach = JonesFalls RS = 13



EcclestonMod Plan: existing 11/5/2018
River = JonesFalls Reach = NorthTrib RS = 2



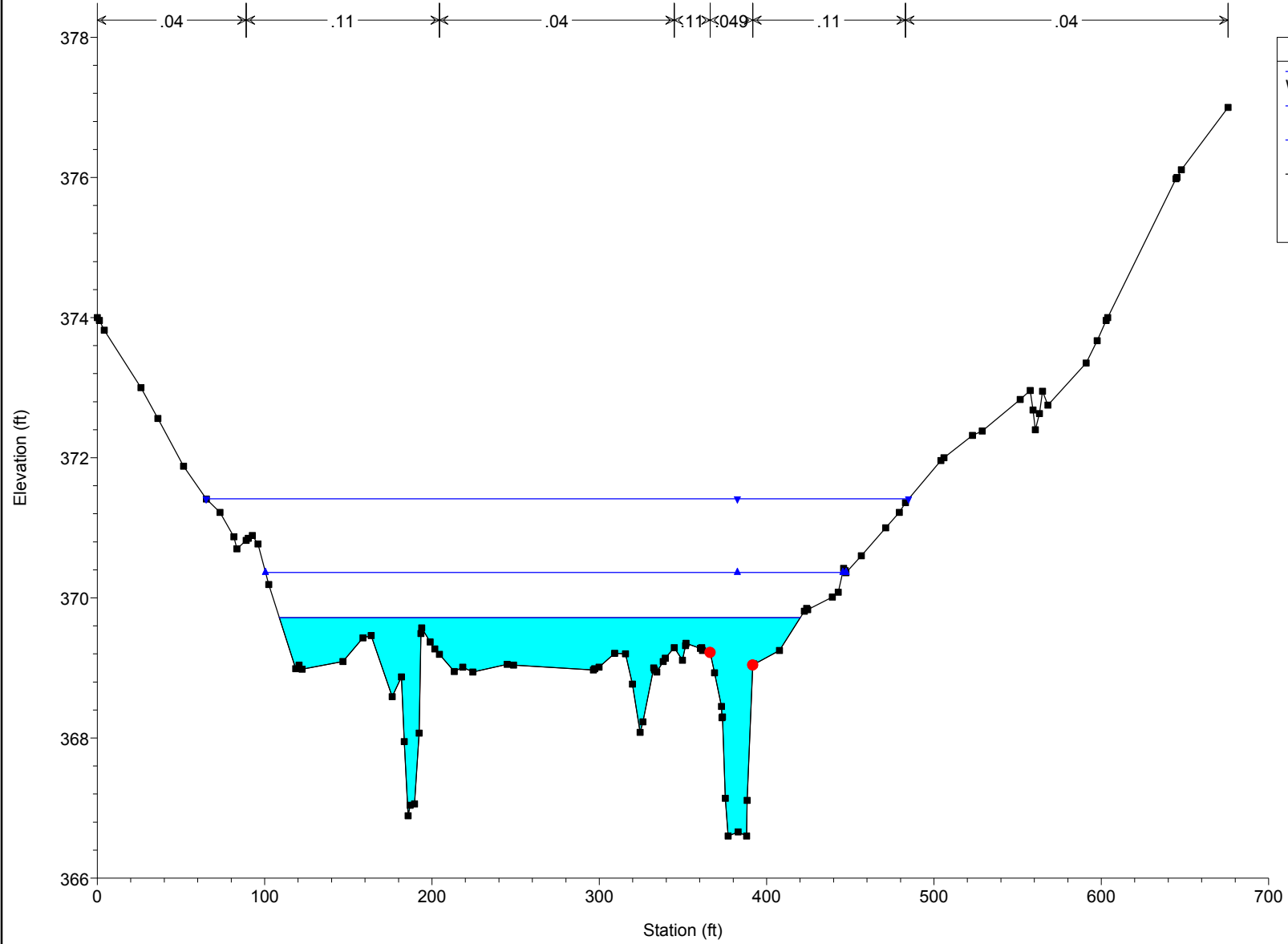
EcclestonMod Plan: existing 11/5/2018
River = JonesFalls Reach = NorthTrib RS = 1



Legend

- WS 100 Yr
- WS 10 Yr
- WS 2 Yr
- Ground
- Bank Sta

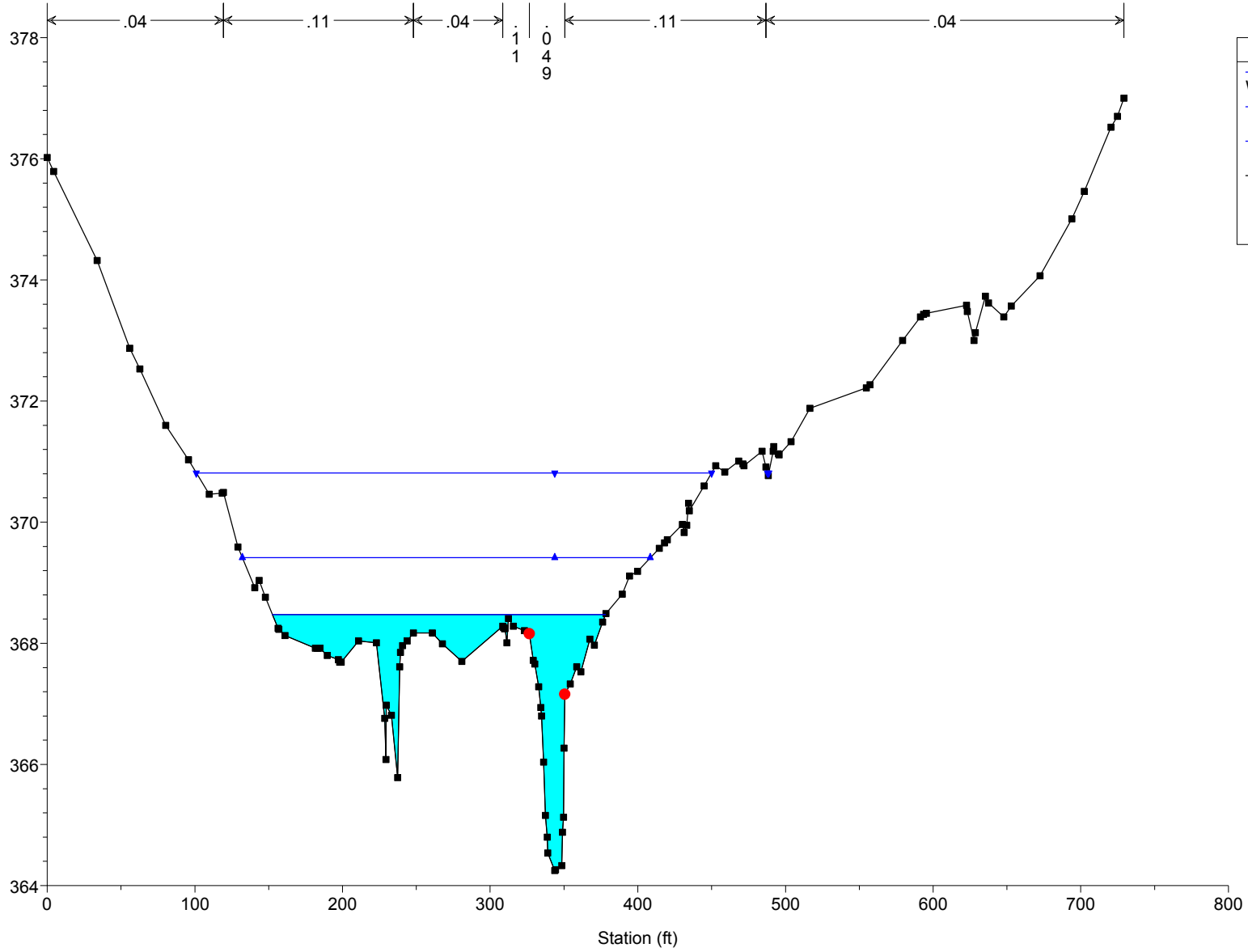
EcclestonMod Plan: existing 11/5/2018
River = JonesFalls Reach = JonesFalls2 RS = 12



Legend

- WS 100 Yr
- WS 10 Yr
- WS 2 Yr
- Ground
- Bank Sta

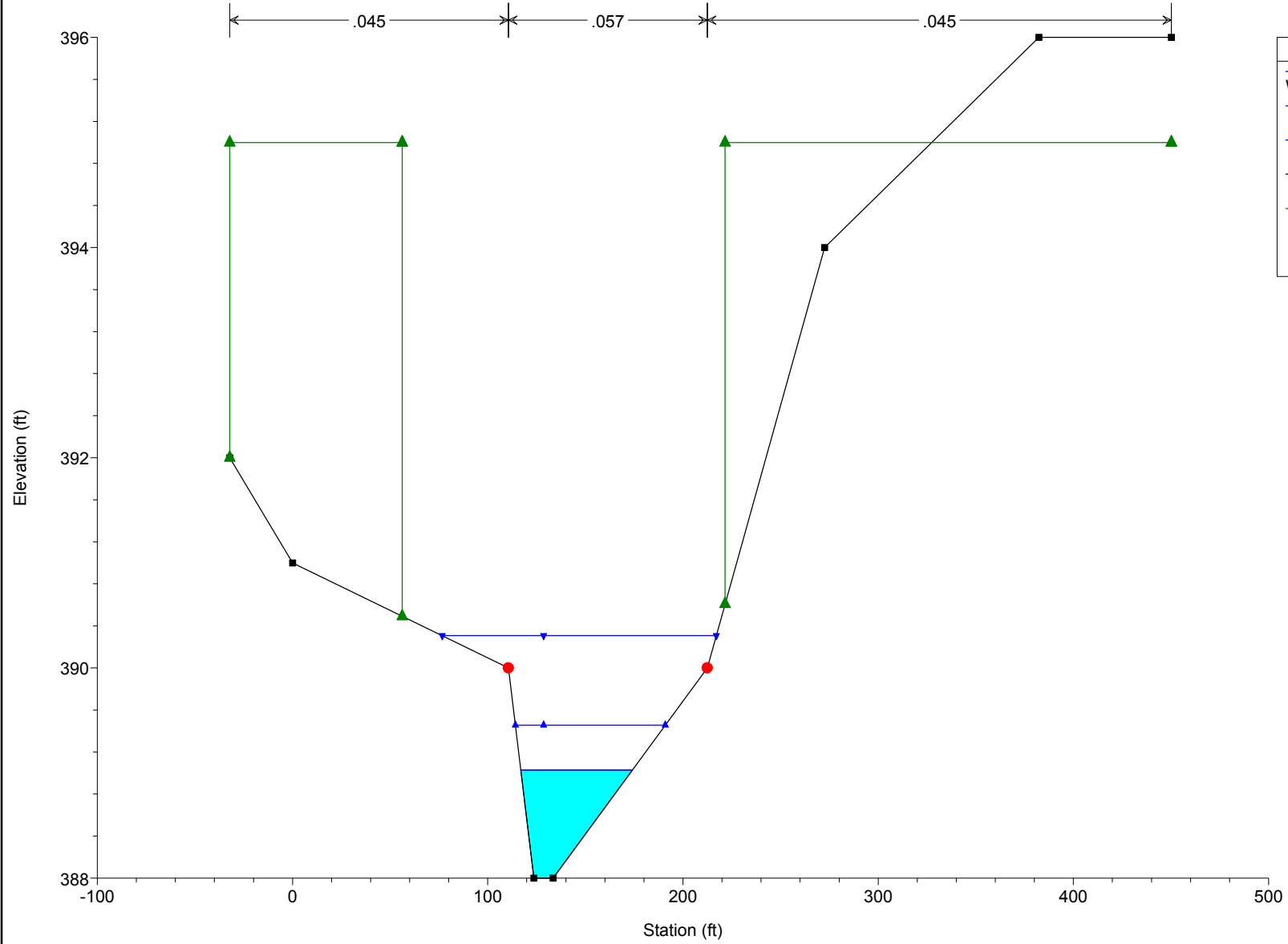
EcclestonMod Plan: existing 11/5/2018
 River = JonesFalls Reach = JonesFalls2 RS = 11



Legend

- WS 100 Yr
- WS 10 Yr
- WS 2 Yr
- Ground
- Bank Sta

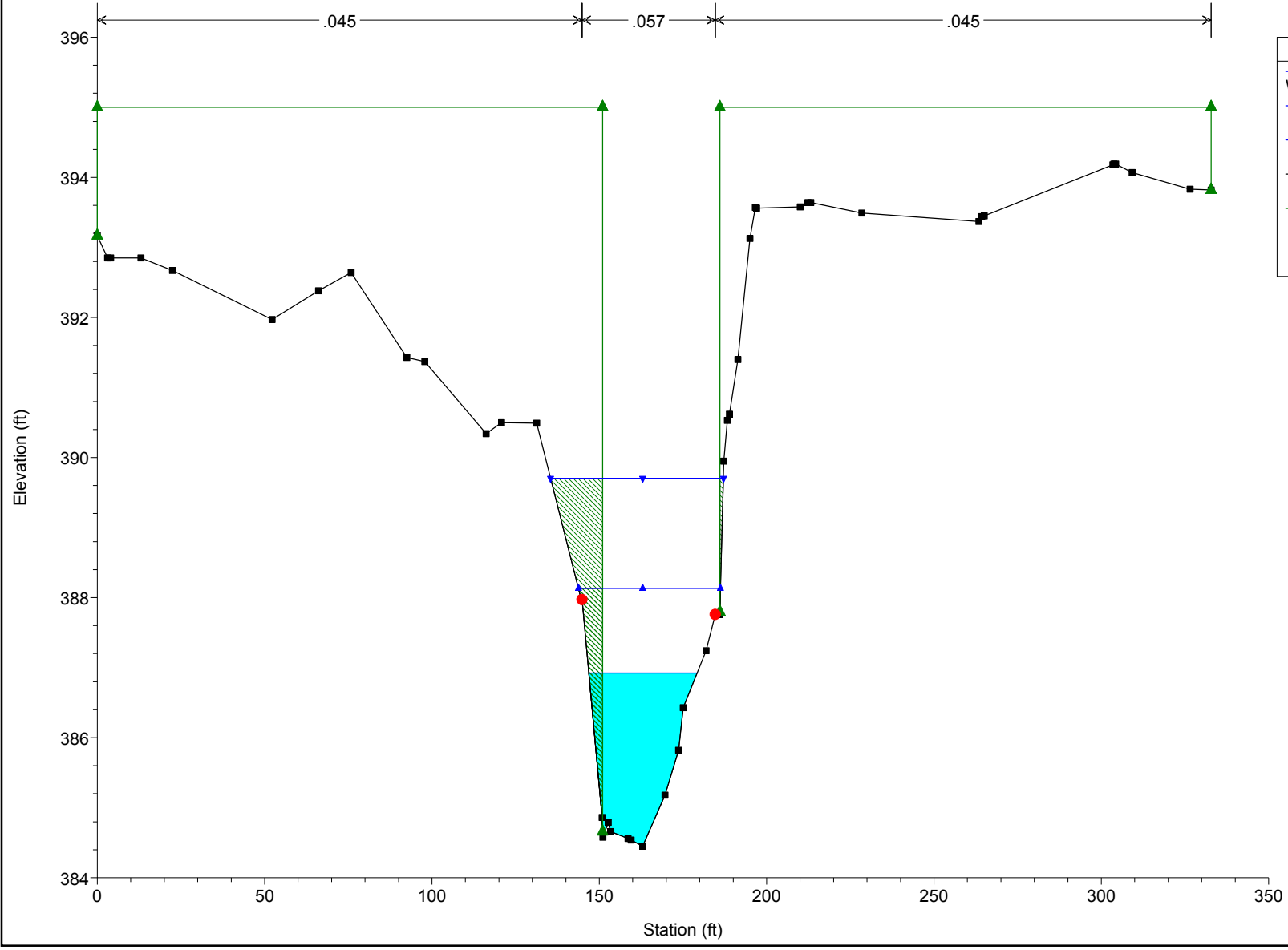
EcclestonMod Plan: existing 11/5/2018
River = JonesFalls Reach = SouthTrib RS = 8



Legend

- WS 100 Yr
- WS 10 Yr
- WS 2 Yr
- Ground
- Ineff
- Bank Sta

EcclestonMod Plan: existing 11/5/2018
 River = JonesFalls Reach = SouthTrib RS = 7

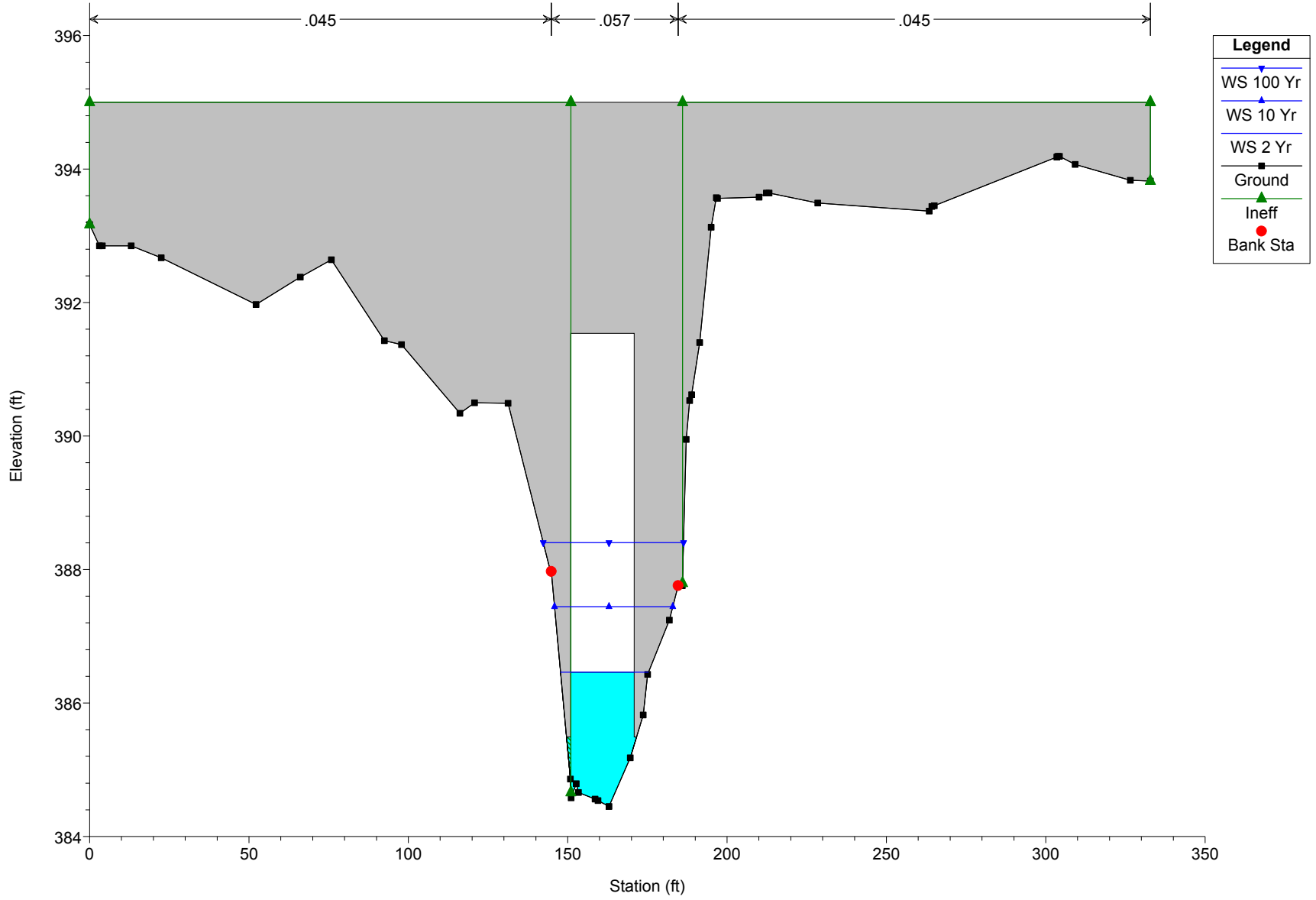


Legend

- WS 100 Yr
- WS 10 Yr
- WS 2 Yr
- Ground
- Ineff
- Bank Sta

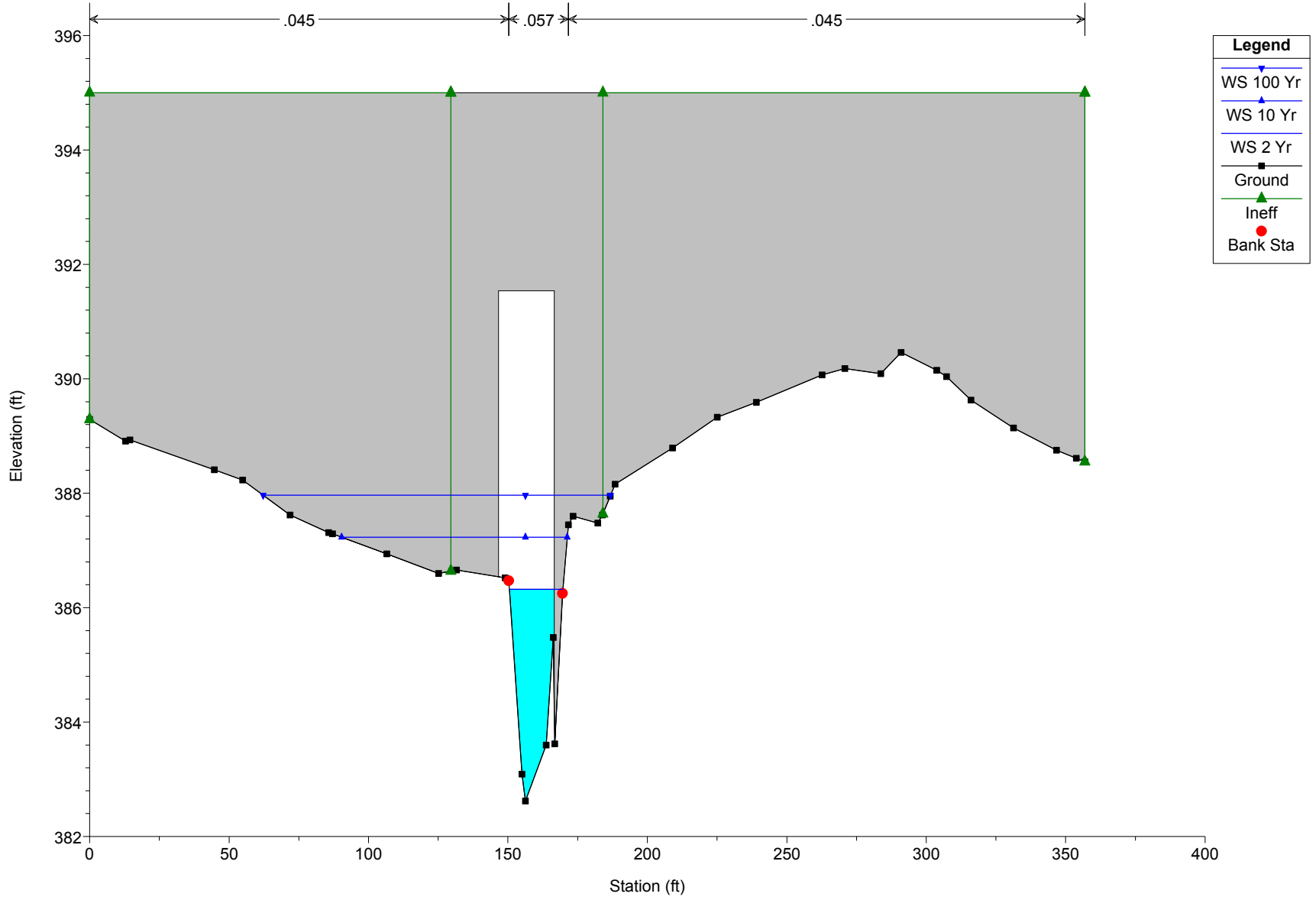
EcclestonMod Plan: existing 11/5/2018

River = JonesFalls Reach = SouthTrib RS = 6.5 BR Cliffholme Rd Bridge

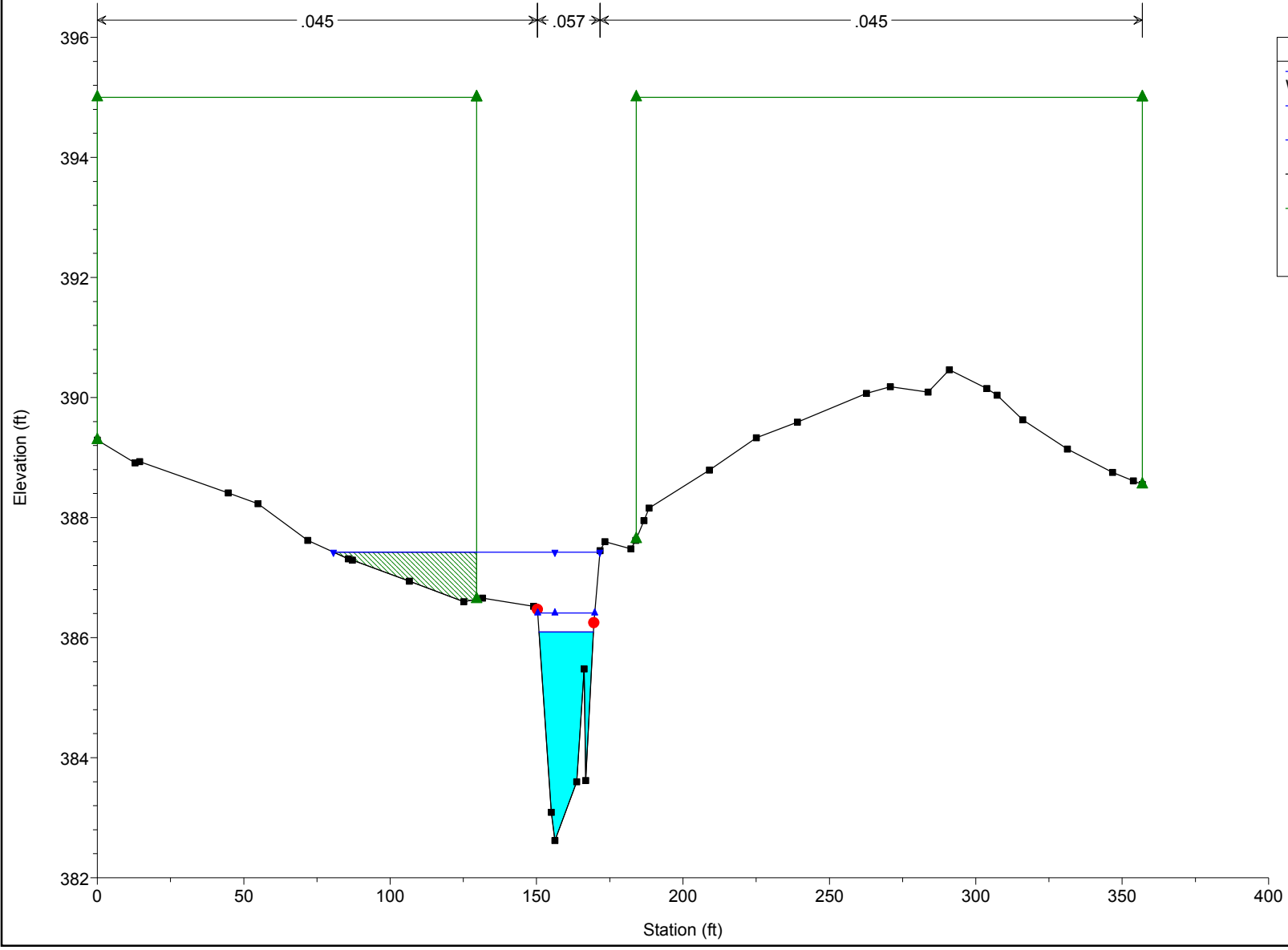


EcclestonMod Plan: existing 11/5/2018

River = JonesFalls Reach = SouthTrib RS = 6.5 BR Cliffholme Rd Bridge

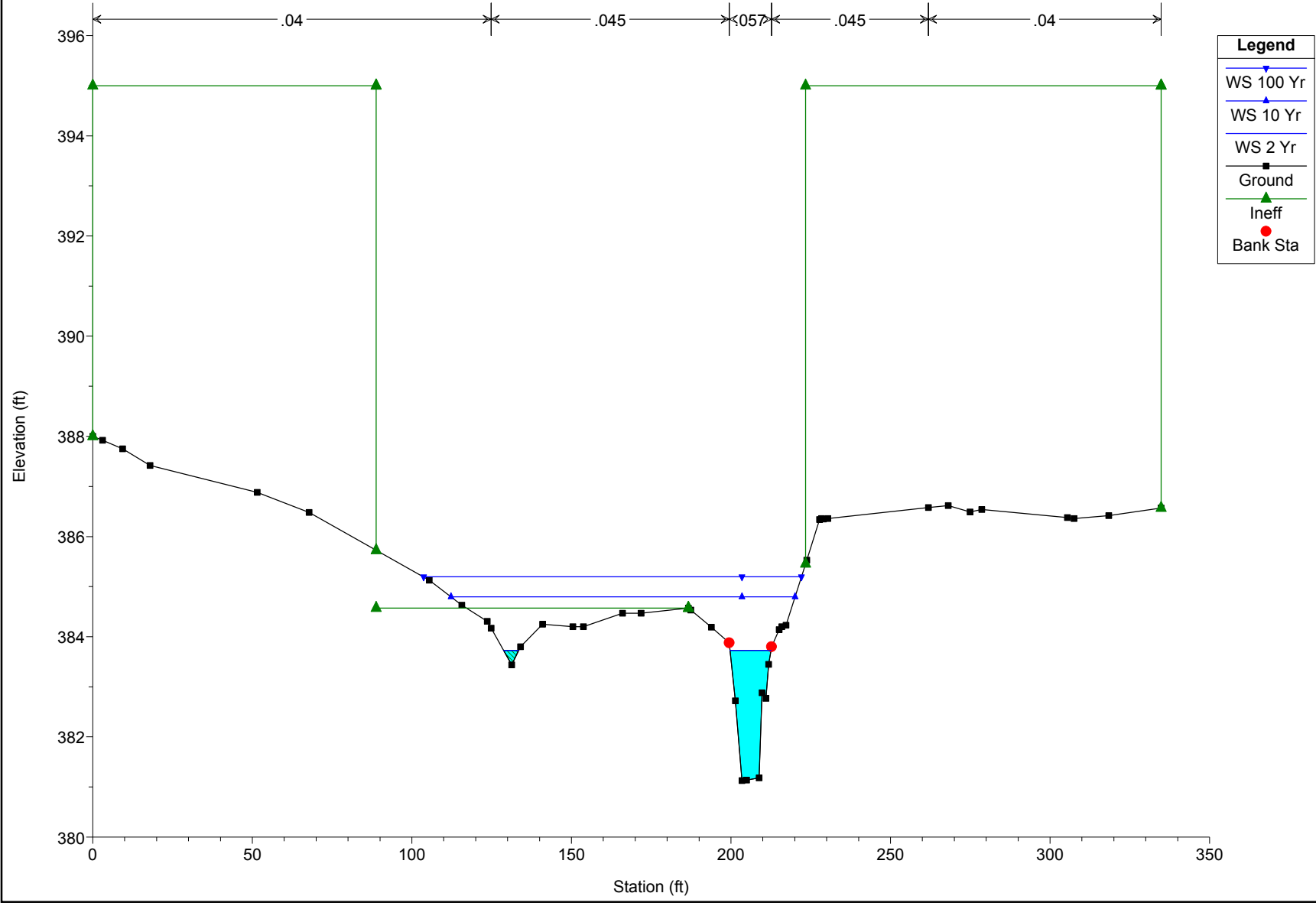


EcclestonMod Plan: existing 11/5/2018
 River = JonesFalls Reach = SouthTrib RS = 6

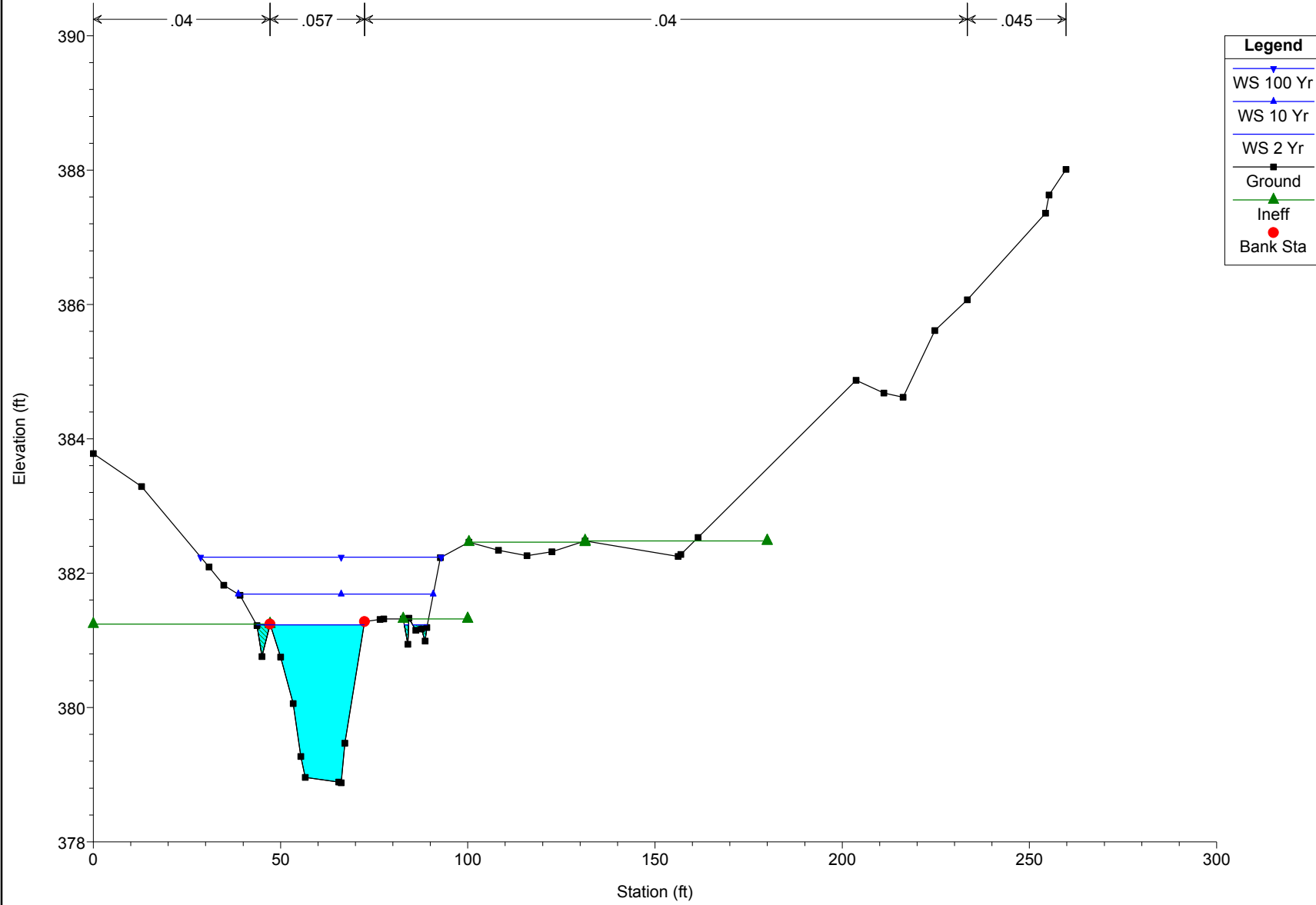


EcclestonMod Plan: existing 11/5/2018

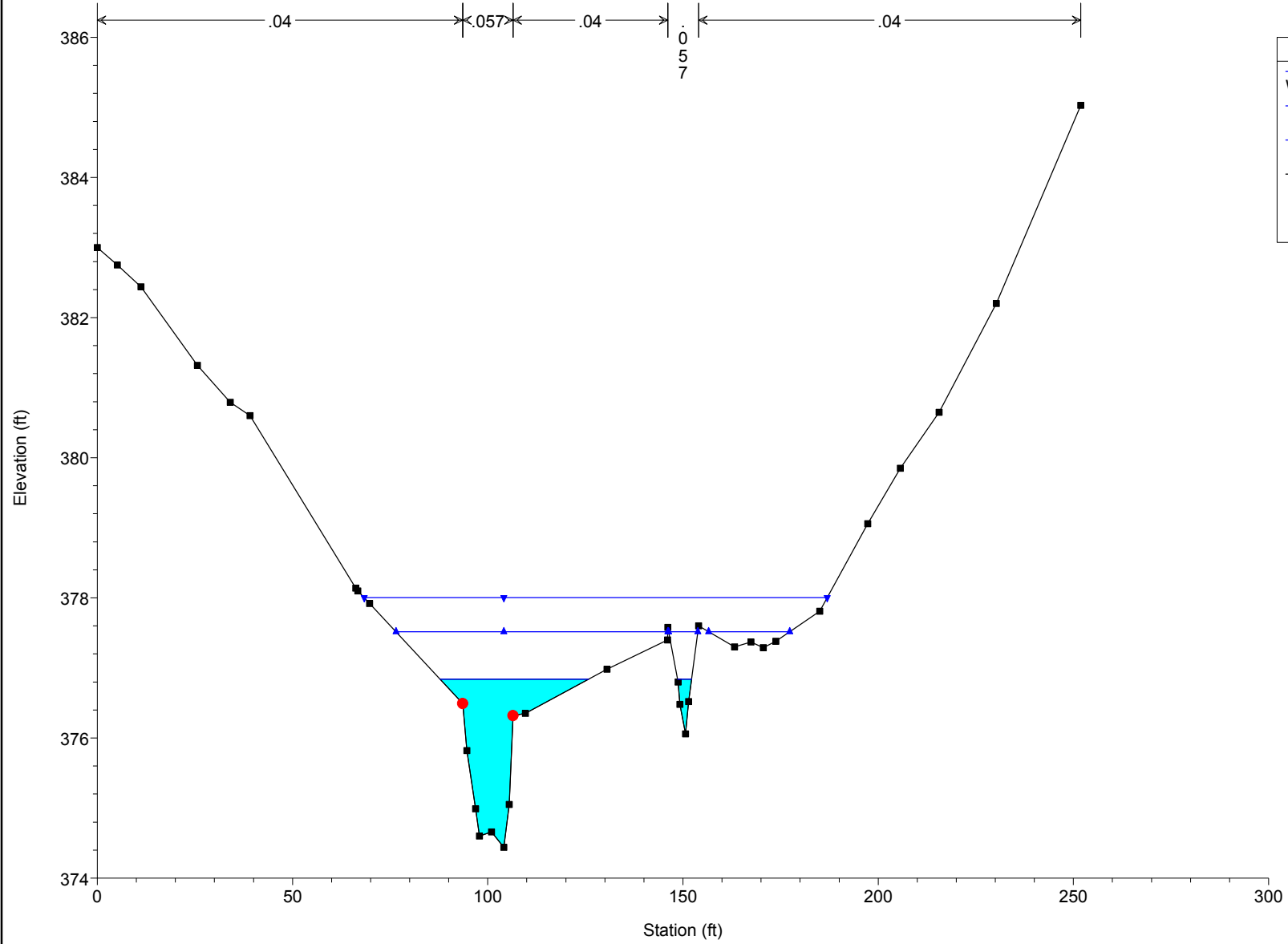
River = JonesFalls Reach = SouthTrib RS = 5



EcclestonMod Plan: existing 11/5/2018
River = JonesFalls Reach = SouthTrib RS = 4



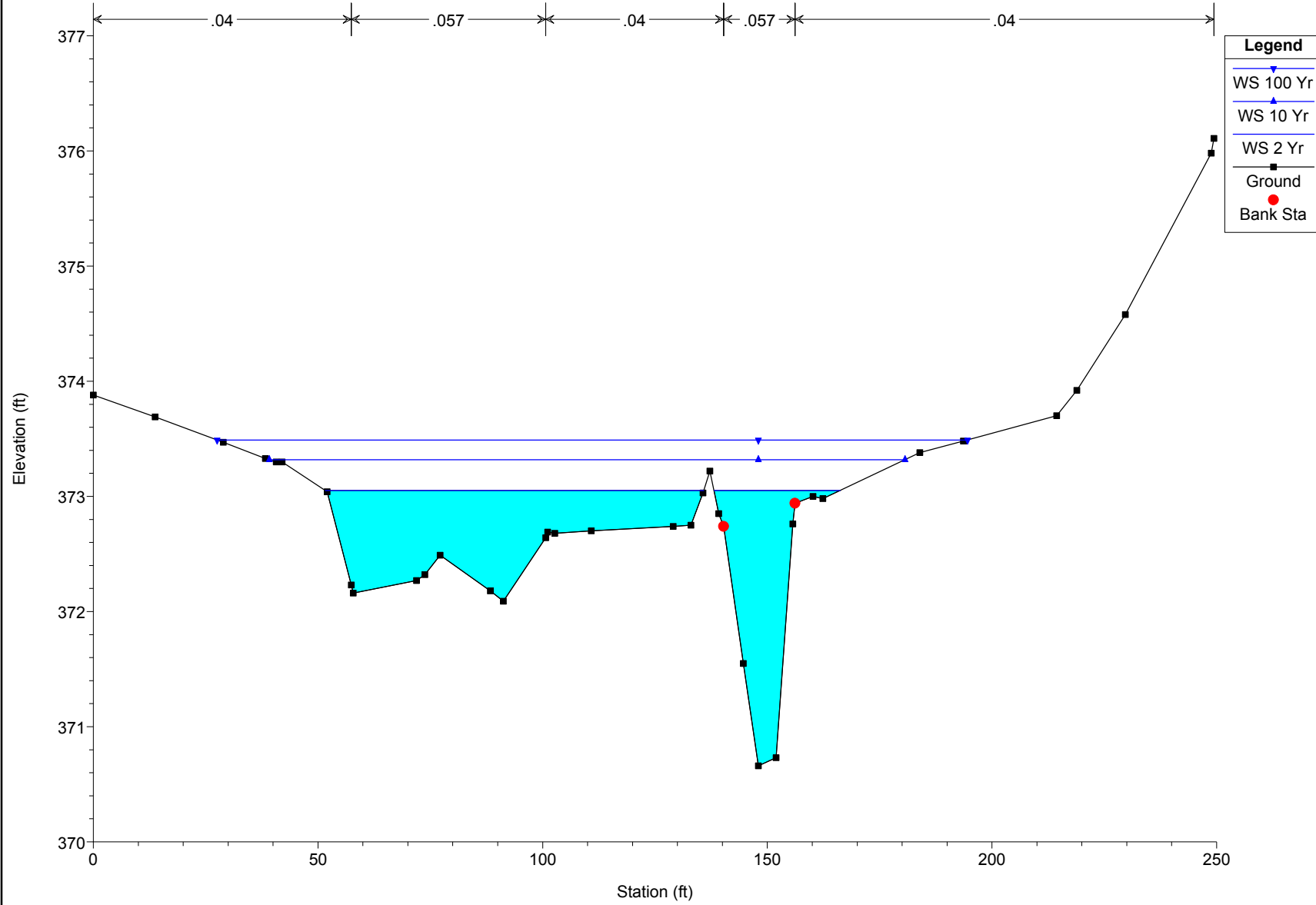
EcclestonMod Plan: existing 11/5/2018
River = JonesFalls Reach = SouthTrib RS = 3



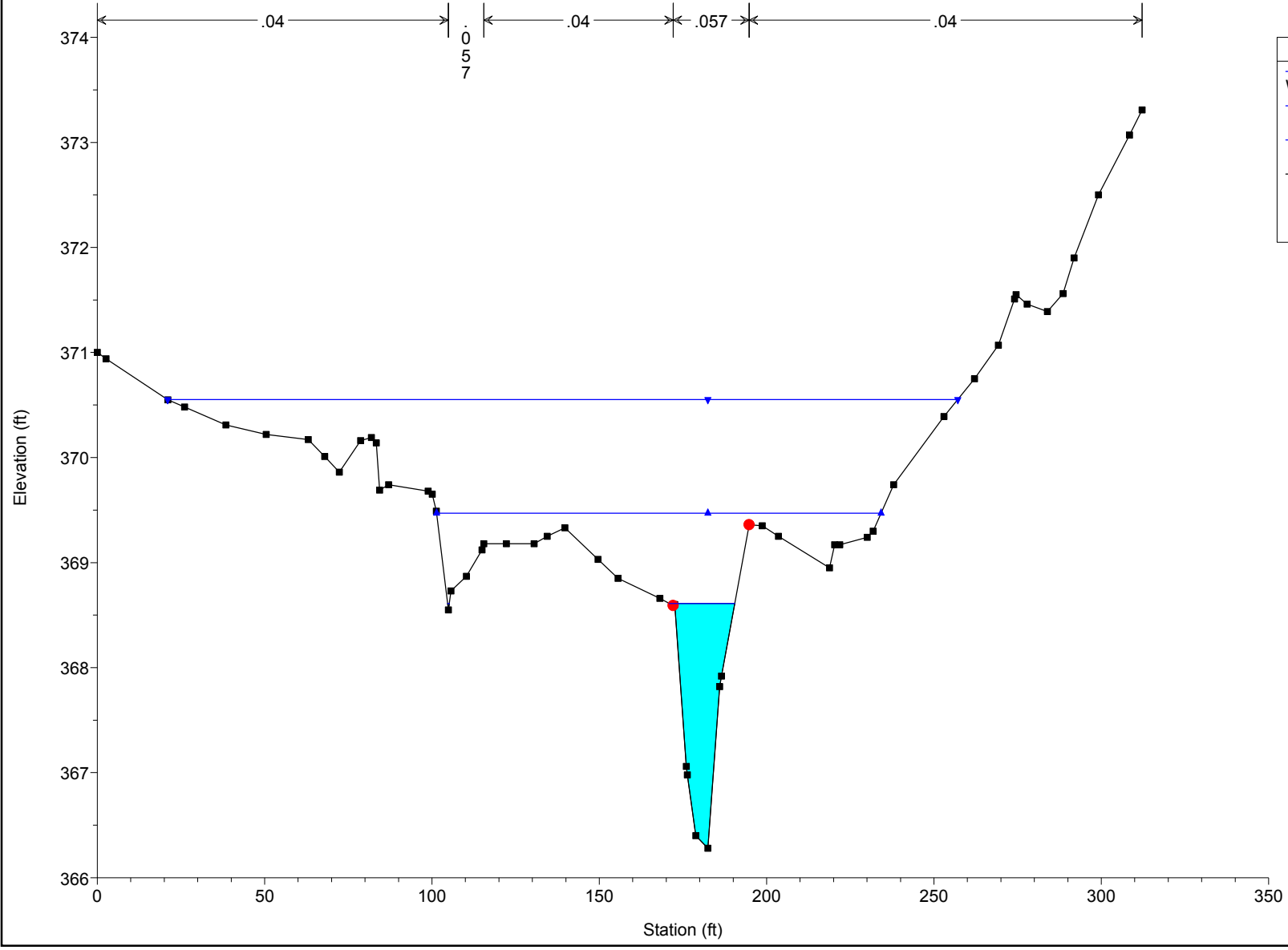
Legend

- WS 100 Yr
- WS 10 Yr
- WS 2 Yr
- Ground
- Bank Sta

EcclestonMod Plan: existing 11/5/2018
River = JonesFalls Reach = SouthTrib RS = 2

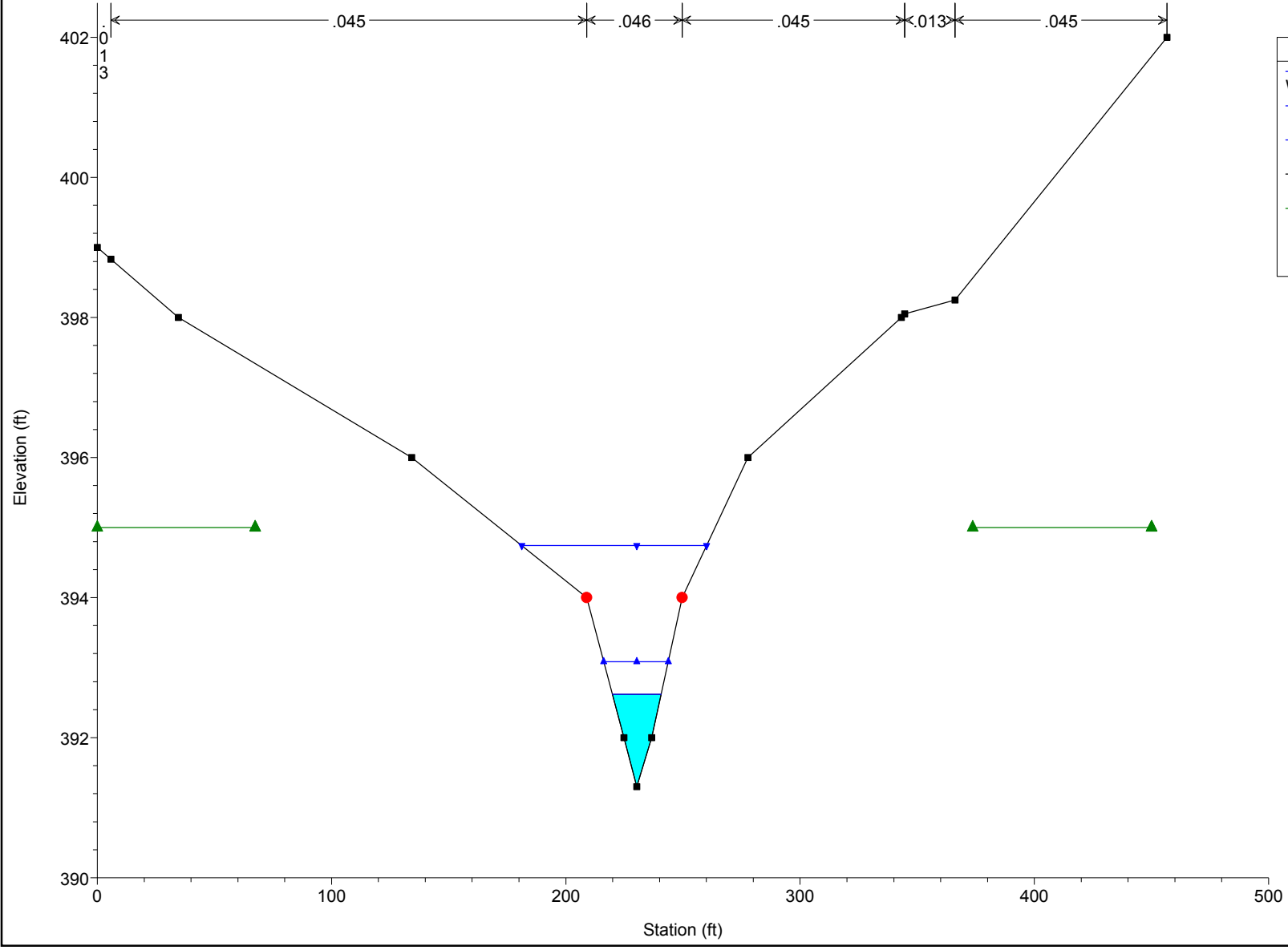


EcclestonMod Plan: existing 11/5/2018
 River = JonesFalls Reach = SouthTrib RS = 1



| Legend | |
|-----------|---|
| WS 100 Yr | Blue line with downward-pointing triangle |
| WS 10 Yr | Blue line with upward-pointing triangle |
| WS 2 Yr | Blue line with downward-pointing triangle |
| Ground | Black line with square markers |
| Bank Sta | Red circle |

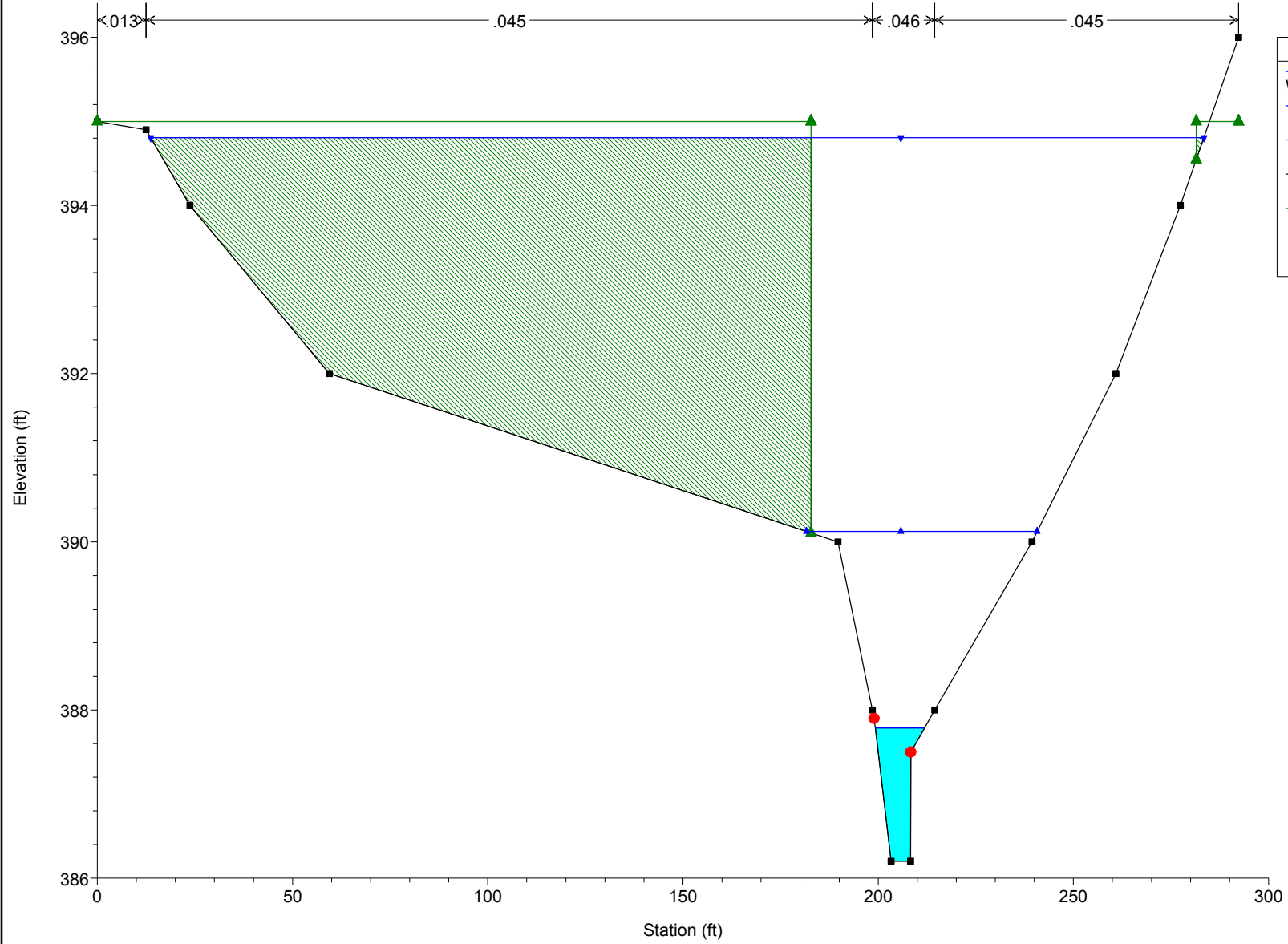
EcclestonMod Plan: existing 11/5/2018
River = JonesFalls Reach = IntsTrib RS = 8



Legend

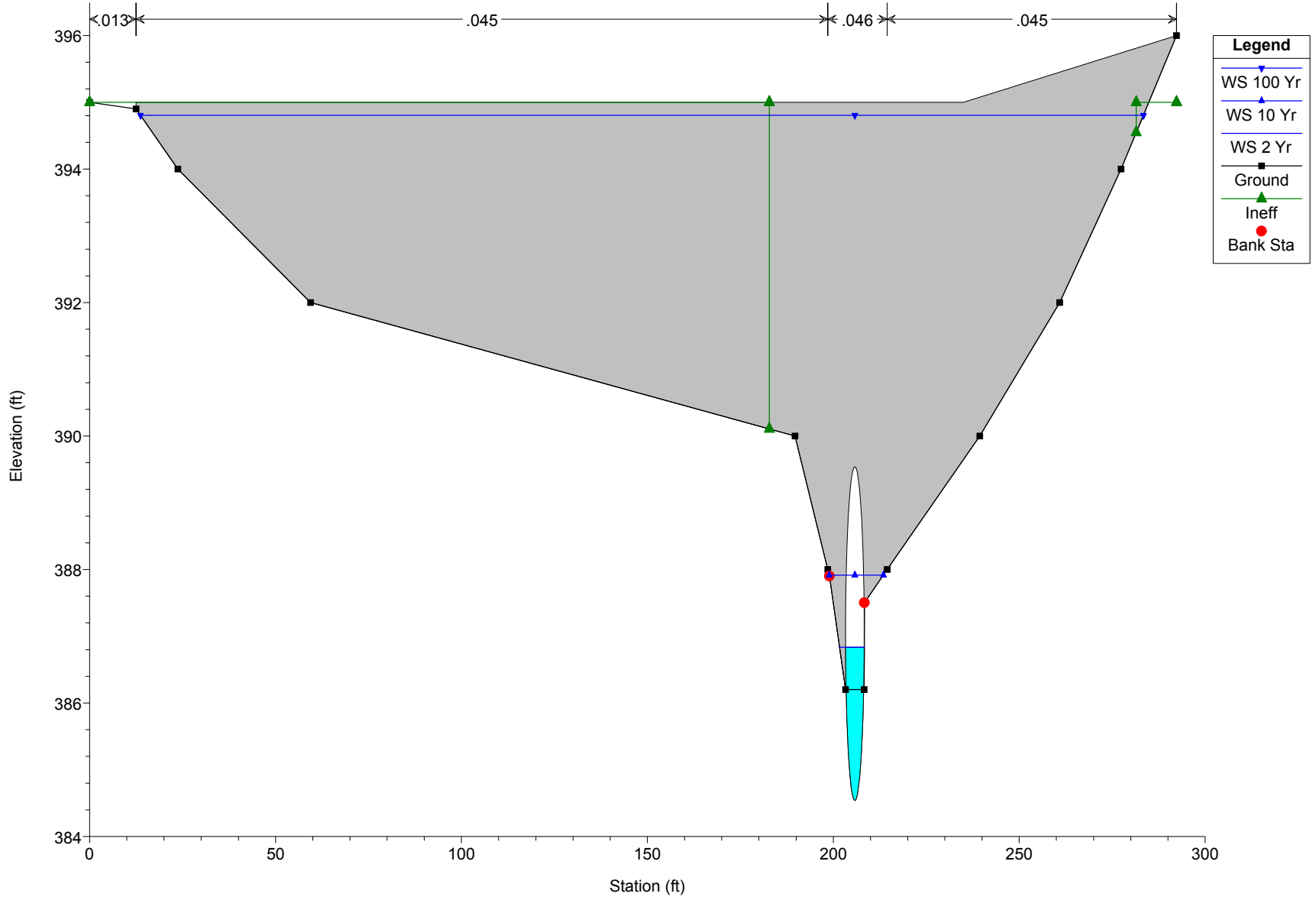
- WS 100 Yr
- WS 10 Yr
- WS 2 Yr
- Ground
- Ineff
- Bank Sta

EcclestonMod Plan: existing 11/5/2018
River = JonesFalls Reach = IntsTrib RS = 7



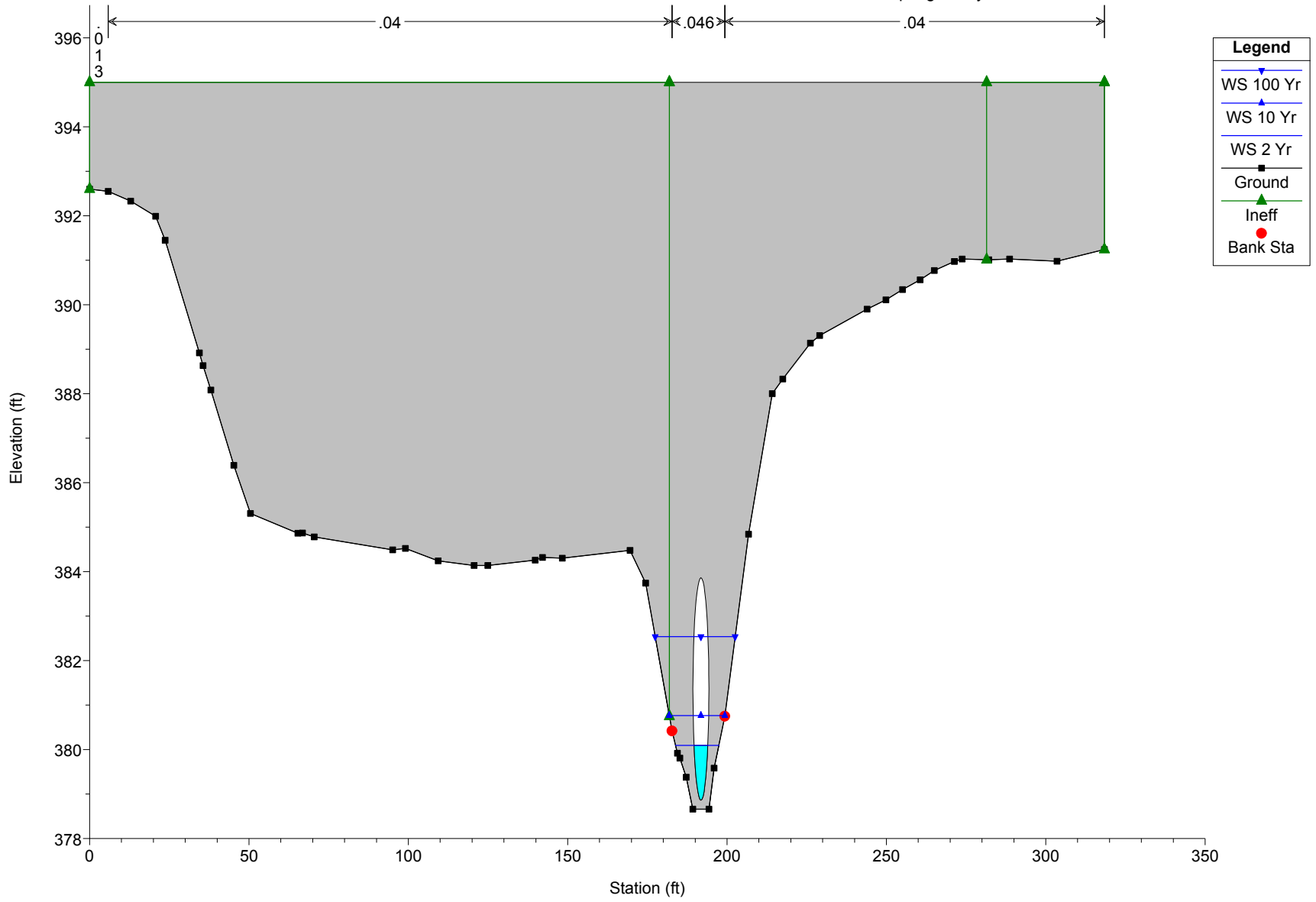
EcclestonMod Plan: existing 11/5/2018

River = JonesFalls Reach = IntsTrib RS = 6.5 Culv Culvert under Greenspring Valley Rd.

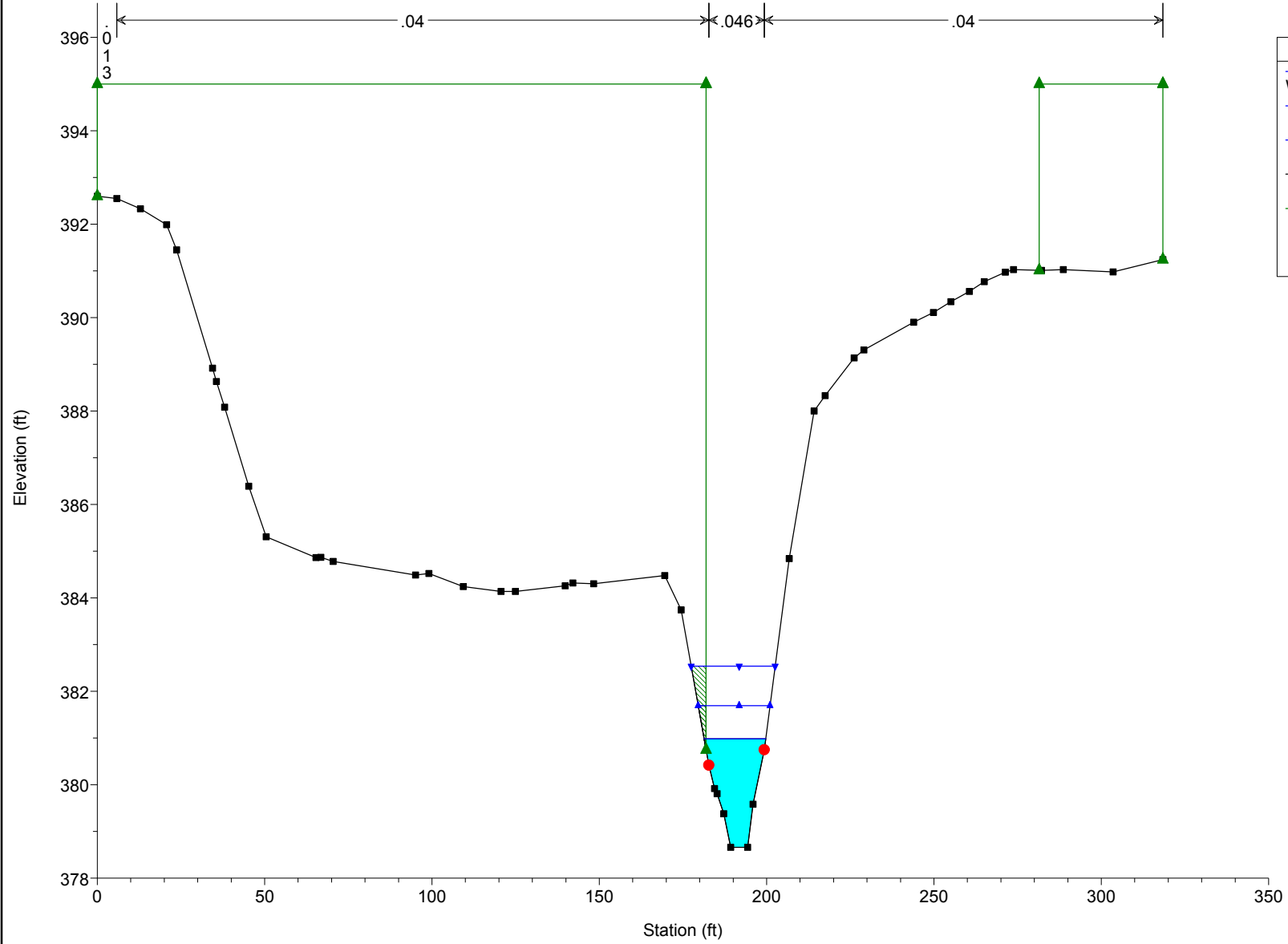


EcclestonMod Plan: existing 11/5/2018

River = JonesFalls Reach = IntsTrib RS = 6.5 Culv Culvert under Greenspring Valley Rd.

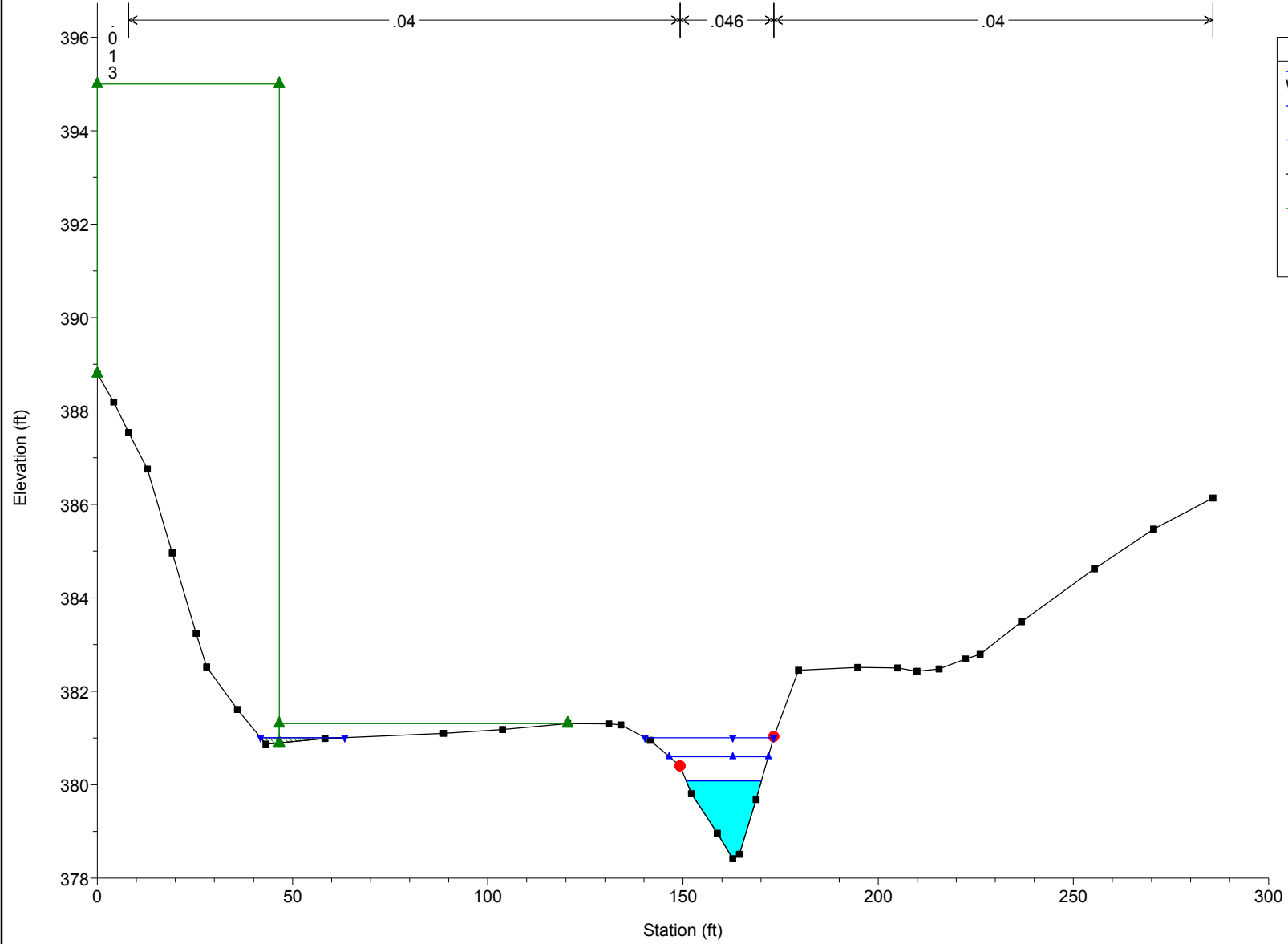


EcclestonMod Plan: existing 11/5/2018
 River = JonesFalls Reach = IntsTrib RS = 6



| Legend | |
|-----------|------------------------|
| WS 100 Yr | Blue inverted triangle |
| WS 10 Yr | Blue triangle |
| WS 2 Yr | Black square |
| Ground | Black square |
| Ineff | Green triangle |
| Bank Sta | Red circle |

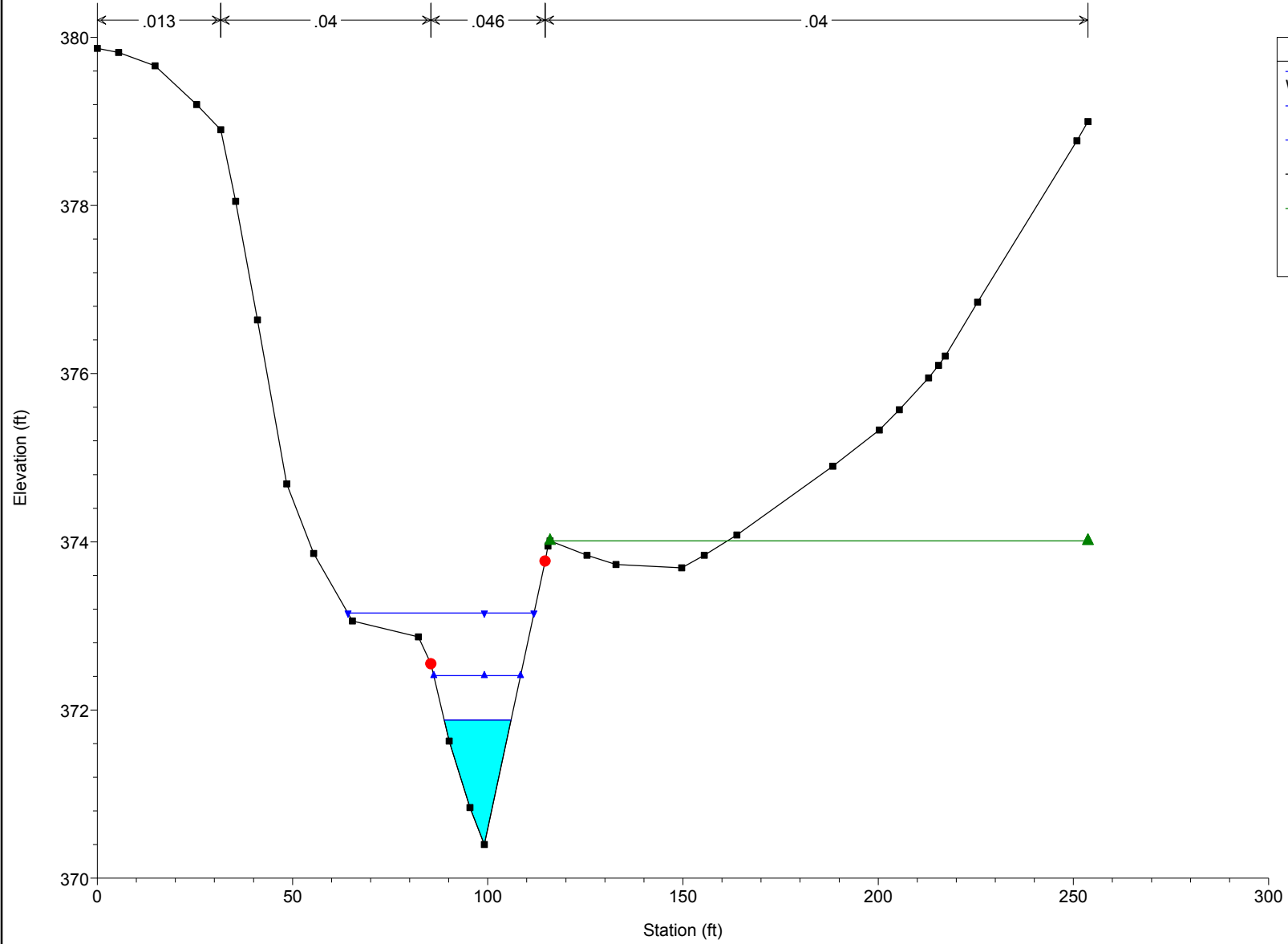
EcclestonMod Plan: existing 11/5/2018
 River = JonesFalls Reach = IntsTrib RS = 5



Legend

- WS 100 Yr
- WS 10 Yr
- WS 2 Yr
- Ground
- Ineff
- Bank Sta

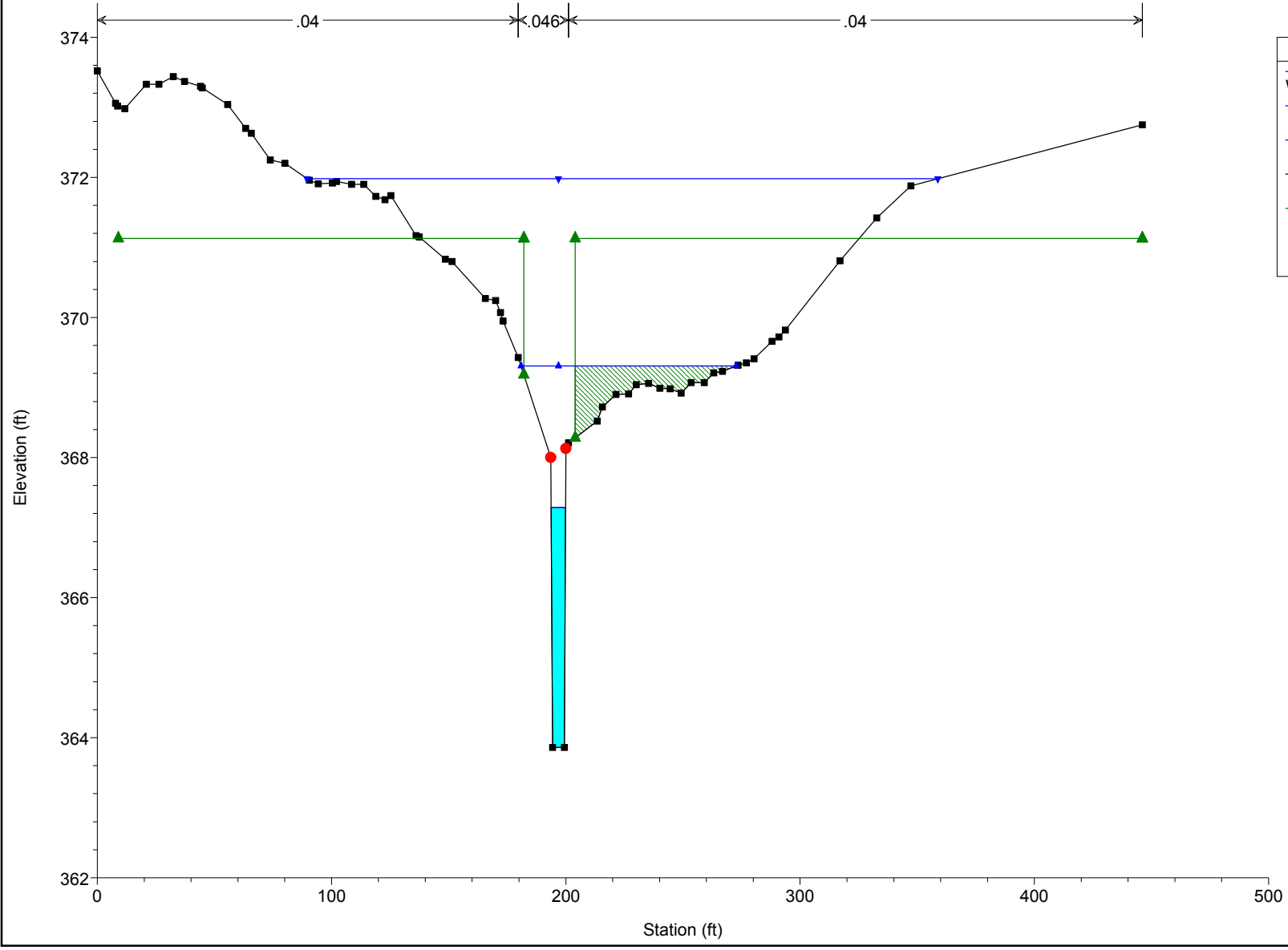
EcclestonMod Plan: existing 11/5/2018
River = JonesFalls Reach = IntsTrib RS = 4



Legend

- WS 100 Yr
- WS 10 Yr
- WS 2 Yr
- Ground
- Ineff
- Bank Sta

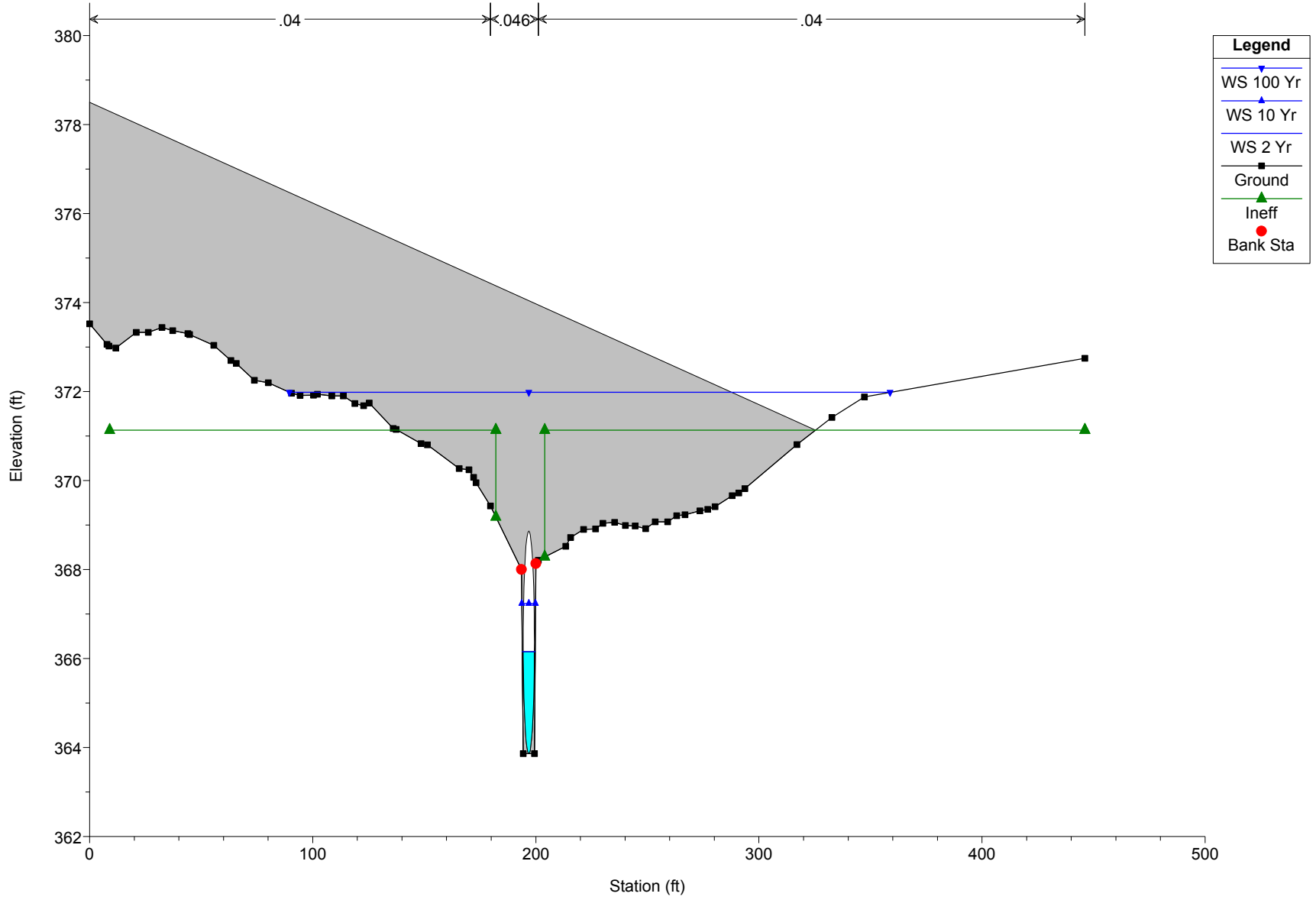
EcclestonMod Plan: existing 11/5/2018
River = JonesFalls Reach = IntsTrib RS = 3



| Legend | |
|-----------|----------------------------------|
| WS 100 Yr | Blue line with downward triangle |
| WS 10 Yr | Blue line with upward triangle |
| WS 2 Yr | Blue line with square |
| Ground | Black line with square |
| Ineff | Green line with upward triangle |
| Bank Sta | Red dot |

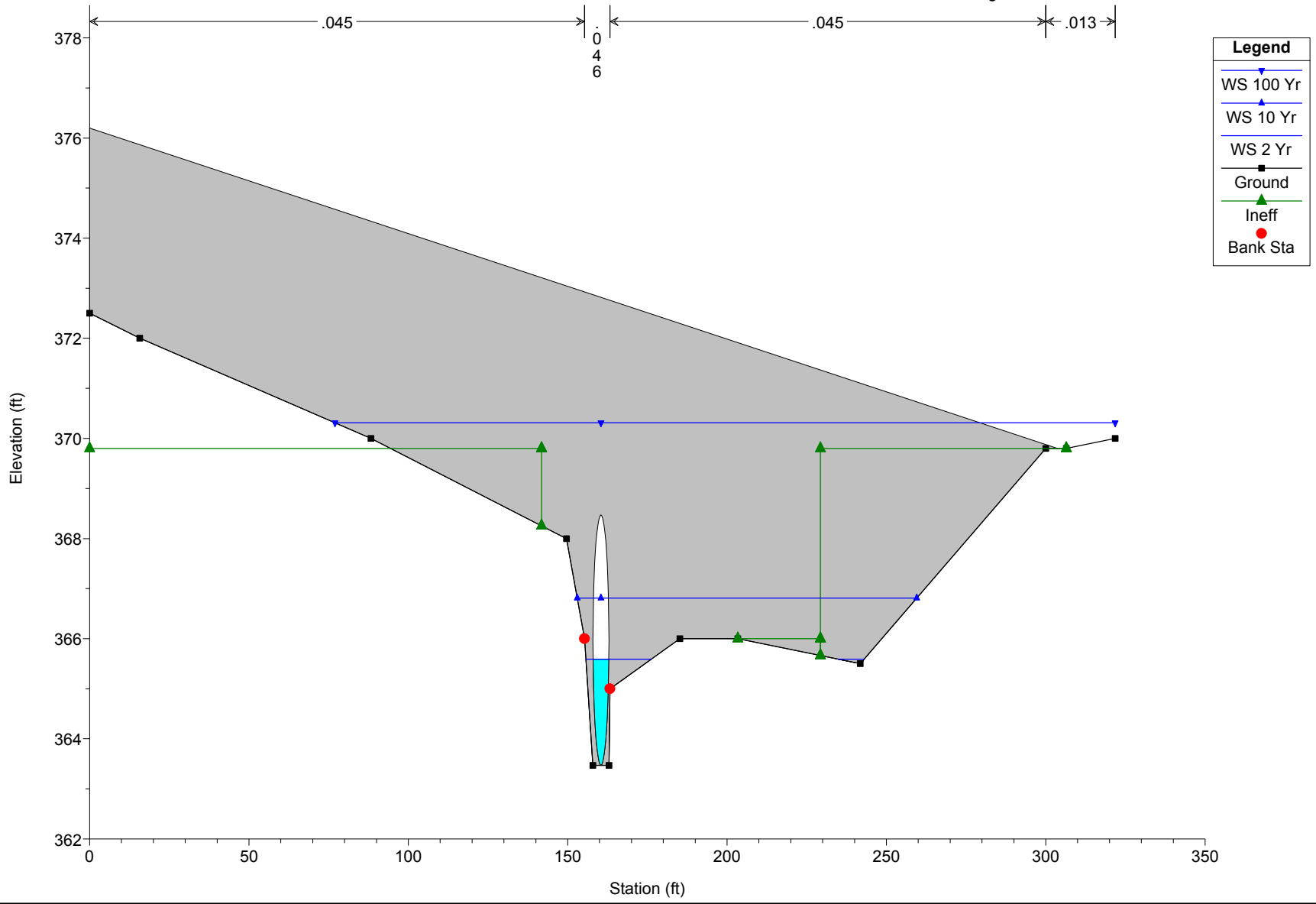
EcclestonMod Plan: existing 11/5/2018

River = JonesFalls Reach = IntsTrib RS = 2.5 Culv Intersection Trib Culvert under Park Heights Ave.

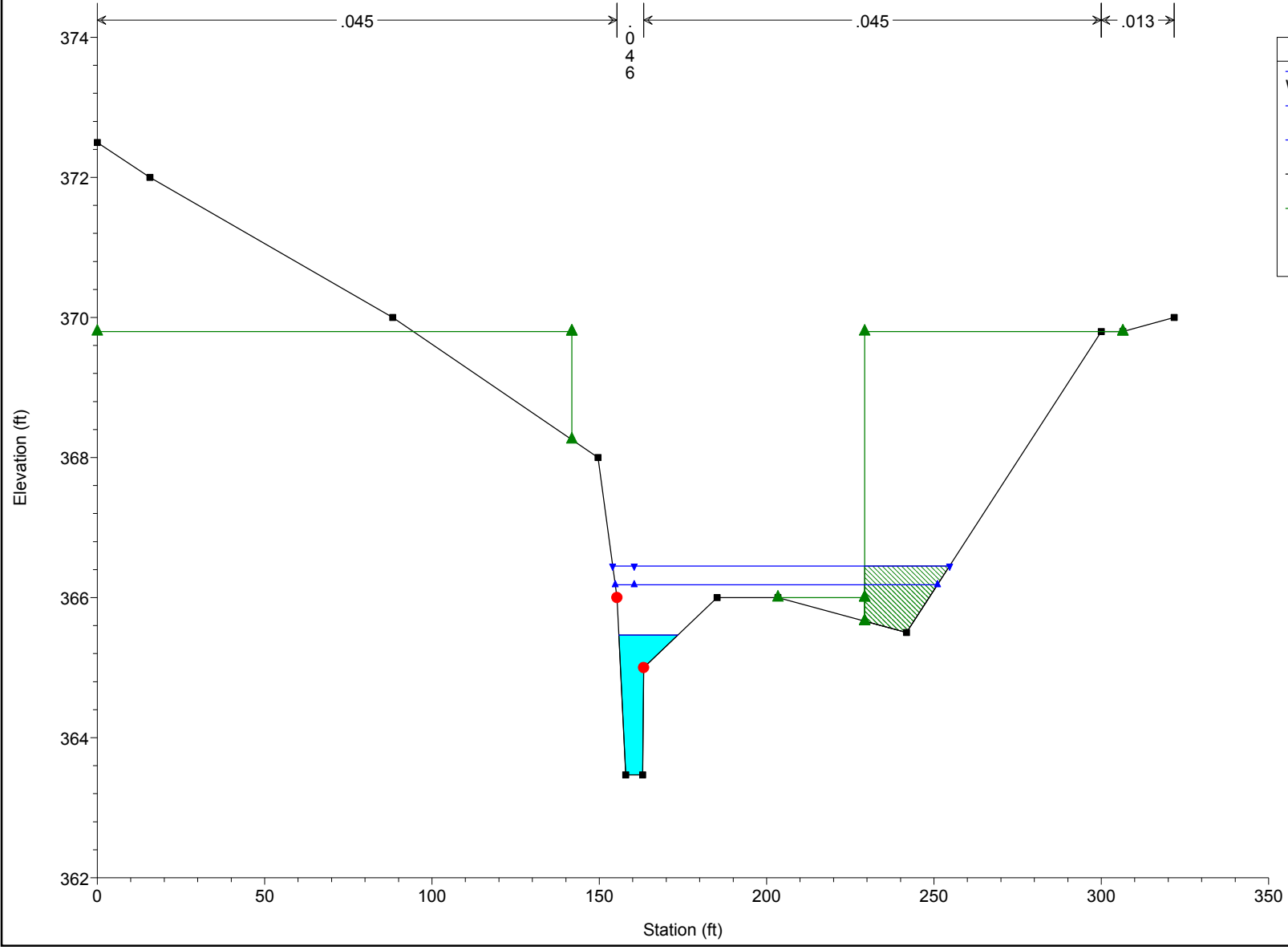


EcclestonMod Plan: existing 11/5/2018

River = JonesFalls Reach = IntsTrib RS = 2.5 Culv Intersection Trib Culvert under Park Heights Ave.



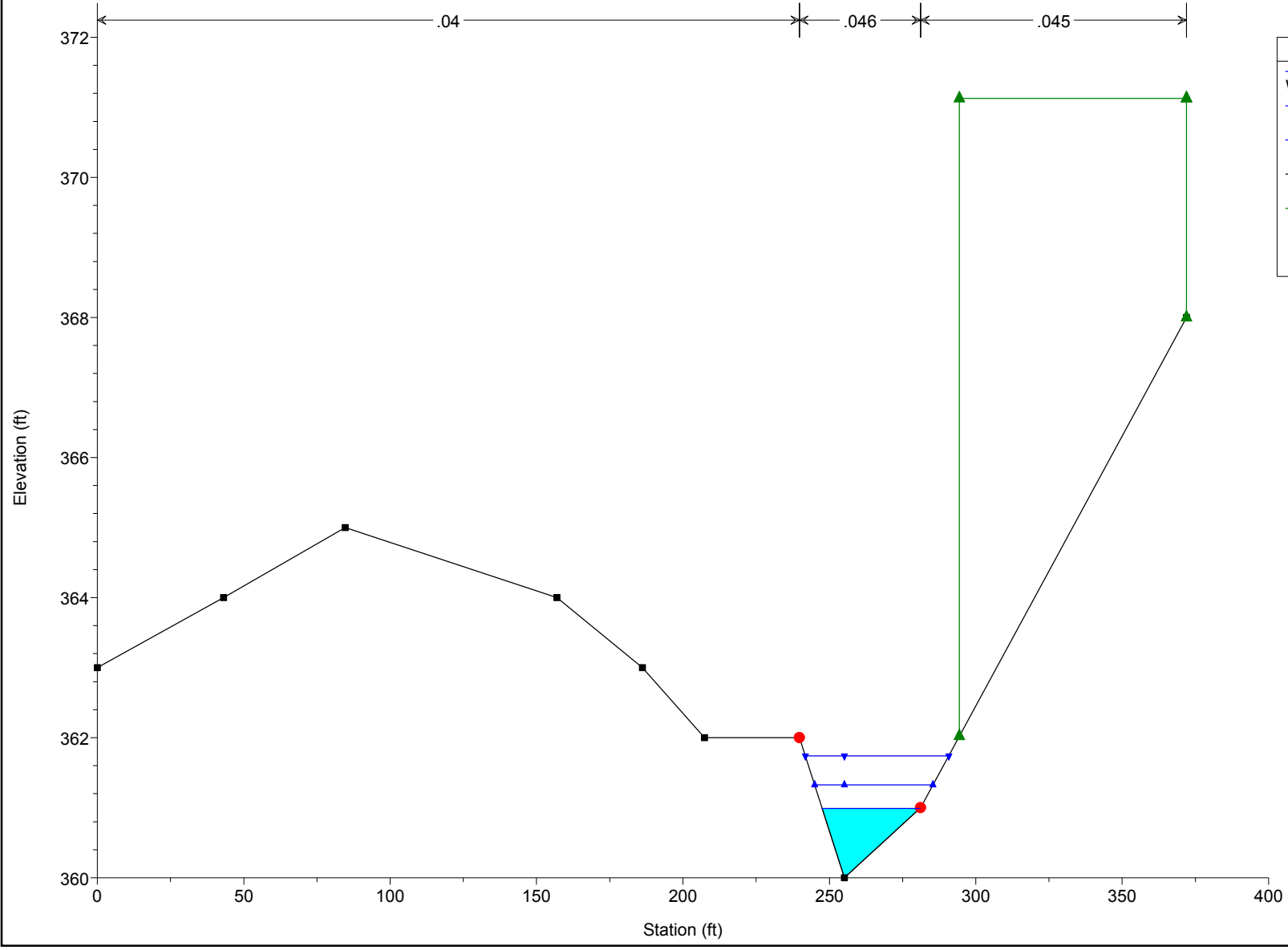
EcclestonMod Plan: existing 11/5/2018
River = JonesFalls Reach = IntsTrib RS = 2



Legend

- WS 100 Yr
- WS 10 Yr
- WS 2 Yr
- Ground
- Ineff
- Bank Sta

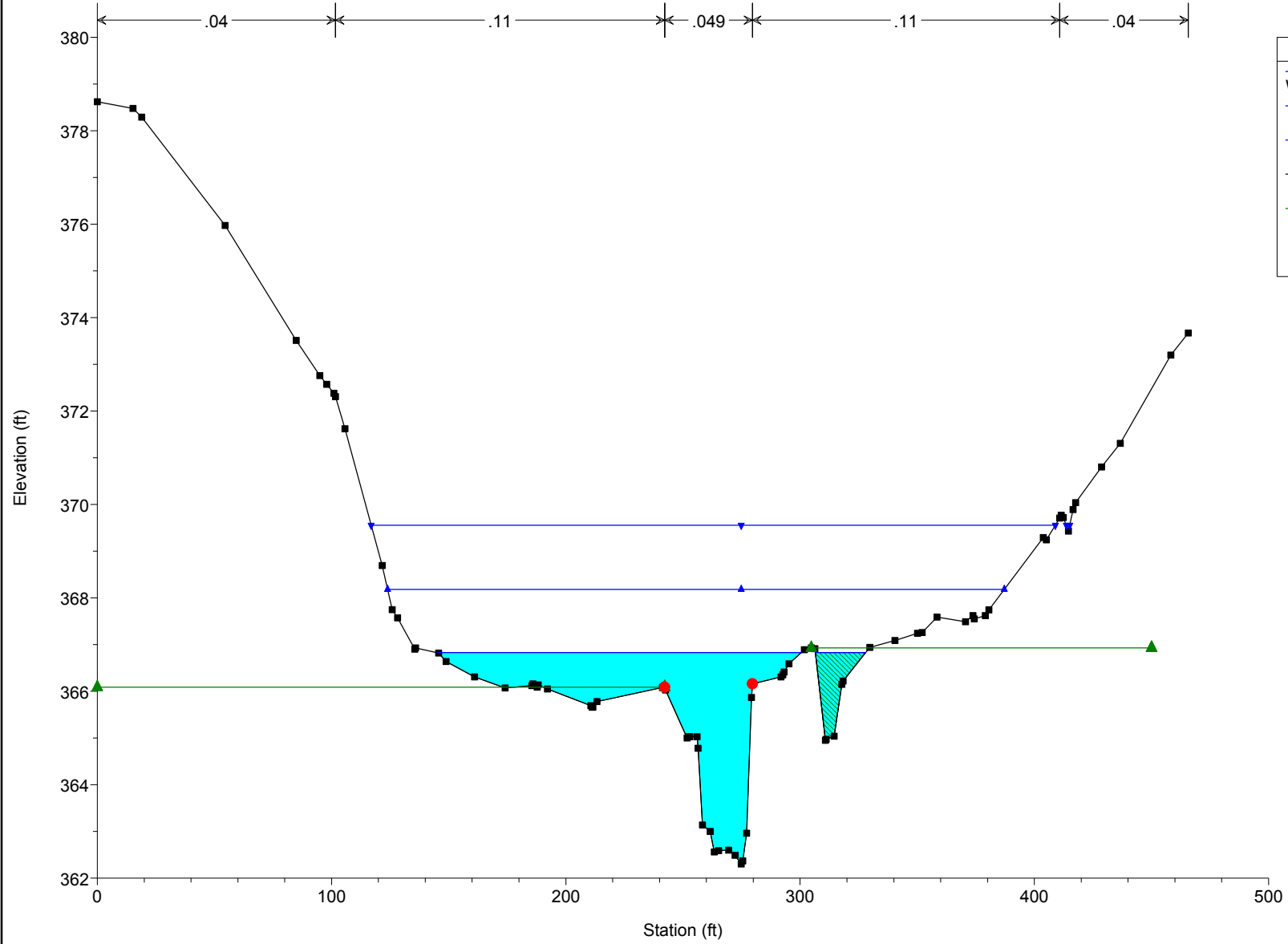
EcclestonMod Plan: existing 11/5/2018
 River = JonesFalls Reach = IntsTrib RS = 1



Legend

- WS 100 Yr
- WS 10 Yr
- WS 2 Yr
- Ground
- Ineff
- Bank Sta

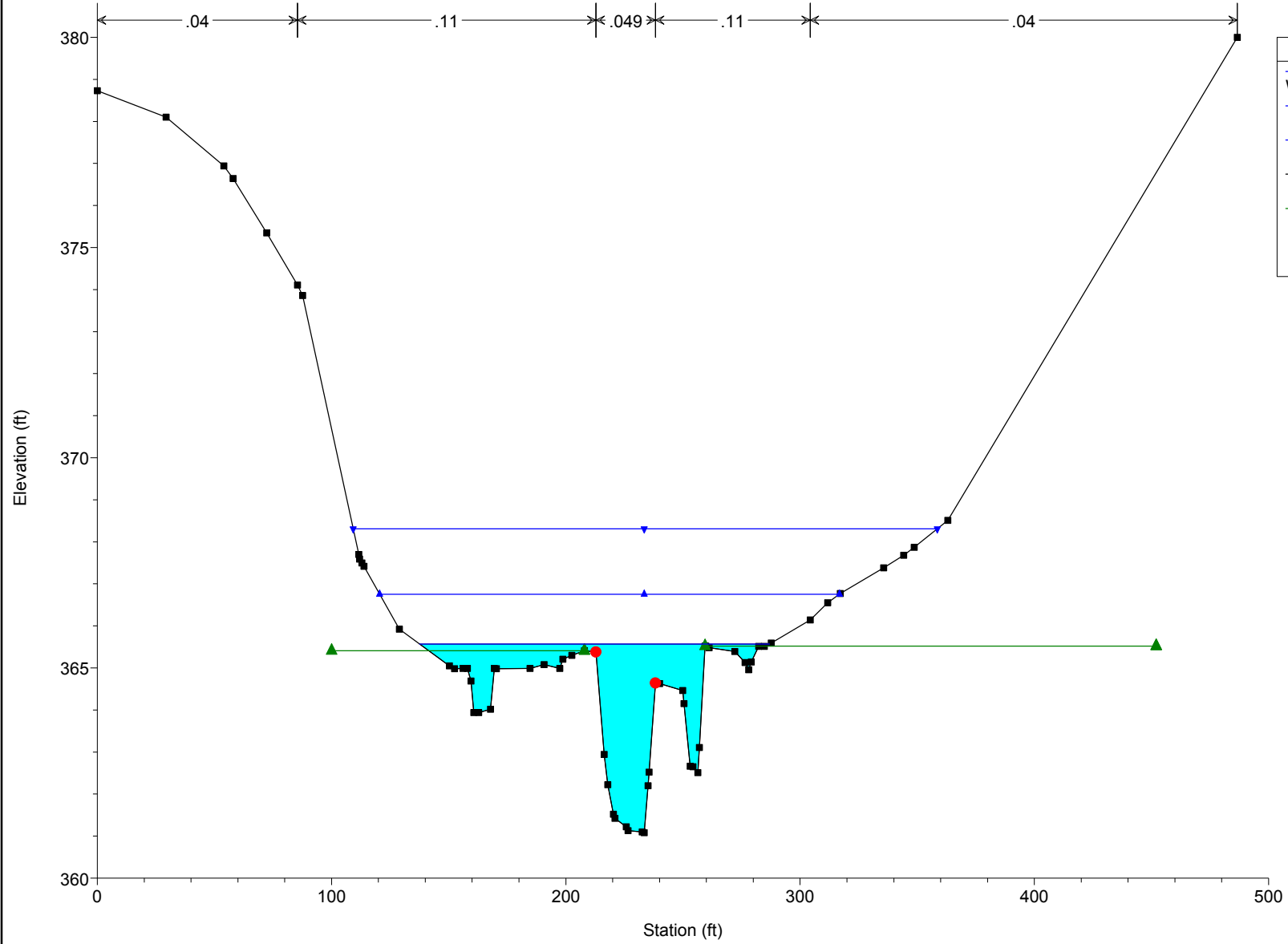
EcclestonMod Plan: existing 11/5/2018
River = JonesFalls Reach = JonesFalls3 RS = 10



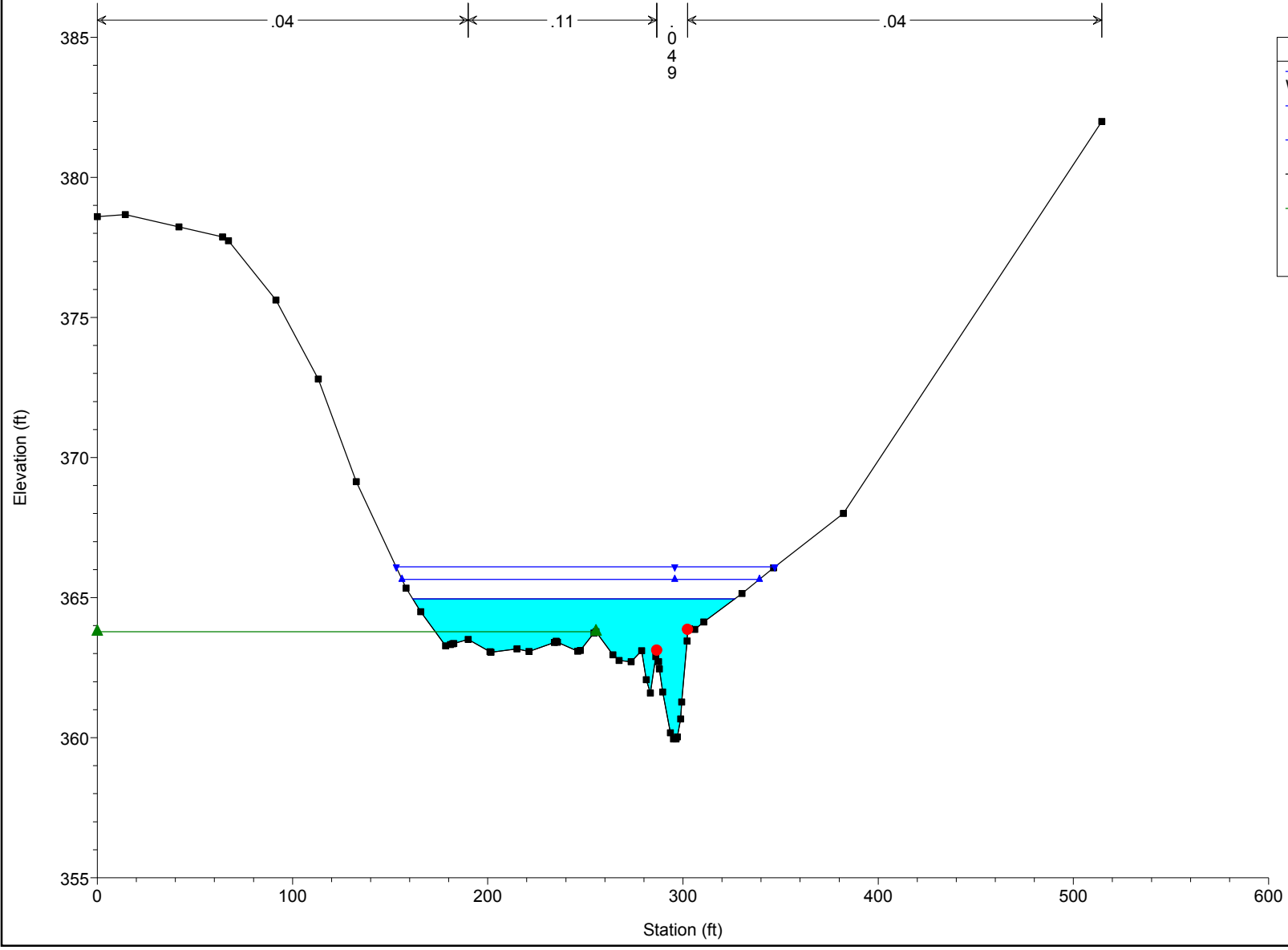
Legend

- WS 100 Yr
- WS 10 Yr
- WS 2 Yr
- Ground
- Ineff
- Bank Sta

EcclestonMod Plan: existing 11/5/2018
River = JonesFalls Reach = JonesFalls3 RS = 9



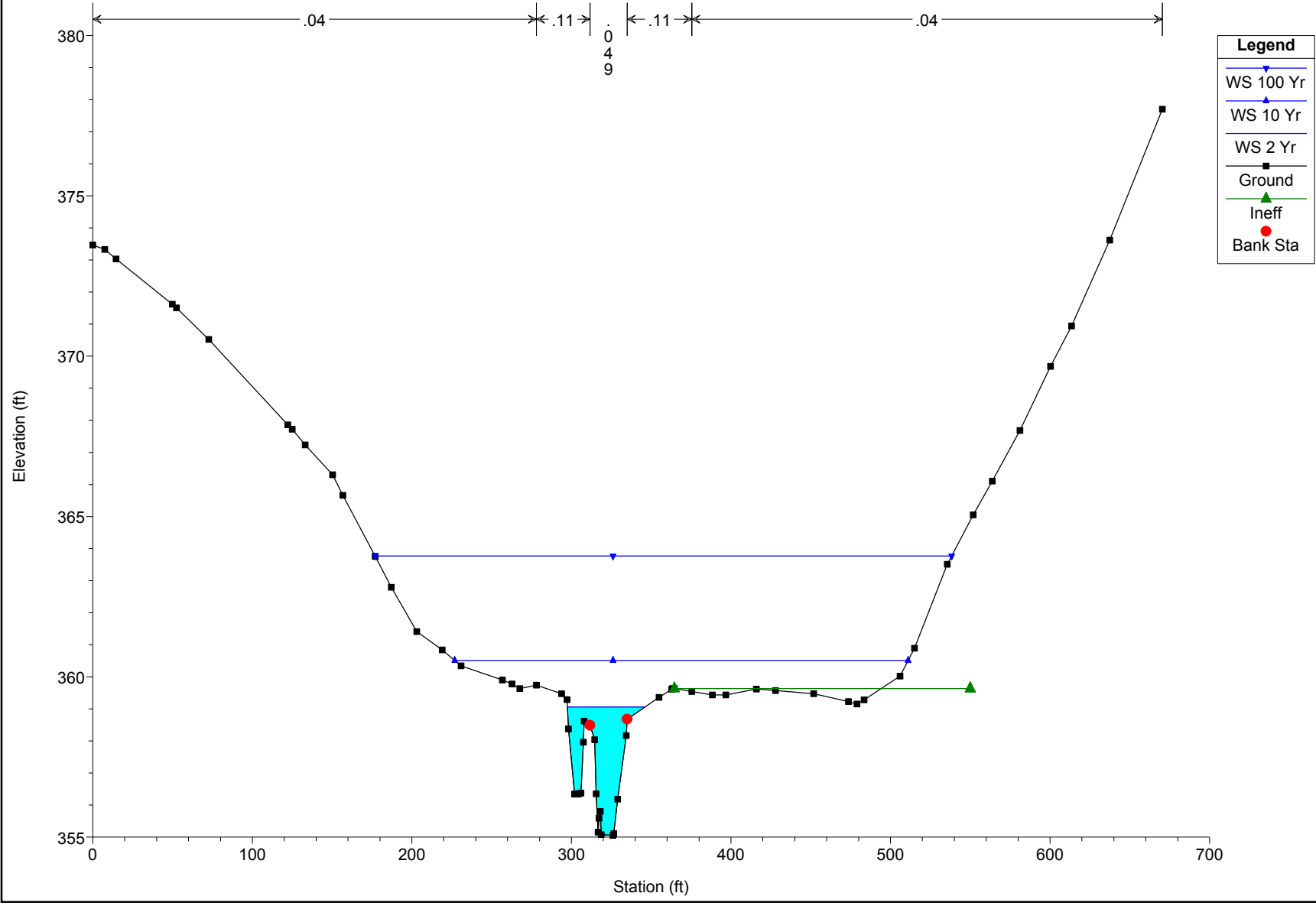
EcclestonMod Plan: existing 11/5/2018
River = JonesFalls Reach = JonesFalls3 RS = 8



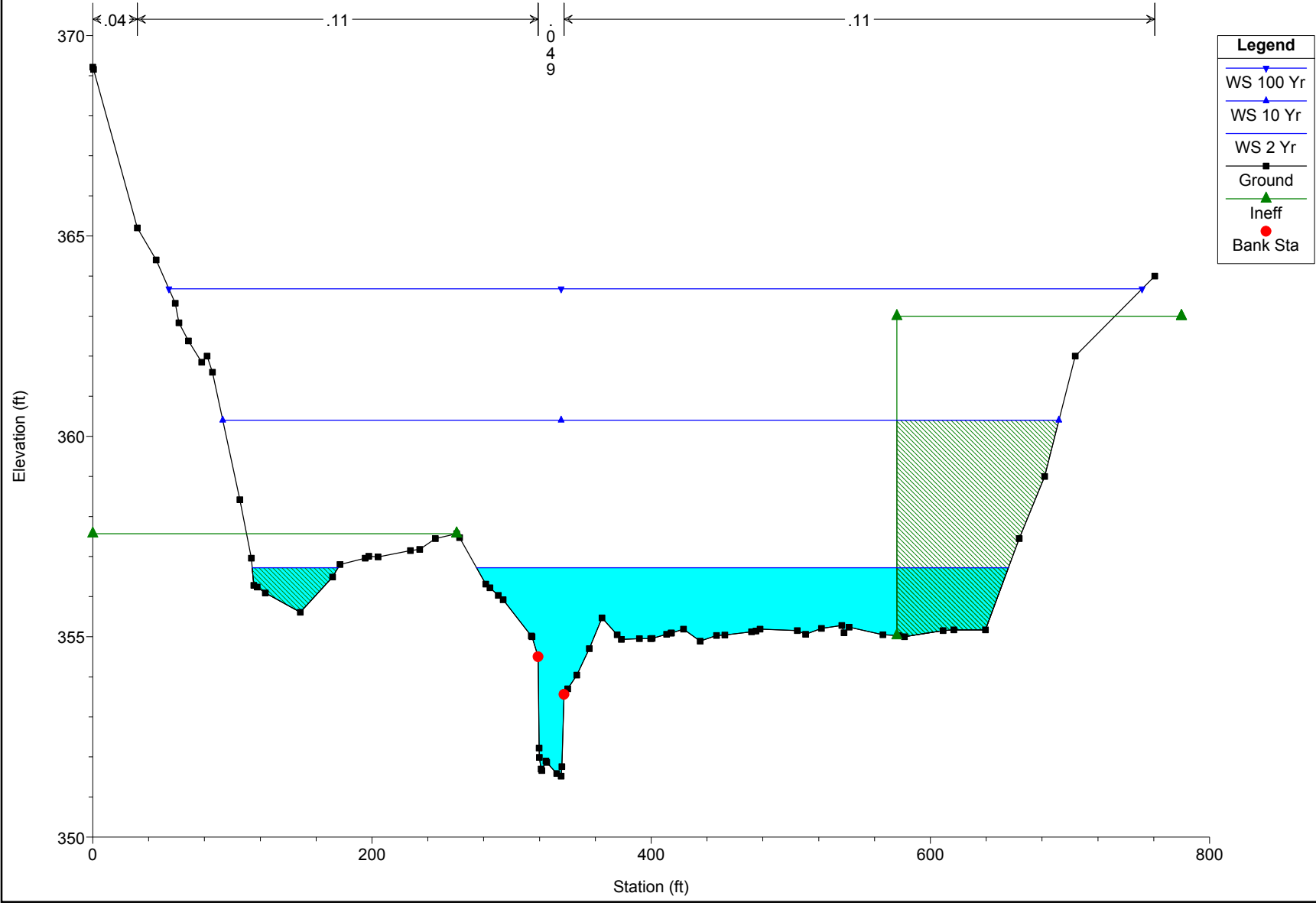
Legend

- WS 100 Yr
- WS 10 Yr
- WS 2 Yr
- Ground
- Ineff
- Bank Sta

EcclestonMod Plan: existing 11/5/2018
 River = JonesFalls Reach = JonesFalls3 RS = 7

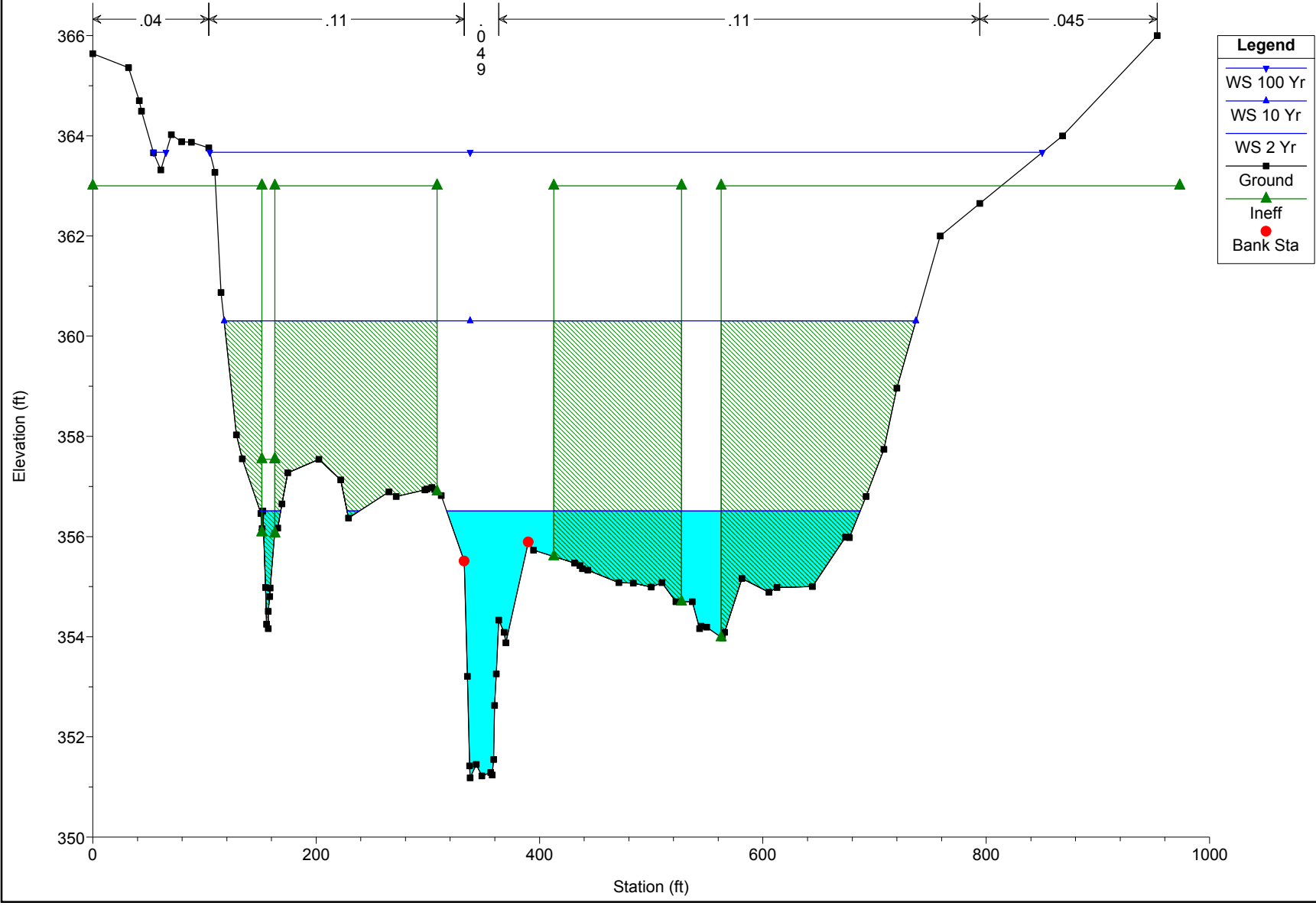


EcclestonMod Plan: existing 11/5/2018
 River = JonesFalls Reach = JonesFalls3 RS = 6



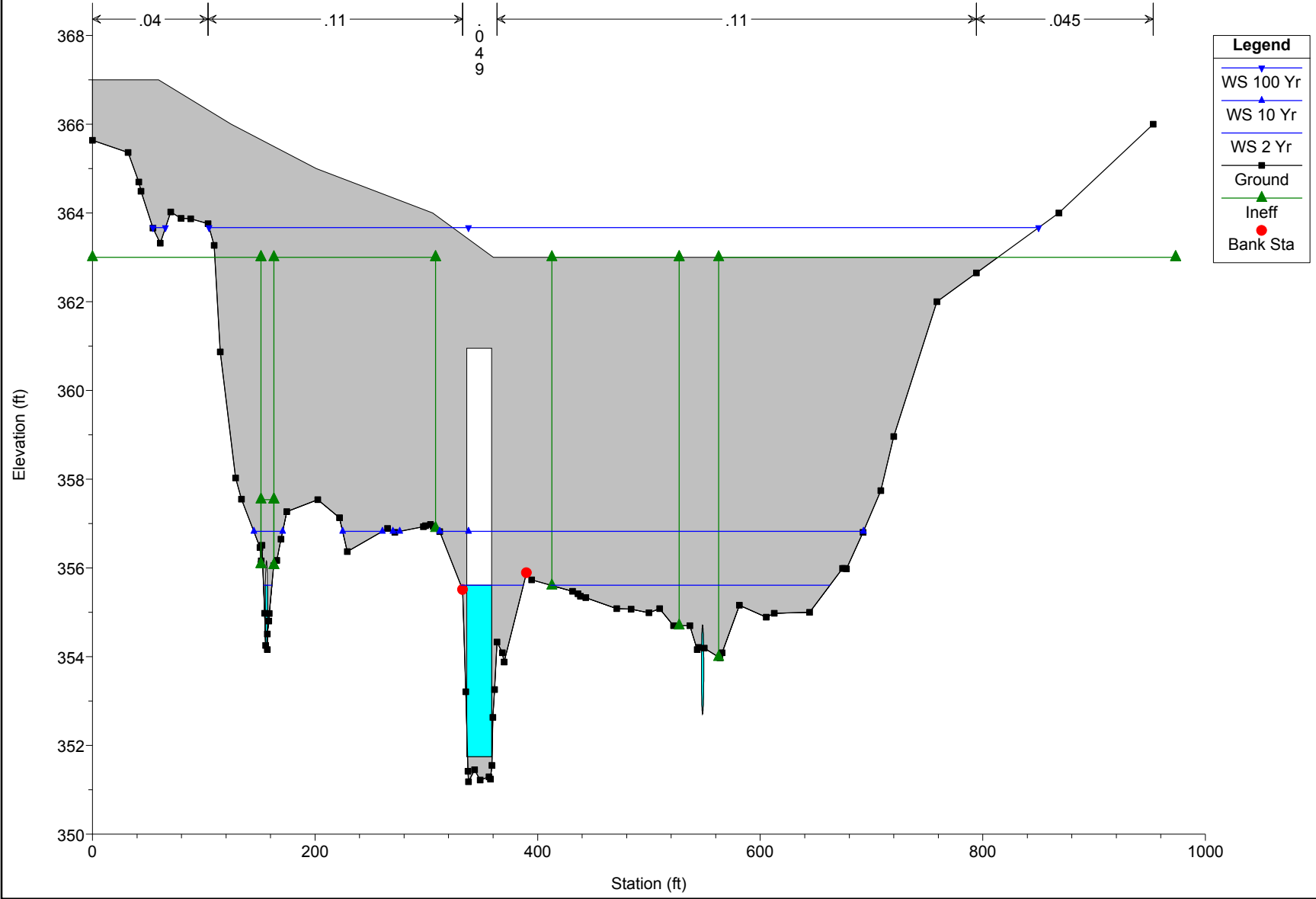
EcclestonMod Plan: existing 11/5/2018

River = JonesFalls Reach = JonesFalls3 RS = 5



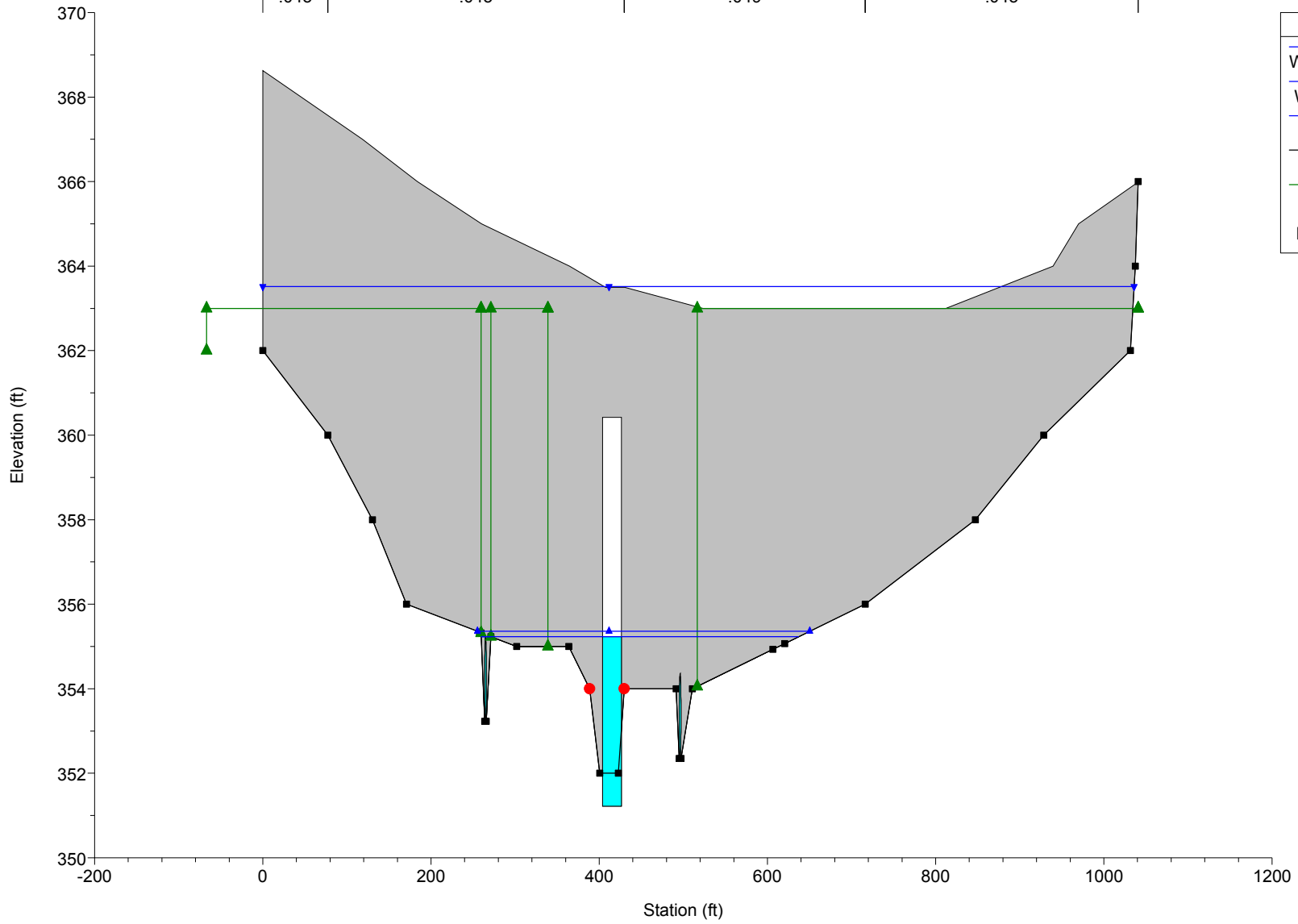
EcclestonMod Plan: existing 11/5/2018

River = JonesFalls Reach = JonesFalls3 RS = 4.5 Culv Bridge over Jones Falls on Park Heights Ave.



EcclestonMod Plan: existing 11/5/2018

River = JonesFalls Reach = JonesFalls3 RS = 4.5 Culv Bridge over Jones Falls on Park Heights Ave.

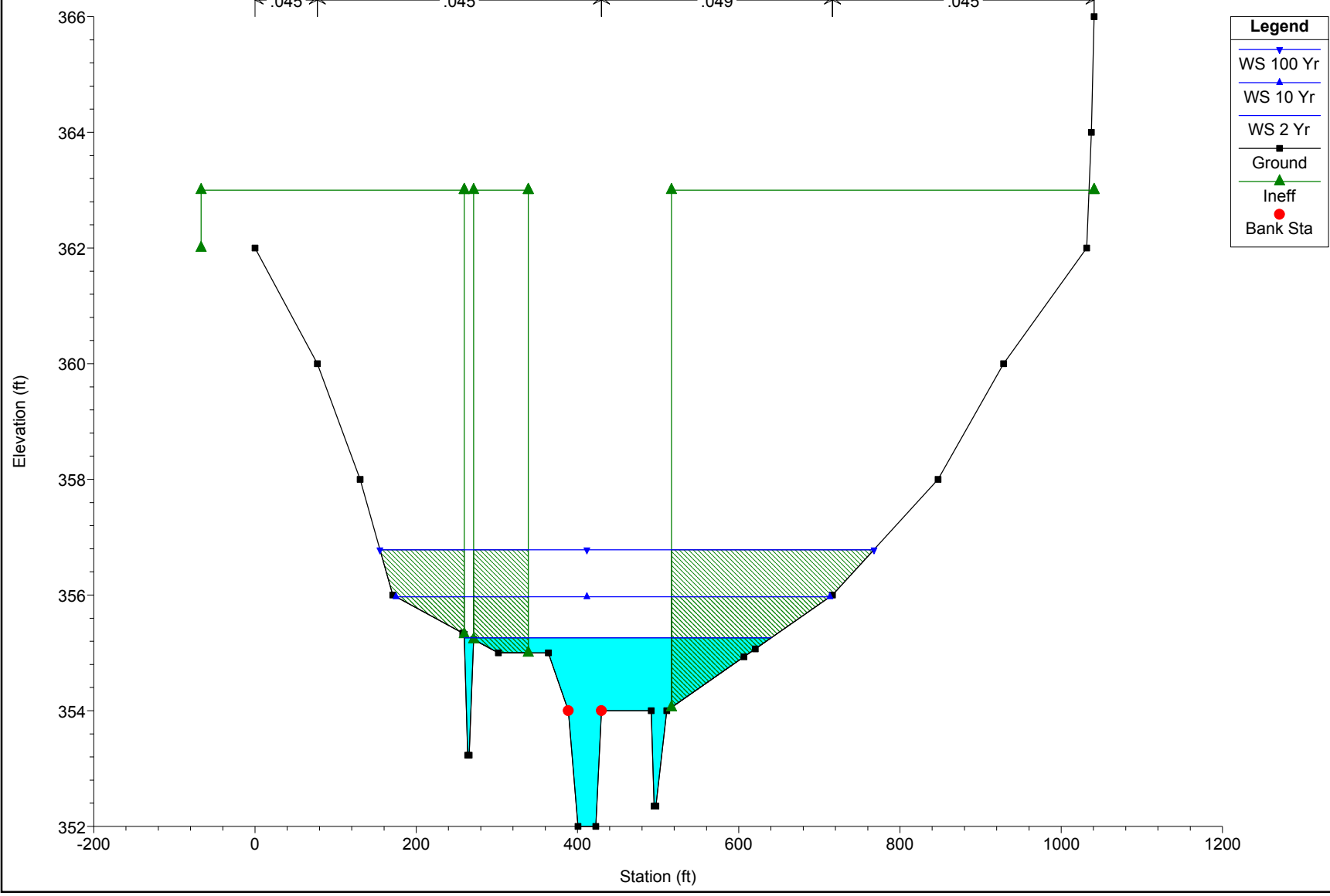


Legend

- WS 100 Yr
- WS 10 Yr
- WS 2 Yr
- Ground
- Ineff
- Bank Sta

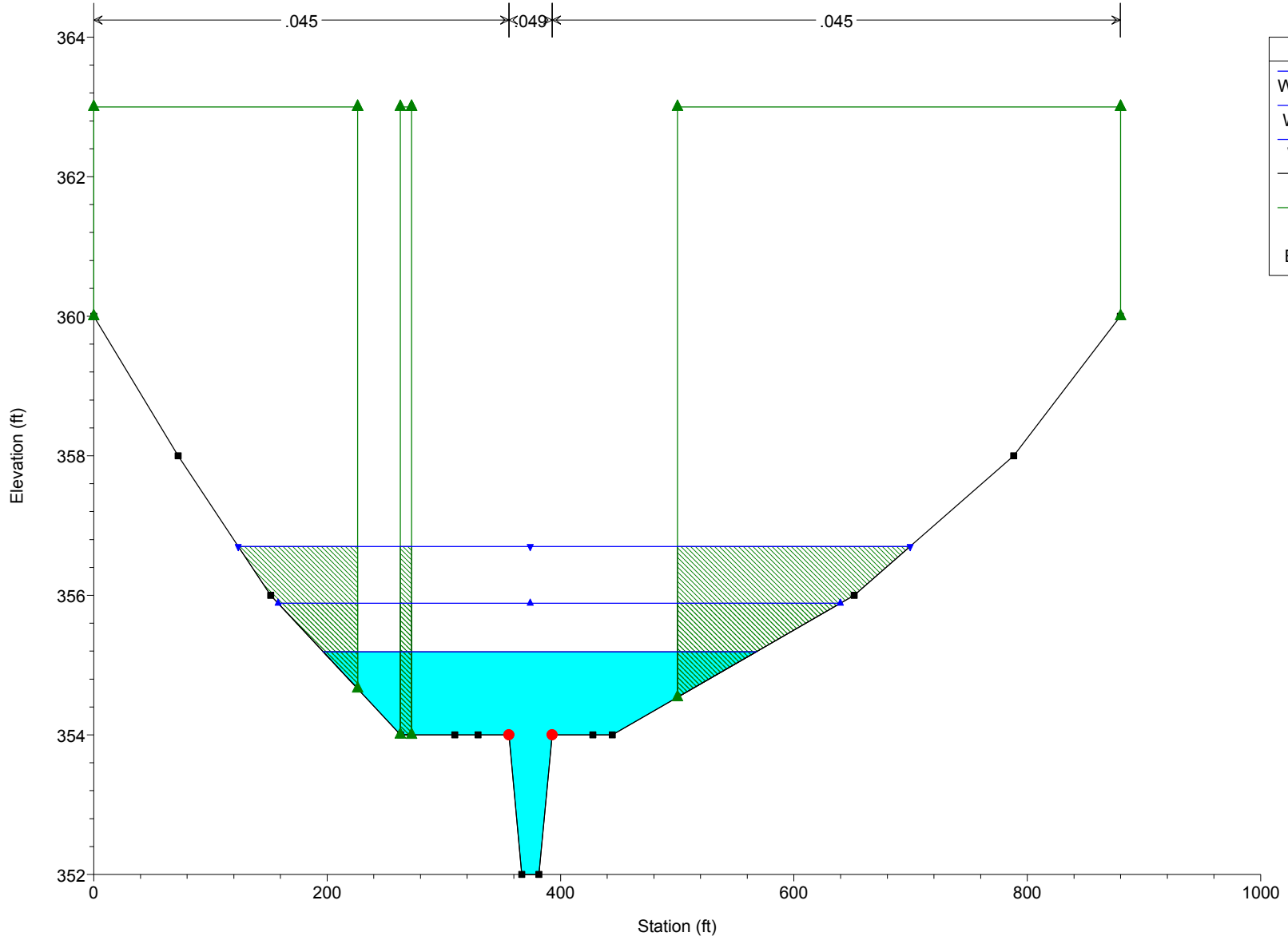
EcclestonMod Plan: existing 11/5/2018
 River = JonesFalls Reach = JonesFalls3 RS = 4

← .045 → .045 ← .049 → .045 →



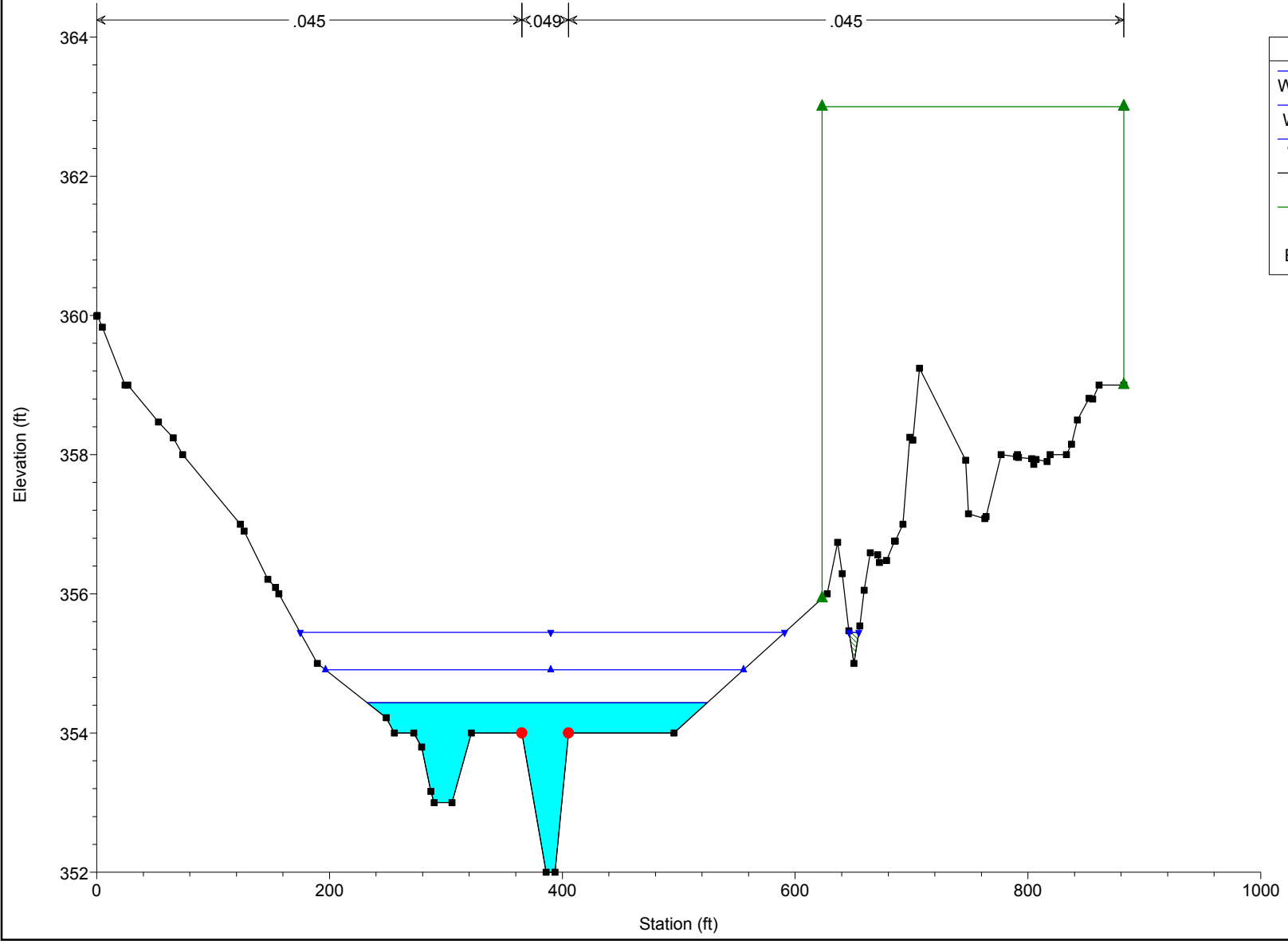
| Legend | |
|-----------|----------------|
| WS 100 Yr | ▲ (inverted) |
| WS 10 Yr | ▲ |
| WS 2 Yr | ■ |
| Ground | — (black line) |
| Ineff | ▲ (green) |
| Bank Sta | ● (red) |

EcclestonMod Plan: existing 11/5/2018
River = JonesFalls Reach = JonesFalls3 RS = 3.5



| Legend | |
|-----------|----------------------------------|
| WS 100 Yr | Blue line with downward triangle |
| WS 10 Yr | Blue line with upward triangle |
| WS 2 Yr | Blue line with downward triangle |
| Ground | Black line with square |
| Ineff | Green line with upward triangle |
| Bank Sta | Red line with circle |

EcclestonMod Plan: existing 11/5/2018
River = JonesFalls Reach = JonesFalls3 RS = 3



Legend

- WS 100 Yr
- WS 10 Yr
- WS 2 Yr
- Ground
- Ineff
- Bank Sta

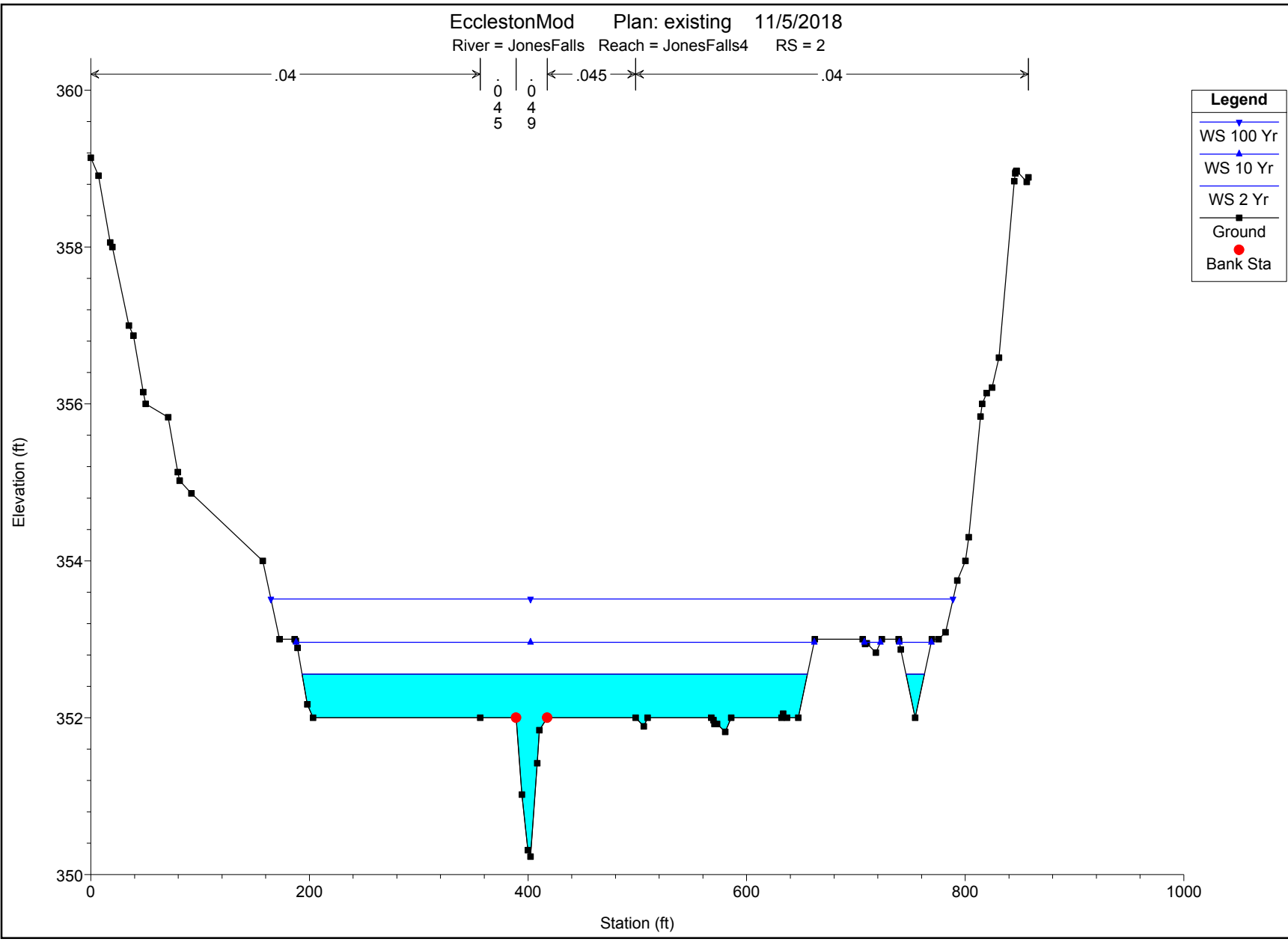
EcclestonMod Plan: existing 11/5/2018

River = JonesFalls Reach = JonesFalls4 RS = 2

0 0
4 4
5 9

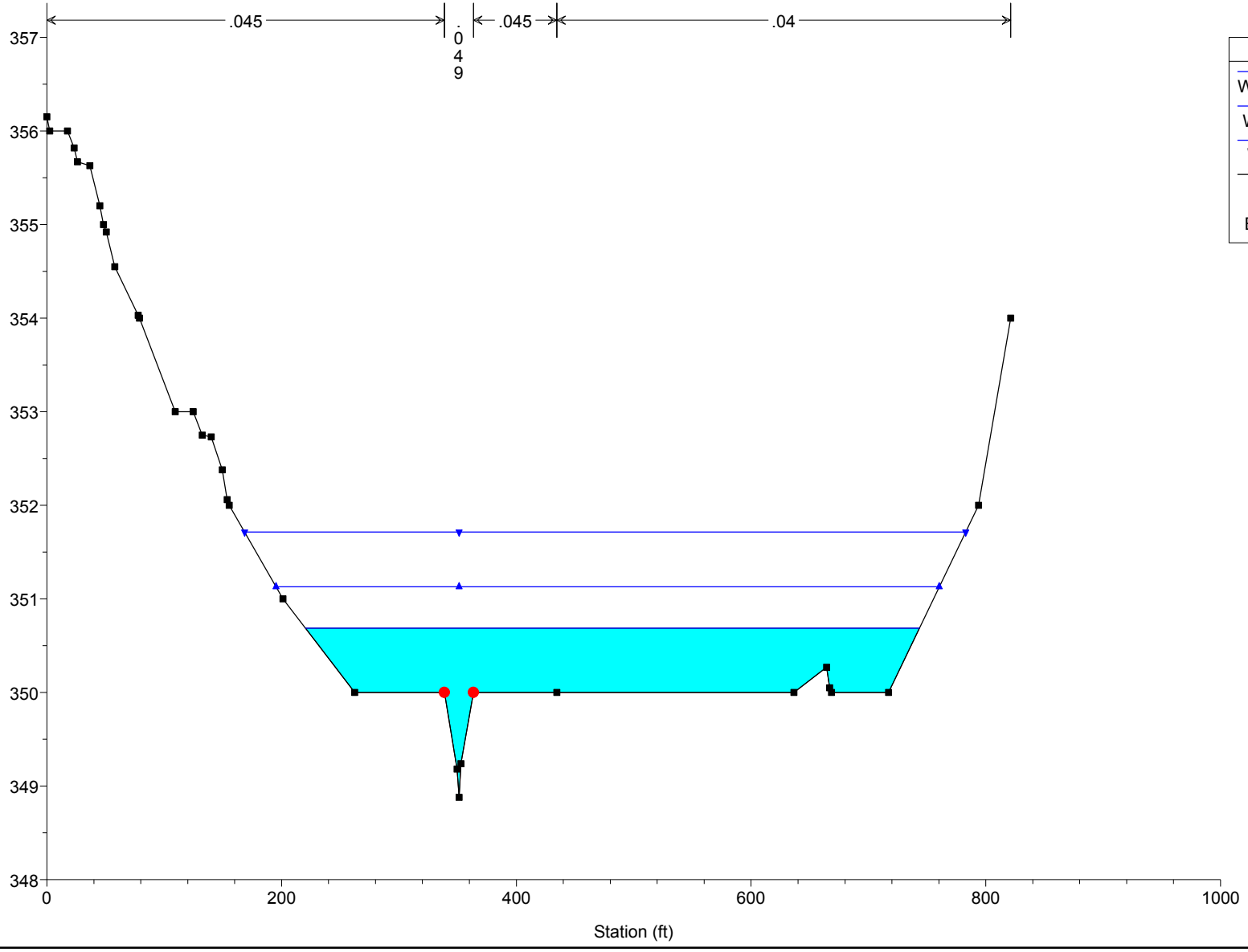
Legend

- WS 100 Yr
- WS 10 Yr
- WS 2 Yr
- Ground
- Bank Sta

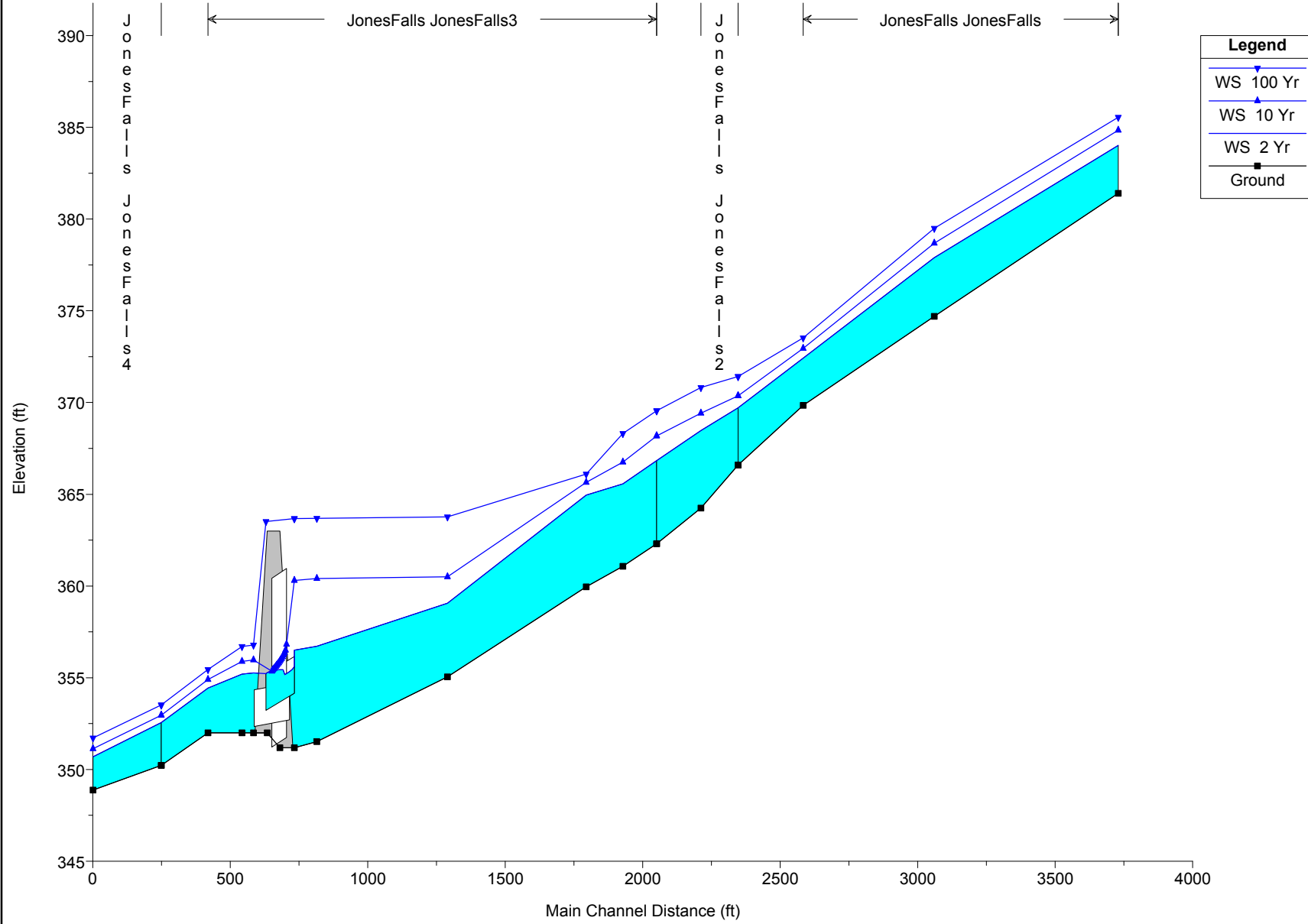


EcclestonMod Plan: existing 11/5/2018

River = JonesFalls Reach = JonesFalls4 RS = 1



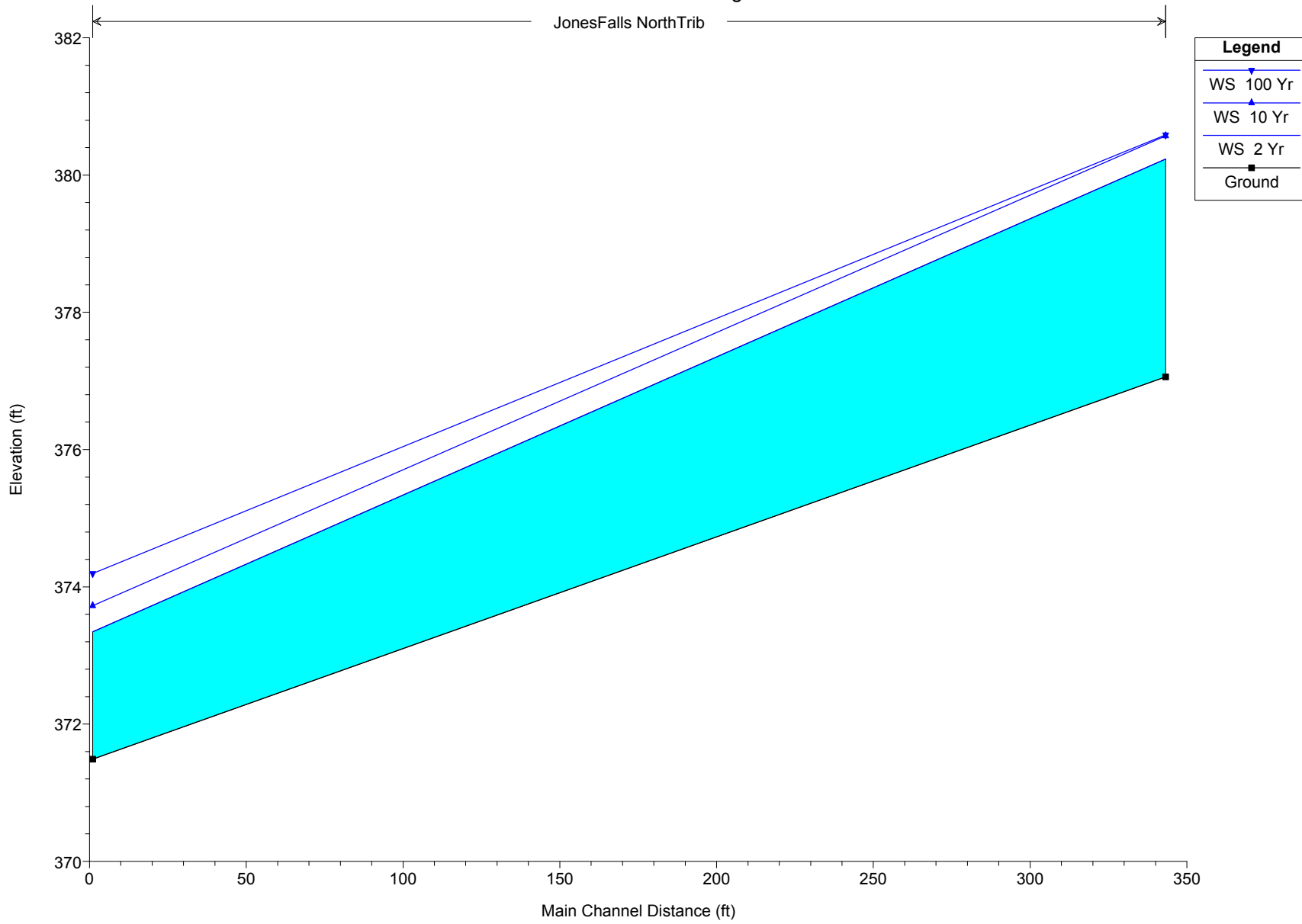
EcclestonMod Plan: existing 11/5/2018



| Legend | |
|-----------|-----------------------------------|
| WS 100 Yr | Blue line with inverted triangles |
| WS 10 Yr | Blue line with triangles |
| WS 2 Yr | Blue line with squares |
| Ground | Cyan shaded area |

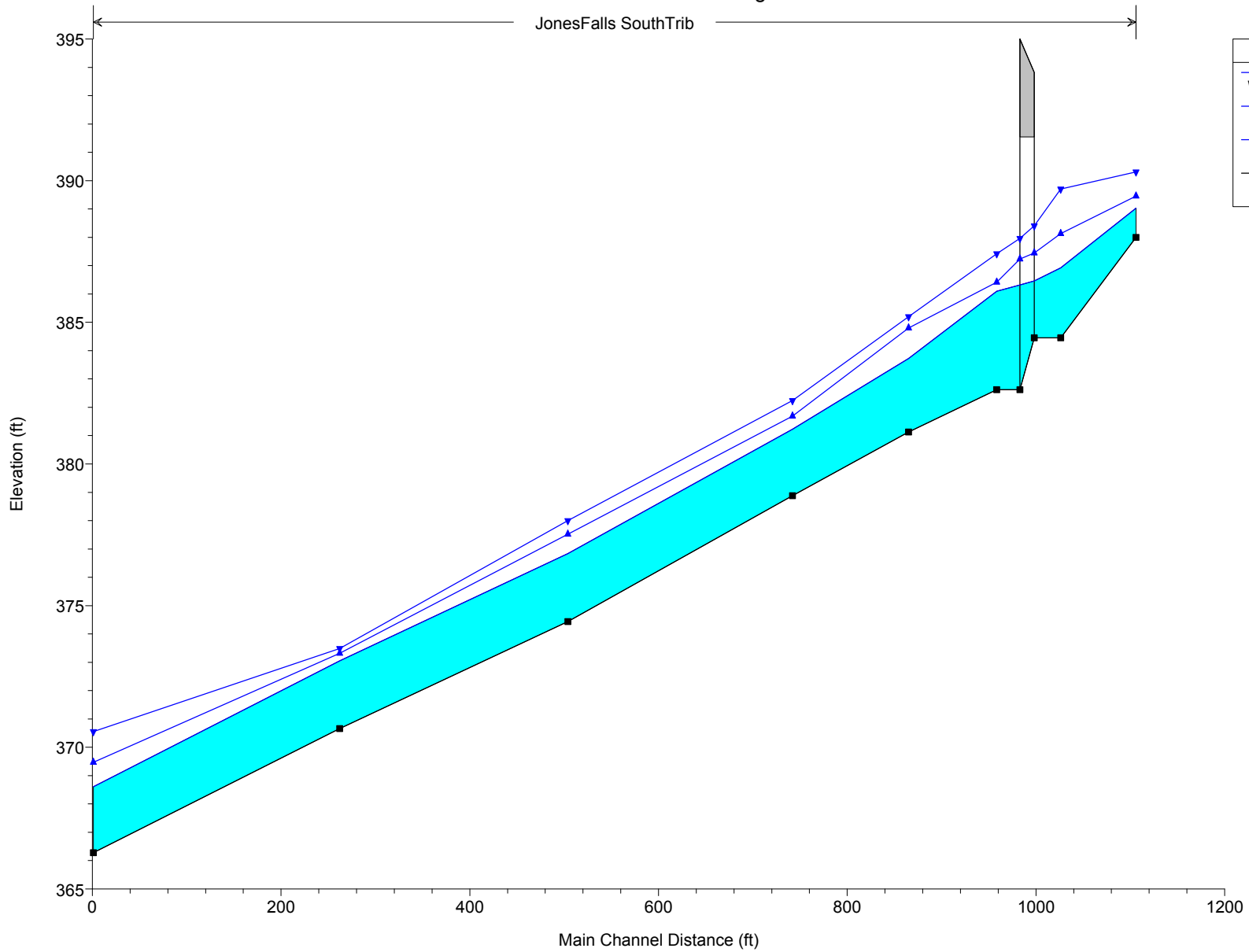
EcclestonMod Plan: existing 11/5/2018

JonesFalls NorthTrib



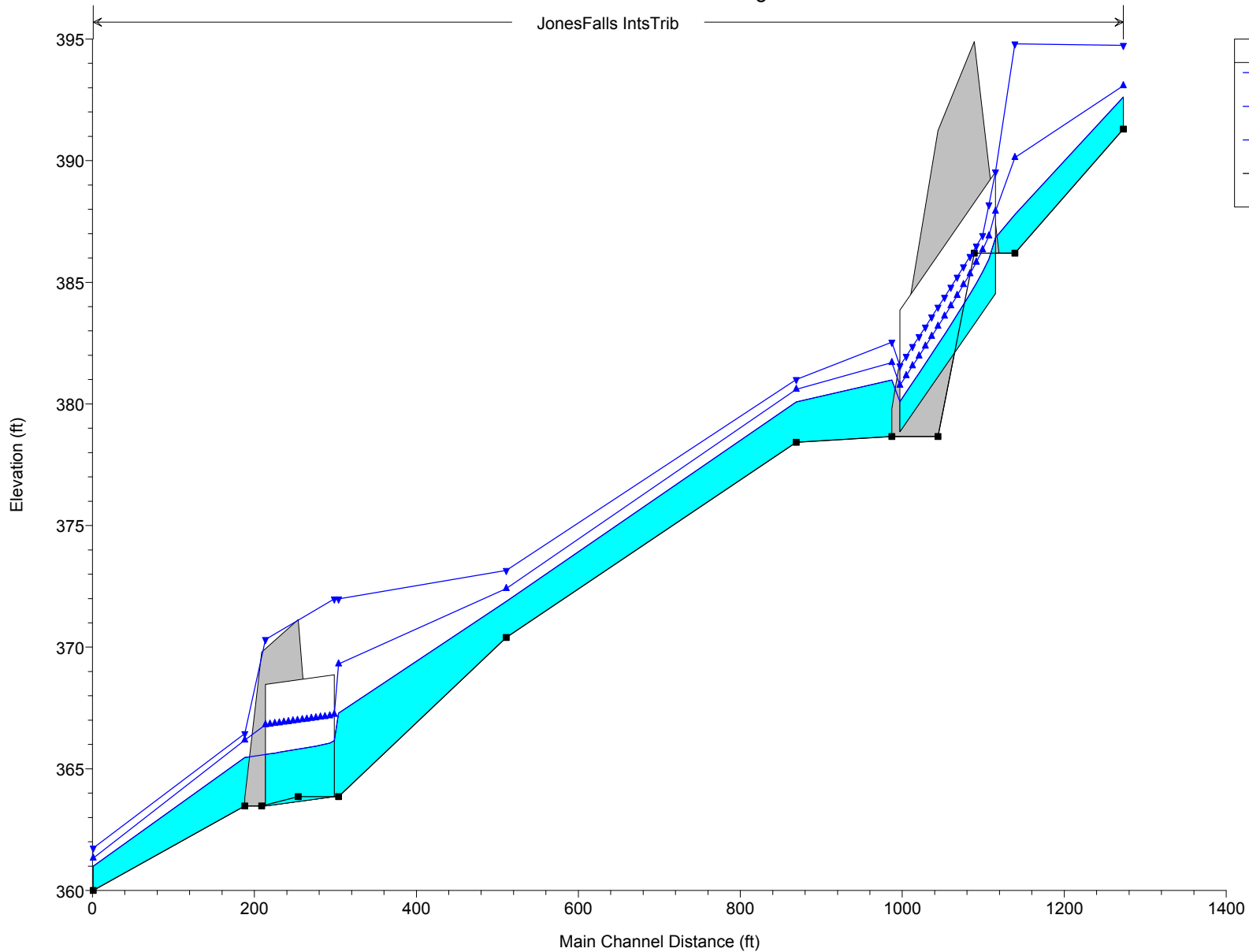
EcclestonMod Plan: existing 11/5/2018

JonesFalls SouthTrib



EcclestonMod Plan: existing 11/5/2018

JonesFalls IntsTrib



| Legend | |
|-----------|-----------------------------------|
| WS 100 Yr | Blue line with inverted triangles |
| WS 10 Yr | Blue line with triangles |
| WS 2 Yr | Blue line with triangles |
| Ground | Black line with squares |

HEC-RAS Plan: existing

| Reach | River Sta | Profile | Q Total (cfs) | W.S. Elev (ft) | Crit W.S. (ft) | E.G. Elev (ft) | E.G. Slope (ft/ft) | Flow Area (sq ft) | Top Width (ft) | Froude # Chl | Vel Total (ft/s) | Vel Chnl (ft/s) | Shear Total (lb/sq ft) | Shear Chan (lb/sq ft) | Shear LOB (lb/sq ft) | Shear ROB (lb/sq ft) |
|-------------|-----------|---------|------------------|-------------------|-------------------|-------------------|-----------------------|----------------------|-------------------|--------------|---------------------|--------------------|---------------------------|--------------------------|-------------------------|-------------------------|
| JonesFalls | 15 | 2 Yr | 363.30 | 384.02 | 383.82 | 384.32 | 0.012619 | 119.71 | 126.26 | 0.66 | 3.03 | 5.62 | 0.74 | 1.67 | 0.57 | 0.67 |
| JonesFalls | 15 | 10 Yr | 798.40 | 384.84 | 384.51 | 385.21 | 0.012592 | 243.79 | 329.25 | 0.69 | 3.27 | 6.89 | 1.09 | 2.27 | 0.93 | 1.08 |
| JonesFalls | 15 | 100 Yr | 1593.40 | 385.55 | 385.28 | 385.89 | 0.013107 | 550.58 | 430.59 | 0.73 | 2.89 | 8.08 | 1.04 | 2.90 | 1.39 | 0.81 |
| JonesFalls | 14 | 2 Yr | 363.30 | 377.89 | 377.63 | 378.08 | 0.007451 | 200.33 | 208.60 | 0.51 | 1.81 | 4.56 | 0.46 | 1.07 | 0.30 | 0.42 |
| JonesFalls | 14 | 10 Yr | 798.40 | 378.68 | 378.14 | 378.90 | 0.007578 | 373.35 | 338.21 | 0.54 | 2.14 | 5.55 | 0.72 | 1.44 | 0.50 | 0.71 |
| JonesFalls | 14 | 100 Yr | 1593.40 | 379.49 | 378.89 | 379.70 | 0.007232 | 722.67 | 411.93 | 0.55 | 2.20 | 6.29 | 0.79 | 1.72 | 0.56 | 0.82 |
| JonesFalls | 13 | 2 Yr | 363.30 | 372.42 | 372.42 | 372.77 | 0.018113 | 105.01 | 141.06 | 0.77 | 3.46 | 5.48 | 0.84 | 1.76 | 0.59 | 0.28 |
| JonesFalls | 13 | 10 Yr | 798.40 | 372.95 | 372.95 | 373.41 | 0.019186 | 187.68 | 174.09 | 0.83 | 4.25 | 6.84 | 1.29 | 2.49 | 1.05 | 0.44 |
| JonesFalls | 13 | 100 Yr | 1593.40 | 373.52 | 373.52 | 374.15 | 0.021060 | 295.93 | 205.56 | 0.90 | 5.38 | 8.40 | 1.88 | 3.47 | 1.69 | 0.67 |
| NorthTrib | 2 | 2 Yr | 175.50 | 380.23 | 379.88 | 380.55 | 0.015832 | 39.92 | 164.78 | 0.57 | 4.40 | 4.69 | 1.28 | 1.87 | | 0.56 |
| NorthTrib | 2 | 10 Yr | 459.70 | 380.57 | 380.57 | 380.63 | 0.002721 | 231.31 | 206.33 | 0.24 | 1.99 | 2.14 | 0.19 | 0.37 | 0.17 | 0.14 |
| NorthTrib | 2 | 100 Yr | 1025.90 | 380.59 | 380.58 | 380.88 | 0.012940 | 234.70 | 206.66 | 0.53 | 4.37 | 4.68 | 0.91 | 1.77 | 0.84 | 0.68 |
| NorthTrib | 1 | 2 Yr | 175.50 | 373.35 | 373.35 | 373.56 | 0.026426 | 51.70 | 114.70 | 0.69 | 3.39 | 4.21 | 0.73 | 1.81 | | 0.46 |
| NorthTrib | 1 | 10 Yr | 459.70 | 373.73 | 373.73 | 374.05 | 0.029422 | 103.17 | 157.67 | 0.76 | 4.46 | 5.22 | 1.19 | 2.57 | | 0.94 |
| NorthTrib | 1 | 100 Yr | 1025.90 | 374.19 | 374.19 | 374.66 | 0.026708 | 188.86 | 200.74 | 0.75 | 5.43 | 5.84 | 1.55 | 2.96 | 0.21 | 1.36 |
| JonesFalls2 | 12 | 2 Yr | 538.80 | 369.72 | 369.47 | 369.84 | 0.006215 | 253.00 | 311.32 | 0.46 | 2.13 | 3.89 | 0.31 | 0.81 | 0.28 | 0.16 |
| JonesFalls2 | 12 | 10 Yr | 1258.10 | 370.36 | | 370.52 | 0.006097 | 466.75 | 345.10 | 0.48 | 2.70 | 4.58 | 0.51 | 1.02 | 0.50 | 0.29 |
| JonesFalls2 | 12 | 100 Yr | 2619.30 | 371.42 | | 371.60 | 0.004519 | 869.13 | 419.90 | 0.44 | 3.01 | 4.87 | 0.58 | 1.04 | 0.61 | 0.36 |
| JonesFalls2 | 11 | 2 Yr | 538.80 | 368.48 | 368.48 | 368.85 | 0.011021 | 181.66 | 225.66 | 0.62 | 2.97 | 5.82 | 0.54 | 1.70 | 0.38 | 0.47 |
| JonesFalls2 | 11 | 10 Yr | 1258.10 | 369.41 | | 369.72 | 0.008405 | 415.44 | 276.27 | 0.57 | 3.03 | 6.19 | 0.78 | 1.74 | 0.72 | 0.53 |
| JonesFalls2 | 11 | 100 Yr | 2619.30 | 370.81 | | 371.06 | 0.005334 | 851.72 | 349.75 | 0.48 | 3.08 | 6.12 | 0.80 | 1.53 | 0.82 | 0.57 |
| SouthTrib | 8 | 2 Yr | 151.70 | 389.03 | 389.03 | 389.33 | 0.056139 | 34.46 | 57.17 | 1.00 | 4.40 | 4.40 | 2.11 | 2.11 | | |
| SouthTrib | 8 | 10 Yr | 322.20 | 389.46 | 389.46 | 389.86 | 0.050145 | 63.03 | 76.80 | 0.99 | 5.11 | 5.11 | 2.57 | 2.57 | | |
| SouthTrib | 8 | 100 Yr | 622.10 | 390.30 | 389.94 | 390.59 | 0.017815 | 147.45 | 139.18 | 0.65 | 4.22 | 4.34 | 1.18 | 1.55 | 0.17 | 0.16 |
| SouthTrib | 7 | 2 Yr | 151.70 | 386.87 | 385.94 | 387.02 | 0.006980 | 48.43 | 31.79 | 0.42 | 3.13 | 3.13 | 0.75 | 0.75 | | |
| SouthTrib | 7 | 10 Yr | 322.20 | 388.06 | 386.70 | 388.28 | 0.005926 | 86.65 | 42.03 | 0.41 | 3.72 | 3.73 | 0.91 | 0.94 | | 0.11 |
| SouthTrib | 7 | 100 Yr | 622.10 | 389.68 | 387.69 | 389.98 | 0.004211 | 143.36 | 51.53 | 0.38 | 4.34 | 4.36 | 1.06 | 1.09 | | 0.50 |
| SouthTrib | 6.5 | | Bridge | | | | | | | | | | | | | |
| SouthTrib | 6 | 2 Yr | 151.70 | 385.93 | 384.86 | 386.15 | 0.008208 | 40.40 | 18.17 | 0.44 | 3.75 | 3.75 | 1.03 | 1.03 | | |
| SouthTrib | 6 | 10 Yr | 322.20 | 386.29 | 385.83 | 387.02 | 0.023740 | 47.15 | 19.08 | 0.76 | 6.83 | 6.83 | 3.28 | 3.29 | | |
| SouthTrib | 6 | 100 Yr | 622.10 | 387.35 | 387.35 | 388.31 | 0.021738 | 84.36 | 87.49 | 0.77 | 7.37 | 8.23 | 2.57 | 4.25 | 1.03 | 0.64 |
| SouthTrib | 5 | 2 Yr | 151.70 | 383.73 | 383.66 | 384.49 | 0.044154 | 21.65 | 17.57 | 0.95 | 7.01 | 7.01 | 3.99 | 3.99 | | |
| SouthTrib | 5 | 10 Yr | 322.20 | 384.80 | 384.80 | 385.12 | 0.014240 | 84.71 | 107.82 | 0.58 | 3.80 | 5.45 | 0.68 | 2.06 | 0.46 | 0.48 |
| SouthTrib | 5 | 100 Yr | 622.10 | 385.19 | 385.16 | 385.62 | 0.017061 | 129.68 | 118.42 | 0.66 | 4.80 | 6.54 | 1.14 | 2.83 | 0.90 | 0.83 |
| SouthTrib | 4 | 2 Yr | 151.70 | 381.23 | 380.62 | 381.48 | 0.014222 | 37.81 | 33.61 | 0.58 | 4.01 | 4.01 | 1.30 | 1.30 | | |
| SouthTrib | 4 | 10 Yr | 322.20 | 381.69 | 381.61 | 382.18 | 0.021461 | 60.50 | 52.11 | 0.74 | 5.33 | 5.85 | 1.52 | 2.54 | 0.54 | 0.55 |
| SouthTrib | 4 | 100 Yr | 622.10 | 382.24 | 382.23 | 383.00 | 0.025387 | 92.88 | 64.27 | 0.84 | 6.70 | 7.51 | 2.24 | 3.86 | 0.96 | 1.38 |
| SouthTrib | 3 | 2 Yr | 151.70 | 376.84 | 376.84 | 377.27 | 0.022367 | 32.02 | 41.58 | 0.72 | 4.74 | 5.57 | 1.04 | 2.38 | 0.24 | 0.42 |
| SouthTrib | 3 | 10 Yr | 322.20 | 377.52 | 377.52 | 377.87 | 0.015393 | 76.27 | 97.87 | 0.63 | 4.22 | 5.68 | 0.73 | 2.24 | 0.49 | 0.49 |
| SouthTrib | 3 | 100 Yr | 622.10 | 378.00 | 377.92 | 378.41 | 0.014773 | 129.92 | 118.54 | 0.63 | 4.79 | 6.26 | 0.99 | 2.56 | 0.70 | 0.82 |

HEC-RAS Plan: existing (Continued)

| Reach | River Sta | Profile | Q Total (cfs) | W.S. Elev (ft) | Crit W.S. (ft) | E.G. Elev (ft) | E.G. Slope (ft/ft) | Flow Area (sq ft) | Top Width (ft) | Froude # Chl | Vel Total (ft/s) | Vel Chnl (ft/s) | Shear Total (lb/sq ft) | Shear Chan (lb/sq ft) | Shear LOB (lb/sq ft) | Shear ROB (lb/sq ft) |
|-------------|-----------|---------|------------------|-------------------|-------------------|-------------------|-----------------------|----------------------|-------------------|--------------|---------------------|--------------------|---------------------------|--------------------------|-------------------------|-------------------------|
| SouthTrib | 2 | 2 Yr | 151.70 | 373.05 | | 373.13 | 0.007095 | 72.19 | 112.33 | 0.40 | 2.10 | 2.85 | 0.28 | 0.66 | 0.24 | 0.03 |
| SouthTrib | 2 | 10 Yr | 322.20 | 373.32 | | 373.49 | 0.011655 | 106.10 | 141.52 | 0.53 | 3.04 | 4.06 | 0.54 | 1.26 | 0.52 | 0.16 |
| SouthTrib | 2 | 100 Yr | 622.10 | 373.49 | 373.49 | 373.88 | 0.024403 | 132.22 | 167.00 | 0.78 | 4.70 | 6.24 | 1.20 | 2.89 | 1.22 | 0.41 |
| SouthTrib | 1 | 2 Yr | 151.70 | 368.61 | 368.61 | 369.26 | 0.046497 | 23.56 | 20.08 | 1.00 | 6.44 | 6.45 | 3.27 | 3.56 | 0.05 | |
| SouthTrib | 1 | 10 Yr | 322.20 | 369.47 | 369.47 | 369.77 | 0.017778 | 84.64 | 132.78 | 0.66 | 3.81 | 5.07 | 0.70 | 1.95 | 0.51 | 0.30 |
| SouthTrib | 1 | 100 Yr | 622.10 | 370.55 | | 370.64 | 0.002841 | 274.98 | 236.14 | 0.29 | 2.26 | 2.76 | 0.21 | 0.50 | 0.17 | 0.18 |
| IntsTrib | 8 | 2 Yr | 66.30 | 392.61 | 392.61 | 392.96 | 0.035629 | 14.12 | 20.71 | 1.00 | 4.70 | 4.70 | 1.50 | 1.50 | | |
| IntsTrib | 8 | 10 Yr | 138.90 | 393.08 | 393.08 | 393.55 | 0.032574 | 25.30 | 27.44 | 1.01 | 5.49 | 5.49 | 1.86 | 1.86 | | |
| IntsTrib | 8 | 100 Yr | 261.20 | 394.74 | | 394.86 | 0.002877 | 101.13 | 78.90 | 0.34 | 2.58 | 2.85 | 0.23 | 0.38 | 0.07 | 0.07 |
| IntsTrib | 7 | 2 Yr | 66.30 | 387.79 | 387.79 | 388.31 | 0.030520 | 11.70 | 12.60 | 0.93 | 5.67 | 5.85 | 1.58 | 2.01 | | 0.27 |
| IntsTrib | 7 | 10 Yr | 138.90 | 390.12 | 388.53 | 390.17 | 0.001015 | 87.17 | 59.09 | 0.20 | 1.59 | 2.16 | 0.09 | 0.19 | 0.04 | 0.08 |
| IntsTrib | 7 | 100 Yr | 261.20 | 394.81 | 389.18 | 394.81 | 0.000035 | 465.97 | 269.77 | 0.04 | 0.56 | 0.71 | 0.01 | 0.02 | 0.01 | 0.01 |
| IntsTrib | 6.5 | | Culvert | | | | | | | | | | | | | |
| IntsTrib | 6 | 2 Yr | 66.30 | 380.98 | 380.06 | 381.08 | 0.003314 | 26.97 | 18.43 | 0.35 | 2.46 | 2.48 | 0.30 | 0.32 | 0.08 | 0.02 |
| IntsTrib | 6 | 10 Yr | 138.90 | 381.69 | 380.68 | 381.88 | 0.004116 | 40.14 | 21.50 | 0.41 | 3.46 | 3.53 | 0.51 | 0.57 | 0.26 | 0.11 |
| IntsTrib | 6 | 100 Yr | 261.20 | 382.54 | 381.37 | 382.88 | 0.004894 | 56.99 | 25.14 | 0.47 | 4.58 | 4.74 | 0.80 | 0.93 | 0.55 | 0.24 |
| IntsTrib | 5 | 2 Yr | 66.30 | 380.08 | 379.85 | 380.30 | 0.015759 | 17.59 | 19.28 | 0.70 | 3.77 | 3.77 | 0.88 | 0.88 | | |
| IntsTrib | 5 | 10 Yr | 138.90 | 380.60 | 380.36 | 380.96 | 0.016866 | 28.88 | 25.38 | 0.76 | 4.81 | 4.85 | 1.18 | 1.31 | 0.11 | |
| IntsTrib | 5 | 100 Yr | 261.20 | 381.01 | 381.01 | 381.69 | 0.023771 | 40.67 | 54.47 | 0.94 | 6.42 | 6.69 | 1.80 | 2.31 | 0.43 | |
| IntsTrib | 4 | 2 Yr | 66.30 | 371.88 | 371.88 | 372.27 | 0.034227 | 13.27 | 17.10 | 1.00 | 5.00 | 5.00 | 1.63 | 1.63 | | |
| IntsTrib | 4 | 10 Yr | 138.90 | 372.41 | 372.41 | 372.94 | 0.031022 | 23.67 | 22.23 | 1.00 | 5.87 | 5.87 | 2.03 | 2.03 | | |
| IntsTrib | 4 | 100 Yr | 261.20 | 373.15 | 373.15 | 373.70 | 0.019080 | 46.67 | 47.64 | 0.84 | 5.60 | 6.01 | 1.16 | 1.86 | 0.26 | |
| IntsTrib | 3 | 2 Yr | 66.30 | 367.28 | 365.59 | 367.47 | 0.006169 | 19.11 | 6.16 | 0.35 | 3.47 | 3.47 | 0.62 | 0.62 | | |
| IntsTrib | 3 | 10 Yr | 138.90 | 369.31 | 366.65 | 369.49 | 0.003947 | 44.60 | 91.80 | 0.28 | 3.11 | 3.60 | 0.38 | 0.58 | 0.18 | 0.27 |
| IntsTrib | 3 | 100 Yr | 261.20 | 371.98 | 368.80 | 371.99 | 0.000077 | 503.10 | 269.29 | 0.04 | 0.52 | 0.67 | 0.01 | 0.02 | 0.01 | 0.01 |
| IntsTrib | 2.5 | | Culvert | | | | | | | | | | | | | |
| IntsTrib | 2 | 2 Yr | 66.30 | 365.47 | 365.18 | 365.83 | 0.016488 | 14.88 | 17.64 | 0.68 | 4.46 | 5.00 | 0.78 | 1.36 | | 0.24 |
| IntsTrib | 2 | 10 Yr | 138.90 | 366.18 | 366.18 | 366.43 | 0.010415 | 45.61 | 96.30 | 0.57 | 3.05 | 4.82 | 0.39 | 1.15 | 0.06 | 0.27 |
| IntsTrib | 2 | 100 Yr | 261.20 | 366.45 | 366.45 | 366.80 | 0.014253 | 65.61 | 100.67 | 0.67 | 3.98 | 6.08 | 0.75 | 1.76 | 0.19 | 0.61 |
| IntsTrib | 1 | 2 Yr | 66.30 | 360.99 | 360.99 | 361.24 | 0.039364 | 16.55 | 33.41 | 1.00 | 4.01 | 4.01 | 1.21 | 1.21 | | |
| IntsTrib | 1 | 10 Yr | 138.90 | 361.33 | 361.33 | 361.69 | 0.031925 | 28.91 | 40.43 | 0.97 | 4.80 | 4.88 | 1.42 | 1.55 | | 0.32 |
| IntsTrib | 1 | 100 Yr | 261.20 | 361.74 | 361.74 | 362.23 | 0.027244 | 47.48 | 49.00 | 0.95 | 5.50 | 5.72 | 1.64 | 1.89 | | 0.63 |
| JonesFalls3 | 10 | 2 Yr | 655.40 | 366.83 | 365.98 | 367.21 | 0.007744 | 191.94 | 176.92 | 0.54 | 3.41 | 5.24 | 0.59 | 1.33 | 0.36 | 0.21 |
| JonesFalls3 | 10 | 10 Yr | 1520.50 | 368.18 | 367.50 | 368.56 | 0.006274 | 523.99 | 263.19 | 0.52 | 2.90 | 6.07 | 0.77 | 1.57 | 0.74 | 0.50 |
| JonesFalls3 | 10 | 100 Yr | 3144.30 | 369.55 | 368.59 | 370.06 | 0.006843 | 904.91 | 293.43 | 0.57 | 3.47 | 7.63 | 1.30 | 2.27 | 1.33 | 0.98 |
| JonesFalls3 | 9 | 2 Yr | 655.40 | 365.57 | 364.46 | 366.14 | 0.009531 | 169.80 | 149.30 | 0.61 | 3.86 | 6.46 | 0.66 | 1.92 | 0.34 | 0.45 |
| JonesFalls3 | 9 | 10 Yr | 1520.50 | 366.76 | 366.61 | 367.53 | 0.011233 | 378.56 | 196.27 | 0.69 | 4.02 | 8.52 | 1.32 | 3.03 | 1.09 | 1.00 |
| JonesFalls3 | 9 | 100 Yr | 3144.30 | 368.31 | 367.88 | 369.06 | 0.009655 | 728.93 | 249.33 | 0.67 | 4.31 | 9.56 | 1.73 | 3.46 | 1.73 | 1.34 |

HEC-RAS Plan: existing (Continued)

| Reach | River Sta | Profile | Q Total (cfs) | W.S. Elev (ft) | Crit W.S. (ft) | E.G. Elev (ft) | E.G. Slope (ft/ft) | Flow Area (sq ft) | Top Width (ft) | Froude # Chl | Vel Total (ft/s) | Vel Chnl (ft/s) | Shear Total (lb/sq ft) | Shear Chan (lb/sq ft) | Shear LOB (lb/sq ft) | Shear ROB (lb/sq ft) |
|-------------|-----------|---------|------------------|-------------------|-------------------|-------------------|-----------------------|----------------------|-------------------|--------------|---------------------|--------------------|---------------------------|--------------------------|-------------------------|-------------------------|
| JonesFalls3 | 8 | 2 Yr | 655.40 | 364.96 | 364.31 | 365.13 | 0.004963 | 284.78 | 165.06 | 0.43 | 2.30 | 4.74 | 0.53 | 1.03 | 0.52 | 0.19 |
| JonesFalls3 | 8 | 10 Yr | 1520.50 | 365.65 | 365.13 | 366.03 | 0.009597 | 406.13 | 183.18 | 0.62 | 3.74 | 7.39 | 1.31 | 2.35 | 1.37 | 0.59 |
| JonesFalls3 | 8 | 100 Yr | 3144.30 | 366.09 | 366.09 | 367.12 | 0.023572 | 489.32 | 193.98 | 0.98 | 6.43 | 12.34 | 3.66 | 6.35 | 3.92 | 1.79 |
| JonesFalls3 | 7 | 2 Yr | 655.40 | 359.06 | 359.06 | 360.22 | 0.026068 | 90.28 | 48.71 | 0.95 | 7.26 | 9.04 | 2.75 | 4.08 | 2.30 | 0.31 |
| JonesFalls3 | 7 | 10 Yr | 1520.50 | 360.51 | 360.51 | 361.01 | 0.010430 | 371.35 | 284.18 | 0.64 | 4.09 | 7.54 | 0.84 | 2.47 | 0.66 | 0.68 |
| JonesFalls3 | 7 | 100 Yr | 3144.30 | 363.77 | 361.16 | 363.85 | 0.000813 | 1440.05 | 361.39 | 0.20 | 2.18 | 3.07 | 0.20 | 0.34 | 0.17 | 0.20 |
| JonesFalls3 | 6 | 2 Yr | 655.40 | 356.72 | 355.74 | 356.81 | 0.001777 | 538.53 | 442.46 | 0.27 | 1.22 | 3.35 | 0.20 | 0.47 | 0.11 | 0.19 |
| JonesFalls3 | 6 | 10 Yr | 1520.50 | 360.40 | 356.50 | 360.42 | 0.000238 | 2276.50 | 598.93 | 0.11 | 0.67 | 1.79 | 0.07 | 0.11 | 0.05 | 0.08 |
| JonesFalls3 | 6 | 100 Yr | 3144.30 | 363.68 | 357.34 | 363.69 | 0.000150 | 4850.53 | 697.26 | 0.09 | 0.65 | 1.76 | 0.06 | 0.10 | 0.06 | 0.07 |
| JonesFalls3 | 5 | 2 Yr | 655.40 | 356.51 | 354.52 | 356.63 | 0.002172 | 292.83 | 399.72 | 0.29 | 2.24 | 3.00 | 0.30 | 0.43 | 0.07 | 0.22 |
| JonesFalls3 | 5 | 10 Yr | 1520.50 | 360.30 | 356.04 | 360.37 | 0.000743 | 881.31 | 619.46 | 0.16 | 1.73 | 2.48 | 0.26 | 0.31 | 0.19 | 0.25 |
| JonesFalls3 | 5 | 100 Yr | 3144.30 | 363.67 | 357.39 | 363.68 | 0.000123 | 5015.79 | 756.66 | 0.07 | 0.63 | 1.25 | 0.05 | 0.08 | 0.05 | 0.05 |
| JonesFalls3 | 4.5 | | Culvert | | | | | | | | | | | | | |
| JonesFalls3 | 4 | 2 Yr | 655.40 | 355.26 | 354.43 | 355.37 | 0.002391 | 281.42 | 380.61 | 0.34 | 2.33 | 3.19 | 0.22 | 0.41 | 0.09 | 0.22 |
| JonesFalls3 | 4 | 10 Yr | 1520.50 | 355.97 | 355.00 | 356.22 | 0.004092 | 415.44 | 538.37 | 0.46 | 3.66 | 4.84 | 0.56 | 0.89 | 0.34 | 0.55 |
| JonesFalls3 | 4 | 100 Yr | 3144.30 | 356.78 | 356.02 | 357.31 | 0.006518 | 569.52 | 612.62 | 0.60 | 5.52 | 7.02 | 1.21 | 1.74 | 0.87 | 1.21 |
| JonesFalls3 | 3.5 | 2 Yr | 655.40 | 355.19 | 354.61 | 355.26 | 0.002228 | 339.79 | 371.32 | 0.29 | 1.93 | 2.68 | 0.18 | 0.36 | 0.15 | 0.15 |
| JonesFalls3 | 3.5 | 10 Yr | 1520.50 | 355.89 | 355.06 | 356.03 | 0.003061 | 523.45 | 481.97 | 0.36 | 2.90 | 3.68 | 0.38 | 0.62 | 0.34 | 0.33 |
| JonesFalls3 | 3.5 | 100 Yr | 3144.30 | 356.70 | 355.65 | 356.99 | 0.004257 | 738.97 | 575.75 | 0.44 | 4.26 | 5.03 | 0.74 | 1.08 | 0.69 | 0.68 |
| JonesFalls3 | 3 | 2 Yr | 655.40 | 354.44 | 353.99 | 354.68 | 0.014080 | 194.01 | 292.32 | 0.68 | 3.38 | 4.95 | 0.58 | 1.42 | 0.55 | 0.34 |
| JonesFalls3 | 3 | 10 Yr | 1520.50 | 354.91 | 354.84 | 355.27 | 0.016323 | 348.16 | 359.27 | 0.77 | 4.37 | 6.32 | 0.99 | 2.13 | 0.93 | 0.74 |
| JonesFalls3 | 3 | 100 Yr | 3144.30 | 355.45 | 355.39 | 356.00 | 0.018691 | 556.75 | 424.49 | 0.85 | 5.65 | 7.88 | 1.56 | 3.05 | 1.54 | 1.25 |
| JonesFalls4 | 2 | 2 Yr | 721.70 | 352.56 | 352.42 | 352.67 | 0.009853 | 281.96 | 479.35 | 0.55 | 2.56 | 3.66 | 0.36 | 0.82 | 0.34 | 0.33 |
| JonesFalls4 | 2 | 10 Yr | 1659.40 | 352.96 | | 353.15 | 0.009669 | 481.49 | 517.87 | 0.57 | 3.45 | 4.31 | 0.56 | 1.05 | 0.56 | 0.51 |
| JonesFalls4 | 2 | 100 Yr | 3405.50 | 353.51 | | 353.79 | 0.009184 | 819.00 | 624.06 | 0.58 | 4.16 | 5.04 | 0.75 | 1.31 | 0.79 | 0.69 |
| JonesFalls4 | 1 | 2 Yr | 721.70 | 350.69 | 350.42 | 350.76 | 0.006131 | 342.99 | 523.08 | 0.43 | 2.10 | 2.61 | 0.25 | 0.44 | 0.22 | 0.25 |
| JonesFalls4 | 1 | 10 Yr | 1659.40 | 351.13 | 350.72 | 351.26 | 0.006135 | 583.50 | 565.06 | 0.45 | 2.84 | 3.24 | 0.40 | 0.61 | 0.33 | 0.40 |
| JonesFalls4 | 1 | 100 Yr | 3405.50 | 351.71 | 351.13 | 351.93 | 0.006131 | 929.09 | 614.41 | 0.48 | 3.67 | 3.99 | 0.58 | 0.83 | 0.49 | 0.60 |

EcclestonMod.rep

HEC-RAS Version 4.1.0 Jan 2010
U.S. Army Corps of Engineers
Hydrologic Engineering Center
609 Second Street
Davis, California

```
X      X  XXXXXX      XXXX      XXXX      XX      XXXX
X      X  X          X      X          X      X      X
X      X  X          X          X      X      X      X
XXXXXXXX XXXX      X          XXX XXXX      XXXXXX      XXXX
X      X  X          X          X      X      X          X
X      X  X          X      X          X      X      X      X
X      X  XXXXXX      XXXX      X      X      X      X      XXXXX
```

PROJECT DATA

Project Title: EcclestonMod
Project File : EcclestonMod.prj
Run Date and Time: 11/8/2018 1:15:52 PM

Project in English units

PLAN DATA

Plan Title: existing
Plan File : q:\2017\1710977_001_Eccleston_Mitigation\working
Data\Model\EcclestonMod.p01

Geometry Title: ExistGeoECC
Geometry File : q:\2017\1710977_001_Eccleston_Mitigation\working
Data\Model\EcclestonMod.g05

Flow Title : EccNormalDepth_ULT
Flow File : q:\2017\1710977_001_Eccleston_Mitigation\working
Data\Model\EcclestonMod.f01

Plan Summary Information:

| | | | | | |
|---------------------------|---|----|--------------------|---|---|
| Number of: Cross Sections | = | 34 | Multiple Openings | = | 0 |
| Culverts | = | 3 | Inline Structures | = | 0 |
| Bridges | = | 1 | Lateral Structures | = | 0 |

Computational Information

| | | |
|--------------------------------------|---|-------|
| Water surface calculation tolerance | = | 0.01 |
| Critical depth calculation tolerance | = | 0.01 |
| Maximum number of iterations | = | 20 |
| Maximum difference tolerance | = | 0.3 |
| Flow tolerance factor | = | 0.001 |

Computation Options

| | |
|--|----------------------------|
| Critical depth computed only where necessary | |
| Conveyance Calculation Method: | At breaks in n values only |
| Friction Slope Method: | Average Conveyance |
| Computational Flow Regime: | Subcritical Flow |

EcclestonMod.rep

FLOW DATA

Flow Title: EccNormalDepth_ULT
 Flow File : q:\2017\1710977_001_Eccleston_Mitigation\working
 Data\Model\EcclestonMod.f01

Flow Data (cfs)

| River | Reach | RS | 2 Yr | 10 Yr |
|------------|-------------|----|-------|--------|
| 100 Yr | | | | |
| JonesFalls | JonesFalls | 15 | 363.3 | 798.4 |
| 1593.4 | | | | |
| JonesFalls | NorthTrib | 2 | 175.5 | 459.7 |
| 1025.9 | | | | |
| JonesFalls | JonesFalls2 | 12 | 538.8 | 1258.1 |
| 2619.3 | | | | |
| JonesFalls | SouthTrib | 8 | 151.7 | 322.2 |
| 622.1 | | | | |
| JonesFalls | IntsTrib | 8 | 66.3 | 138.9 |
| 261.2 | | | | |
| JonesFalls | JonesFalls3 | 10 | 655.4 | 1520.5 |
| 3144.3 | | | | |
| JonesFalls | JonesFalls4 | 2 | 721.7 | 1659.4 |
| 3405.5 | | | | |

Boundary Conditions

| River | Reach | Profile | Upstream |
|--------------------|-------------|---------|----------|
| Downstream | | | |
| JonesFalls | JonesFalls4 | 2 Yr | |
| Normal S = 0.00613 | | | |
| JonesFalls | JonesFalls4 | 10 Yr | |
| Normal S = 0.00613 | | | |
| JonesFalls | JonesFalls4 | 100 Yr | |
| Normal S = 0.00613 | | | |

CROSS SECTION

RIVER: JonesFalls
 REACH: JonesFalls RS: 15

CROSS SECTION OUTPUT Profile #2 Yr

| E.G. Elev (ft) | | Element | Left OB | Channel |
|--------------------|----------|-------------------|---------|---------|
| Right OB | 384.32 | | | |
| Vel Head (ft) | 0.30 | wt. n-val. | 0.110 | 0.049 |
| 0.055 | | | | |
| W.S. Elev (ft) | 384.02 | Reach Len. (ft) | 728.00 | 669.00 |
| 602.00 | | | | |
| Crit w.s. (ft) | 383.82 | Flow Area (sq ft) | 49.25 | 32.54 |
| 37.93 | | | | |
| E.G. slope (ft/ft) | 0.012619 | Area (sq ft) | 49.25 | 32.54 |

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| | | | | |
|-------------------|--------|------------------------|--------|--------|
| 37.93 | | | | |
| Q Total (cfs) | 363.30 | Flow (cfs) | 60.18 | 182.79 |
| 120.33 | | | | |
| Top width (ft) | 126.26 | Top width (ft) | 68.13 | 14.39 |
| 43.73 | | | | |
| Vel Total (ft/s) | 3.03 | Avg. Vel. (ft/s) | 1.22 | 5.62 |
| 3.17 | | | | |
| Max Chl Dpth (ft) | 2.62 | Hydr. Depth (ft) | 0.72 | 2.26 |
| 0.87 | | | | |
| Conv. Total (cfs) | 3234.1 | Conv. (cfs) | 535.7 | 1627.2 |
| 1071.1 | | | | |
| Length wtd. (ft) | 651.71 | wetted Per. (ft) | 68.16 | 15.36 |
| 44.28 | | | | |
| Min Ch El (ft) | 381.40 | Shear (lb/sq ft) | 0.57 | 1.67 |
| 0.67 | | | | |
| Alpha | 2.11 | Stream Power (lb/ft s) | 456.22 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 6.21 | Cum Volume (acre-ft) | 1.76 | 1.36 |
| 1.92 | | | | |
| C & E Loss (ft) | 0.04 | Cum SA (acres) | 1.74 | 0.51 |
| 2.17 | | | | |

Warning: The energy loss was greater than 1.0 ft (0.3m). between the current and previous cross section. This may indicate the need for additional cross sections.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, energy was used.

CROSS SECTION OUTPUT Profile #10 Yr

| | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 385.21 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.37 | wt. n-val. | 0.110 | 0.049 |
| 0.061 | | | | |
| w.s. Elev (ft) | 384.84 | Reach Len. (ft) | 728.00 | 669.00 |
| 602.00 | | | | |
| Crit w.s. (ft) | 384.51 | Flow Area (sq ft) | 120.25 | 44.30 |
| 79.24 | | | | |
| E.G. Slope (ft/ft) | 0.012592 | Area (sq ft) | 120.25 | 44.30 |
| 112.84 | | | | |
| Q Total (cfs) | 798.40 | Flow (cfs) | 203.44 | 305.47 |
| 289.49 | | | | |
| Top width (ft) | 329.25 | Top width (ft) | 101.82 | 14.39 |
| 213.04 | | | | |
| Vel Total (ft/s) | 3.27 | Avg. Vel. (ft/s) | 1.69 | 6.89 |
| 3.65 | | | | |
| Max Chl Dpth (ft) | 3.44 | Hydr. Depth (ft) | 1.18 | 3.08 |
| 1.38 | | | | |
| Conv. Total (cfs) | 7115.1 | Conv. (cfs) | 1813.0 | 2722.2 |
| 2579.9 | | | | |
| Length wtd. (ft) | 651.23 | wetted Per. (ft) | 101.98 | 15.36 |
| 57.86 | | | | |
| Min Ch El (ft) | 381.40 | Shear (lb/sq ft) | 0.93 | 2.27 |
| 1.08 | | | | |
| Alpha | 2.22 | Stream Power (lb/ft s) | 456.22 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 6.26 | Cum Volume (acre-ft) | 3.84 | 1.81 |
| 4.54 | | | | |
| C & E Loss (ft) | 0.05 | Cum SA (acres) | 2.43 | 0.51 |
| 4.75 | | | | |

EcclestonMod.rep

Warning: Divided flow computed for this cross-section.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, energy was used.

CROSS SECTION OUTPUT Profile #100 Yr

| | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 385.89 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.34 | wt. n-val. | 0.110 | 0.049 |
| 0.078 | | | | |
| W.S. Elev (ft) | 385.55 | Reach Len. (ft) | 728.00 | 669.00 |
| 602.00 | | | | |
| Crit w.s. (ft) | 385.28 | Flow Area (sq ft) | 198.04 | 54.51 |
| 298.04 | | | | |
| E.G. slope (ft/ft) | 0.013107 | Area (sq ft) | 198.04 | 54.51 |
| 298.04 | | | | |
| Q Total (cfs) | 1593.40 | Flow (cfs) | 436.48 | 440.22 |
| 716.70 | | | | |
| Top width (ft) | 430.59 | Top width (ft) | 116.23 | 14.39 |
| 299.98 | | | | |
| Vel Total (ft/s) | 2.89 | Avg. vel. (ft/s) | 2.20 | 8.08 |
| 2.40 | | | | |
| Max Chl Dpth (ft) | 4.15 | Hydr. Depth (ft) | 1.70 | 3.79 |
| 0.99 | | | | |
| Conv. Total (cfs) | 13918.1 | Conv. (cfs) | 3812.6 | 3845.3 |
| 6260.2 | | | | |
| Length wtd. (ft) | 645.39 | wetted Per. (ft) | 116.40 | 15.36 |
| 300.68 | | | | |
| Min Ch El (ft) | 381.40 | Shear (lb/sq ft) | 1.39 | 2.90 |
| 0.81 | | | | |
| Alpha | 2.62 | Stream Power (lb/ft s) | 456.22 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 6.15 | Cum volume (acre-ft) | 7.08 | 2.29 |
| 8.77 | | | | |
| C & E Loss (ft) | 0.04 | Cum SA (acres) | 3.43 | 0.51 |
| 5.63 | | | | |

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, energy was used.

CROSS SECTION

RIVER: JonesFalls
 REACH: JonesFalls RS: 14

CROSS SECTION OUTPUT Profile #2 Yr

| | | | | |
|----------------|--------|---------|---------|---------|
| E.G. Elev (ft) | 378.08 | Element | Left OB | Channel |
| | | Page 4 | | |

EcclestonMod.rep

| | | | | |
|--------------------|----------|------------------------|--------|--------|
| Right OB | | | | |
| Vel Head (ft) | 0.18 | wt. n-val. | 0.110 | 0.049 |
| 0.110 | | | | |
| W.S. Elev (ft) | 377.89 | Reach Len. (ft) | 479.00 | 477.00 |
| 479.00 | | | | |
| Crit w.s. (ft) | 377.63 | Flow Area (sq ft) | 27.13 | 43.46 |
| 129.74 | | | | |
| E.G. slope (ft/ft) | 0.007451 | Area (sq ft) | 27.13 | 43.46 |
| 130.95 | | | | |
| Q Total (cfs) | 363.30 | Flow (cfs) | 23.85 | 198.33 |
| 141.12 | | | | |
| Top width (ft) | 208.60 | Top width (ft) | 41.30 | 17.76 |
| 149.54 | | | | |
| Vel Total (ft/s) | 1.81 | Avg. vel. (ft/s) | 0.88 | 4.56 |
| 1.09 | | | | |
| Max Chl Dpth (ft) | 3.19 | Hydr. Depth (ft) | 0.66 | 2.45 |
| 0.90 | | | | |
| Conv. Total (cfs) | 4208.7 | Conv. (cfs) | 276.3 | 2297.6 |
| 1634.9 | | | | |
| Length wtd. (ft) | 477.74 | wetted Per. (ft) | 41.43 | 18.88 |
| 144.01 | | | | |
| Min Ch El (ft) | 374.70 | Shear (lb/sq ft) | 0.30 | 1.07 |
| 0.42 | | | | |
| Alpha | 3.61 | Stream Power (lb/ft s) | 568.17 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 5.29 | Cum Volume (acre-ft) | 1.12 | 0.78 |
| 0.76 | | | | |
| C & E Loss (ft) | 0.02 | Cum SA (acres) | 0.83 | 0.26 |
| 0.83 | | | | |

Warning: Divided flow computed for this cross-section.

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

This may indicate the need for additional cross sections.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the

need for additional cross sections.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, energy was used.

CROSS SECTION OUTPUT Profile #10 Yr

| | | | | |
|--------------------|----------|-------------------|---------|---------|
| E.G. Elev (ft) | 378.90 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.21 | wt. n-val. | 0.110 | 0.049 |
| 0.110 | | | | |
| W.S. Elev (ft) | 378.68 | Reach Len. (ft) | 479.00 | 477.00 |
| 479.00 | | | | |
| Crit w.s. (ft) | 378.14 | Flow Area (sq ft) | 62.59 | 57.55 |
| 253.21 | | | | |
| E.G. slope (ft/ft) | 0.007578 | Area (sq ft) | 62.59 | 57.55 |
| 293.01 | | | | |
| Q Total (cfs) | 798.40 | Flow (cfs) | 88.20 | 319.43 |
| 390.77 | | | | |
| Top width (ft) | 338.21 | Top width (ft) | 58.57 | 17.76 |
| 261.89 | | | | |
| Vel Total (ft/s) | 2.14 | Avg. vel. (ft/s) | 1.41 | 5.55 |
| 1.54 | | | | |
| Max Chl Dpth (ft) | 3.98 | Hydr. Depth (ft) | 1.07 | 3.24 |
| 1.51 | | | | |

| EcclestonMod.rep | | | | |
|----------------------------|--------|------------------------|--------|--------|
| Conv. Total (cfs) | 9171.8 | Conv. (cfs) | 1013.2 | 3669.5 |
| 4489.1 Length wtd. (ft) | 478.06 | wetted Per. (ft) | 58.76 | 18.88 |
| 168.42 Min Ch El (ft) | 374.70 | Shear (lb/sq ft) | 0.50 | 1.44 |
| 0.71 Alpha | 3.00 | Stream Power (lb/ft s) | 568.17 | 0.00 |
| 0.00 Frctn Loss (ft) | 5.46 | Cum Volume (acre-ft) | 2.31 | 1.03 |
| 1.74 C & E Loss (ft) | 0.02 | Cum SA (acres) | 1.09 | 0.26 |
| 1.47 | | | | |

Warning: Divided flow computed for this cross-section.
Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.
This may indicate the need for additional cross sections.
Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, energy was used.

CROSS SECTION OUTPUT Profile #100 Yr

| E.G. Elev (ft) | 379.70 | Element | Left OB | Channel |
|------------------------------|----------|------------------------|---------|---------|
| Right OB | | | | |
| Vel Head (ft) | 0.21 | wt. n-val. | 0.110 | 0.049 |
| 0.103 W.S. Elev (ft) | 379.49 | Reach Len. (ft) | 479.00 | 477.00 |
| 479.00 Crit w.s. (ft) | 378.89 | Flow Area (sq ft) | 140.81 | 71.87 |
| 509.99 E.G. slope (ft/ft) | 0.007232 | Area (sq ft) | 140.81 | 71.87 |
| 509.99 Q Total (cfs) | 1593.40 | Flow (cfs) | 186.60 | 451.94 |
| 954.86 Top width (ft) | 411.93 | Top width (ft) | 113.40 | 17.76 |
| 280.78 Vel Total (ft/s) | 2.20 | Avg. vel. (ft/s) | 1.33 | 6.29 |
| 1.87 Max Chl Dpth (ft) | 4.79 | Hydr. Depth (ft) | 1.24 | 4.05 |
| 1.82 Conv. Total (cfs) | 18736.9 | Conv. (cfs) | 2194.3 | 5314.4 |
| 11228.2 Length wtd. (ft) | 478.29 | wetted Per. (ft) | 113.64 | 18.88 |
| 281.31 Min Ch El (ft) | 374.70 | Shear (lb/sq ft) | 0.56 | 1.72 |
| 0.82 Alpha | 2.78 | Stream Power (lb/ft s) | 568.17 | 0.00 |
| 0.00 Frctn Loss (ft) | 5.50 | Cum volume (acre-ft) | 4.25 | 1.32 |
| 3.19 C & E Loss (ft) | 0.04 | Cum SA (acres) | 1.51 | 0.26 |
| 1.62 | | | | |

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

This may indicate the need for additional cross sections.
 Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

CROSS SECTION

RIVER: JonesFalls
 REACH: JonesFalls RS: 13

CROSS SECTION OUTPUT Profile #2 Yr

| | | Element | Left OB | Channel |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 372.77 | | | |
| Right OB | | | | |
| Vel Head (ft) | 0.35 | wt. n-Val. | 0.076 | 0.049 |
| 0.040 | | | | |
| W.S. Elev (ft) | 372.42 | Reach Len. (ft) | 236.77 | 236.77 |
| 236.77 | | | | |
| Crit w.s. (ft) | 372.42 | Flow Area (sq ft) | 57.07 | 47.53 |
| 0.41 | | | | |
| E.G. Slope (ft/ft) | 0.018113 | Area (sq ft) | 57.07 | 47.53 |
| 0.41 | | | | |
| Q Total (cfs) | 363.30 | Flow (cfs) | 102.13 | 260.36 |
| 0.81 | | | | |
| Top width (ft) | 141.06 | Top width (ft) | 109.47 | 30.01 |
| 1.58 | | | | |
| Vel Total (ft/s) | 3.46 | Avg. Vel. (ft/s) | 1.79 | 5.48 |
| 1.97 | | | | |
| Max Chl Dpth (ft) | 2.58 | Hydr. Depth (ft) | 0.52 | 1.58 |
| 0.26 | | | | |
| Conv. Total (cfs) | 2699.4 | Conv. (cfs) | 758.8 | 1934.5 |
| 6.0 | | | | |
| Length wtd. (ft) | 236.77 | wetted Per. (ft) | 109.48 | 30.56 |
| 1.67 | | | | |
| Min Ch El (ft) | 369.84 | Shear (lb/sq ft) | 0.59 | 1.76 |
| 0.28 | | | | |
| Alpha | 1.87 | Stream Power (lb/ft s) | 433.72 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 2.12 | Cum Volume (acre-ft) | 0.66 | 0.28 |
| 0.03 | | | | |
| C & E Loss (ft) | 0.07 | Cum SA (acres) | | |

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION OUTPUT Profile #10 Yr

| EcclestonMod.rep | | | | |
|--------------------|----------|------------------------|---------|---------|
| | | Element | Left OB | Channel |
| E.G. Elev (ft) | 373.41 | | | |
| Right OB | | | | |
| Vel Head (ft) | 0.46 | wt. n-Val. | 0.068 | 0.049 |
| 0.040 | | | | |
| W.S. Elev (ft) | 372.95 | Reach Len. (ft) | 236.77 | 236.77 |
| 236.77 | | | | |
| Crit w.s. (ft) | 372.95 | Flow Area (sq ft) | 122.32 | 63.46 |
| 1.91 | | | | |
| E.G. Slope (ft/ft) | 0.019186 | Area (sq ft) | 122.32 | 63.46 |
| 1.91 | | | | |
| Q Total (cfs) | 798.40 | Flow (cfs) | 359.58 | 433.79 |
| 5.03 | | | | |
| Top width (ft) | 174.09 | Top width (ft) | 139.00 | 30.01 |
| 5.08 | | | | |
| Vel Total (ft/s) | 4.25 | Avg. Vel. (ft/s) | 2.94 | 6.84 |
| 2.63 | | | | |
| Max Chl Dpth (ft) | 3.11 | Hydr. Depth (ft) | 0.88 | 2.11 |
| 0.38 | | | | |
| Conv. Total (cfs) | 5764.0 | Conv. (cfs) | 2596.0 | 3131.7 |
| 36.3 | | | | |
| Length wtd. (ft) | 236.77 | wetted Per. (ft) | 139.02 | 30.56 |
| 5.22 | | | | |
| Min Ch El (ft) | 369.84 | Shear (lb/sq ft) | 1.05 | 2.49 |
| 0.44 | | | | |
| Alpha | 1.62 | Stream Power (lb/ft s) | 433.72 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 2.09 | Cum Volume (acre-ft) | 1.29 | 0.37 |
| 0.12 | | | | |
| C & E Loss (ft) | 0.09 | Cum SA (acres) | | |

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth

for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the

need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated

water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program

defaulted to critical depth.

CROSS SECTION OUTPUT Profile #100 Yr

| | | Element | Left OB | Channel |
|--------------------|----------|-------------------|---------|---------|
| E.G. Elev (ft) | 374.15 | | | |
| Right OB | | | | |
| Vel Head (ft) | 0.63 | wt. n-Val. | 0.062 | 0.049 |
| 0.040 | | | | |
| W.S. Elev (ft) | 373.52 | Reach Len. (ft) | 236.77 | 236.77 |
| 236.77 | | | | |
| Crit w.s. (ft) | 373.52 | Flow Area (sq ft) | 208.27 | 80.64 |
| 7.02 | | | | |
| E.G. Slope (ft/ft) | 0.021060 | Area (sq ft) | 208.27 | 80.64 |
| 7.02 | | | | |
| Q Total (cfs) | 1593.40 | Flow (cfs) | 889.28 | 677.53 |
| 26.59 | | | | |
| Top width (ft) | 205.56 | Top width (ft) | 161.96 | 30.01 |
| 13.59 | | | | |
| Vel Total (ft/s) | 5.38 | Avg. Vel. (ft/s) | 4.27 | 8.40 |

EcclestonMod.rep

| | | | | |
|-------------------|---------|------------------------|--------|--------|
| 3.79 | | | | |
| Max Chl Dpth (ft) | 3.68 | Hydr. Depth (ft) | 1.29 | 2.69 |
| 0.52 | | | | |
| Conv. Total (cfs) | 10979.8 | Conv. (cfs) | 6127.8 | 4668.7 |
| 183.2 | | | | |
| Length wtd. (ft) | 236.77 | wetted Per. (ft) | 161.99 | 30.56 |
| 13.87 | | | | |
| Min Ch El (ft) | 369.84 | Shear (lb/sq ft) | 1.69 | 3.47 |
| 0.67 | | | | |
| Alpha | 1.39 | Stream Power (lb/ft s) | 433.72 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 1.68 | Cum Volume (acre-ft) | 2.33 | 0.49 |
| 0.34 | | | | |
| C & E Loss (ft) | 0.13 | Cum SA (acres) | | |

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth

for the water surface and continued on with the calculations.

Warning: Divided flow computed for this cross-section.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: JonesFalls

REACH: NorthTrib

RS: 2

CROSS SECTION OUTPUT Profile #2 Yr

| | | | | |
|--------------------|----------|-------------------|---------|---------|
| E.G. Elev (ft) | 380.55 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.32 | wt. n-Val. | | 0.061 |
| 0.040 | | | | |
| W.S. Elev (ft) | 380.23 | Reach Len. (ft) | 337.47 | 342.24 |
| 354.84 | | | | |
| Crit w.s. (ft) | 379.88 | Flow Area (sq ft) | | 32.25 |
| 7.67 | | | | |
| E.G. Slope (ft/ft) | 0.015832 | Area (sq ft) | 129.10 | 32.25 |
| 7.67 | | | | |
| Q Total (cfs) | 175.50 | Flow (cfs) | | 151.07 |
| 24.43 | | | | |
| Top width (ft) | 164.78 | Top width (ft) | 135.97 | 15.26 |
| 13.54 | | | | |
| Vel Total (ft/s) | 4.40 | Avg. Vel. (ft/s) | | 4.69 |
| 3.18 | | | | |
| Max Chl Dpth (ft) | 3.17 | Hydr. Depth (ft) | | 2.11 |
| 0.57 | | | | |
| Conv. Total (cfs) | 1394.8 | Conv. (cfs) | | 1200.6 |
| 194.1 | | | | |
| Length wtd. (ft) | 345.55 | wetted Per. (ft) | | 17.06 |
| 13.64 | | | | |

| EcclestonMod.rep | | | | |
|------------------|--------|------------------------|--------|------|
| Min Ch El (ft) | 377.06 | Shear (lb/sq ft) | | 1.87 |
| 0.56 | | | | |
| Alpha | 1.05 | Stream Power (lb/ft s) | 343.62 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 6.95 | Cum volume (acre-ft) | 1.01 | 0.45 |
| 0.24 | | | | |
| C & E Loss (ft) | 0.03 | Cum SA (acres) | 0.53 | 0.15 |
| 0.43 | | | | |

Warning: Divided flow computed for this cross-section.
Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, energy was used.

CROSS SECTION OUTPUT Profile #10 Yr

| | | Element | Left OB | Channel |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 380.63 | | | |
| Right OB | | | | |
| Vel Head (ft) | 0.06 | wt. n-Val. | 0.040 | 0.061 |
| 0.040 | | | | |
| W.S. Elev (ft) | 380.57 | Reach Len. (ft) | 337.47 | 342.24 |
| 354.84 | | | | |
| Crit w.s. (ft) | 380.57 | Flow Area (sq ft) | 181.46 | 37.41 |
| 12.44 | | | | |
| E.G. Slope (ft/ft) | 0.002721 | Area (sq ft) | 181.46 | 37.41 |
| 12.44 | | | | |
| Q Total (cfs) | 459.70 | Flow (cfs) | 358.48 | 79.87 |
| 21.35 | | | | |
| Top width (ft) | 206.33 | Top width (ft) | 176.21 | 15.33 |
| 14.79 | | | | |
| Vel Total (ft/s) | 1.99 | Avg. Vel. (ft/s) | 1.98 | 2.14 |
| 1.72 | | | | |
| Max Chl Dpth (ft) | 3.51 | Hydr. Depth (ft) | 1.03 | 2.44 |
| 0.84 | | | | |
| Conv. Total (cfs) | 8812.6 | Conv. (cfs) | 6872.2 | 1531.2 |
| 409.2 | | | | |
| Length wtd. (ft) | 344.52 | wetted Per. (ft) | 176.29 | 17.17 |
| 14.94 | | | | |
| Min Ch El (ft) | 377.06 | Shear (lb/sq ft) | 0.17 | 0.37 |
| 0.14 | | | | |
| Alpha | 1.01 | Stream Power (lb/ft s) | 343.62 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 2.20 | Cum volume (acre-ft) | 1.67 | 0.57 |
| 0.63 | | | | |
| C & E Loss (ft) | 0.03 | Cum SA (acres) | 0.68 | 0.15 |
| 0.61 | | | | |

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.
Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION OUTPUT Profile #100 Yr

| | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 380.88 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.30 | wt. n-Val. | 0.040 | 0.061 |
| 0.040 | | | | |
| W.S. Elev (ft) | 380.59 | Reach Len. (ft) | 337.47 | 342.24 |
| 354.84 | | | | |
| Crit w.s. (ft) | 380.58 | Flow Area (sq ft) | 184.36 | 37.66 |
| 12.69 | | | | |
| E.G. Slope (ft/ft) | 0.012940 | Area (sq ft) | 184.36 | 37.66 |
| 12.69 | | | | |
| Q Total (cfs) | 1025.90 | Flow (cfs) | 801.82 | 176.13 |
| 47.94 | | | | |
| Top width (ft) | 206.66 | Top width (ft) | 176.48 | 15.33 |
| 14.86 | | | | |
| Vel Total (ft/s) | 4.37 | Avg. Vel. (ft/s) | 4.35 | 4.68 |
| 3.78 | | | | |
| Max Chl Dpth (ft) | 3.53 | Hydr. Depth (ft) | 1.04 | 2.46 |
| 0.85 | | | | |
| Conv. Total (cfs) | 9018.7 | Conv. (cfs) | 7048.8 | 1548.4 |
| 421.5 | | | | |
| Length wtd. (ft) | 345.34 | wetted Per. (ft) | 176.55 | 17.17 |
| 15.00 | | | | |
| Min Ch El (ft) | 377.06 | Shear (lb/sq ft) | 0.84 | 1.77 |
| 0.68 | | | | |
| Alpha | 1.01 | Stream Power (lb/ft s) | 343.62 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 6.21 | Cum Volume (acre-ft) | 2.50 | 0.72 |
| 1.36 | | | | |
| C & E Loss (ft) | 0.02 | Cum SA (acres) | 0.69 | 0.15 |
| 0.77 | | | | |

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

This may indicate the need for additional cross sections.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

CROSS SECTION

RIVER: JonesFalls
 REACH: NorthTrib RS: 1

CROSS SECTION OUTPUT Profile #2 Yr

| | | | | |
|----------------|--------|------------|---------|---------|
| E.G. Elev (ft) | 373.56 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.21 | wt. n-Val. | | 0.061 |
| 0.040 | | | | |

EcclestonMod.rep

| | | | | |
|--------------------|----------|------------------------|--------|--------|
| W.S. Elev (ft) | 373.35 | Reach Len. (ft) | 238.81 | 238.81 |
| 238.81 | | | | |
| Crit w.s. (ft) | 373.35 | Flow Area (sq ft) | | 25.59 |
| 26.11 | | | | |
| E.G. slope (ft/ft) | 0.026426 | Area (sq ft) | | 25.59 |
| 26.11 | | | | |
| Q Total (cfs) | 175.50 | Flow (cfs) | | 107.79 |
| 67.71 | | | | |
| Top width (ft) | 114.70 | Top width (ft) | | 22.30 |
| 92.40 | | | | |
| Vel Total (ft/s) | 3.39 | Avg. vel. (ft/s) | | 4.21 |
| 2.59 | | | | |
| Max Chl Dpth (ft) | 1.86 | Hydr. Depth (ft) | | 1.15 |
| 0.28 | | | | |
| Conv. Total (cfs) | 1079.6 | Conv. (cfs) | | 663.1 |
| 416.5 | | | | |
| Length wtd. (ft) | 238.81 | wetted Per. (ft) | | 23.33 |
| 92.74 | | | | |
| Min Ch El (ft) | 371.49 | Shear (lb/sq ft) | | 1.81 |
| 0.46 | | | | |
| Alpha | 1.17 | Stream Power (lb/ft s) | 378.27 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 1.95 | Cum Volume (acre-ft) | 0.51 | 0.22 |
| 0.10 | | | | |
| C & E Loss (ft) | 0.03 | Cum SA (acres) | | |

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: Divided flow computed for this cross-section.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION OUTPUT Profile #10 Yr

| | | | | |
|--------------------|----------|-------------------|---------|---------|
| E.G. Elev (ft) | 374.05 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.32 | wt. n-val. | | 0.061 |
| 0.040 | | | | |
| W.S. Elev (ft) | 373.73 | Reach Len. (ft) | 238.81 | 238.81 |
| 238.81 | | | | |
| Crit w.s. (ft) | 373.73 | Flow Area (sq ft) | | 34.25 |
| 68.92 | | | | |
| E.G. slope (ft/ft) | 0.029422 | Area (sq ft) | | 34.25 |
| 68.92 | | | | |
| Q Total (cfs) | 459.70 | Flow (cfs) | | 178.93 |
| 280.77 | | | | |
| Top width (ft) | 157.67 | Top width (ft) | | 23.19 |
| 134.48 | | | | |
| Vel Total (ft/s) | 4.46 | Avg. vel. (ft/s) | | 5.22 |
| 4.07 | | | | |
| Max Chl Dpth (ft) | 2.24 | Hydr. Depth (ft) | | 1.48 |
| 0.51 | | | | |

EcclestonMod.rep

| | | | |
|----------------------------|--------|------------------------|--------|
| Conv. Total (cfs) | 2680.0 | Conv. (cfs) | 1043.1 |
| 1636.9 Length wtd. (ft) | 238.81 | wetted Per. (ft) | 24.50 |
| 134.82 Min Ch El (ft) | 371.49 | Shear (lb/sq ft) | 2.57 |
| 0.94 Alpha | 1.05 | Stream Power (lb/ft s) | 378.27 |
| 0.00 Frctn Loss (ft) | 2.00 | Cum Volume (acre-ft) | 0.97 |
| 0.30 C & E Loss (ft) | 0.05 | Cum SA (acres) | 0.29 |

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth

for the water surface and continued on with the calculations.

Warning: Divided flow computed for this cross-section.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION OUTPUT Profile #100 Yr

| | | | | |
|------------------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 374.66 | Element | Left OB | Channel |
| Right OB vel Head (ft) | 0.46 | wt. n-val. | 0.040 | 0.061 |
| 0.040 W.S. Elev (ft) | 374.19 | Reach Len. (ft) | 238.81 | 238.81 |
| 238.81 Crit w.s. (ft) | 374.19 | Flow Area (sq ft) | 0.26 | 45.32 |
| 143.27 E.G. slope (ft/ft) | 0.026708 | Area (sq ft) | 0.26 | 45.32 |
| 143.27 Q Total (cfs) | 1025.90 | Flow (cfs) | 0.39 | 264.51 |
| 761.00 Top width (ft) | 200.74 | Top width (ft) | 2.05 | 23.97 |
| 174.72 vel Total (ft/s) | 5.43 | Avg. vel. (ft/s) | 1.52 | 5.84 |
| 5.31 Max Chl Dpth (ft) | 2.70 | Hydr. Depth (ft) | 0.13 | 1.89 |
| 0.82 Conv. Total (cfs) | 6277.5 | Conv. (cfs) | 2.4 | 1618.5 |
| 4656.6 Length wtd. (ft) | 238.81 | wetted Per. (ft) | 2.07 | 25.54 |
| 175.08 Min Ch El (ft) | 371.49 | Shear (lb/sq ft) | 0.21 | 2.96 |
| 1.36 Alpha | 1.01 | Stream Power (lb/ft s) | 378.27 | 0.00 |
| 0.00 Frctn Loss (ft) | 1.55 | Cum volume (acre-ft) | 1.78 | 0.39 |
| 0.72 C & E Loss (ft) | 0.08 | Cum SA (acres) | | |

EcclestonMod.rep

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: Divided flow computed for this cross-section.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: JonesFalls
 REACH: JonesFalls2 RS: 12

CROSS SECTION OUTPUT Profile #2 Yr

| | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 369.84 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.12 | wt. n-Val. | 0.055 | 0.049 |
| 0.110 | | | | |
| W.S. Elev (ft) | 369.72 | Reach Len. (ft) | 95.54 | 134.75 |
| 134.02 | | | | |
| Crit w.s. (ft) | 369.47 | Flow Area (sq ft) | 185.42 | 55.57 |
| 12.01 | | | | |
| E.G. Slope (ft/ft) | 0.006215 | Area (sq ft) | 185.42 | 55.57 |
| 12.01 | | | | |
| Q Total (cfs) | 538.80 | Flow (cfs) | 315.31 | 216.27 |
| 7.22 | | | | |
| Top width (ft) | 311.32 | Top width (ft) | 257.55 | 25.44 |
| 28.32 | | | | |
| Vel Total (ft/s) | 2.13 | Avg. vel. (ft/s) | 1.70 | 3.89 |
| 0.60 | | | | |
| Max Chl Dpth (ft) | 3.12 | Hydr. Depth (ft) | 0.72 | 2.18 |
| 0.42 | | | | |
| Conv. Total (cfs) | 6834.4 | Conv. (cfs) | 3999.5 | 2743.3 |
| 91.6 | | | | |
| Length wtd. (ft) | 118.18 | wetted Per. (ft) | 259.18 | 26.75 |
| 28.33 | | | | |
| Min Ch El (ft) | 366.60 | Shear (lb/sq ft) | 0.28 | 0.81 |
| 0.16 | | | | |
| Alpha | 1.71 | Stream Power (lb/ft s) | 675.78 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 0.96 | Cum Volume (acre-ft) | 0.63 | 0.51 |
| 0.13 | | | | |
| C & E Loss (ft) | 0.03 | Cum SA (acres) | 0.47 | 0.08 |
| 0.09 | | | | |

CROSS SECTION OUTPUT Profile #10 Yr

| | | | | |
|----------------|--------|------------|---------|---------|
| E.G. Elev (ft) | 370.52 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.16 | wt. n-Val. | 0.056 | 0.049 |

EcclestonMod.rep

| | | | | |
|--------------------|----------|------------------------|---------|--------|
| 0.110 | | | | |
| W.S. Elev (ft) | 370.36 | Reach Len. (ft) | 95.54 | 134.75 |
| 134.02 | | | | |
| Crit w.s. (ft) | | Flow Area (sq ft) | 354.00 | 71.95 |
| 40.80 | | | | |
| E.G. slope (ft/ft) | 0.006097 | Area (sq ft) | 354.00 | 71.95 |
| 40.80 | | | | |
| Q Total (cfs) | 1258.10 | Flow (cfs) | 892.83 | 329.47 |
| 35.80 | | | | |
| Top width (ft) | 345.10 | Top width (ft) | 265.81 | 25.44 |
| 53.85 | | | | |
| Vel Total (ft/s) | 2.70 | Avg. Vel. (ft/s) | 2.52 | 4.58 |
| 0.88 | | | | |
| Max Chl Dpth (ft) | 3.76 | Hydr. Depth (ft) | 1.33 | 2.83 |
| 0.76 | | | | |
| Conv. Total (cfs) | 16112.1 | Conv. (cfs) | 11434.2 | 4219.4 |
| 458.5 | | | | |
| Length wtd. (ft) | 110.77 | wetted Per. (ft) | 267.46 | 26.75 |
| 53.88 | | | | |
| Min Ch El (ft) | 366.60 | Shear (lb/sq ft) | 0.50 | 1.02 |
| 0.29 | | | | |
| Alpha | 1.38 | Stream Power (lb/ft s) | 675.78 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 0.79 | Cum Volume (acre-ft) | 1.60 | 0.71 |
| 0.52 | | | | |
| C & E Loss (ft) | 0.01 | Cum SA (acres) | 0.50 | 0.08 |
| 0.17 | | | | |

Warning: Divided flow computed for this cross-section.

CROSS SECTION OUTPUT Profile #100 Yr

| | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 371.60 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.18 | wt. n-Val. | 0.056 | 0.049 |
| 0.110 | | | | |
| W.S. Elev (ft) | 371.42 | Reach Len. (ft) | 95.54 | 134.75 |
| 134.02 | | | | |
| Crit w.s. (ft) | | Flow Area (sq ft) | 650.49 | 98.74 |
| 119.89 | | | | |
| E.G. slope (ft/ft) | 0.004519 | Area (sq ft) | 650.49 | 98.74 |
| 119.89 | | | | |
| Q Total (cfs) | 2619.30 | Flow (cfs) | 2008.01 | 480.73 |
| 130.57 | | | | |
| Top width (ft) | 419.90 | Top width (ft) | 301.36 | 25.44 |
| 93.10 | | | | |
| Vel Total (ft/s) | 3.01 | Avg. Vel. (ft/s) | 3.09 | 4.87 |
| 1.09 | | | | |
| Max Chl Dpth (ft) | 4.82 | Hydr. Depth (ft) | 2.16 | 3.88 |
| 1.29 | | | | |
| Conv. Total (cfs) | 38964.4 | Conv. (cfs) | 29870.9 | 7151.2 |
| 1942.3 | | | | |
| Length wtd. (ft) | 107.45 | wetted Per. (ft) | 303.05 | 26.75 |
| 93.15 | | | | |
| Min Ch El (ft) | 366.60 | Shear (lb/sq ft) | 0.61 | 1.04 |
| 0.36 | | | | |
| Alpha | 1.29 | Stream Power (lb/ft s) | 675.78 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 0.53 | Cum Volume (acre-ft) | 3.08 | 0.96 |
| 1.32 | | | | |

| | | | | |
|-----------------|------|------------------------------------|------|------|
| C & E Loss (ft) | 0.01 | EcclestonMod.rep Cum SA (acres) | 0.58 | 0.08 |
| 0.30 | | | | |

CROSS SECTION

RIVER: JonesFalls
 REACH: JonesFalls2 RS: 11

CROSS SECTION OUTPUT Profile #2 Yr

| | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 368.85 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.38 | wt. n-Val. | 0.076 | 0.049 |
| 0.110 | | | | |
| w.s. Elev (ft) | 368.48 | Reach Len. (ft) | 161.20 | 161.20 |
| 161.20 | | | | |
| Crit w.s. (ft) | 368.48 | Flow Area (sq ft) | 97.64 | 65.08 |
| 18.95 | | | | |
| E.G. Slope (ft/ft) | 0.011021 | Area (sq ft) | 97.64 | 65.08 |
| 18.95 | | | | |
| Q Total (cfs) | 538.80 | Flow (cfs) | 139.46 | 378.47 |
| 20.87 | | | | |
| Top width (ft) | 225.66 | Top width (ft) | 174.03 | 24.00 |
| 27.63 | | | | |
| Vel Total (ft/s) | 2.97 | Avg. Vel. (ft/s) | 1.43 | 5.82 |
| 1.10 | | | | |
| Max Chl Dpth (ft) | 4.23 | Hydr. Depth (ft) | 0.56 | 2.71 |
| 0.69 | | | | |
| Conv. Total (cfs) | 5132.3 | Conv. (cfs) | 1328.4 | 3605.1 |
| 198.8 | | | | |
| Length wtd. (ft) | 161.20 | wetted Per. (ft) | 176.37 | 26.36 |
| 27.69 | | | | |
| Min Ch El (ft) | 364.25 | Shear (lb/sq ft) | 0.38 | 1.70 |
| 0.47 | | | | |
| Alpha | 2.77 | Stream Power (lb/ft s) | 729.24 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 1.45 | Cum Volume (acre-ft) | 0.31 | 0.32 |
| 0.09 | | | | |
| C & E Loss (ft) | 0.00 | Cum SA (acres) | | |

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION OUTPUT Profile #10 Yr

| EcclestonMod.rep | | | | |
|--------------------|----------|------------------------|---------|---------|
| | | Element | Left OB | Channel |
| E.G. Elev (ft) | 369.72 | | | |
| Right OB | | | | |
| Vel Head (ft) | 0.30 | wt. n-val. | 0.071 | 0.049 |
| 0.110 | | | | |
| W.S. Elev (ft) | 369.41 | Reach Len. (ft) | 161.20 | 161.20 |
| 161.20 | | | | |
| Crit w.s. (ft) | | Flow Area (sq ft) | 269.79 | 87.54 |
| 58.11 | | | | |
| E.G. slope (ft/ft) | 0.008405 | Area (sq ft) | 269.79 | 87.54 |
| 58.11 | | | | |
| Q Total (cfs) | 1258.10 | Flow (cfs) | 644.22 | 541.83 |
| 72.05 | | | | |
| Top width (ft) | 276.27 | Top width (ft) | 194.35 | 24.00 |
| 57.93 | | | | |
| Vel Total (ft/s) | 3.03 | Avg. Vel. (ft/s) | 2.39 | 6.19 |
| 1.24 | | | | |
| Max Chl Dpth (ft) | 5.16 | Hydr. Depth (ft) | 1.39 | 3.65 |
| 1.00 | | | | |
| Conv. Total (cfs) | 13722.5 | Conv. (cfs) | 7026.7 | 5909.9 |
| 785.9 | | | | |
| Length wtd. (ft) | 161.20 | wetted Per. (ft) | 196.72 | 26.36 |
| 58.00 | | | | |
| Min Ch El (ft) | 364.25 | Shear (lb/sq ft) | 0.72 | 1.74 |
| 0.53 | | | | |
| Alpha | 2.13 | Stream Power (lb/ft s) | 729.24 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 1.15 | Cum Volume (acre-ft) | 0.91 | 0.46 |
| 0.36 | | | | |
| C & E Loss (ft) | 0.01 | Cum SA (acres) | | |

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

CROSS SECTION OUTPUT Profile #100 Yr

| | | Element | Left OB | Channel |
|--------------------|----------|-------------------|---------|---------|
| E.G. Elev (ft) | 371.06 | | | |
| Right OB | | | | |
| Vel Head (ft) | 0.25 | wt. n-val. | 0.070 | 0.049 |
| 0.110 | | | | |
| W.S. Elev (ft) | 370.81 | Reach Len. (ft) | 161.20 | 161.20 |
| 161.20 | | | | |
| Crit w.s. (ft) | | Flow Area (sq ft) | 558.38 | 121.15 |
| 172.19 | | | | |
| E.G. slope (ft/ft) | 0.005334 | Area (sq ft) | 558.38 | 121.15 |
| 172.19 | | | | |
| Q Total (cfs) | 2619.30 | Flow (cfs) | 1632.72 | 741.88 |
| 244.70 | | | | |
| Top width (ft) | 349.75 | Top width (ft) | 225.52 | 24.00 |
| 100.23 | | | | |
| Vel Total (ft/s) | 3.08 | Avg. Vel. (ft/s) | 2.92 | 6.12 |
| 1.42 | | | | |
| Max Chl Dpth (ft) | 6.56 | Hydr. Depth (ft) | 2.48 | 5.05 |
| 1.72 | | | | |
| Conv. Total (cfs) | 35862.9 | Conv. (cfs) | 22354.9 | 10157.6 |
| 3350.4 | | | | |
| Length wtd. (ft) | 161.20 | wetted Per. (ft) | 227.95 | 26.36 |
| 100.41 | | | | |
| Min Ch El (ft) | 364.25 | Shear (lb/sq ft) | 0.82 | 1.53 |

EcclestonMod.rep

| | | | | |
|-------------------------|------|------------------------|--------|------|
| 0.57 Alpha | 1.71 | Stream Power (lb/ft s) | 729.24 | 0.00 |
| 0.00 Frctn Loss (ft) | 0.98 | Cum Volume (acre-ft) | 1.76 | 0.62 |
| 0.87 C & E Loss (ft) | 0.03 | Cum SA (acres) | | |

Warning: Divided flow computed for this cross-section.
 Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

CROSS SECTION

RIVER: JonesFalls
 REACH: SouthTrib RS: 8

CROSS SECTION OUTPUT Profile #2 Yr

| | | | | |
|---------------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 389.33 | Element | Left OB | Channel |
| Right OB Vel Head (ft) | 0.30 | wt. n-val. | | 0.057 |
| W.S. Elev (ft) | 389.03 | Reach Len. (ft) | 75.00 | 80.00 |
| 75.00 Crit w.s. (ft) | 389.03 | Flow Area (sq ft) | | 34.46 |
| E.G. slope (ft/ft) | 0.056139 | Area (sq ft) | | 34.46 |
| Q Total (cfs) | 151.70 | Flow (cfs) | | 151.70 |
| Top width (ft) | 57.17 | Top width (ft) | | 57.17 |
| Vel Total (ft/s) | 4.40 | Avg. Vel. (ft/s) | | 4.40 |
| Max Chl Dpth (ft) | 1.03 | Hydr. Depth (ft) | | 0.60 |
| Conv. Total (cfs) | 640.3 | Conv. (cfs) | | 640.3 |
| Length Wtd. (ft) | 80.00 | wetted Per. (ft) | | 57.26 |
| Min Ch El (ft) | 388.00 | Shear (lb/sq ft) | | 2.11 |
| Alpha | 1.00 | Stream Power (lb/ft s) | 450.20 | 0.00 |
| 0.00 Frctn Loss (ft) | 1.22 | Cum volume (acre-ft) | 0.36 | 0.89 |
| 0.07 C & E Loss (ft) | 0.04 | Cum SA (acres) | 0.57 | 0.49 |
| 0.20 | | | | |

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
 Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

This may indicate the need for additional cross sections.
 Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
 Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.
 Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, energy was used.

CROSS SECTION OUTPUT Profile #10 Yr

| | | | | |
|---------------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 389.86 | Element | Left OB | Channel |
| Right OB Vel Head (ft) | 0.41 | wt. n-Val. | | 0.057 |
| w.s. Elev (ft) | 389.46 | Reach Len. (ft) | 75.00 | 80.00 |
| 75.00 Crit w.s. (ft) | 389.46 | Flow Area (sq ft) | | 63.03 |
| E.G. Slope (ft/ft) | 0.050145 | Area (sq ft) | | 63.03 |
| Q Total (cfs) | 322.20 | Flow (cfs) | | 322.20 |
| Top width (ft) | 76.80 | Top width (ft) | | 76.80 |
| Vel Total (ft/s) | 5.11 | Avg. Vel. (ft/s) | | 5.11 |
| Max Chl Dpth (ft) | 1.46 | Hydr. Depth (ft) | | 0.82 |
| Conv. Total (cfs) | 1438.8 | Conv. (cfs) | | 1438.8 |
| Length wtd. (ft) | 80.00 | wetted Per. (ft) | | 76.93 |
| Min Ch El (ft) | 388.00 | Shear (lb/sq ft) | | 2.57 |
| Alpha 0.00 | 1.00 | Stream Power (lb/ft s) | 450.20 | 0.00 |
| Frctn Loss (ft) | 1.05 | Cum Volume (acre-ft) | 0.97 | 1.27 |
| 0.45 C & E Loss (ft) | 0.06 | Cum SA (acres) | 1.17 | 0.53 |
| 0.72 | | | | |

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
 Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.
 This may indicate the need for additional cross sections.
 Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
 Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.
 Note: Multiple critical depths were found at this location. The critical depth

with the lowest, valid, energy was used.

CROSS SECTION OUTPUT Profile #100 Yr

| | | Element | Left OB | Channel |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 390.59 | | | |
| Right OB | | | | |
| Vel Head (ft) | 0.29 | wt. n-val. | 0.045 | 0.057 |
| 0.045 | | | | |
| W.S. Elev (ft) | 390.30 | Reach Len. (ft) | 75.00 | 80.00 |
| 75.00 | | | | |
| Crit w.s. (ft) | 389.94 | Flow Area (sq ft) | 4.88 | 141.91 |
| 0.66 | | | | |
| E.G. slope (ft/ft) | 0.017815 | Area (sq ft) | 4.88 | 141.91 |
| 0.66 | | | | |
| Q Total (cfs) | 622.10 | Flow (cfs) | 6.04 | 615.24 |
| 0.82 | | | | |
| Top width (ft) | 139.18 | Top width (ft) | 32.87 | 101.85 |
| 4.46 | | | | |
| Vel Total (ft/s) | 4.22 | Avg. vel. (ft/s) | 1.24 | 4.34 |
| 1.23 | | | | |
| Max Chl Dpth (ft) | 2.30 | Hydr. Depth (ft) | 0.15 | 1.39 |
| 0.15 | | | | |
| Conv. Total (cfs) | 4660.9 | Conv. (cfs) | 45.2 | 4609.5 |
| 6.1 | | | | |
| Length wtd. (ft) | 79.94 | wetted Per. (ft) | 32.87 | 102.03 |
| 4.47 | | | | |
| Min Ch El (ft) | 388.00 | Shear (lb/sq ft) | 0.17 | 1.55 |
| 0.16 | | | | |
| Alpha | 1.05 | Stream Power (lb/ft s) | 450.20 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 0.61 | Cum Volume (acre-ft) | 1.97 | 1.75 |
| 1.13 | | | | |
| C & E Loss (ft) | 0.00 | Cum SA (acres) | 1.72 | 0.55 |
| 0.95 | | | | |

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

This may indicate the need for additional cross sections.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, energy was used.

CROSS SECTION

RIVER: JonesFalls
 REACH: SouthTrib RS: 7

CROSS SECTION OUTPUT Profile #2 Yr

| | | Element | Left OB | Channel |
|--------------------|----------|-------------------|---------|---------|
| E.G. Elev (ft) | 387.02 | | | |
| Right OB | | | | |
| Vel Head (ft) | 0.15 | wt. n-val. | | 0.057 |
| | | | | |
| W.S. Elev (ft) | 386.87 | Reach Len. (ft) | 28.00 | 28.00 |
| 28.00 | | | | |
| Crit w.s. (ft) | 385.94 | Flow Area (sq ft) | | 48.43 |
| | | | | |
| E.G. slope (ft/ft) | 0.006980 | Area (sq ft) | | 52.67 |
| | | | | |

EcclestonMod.rep

| | | | | |
|-------------------|--------|------------------------|--------|--------|
| Q Total (cfs) | 151.70 | Flow (cfs) | | 151.70 |
| Top width (ft) | 31.79 | Top width (ft) | | 31.79 |
| Vel Total (ft/s) | 3.13 | Avg. Vel. (ft/s) | | 3.13 |
| Max Chl Dpth (ft) | 2.42 | Hydr. Depth (ft) | | 1.74 |
| Conv. Total (cfs) | 1815.8 | Conv. (cfs) | | 1815.8 |
| Length wtd. (ft) | 28.00 | wetted Per. (ft) | | 28.09 |
| Min Ch El (ft) | 384.45 | Shear (lb/sq ft) | | 0.75 |
| Alpha | 1.00 | Stream Power (lb/ft s) | 332.83 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 0.33 | Cum Volume (acre-ft) | 0.36 | 0.81 |
| 0.07 | | | | |
| C & E Loss (ft) | 0.07 | Cum SA (acres) | 0.57 | 0.41 |
| 0.20 | | | | |

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

This may indicate the need for additional cross sections.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION OUTPUT Profile #10 Yr

| E.G. Elev (ft) | | Element | Left OB | Channel |
|--------------------|----------|------------------------|---------|---------|
| Right OB | | | | |
| Vel Head (ft) | 0.22 | wt. n-Val. | | 0.057 |
| 0.045 | | | | |
| W.S. Elev (ft) | 388.06 | Reach Len. (ft) | 28.00 | 28.00 |
| 28.00 | | | | |
| Crit w.s. (ft) | 386.70 | Flow Area (sq ft) | | 86.23 |
| 0.41 | | | | |
| E.G. Slope (ft/ft) | 0.005926 | Area (sq ft) | 0.05 | 96.60 |
| 0.43 | | | | |
| Q Total (cfs) | 322.20 | Flow (cfs) | | 321.73 |
| 0.47 | | | | |
| Top width (ft) | 42.03 | Top width (ft) | 0.76 | 39.75 |
| 1.52 | | | | |
| Vel Total (ft/s) | 3.72 | Avg. Vel. (ft/s) | | 3.73 |
| 1.13 | | | | |
| Max Chl Dpth (ft) | 3.61 | Hydr. Depth (ft) | | 2.56 |
| 0.30 | | | | |
| Conv. Total (cfs) | 4185.5 | Conv. (cfs) | | 4179.4 |
| 6.1 | | | | |
| Length wtd. (ft) | 28.00 | wetted Per. (ft) | | 34.02 |
| 1.39 | | | | |
| Min Ch El (ft) | 384.45 | Shear (lb/sq ft) | | 0.94 |
| 0.11 | | | | |
| Alpha | 1.01 | Stream Power (lb/ft s) | 332.83 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 0.29 | Cum Volume (acre-ft) | 0.97 | 1.13 |
| 0.45 | | | | |
| C & E Loss (ft) | 0.13 | Cum SA (acres) | 1.17 | 0.42 |
| 0.71 | | | | |

EcclestonMod.rep

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

This may indicate the need for additional cross sections.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION OUTPUT Profile #100 Yr

| | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 389.98 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.29 | wt. n-Val. | | 0.057 |
| 0.045 | | | | |
| W.S. Elev (ft) | 389.68 | Reach Len. (ft) | 28.00 | 28.00 |
| 28.00 | | | | |
| Crit w.s. (ft) | 387.69 | Flow Area (sq ft) | | 140.73 |
| 2.63 | | | | |
| E.G. Slope (ft/ft) | 0.004211 | Area (sq ft) | 8.23 | 160.99 |
| 3.64 | | | | |
| Q Total (cfs) | 622.10 | Flow (cfs) | | 613.46 |
| 8.64 | | | | |
| Top width (ft) | 51.53 | Top width (ft) | 9.34 | 39.75 |
| 2.44 | | | | |
| Vel Total (ft/s) | 4.34 | Avg. Vel. (ft/s) | | 4.36 |
| 3.28 | | | | |
| Max Chl Dpth (ft) | 5.23 | Hydr. Depth (ft) | | 4.18 |
| 1.92 | | | | |
| Conv. Total (cfs) | 9587.1 | Conv. (cfs) | | 9454.0 |
| 133.1 | | | | |
| Length wtd. (ft) | 28.00 | wetted Per. (ft) | | 34.02 |
| 1.39 | | | | |
| Min Ch El (ft) | 384.45 | Shear (lb/sq ft) | | 1.09 |
| 0.50 | | | | |
| Alpha | 1.00 | Stream Power (lb/ft s) | 332.83 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 0.25 | Cum Volume (acre-ft) | 1.96 | 1.47 |
| 1.12 | | | | |
| C & E Loss (ft) | 0.29 | Cum SA (acres) | 1.68 | 0.42 |
| 0.95 | | | | |

Warning: The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

This may indicate the need for additional cross sections.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION

RIVER: JonesFalls
 REACH: SouthTrib RS: 6

CROSS SECTION OUTPUT Profile #2 Yr

| EcclestonMod.rep | | | | |
|--------------------|----------|------------------------|---------|---------|
| | | Element | Left OB | Channel |
| E.G. Elev (ft) | 386.15 | | | |
| Right OB | | | | |
| Vel Head (ft) | 0.22 | wt. n-Val. | | 0.057 |
| W.S. Elev (ft) | 385.93 | Reach Len. (ft) | 96.56 | 93.29 |
| 86.62 | | | | |
| Crit w.s. (ft) | 384.86 | Flow Area (sq ft) | | 40.40 |
| E.G. Slope (ft/ft) | 0.008208 | Area (sq ft) | | 40.40 |
| Q Total (cfs) | 151.70 | Flow (cfs) | | 151.70 |
| Top width (ft) | 18.17 | Top width (ft) | | 18.17 |
| Vel Total (ft/s) | 3.75 | Avg. Vel. (ft/s) | | 3.75 |
| Max Chl Dpth (ft) | 3.31 | Hydr. Depth (ft) | | 2.22 |
| Conv. Total (cfs) | 1674.5 | Conv. (cfs) | | 1674.5 |
| Length wtd. (ft) | 93.29 | wetted Per. (ft) | | 20.15 |
| Min Ch El (ft) | 382.62 | Shear (lb/sq ft) | | 1.03 |
| Alpha | 1.00 | Stream Power (lb/ft s) | 356.91 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 1.50 | Cum Volume (acre-ft) | 0.36 | 0.74 |
| 0.07 | | | | |
| C & E Loss (ft) | 0.16 | Cum SA (acres) | 0.57 | 0.37 |
| 0.20 | | | | |

Warning: The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.
This may indicate the need for additional cross sections.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION OUTPUT Profile #10 Yr

| | | Element | Left OB | Channel |
|--------------------|----------|-------------------|---------|---------|
| E.G. Elev (ft) | 387.02 | | | |
| Right OB | | | | |
| Vel Head (ft) | 0.73 | wt. n-Val. | | 0.057 |
| 0.000 | | | | |
| W.S. Elev (ft) | 386.29 | Reach Len. (ft) | 96.56 | 93.29 |
| 86.62 | | | | |
| Crit w.s. (ft) | 385.83 | Flow Area (sq ft) | | 47.14 |
| 0.00 | | | | |
| E.G. Slope (ft/ft) | 0.023740 | Area (sq ft) | | 47.14 |
| 0.00 | | | | |
| Q Total (cfs) | 322.20 | Flow (cfs) | | 322.20 |
| 0.00 | | | | |
| Top width (ft) | 19.08 | Top width (ft) | | 19.01 |
| 0.07 | | | | |
| Vel Total (ft/s) | 6.83 | Avg. Vel. (ft/s) | | 6.83 |
| 0.27 | | | | |

| EcclestonMod.rep | | | | |
|-------------------|--------|------------------------|--------|--------|
| Max Chl Dpth (ft) | 3.67 | Hydr. Depth (ft) | | 2.48 |
| 0.02 | | | | |
| Conv. Total (cfs) | 2091.2 | Conv. (cfs) | | 2091.2 |
| 0.0 | | | | |
| Length Wtd. (ft) | 93.77 | wetted Per. (ft) | | 21.24 |
| 0.08 | | | | |
| Min Ch El (ft) | 382.62 | Shear (lb/sq ft) | | 3.29 |
| Alpha | 1.00 | Stream Power (lb/ft s) | 356.91 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 1.70 | Cum Volume (acre-ft) | 0.97 | 1.03 |
| 0.45 | | | | |
| C & E Loss (ft) | 0.20 | Cum SA (acres) | 1.16 | 0.39 |
| 0.71 | | | | |

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION OUTPUT Profile #100 Yr

| | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 388.31 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.97 | wt. n-Val. | 0.045 | 0.057 |
| 0.057 | | | | |
| W.S. Elev (ft) | 387.35 | Reach Len. (ft) | 96.56 | 93.29 |
| 86.62 | | | | |
| Crit w.s. (ft) | 387.35 | Flow Area (sq ft) | 15.82 | 67.51 |
| 1.03 | | | | |
| E.G. slope (ft/ft) | 0.021738 | Area (sq ft) | 34.41 | 67.51 |
| 1.03 | | | | |
| Q Total (cfs) | 622.10 | Flow (cfs) | 64.06 | 555.63 |
| 2.41 | | | | |
| Top width (ft) | 87.49 | Top width (ft) | 66.35 | 19.26 |
| 1.88 | | | | |
| Vel Total (ft/s) | 7.37 | Avg. Vel. (ft/s) | 4.05 | 8.23 |
| 2.34 | | | | |
| Max Chl Dpth (ft) | 4.73 | Hydr. Depth (ft) | 0.76 | 3.51 |
| 0.55 | | | | |
| Conv. Total (cfs) | 4219.4 | Conv. (cfs) | 434.5 | 3768.5 |
| 16.3 | | | | |
| Length Wtd. (ft) | 94.16 | wetted Per. (ft) | 20.84 | 21.55 |
| 2.18 | | | | |
| Min Ch El (ft) | 382.62 | Shear (lb/sq ft) | 1.03 | 4.25 |
| 0.64 | | | | |
| Alpha | 1.14 | Stream Power (lb/ft s) | 356.91 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 1.81 | Cum Volume (acre-ft) | 1.94 | 1.33 |
| 1.12 | | | | |
| C & E Loss (ft) | 0.27 | Cum SA (acres) | 1.66 | 0.39 |
| 0.95 | | | | |

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The velocity head has changed by more than 0.5 ft (0.15 m). This may

indicate the need for additional cross sections.
 Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
 Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.
 Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION

RIVER: JonesFalls
 REACH: SouthTrib RS: 5

CROSS SECTION OUTPUT Profile #2 Yr

| | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 384.49 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.76 | wt. n-val. | | 0.057 |
| W.S. Elev (ft) | 383.73 | Reach Len. (ft) | 136.21 | 123.08 |
| 111.20 | | | | |
| Crit w.s. (ft) | 383.66 | Flow Area (sq ft) | | 21.65 |
| E.G. slope (ft/ft) | 0.044154 | Area (sq ft) | 0.67 | 21.65 |
| Q Total (cfs) | 151.70 | Flow (cfs) | | 151.70 |
| Top width (ft) | 17.57 | Top width (ft) | 4.71 | 12.86 |
| vel Total (ft/s) | 7.01 | Avg. vel. (ft/s) | | 7.01 |
| Max Chl Dpth (ft) | 2.60 | Hydr. Depth (ft) | | 1.68 |
| Conv. Total (cfs) | 721.9 | Conv. (cfs) | | 721.9 |
| Length Wtd. (ft) | 123.08 | wetted Per. (ft) | | 14.97 |
| Min Ch El (ft) | 381.13 | Shear (lb/sq ft) | | 3.99 |
| Alpha | 1.00 | Stream Power (lb/ft s) | 334.83 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 2.85 | Cum volume (acre-ft) | 0.36 | 0.68 |
| 0.07 | | | | |
| C & E Loss (ft) | 0.15 | Cum SA (acres) | 0.56 | 0.34 |
| 0.20 | | | | |

Warning: Divided flow computed for this cross-section.
 Warning: The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.
 Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.
 This may indicate the need for additional cross sections.
 Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the

need for additional cross sections.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, energy was used.

CROSS SECTION OUTPUT Profile #10 Yr

| | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 385.12 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.32 | wt. n-val. | 0.045 | 0.057 |
| 0.045 | | | | |
| W.S. Elev (ft) | 384.80 | Reach Len. (ft) | 136.21 | 123.08 |
| 111.20 | | | | |
| Crit w.s. (ft) | 384.80 | Flow Area (sq ft) | 44.80 | 35.86 |
| 4.05 | | | | |
| E.G. slope (ft/ft) | 0.014240 | Area (sq ft) | 44.80 | 35.86 |
| 4.05 | | | | |
| Q Total (cfs) | 322.20 | Flow (cfs) | 116.18 | 195.38 |
| 10.64 | | | | |
| Top width (ft) | 107.82 | Top width (ft) | 87.16 | 13.31 |
| 7.35 | | | | |
| Vel Total (ft/s) | 3.80 | Avg. vel. (ft/s) | 2.59 | 5.45 |
| 2.63 | | | | |
| Max Chl Dpth (ft) | 3.67 | Hydr. Depth (ft) | 0.51 | 2.69 |
| 0.55 | | | | |
| Conv. Total (cfs) | 2700.1 | Conv. (cfs) | 973.6 | 1637.3 |
| 89.2 | | | | |
| Length wtd. (ft) | 125.04 | wetted Per. (ft) | 87.28 | 15.47 |
| 7.43 | | | | |
| Min Ch El (ft) | 381.13 | Shear (lb/sq ft) | 0.46 | 2.06 |
| 0.48 | | | | |
| Alpha | 1.43 | Stream Power (lb/ft s) | 334.83 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 2.16 | Cum volume (acre-ft) | 0.92 | 0.94 |
| 0.44 | | | | |
| C & E Loss (ft) | 0.02 | Cum SA (acres) | 1.07 | 0.35 |
| 0.71 | | | | |

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, energy was used.

CROSS SECTION OUTPUT Profile #100 Yr

| | | | | |
|----------------|--------|-----------------|---------|---------|
| E.G. Elev (ft) | 385.62 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.43 | wt. n-val. | 0.045 | 0.057 |
| 0.045 | | | | |
| W.S. Elev (ft) | 385.19 | Reach Len. (ft) | 136.21 | 123.08 |
| 111.20 | | | | |

| EcclestonMod.rep | | | | |
|--------------------|----------|------------------------|--------|--------|
| Crit w.s. (ft) | 385.16 | Flow Area (sq ft) | 81.15 | 41.16 |
| 7.37 | | | | |
| E.G. Slope (ft/ft) | 0.017061 | Area (sq ft) | 81.15 | 41.16 |
| 7.37 | | | | |
| Q Total (cfs) | 622.10 | Flow (cfs) | 326.08 | 269.10 |
| 26.92 | | | | |
| Top width (ft) | 118.42 | Top width (ft) | 95.77 | 13.31 |
| 9.34 | | | | |
| Vel Total (ft/s) | 4.80 | Avg. Vel. (ft/s) | 4.02 | 6.54 |
| 3.65 | | | | |
| Max Chl Dpth (ft) | 4.06 | Hydr. Depth (ft) | 0.85 | 3.09 |
| 0.79 | | | | |
| Conv. Total (cfs) | 4762.7 | Conv. (cfs) | 2496.4 | 2060.2 |
| 206.1 | | | | |
| Length wtd. (ft) | 125.83 | wetted Per. (ft) | 95.90 | 15.47 |
| 9.46 | | | | |
| Min Ch El (ft) | 381.13 | Shear (lb/sq ft) | 0.90 | 2.83 |
| 0.83 | | | | |
| Alpha | 1.20 | Stream Power (lb/ft s) | 334.83 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 2.59 | Cum Volume (acre-ft) | 1.81 | 1.21 |
| 1.11 | | | | |
| C & E Loss (ft) | 0.03 | Cum SA (acres) | 1.48 | 0.35 |
| 0.93 | | | | |

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, energy was used.

CROSS SECTION

RIVER: JonesFalls
 REACH: SouthTrib RS: 4

CROSS SECTION OUTPUT Profile #2 Yr

| | | | | |
|--------------------|----------|-------------------|---------|---------|
| E.G. Elev (ft) | 381.48 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.25 | wt. n-val. | | 0.057 |
| W.S. Elev (ft) | 381.23 | Reach Len. (ft) | 261.13 | 237.95 |
| 226.16 | | | | |
| Crit w.s. (ft) | 380.62 | Flow Area (sq ft) | | 37.81 |
| E.G. slope (ft/ft) | 0.014222 | Area (sq ft) | 0.81 | 37.81 |
| 0.52 | | | | |
| Q Total (cfs) | 151.70 | Flow (cfs) | | 151.70 |
| Top width (ft) | 33.61 | Top width (ft) | 3.52 | 25.03 |
| 5.06 | | | | |
| Vel Total (ft/s) | 4.01 | Avg. Vel. (ft/s) | | 4.01 |
| Max Chl Dpth (ft) | 2.35 | Hydr. Depth (ft) | | 1.51 |
| Conv. Total (cfs) | 1272.1 | Conv. (cfs) | | 1272.1 |

| EcclestonMod.rep | | | | |
|-------------------------|--------|------------------------|--------|-------|
| Length wtd. (ft) | 237.45 | Wetted Per. (ft) | | 25.78 |
| Min Ch El (ft) | 378.88 | Shear (lb/sq ft) | | 1.30 |
| Alpha 0.00 | 1.00 | Stream Power (lb/ft s) | 259.77 | 0.00 |
| Frctn Loss (ft) 0.07 | 4.18 | Cum Volume (acre-ft) | 0.36 | 0.59 |
| C & E Loss (ft) 0.19 | 0.02 | Cum SA (acres) | 0.55 | 0.29 |

Warning: Divided flow computed for this cross-section.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, energy was used.

CROSS SECTION OUTPUT Profile #10 Yr

| E.G. Elev (ft) | 382.18 | Element | Left OB | Channel |
|------------------------------------|----------|------------------------|---------|---------|
| Right OB Vel Head (ft) 0.040 | 0.49 | wt. n-Val. | 0.040 | 0.057 |
| W.S. Elev (ft) 226.16 | 381.69 | Reach Len. (ft) | 261.13 | 237.95 |
| Crit w.s. (ft) 7.66 | 381.61 | Flow Area (sq ft) | 3.50 | 49.34 |
| E.G. slope (ft/ft) 7.66 | 0.021461 | Area (sq ft) | 3.50 | 49.34 |
| Q Total (cfs) 22.94 | 322.20 | Flow (cfs) | 10.42 | 288.83 |
| Top width (ft) 18.36 | 52.11 | Top width (ft) | 8.52 | 25.23 |
| Vel Total (ft/s) 3.00 | 5.33 | Avg. Vel. (ft/s) | 2.97 | 5.85 |
| Max Chl Dpth (ft) 0.42 | 2.81 | Hydr. Depth (ft) | 0.41 | 1.96 |
| Conv. Total (cfs) 156.6 | 2199.4 | Conv. (cfs) | 71.1 | 1971.6 |
| Length wtd. (ft) 18.74 | 236.82 | wetted Per. (ft) | 8.68 | 26.00 |
| Min Ch El (ft) 0.55 | 378.88 | Shear (lb/sq ft) | 0.54 | 2.54 |
| Alpha 0.00 | 1.12 | Stream Power (lb/ft s) | 259.77 | 0.00 |
| Frctn Loss (ft) 0.43 | 4.27 | Cum Volume (acre-ft) | 0.85 | 0.82 |
| C & E Loss (ft) 0.67 | 0.04 | Cum SA (acres) | 0.92 | 0.30 |

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, energy was used.

CROSS SECTION OUTPUT Profile #100 Yr

EcclestonMod.rep

| | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 383.00 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.76 | wt. n-val. | 0.040 | 0.057 |
| 0.040 | | | | |
| W.S. Elev (ft) | 382.24 | Reach Len. (ft) | 261.13 | 237.95 |
| 226.16 | | | | |
| Crit w.s. (ft) | 382.23 | Flow Area (sq ft) | 11.34 | 63.24 |
| 18.30 | | | | |
| E.G. slope (ft/ft) | 0.025387 | Area (sq ft) | 11.34 | 63.24 |
| 18.30 | | | | |
| Q Total (cfs) | 622.10 | Flow (cfs) | 48.10 | 475.09 |
| 98.91 | | | | |
| Top width (ft) | 64.27 | Top width (ft) | 18.54 | 25.23 |
| 20.50 | | | | |
| Vel Total (ft/s) | 6.70 | Avg. vel. (ft/s) | 4.24 | 7.51 |
| 5.41 | | | | |
| Max Chl Dpth (ft) | 3.36 | Hydr. Depth (ft) | 0.61 | 2.51 |
| 0.89 | | | | |
| Conv. Total (cfs) | 3904.4 | Conv. (cfs) | 301.9 | 2981.8 |
| 620.8 | | | | |
| Length wtd. (ft) | 236.33 | wetted Per. (ft) | 18.71 | 26.00 |
| 20.96 | | | | |
| Min Ch El (ft) | 378.88 | Shear (lb/sq ft) | 0.96 | 3.86 |
| 1.38 | | | | |
| Alpha | 1.10 | Stream Power (lb/ft s) | 259.77 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 4.49 | Cum Volume (acre-ft) | 1.67 | 1.07 |
| 1.08 | | | | |
| C & E Loss (ft) | 0.11 | Cum SA (acres) | 1.30 | 0.30 |
| 0.90 | | | | |

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, energy was used.

CROSS SECTION

RIVER: JonesFalls
 REACH: SouthTrib RS: 3

CROSS SECTION OUTPUT Profile #2 Yr

| | | | | |
|--------------------|----------|-------------------|---------|---------|
| E.G. Elev (ft) | 377.27 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.43 | wt. n-val. | 0.040 | 0.057 |
| 0.043 | | | | |
| W.S. Elev (ft) | 376.84 | Reach Len. (ft) | 243.00 | 242.00 |
| 242.00 | | | | |
| Crit w.s. (ft) | 376.84 | Flow Area (sq ft) | 1.00 | 24.01 |
| 7.01 | | | | |
| E.G. slope (ft/ft) | 0.022367 | Area (sq ft) | 1.00 | 24.01 |
| 7.01 | | | | |
| Q Total (cfs) | 151.70 | Flow (cfs) | 1.73 | 133.64 |
| 16.33 | | | | |

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| | | | | |
|-------------------|--------|------------------------|--------|-------|
| Top width (ft) | 41.58 | Top width (ft) | 5.78 | 12.90 |
| 22.90 | | | | |
| Vel Total (ft/s) | 4.74 | Avg. Vel. (ft/s) | 1.73 | 5.57 |
| 2.33 | | | | |
| Max Chl Dpth (ft) | 2.40 | Hydr. Depth (ft) | 0.17 | 1.86 |
| 0.31 | | | | |
| Conv. Total (cfs) | 1014.3 | Conv. (cfs) | 11.6 | 893.6 |
| 109.2 | | | | |
| Length wtd. (ft) | 242.27 | wetted Per. (ft) | 5.79 | 14.07 |
| 23.26 | | | | |
| Min Ch El (ft) | 374.44 | Shear (lb/sq ft) | 0.24 | 2.38 |
| 0.42 | | | | |
| Alpha | 1.24 | Stream Power (lb/ft s) | 251.86 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 2.81 | Cum Volume (acre-ft) | 0.35 | 0.42 |
| 0.05 | | | | |
| C & E Loss (ft) | 0.11 | Cum SA (acres) | 0.52 | 0.18 |
| 0.12 | | | | |

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: Divided flow computed for this cross-section.

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION OUTPUT Profile #10 Yr

| | | | | |
|--------------------|----------|-------------------|---------|---------|
| E.G. Elev (ft) | 377.87 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.35 | wt. n-val. | 0.040 | 0.057 |
| 0.042 | | | | |
| W.S. Elev (ft) | 377.52 | Reach Len. (ft) | 243.00 | 242.00 |
| 242.00 | | | | |
| Crit w.s. (ft) | 377.52 | Flow Area (sq ft) | 8.78 | 32.77 |
| 34.72 | | | | |
| E.G. slope (ft/ft) | 0.015393 | Area (sq ft) | 8.78 | 32.77 |
| 34.72 | | | | |
| Q Total (cfs) | 322.20 | Flow (cfs) | 25.89 | 186.21 |
| 110.10 | | | | |
| Top width (ft) | 97.87 | Top width (ft) | 17.10 | 12.90 |
| 67.87 | | | | |
| Vel Total (ft/s) | 4.22 | Avg. Vel. (ft/s) | 2.95 | 5.68 |
| 3.17 | | | | |
| Max Chl Dpth (ft) | 3.08 | Hydr. Depth (ft) | 0.51 | 2.54 |
| 0.51 | | | | |
| Conv. Total (cfs) | 2596.9 | Conv. (cfs) | 208.7 | 1500.8 |
| 887.4 | | | | |
| Length wtd. (ft) | 242.35 | wetted Per. (ft) | 17.14 | 14.07 |
| 68.57 | | | | |
| Min Ch El (ft) | 374.44 | Shear (lb/sq ft) | 0.49 | 2.24 |

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| | | | | |
|-------------------------|------|------------------------|--------|------|
| 0.49 Alpha 0.00 | 1.28 | Stream Power (lb/ft s) | 251.86 | 0.00 |
| Frctn Loss (ft) 0.32 | 3.23 | Cum Volume (acre-ft) | 0.81 | 0.60 |
| C & E Loss (ft) 0.45 | 0.06 | Cum SA (acres) | 0.84 | 0.20 |

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: Divided flow computed for this cross-section.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION OUTPUT Profile #100 Yr

| | | | | |
|-----------------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) Right OB | 378.41 | Element | Left OB | Channel |
| Vel Head (ft) 0.042 | 0.40 | wt. n-Val. | 0.040 | 0.057 |
| W.S. Elev (ft) 242.00 | 378.00 | Reach Len. (ft) | 243.00 | 242.00 |
| Crit w.s. (ft) 71.83 | 377.92 | Flow Area (sq ft) | 19.06 | 39.04 |
| E.G. slope (ft/ft) 71.83 | 0.014773 | Area (sq ft) | 19.06 | 39.04 |
| Q Total (cfs) 306.56 | 622.10 | Flow (cfs) | 71.32 | 244.22 |
| Top width (ft) 80.43 | 118.54 | Top width (ft) | 25.22 | 12.90 |
| Vel Total (ft/s) 4.27 | 4.79 | Avg. Vel. (ft/s) | 3.74 | 6.26 |
| Max Chl Dpth (ft) 0.89 | 3.56 | Hydr. Depth (ft) | 0.76 | 3.03 |
| Conv. Total (cfs) 2522.2 | 5118.3 | Conv. (cfs) | 586.7 | 2009.3 |
| Length wtd. (ft) 81.21 | 242.38 | wetted Per. (ft) | 25.26 | 14.07 |
| Min Ch El (ft) 0.82 | 374.44 | Shear (lb/sq ft) | 0.70 | 2.56 |
| Alpha 0.00 | 1.13 | Stream Power (lb/ft s) | 251.86 | 0.00 |
| Frctn Loss (ft) 0.85 | 4.53 | Cum Volume (acre-ft) | 1.58 | 0.79 |
| C & E Loss (ft) 0.63 | 0.00 | Cum SA (acres) | 1.17 | 0.20 |

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

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CROSS SECTION

RIVER: JonesFalls
 REACH: SouthTrib RS: 2

CROSS SECTION OUTPUT Profile #2 Yr

| | | Element | Left OB | Channel |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 373.13 | | | |
| Right OB | | | | |
| Vel Head (ft) | 0.08 | wt. n-val. | 0.053 | 0.057 |
| 0.040 | | | | |
| W.S. Elev (ft) | 373.05 | Reach Len. (ft) | 259.00 | 261.00 |
| 263.00 | | | | |
| Crit w.s. (ft) | | Flow Area (sq ft) | 46.87 | 24.73 |
| 0.60 | | | | |
| E.G. slope (ft/ft) | 0.007095 | Area (sq ft) | 46.87 | 24.73 |
| 0.60 | | | | |
| Q Total (cfs) | 151.70 | Flow (cfs) | 80.88 | 70.53 |
| 0.28 | | | | |
| Top width (ft) | 112.33 | Top width (ft) | 86.40 | 15.88 |
| 10.05 | | | | |
| Vel Total (ft/s) | 2.10 | Avg. vel. (ft/s) | 1.73 | 2.85 |
| 0.48 | | | | |
| Max Chl Dpth (ft) | 2.39 | Hydr. Depth (ft) | 0.54 | 1.56 |
| 0.06 | | | | |
| Conv. Total (cfs) | 1801.0 | Conv. (cfs) | 960.3 | 837.4 |
| 3.4 | | | | |
| Length wtd. (ft) | 260.47 | wetted Per. (ft) | 86.54 | 16.70 |
| 10.05 | | | | |
| Min Ch El (ft) | 370.66 | Shear (lb/sq ft) | 0.24 | 0.66 |
| 0.03 | | | | |
| Alpha | 1.22 | Stream Power (lb/ft s) | 249.38 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 3.82 | Cum volume (acre-ft) | 0.22 | 0.29 |
| 0.03 | | | | |
| C & E Loss (ft) | 0.06 | Cum SA (acres) | 0.26 | 0.10 |
| 0.03 | | | | |

Warning: Divided flow computed for this cross-section.
 Warning: The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.
 Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.
 This may indicate the need for additional cross sections.
 Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

CROSS SECTION OUTPUT Profile #10 Yr

| | | Element | Left OB | Channel |
|----------------|--------|-------------------|---------|---------|
| E.G. Elev (ft) | 373.49 | | | |
| Right OB | | | | |
| Vel Head (ft) | 0.17 | wt. n-val. | 0.051 | 0.057 |
| 0.040 | | | | |
| W.S. Elev (ft) | 373.32 | Reach Len. (ft) | 259.00 | 261.00 |
| 263.00 | | | | |
| Crit w.s. (ft) | | Flow Area (sq ft) | 71.88 | 28.99 |

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| | | | | |
|--------------------|----------|------------------------|--------|--------|
| 5.23 | | | | |
| E.G. Slope (ft/ft) | 0.011655 | Area (sq ft) | 71.88 | 28.99 |
| 5.23 | | | | |
| Q Total (cfs) | 322.20 | Flow (cfs) | 196.88 | 117.82 |
| 7.49 | | | | |
| Top width (ft) | 141.52 | Top width (ft) | 101.13 | 15.88 |
| 24.51 | | | | |
| Vel Total (ft/s) | 3.04 | Avg. Vel. (ft/s) | 2.74 | 4.06 |
| 1.43 | | | | |
| Max Chl Dpth (ft) | 2.66 | Hydr. Depth (ft) | 0.71 | 1.83 |
| 0.21 | | | | |
| Conv. Total (cfs) | 2984.5 | Conv. (cfs) | 1823.7 | 1091.4 |
| 69.4 | | | | |
| Length wtd. (ft) | 260.20 | wetted Per. (ft) | 101.29 | 16.70 |
| 24.52 | | | | |
| Min Ch El (ft) | 370.66 | Shear (lb/sq ft) | 0.52 | 1.26 |
| 0.16 | | | | |
| Alpha | 1.16 | Stream Power (lb/ft s) | 249.38 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 3.70 | Cum Volume (acre-ft) | 0.59 | 0.43 |
| 0.21 | | | | |
| C & E Loss (ft) | 0.01 | Cum SA (acres) | 0.51 | 0.12 |
| 0.19 | | | | |

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

CROSS SECTION OUTPUT Profile #100 Yr

| | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 373.88 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.39 | wt. n-val. | 0.050 | 0.057 |
| 0.040 | | | | |
| W.S. Elev (ft) | 373.49 | Reach Len. (ft) | 259.00 | 261.00 |
| 263.00 | | | | |
| Crit w.s. (ft) | 373.49 | Flow Area (sq ft) | 90.09 | 31.69 |
| 10.44 | | | | |
| E.G. Slope (ft/ft) | 0.024403 | Area (sq ft) | 90.09 | 31.69 |
| 10.44 | | | | |
| Q Total (cfs) | 622.10 | Flow (cfs) | 398.87 | 197.79 |
| 25.44 | | | | |
| Top width (ft) | 167.00 | Top width (ft) | 112.72 | 15.88 |
| 38.40 | | | | |
| Vel Total (ft/s) | 4.70 | Avg. Vel. (ft/s) | 4.43 | 6.24 |
| 2.44 | | | | |
| Max Chl Dpth (ft) | 2.83 | Hydr. Depth (ft) | 0.80 | 2.00 |
| 0.27 | | | | |
| Conv. Total (cfs) | 3982.4 | Conv. (cfs) | 2553.3 | 1266.2 |
| 162.9 | | | | |
| Length wtd. (ft) | 260.11 | wetted Per. (ft) | 112.89 | 16.70 |
| 38.40 | | | | |
| Min Ch El (ft) | 370.66 | Shear (lb/sq ft) | 1.22 | 2.89 |
| 0.41 | | | | |
| Alpha | 1.14 | Stream Power (lb/ft s) | 249.38 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 1.64 | Cum Volume (acre-ft) | 1.27 | 0.59 |
| 0.62 | | | | |
| C & E Loss (ft) | 0.09 | Cum SA (acres) | 0.78 | 0.12 |
| 0.30 | | | | |

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
 Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.
 Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
 Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: JonesFalls
 REACH: SouthTrib RS: 1

CROSS SECTION OUTPUT Profile #2 Yr

| | | Element | Left OB | Channel |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 369.26 | | | |
| Right OB | | | | |
| Vel Head (ft) | 0.65 | wt. n-val. | 0.045 | 0.057 |
| W.S. Elev (ft) | 368.61 | Reach Len. (ft) | 93.43 | 93.43 |
| 93.43 | | | | |
| Crit w.s. (ft) | 368.61 | Flow Area (sq ft) | 0.03 | 23.53 |
| E.G. slope (ft/ft) | 0.046497 | Area (sq ft) | 0.03 | 23.53 |
| Q Total (cfs) | 151.70 | Flow (cfs) | 0.01 | 151.69 |
| Top width (ft) | 20.08 | Top width (ft) | 1.71 | 18.37 |
| Vel Total (ft/s) | 6.44 | Avg. vel. (ft/s) | 0.53 | 6.45 |
| Max Chl Dpth (ft) | 2.33 | Hydr. Depth (ft) | 0.02 | 1.28 |
| Conv. Total (cfs) | 703.5 | Conv. (cfs) | 0.1 | 703.4 |
| Length Wtd. (ft) | 93.43 | wetted Per. (ft) | 1.73 | 19.17 |
| Min Ch El (ft) | 366.28 | Shear (lb/sq ft) | 0.05 | 3.56 |
| Alpha | 1.00 | Stream Power (lb/ft s) | 312.19 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 0.92 | Cum volume (acre-ft) | 0.08 | 0.14 |
| 0.03 | | | | |
| C & E Loss (ft) | 0.08 | Cum SA (acres) | | |

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth

for the water surface and continued on with the calculations.

Warning: Divided flow computed for this cross-section.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION OUTPUT Profile #10 Yr

| | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 369.77 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.30 | wt. n-val. | 0.043 | 0.057 |
| 0.040 | | | | |
| W.S. Elev (ft) | 369.47 | Reach Len. (ft) | 93.43 | 93.43 |
| 93.43 | | | | |
| Crit w.s. (ft) | 369.47 | Flow Area (sq ft) | 32.46 | 41.40 |
| 10.78 | | | | |
| E.G. slope (ft/ft) | 0.017778 | Area (sq ft) | 32.46 | 41.40 |
| 10.78 | | | | |
| Q Total (cfs) | 322.20 | Flow (cfs) | 89.90 | 209.82 |
| 22.48 | | | | |
| Top width (ft) | 132.78 | Top width (ft) | 70.71 | 22.65 |
| 39.42 | | | | |
| Vel Total (ft/s) | 3.81 | Avg. Vel. (ft/s) | 2.77 | 5.07 |
| 2.09 | | | | |
| Max Chl Dpth (ft) | 3.19 | Hydr. Depth (ft) | 0.46 | 1.83 |
| 0.27 | | | | |
| Conv. Total (cfs) | 2416.5 | Conv. (cfs) | 674.3 | 1573.6 |
| 168.6 | | | | |
| Length wtd. (ft) | 93.43 | wetted Per. (ft) | 70.87 | 23.51 |
| 39.45 | | | | |
| Min Ch El (ft) | 366.28 | shear (lb/sq ft) | 0.51 | 1.95 |
| 0.30 | | | | |
| Alpha | 1.32 | Stream Power (lb/ft s) | 312.19 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 0.68 | Cum Volume (acre-ft) | 0.28 | 0.22 |
| 0.16 | | | | |
| C & E Loss (ft) | 0.01 | Cum SA (acres) | | |

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth

for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION OUTPUT Profile #100 Yr

| | | | | |
|----------------|--------|---------|---------|---------|
| E.G. Elev (ft) | 370.64 | Element | Left OB | Channel |
|----------------|--------|---------|---------|---------|

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| | | | | |
|--------------------|----------|------------------------|--------|--------|
| Right OB | | | | |
| Vel Head (ft) | 0.08 | Wt. n-val. | 0.042 | 0.057 |
| 0.040 | | | | |
| W.S. Elev (ft) | 370.55 | Reach Len. (ft) | 93.43 | 93.43 |
| 93.43 | | | | |
| Crit w.s. (ft) | | Flow Area (sq ft) | 144.43 | 65.89 |
| 64.65 | | | | |
| E.G. slope (ft/ft) | 0.002841 | Area (sq ft) | 144.43 | 65.89 |
| 64.65 | | | | |
| Q Total (cfs) | 622.10 | Flow (cfs) | 309.04 | 182.00 |
| 131.06 | | | | |
| Top width (ft) | 236.14 | Top width (ft) | 151.12 | 22.65 |
| 62.37 | | | | |
| Vel Total (ft/s) | 2.26 | Avg. vel. (ft/s) | 2.14 | 2.76 |
| 2.03 | | | | |
| Max Chl Dpth (ft) | 4.27 | Hydr. Depth (ft) | 0.96 | 2.91 |
| 1.04 | | | | |
| Conv. Total (cfs) | 11670.5 | Conv. (cfs) | 5797.5 | 3414.4 |
| 2458.6 | | | | |
| Length wtd. (ft) | 93.43 | wetted Per. (ft) | 151.41 | 23.51 |
| 62.42 | | | | |
| Min Ch El (ft) | 366.28 | Shear (lb/sq ft) | 0.17 | 0.50 |
| 0.18 | | | | |
| Alpha | 1.05 | Stream Power (lb/ft s) | 312.19 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 0.54 | Cum Volume (acre-ft) | 0.58 | 0.30 |
| 0.39 | | | | |
| C & E Loss (ft) | 0.04 | Cum SA (acres) | | |

CROSS SECTION

RIVER: JonesFalls
 REACH: IntsTrib RS: 8

CROSS SECTION OUTPUT Profile #2 Yr

| | | | | |
|--------------------|----------|-------------------|---------|---------|
| E.G. Elev (ft) | 392.96 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.34 | Wt. n-val. | | 0.046 |
| W.S. Elev (ft) | 392.61 | Reach Len. (ft) | 135.00 | 134.00 |
| 134.00 | | | | |
| Crit w.s. (ft) | 392.61 | Flow Area (sq ft) | | 14.12 |
| E.G. slope (ft/ft) | 0.035629 | Area (sq ft) | | 14.12 |
| Q Total (cfs) | 66.30 | Flow (cfs) | | 66.30 |
| Top width (ft) | 20.71 | Top width (ft) | | 20.71 |
| Vel Total (ft/s) | 4.70 | Avg. vel. (ft/s) | | 4.70 |
| Max Chl Dpth (ft) | 1.31 | Hydr. Depth (ft) | | 0.68 |
| Conv. Total (cfs) | 351.2 | Conv. (cfs) | | 351.2 |
| Length wtd. (ft) | 134.00 | wetted Per. (ft) | | 20.88 |

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| | | | | |
|-------------------------|--------|------------------------|--------|------|
| Min Ch El (ft) | 391.30 | Shear (lb/sq ft) | | 1.50 |
| Alpha 0.00 | 1.00 | Stream Power (lb/ft s) | 456.60 | 0.00 |
| Frctn Loss (ft) 0.80 | 4.41 | Cum Volume (acre-ft) | 0.62 | 0.73 |
| C & E Loss (ft) 0.05 | 0.02 | Cum SA (acres) | 0.00 | 0.45 |

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth

for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION OUTPUT Profile #10 Yr

| | | | | |
|---------------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 393.55 | Element | Left OB | Channel |
| Right OB Vel Head (ft) | 0.47 | wt. n-Val. | | 0.046 |
| W.S. Elev (ft) 134.00 | 393.08 | Reach Len. (ft) | 135.00 | 134.00 |
| Crit w.s. (ft) | 393.08 | Flow Area (sq ft) | | 25.30 |
| E.G. Slope (ft/ft) | 0.032574 | Area (sq ft) | | 25.30 |
| Q Total (cfs) | 138.90 | Flow (cfs) | | 138.90 |
| Top width (ft) | 27.44 | Top width (ft) | | 27.44 |
| Vel Total (ft/s) | 5.49 | Avg. Vel. (ft/s) | | 5.49 |
| Max Chl Dpth (ft) | 1.78 | Hydr. Depth (ft) | | 0.92 |
| Conv. Total (cfs) | 769.6 | Conv. (cfs) | | 769.6 |
| Length wtd. (ft) | 134.04 | wetted Per. (ft) | | 27.67 |
| Min Ch El (ft) | 391.30 | Shear (lb/sq ft) | | 1.86 |
| Alpha 0.00 | 1.00 | Stream Power (lb/ft s) | 456.60 | 0.00 |
| Frctn Loss (ft) 1.65 | 0.39 | Cum Volume (acre-ft) | 1.13 | 1.20 |
| C & E Loss (ft) 0.69 | 0.13 | Cum SA (acres) | 0.13 | 0.52 |

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth

for the water surface and continued on with the calculations.

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

This may indicate the need for additional cross sections.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION OUTPUT Profile #100 Yr

| | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 394.86 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.12 | wt. n-Val. | 0.045 | 0.046 |
| 0.045 | | | | |
| W.S. Elev (ft) | 394.74 | Reach Len. (ft) | 135.00 | 134.00 |
| 134.00 | | | | |
| Crit w.s. (ft) | | Flow Area (sq ft) | 10.28 | 87.00 |
| 3.85 | | | | |
| E.G. Slope (ft/ft) | 0.002877 | Area (sq ft) | 10.28 | 87.00 |
| 3.85 | | | | |
| Q Total (cfs) | 261.20 | Flow (cfs) | 9.40 | 248.28 |
| 3.52 | | | | |
| Top Width (ft) | 78.90 | Top width (ft) | 27.71 | 40.80 |
| 10.39 | | | | |
| Vel Total (ft/s) | 2.58 | Avg. Vel. (ft/s) | 0.91 | 2.85 |
| 0.91 | | | | |
| Max Chl Dpth (ft) | 3.44 | Hydr. Depth (ft) | 0.37 | 2.13 |
| 0.37 | | | | |
| Conv. Total (cfs) | 4869.5 | Conv. (cfs) | 175.2 | 4628.7 |
| 65.6 | | | | |
| Length wtd. (ft) | 134.12 | wetted Per. (ft) | 27.72 | 41.16 |
| 10.41 | | | | |
| Min Ch El (ft) | 391.30 | Shear (lb/sq ft) | 0.07 | 0.38 |
| 0.07 | | | | |
| Alpha | 1.17 | Stream Power (lb/ft s) | 456.60 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 0.02 | Cum Volume (acre-ft) | 3.09 | 2.44 |
| 4.05 | | | | |
| C & E Loss (ft) | 0.03 | Cum SA (acres) | 1.33 | 0.58 |
| 1.21 | | | | |

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

This may indicate the need for additional cross sections.

CROSS SECTION

RIVER: JonesFalls
 REACH: IntsTrib RS: 7

CROSS SECTION OUTPUT Profile #2 Yr

| | | | | |
|----------------|--------|---------|---------|---------|
| E.G. Elev (ft) | 388.31 | Element | Left OB | Channel |
|----------------|--------|---------|---------|---------|

EcclestonMod.rep

| | | | | |
|--------------------|----------|------------------------|--------|--------|
| Right OB | | | | |
| Vel Head (ft) | 0.53 | Wt. n-val. | | 0.046 |
| 0.046 | | | | |
| W.S. Elev (ft) | 387.79 | Reach Len. (ft) | 151.00 | 152.00 |
| 154.00 | | | | |
| Crit w.s. (ft) | 387.79 | Flow Area (sq ft) | | 11.20 |
| 0.50 | | | | |
| E.G. slope (ft/ft) | 0.030520 | Area (sq ft) | | 11.20 |
| 0.50 | | | | |
| Q Total (cfs) | 66.30 | Flow (cfs) | | 65.53 |
| 0.77 | | | | |
| Top width (ft) | 12.60 | Top width (ft) | | 9.11 |
| 3.49 | | | | |
| Vel Total (ft/s) | 5.67 | Avg. vel. (ft/s) | | 5.85 |
| 1.54 | | | | |
| Max Chl Dpth (ft) | 1.59 | Hydr. Depth (ft) | | 1.23 |
| 0.14 | | | | |
| Conv. Total (cfs) | 379.5 | Conv. (cfs) | | 375.1 |
| 4.4 | | | | |
| Length wtd. (ft) | 152.00 | wetted Per. (ft) | | 10.62 |
| 3.50 | | | | |
| Min Ch El (ft) | 386.20 | Shear (lb/sq ft) | | 2.01 |
| 0.27 | | | | |
| Alpha | 1.05 | Stream Power (lb/ft s) | 292.30 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | | Cum Volume (acre-ft) | 0.62 | 0.69 |
| 0.80 | | | | |
| C & E Loss (ft) | | Cum SA (acres) | 0.00 | 0.40 |
| 0.04 | | | | |

Warning: During subcritical analysis, the water surface upstream of culvert went to critical depth.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION OUTPUT Profile #10 Yr

| | | | | |
|--------------------|----------|-------------------|---------|---------|
| E.G. Elev (ft) | 390.17 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.05 | Wt. n-val. | 0.045 | 0.046 |
| 0.045 | | | | |
| W.S. Elev (ft) | 390.12 | Reach Len. (ft) | 151.00 | 152.00 |
| 154.00 | | | | |
| Crit w.s. (ft) | 388.53 | Flow Area (sq ft) | 11.46 | 33.16 |
| 42.54 | | | | |
| E.G. slope (ft/ft) | 0.001015 | Area (sq ft) | 11.47 | 33.16 |
| 42.54 | | | | |
| Q Total (cfs) | 138.90 | Flow (cfs) | 10.07 | 71.55 |
| 57.28 | | | | |
| Top width (ft) | 59.09 | Top width (ft) | 17.36 | 9.40 |
| 32.33 | | | | |
| Vel Total (ft/s) | 1.59 | Avg. vel. (ft/s) | 0.88 | 2.16 |
| 1.35 | | | | |
| Max Chl Dpth (ft) | 3.92 | Hydr. Depth (ft) | 0.71 | 3.53 |
| 1.32 | | | | |
| Conv. Total (cfs) | 4359.1 | Conv. (cfs) | 315.9 | 2245.5 |
| 1797.7 | | | | |
| Length wtd. (ft) | 152.00 | wetted Per. (ft) | 16.42 | 10.93 |
| 32.44 | | | | |
| Min Ch El (ft) | 386.20 | Shear (lb/sq ft) | 0.04 | 0.19 |

EcclestonMod.rep

| | | | | |
|-----------------|------|------------------------|--------|------|
| 0.08 | | | | |
| Alpha | 1.26 | Stream Power (lb/ft s) | 292.30 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | | Cum Volume (acre-ft) | 1.11 | 1.11 |
| 1.58 | | | | |
| C & E Loss (ft) | | Cum SA (acres) | 0.10 | 0.46 |
| 0.64 | | | | |

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION OUTPUT Profile #100 Yr

| | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 394.81 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.01 | wt. n-val. | 0.045 | 0.046 |
| 0.045 | | | | |
| W.S. Elev (ft) | 394.81 | Reach Len. (ft) | 151.00 | 152.00 |
| 154.00 | | | | |
| Crit w.s. (ft) | 389.18 | Flow Area (sq ft) | 87.25 | 77.19 |
| 301.53 | | | | |
| E.G. slope (ft/ft) | 0.000035 | Area (sq ft) | 619.25 | 77.19 |
| 301.78 | | | | |
| Q Total (cfs) | 261.20 | Flow (cfs) | 52.11 | 54.51 |
| 154.58 | | | | |
| Top width (ft) | 269.77 | Top width (ft) | 185.35 | 9.40 |
| 75.02 | | | | |
| Vel Total (ft/s) | 0.56 | Avg. vel. (ft/s) | 0.60 | 0.71 |
| 0.51 | | | | |
| Max Chl Dpth (ft) | 8.61 | Hydr. Depth (ft) | 5.39 | 8.21 |
| 4.13 | | | | |
| Conv. Total (cfs) | 43990.9 | Conv. (cfs) | 8776.3 | 9179.8 |
| 26034.8 | | | | |
| Length wtd. (ft) | 152.00 | wetted Per. (ft) | 16.42 | 10.93 |
| 73.43 | | | | |
| Min Ch El (ft) | 386.20 | Shear (lb/sq ft) | 0.01 | 0.02 |
| 0.01 | | | | |
| Alpha | 1.05 | Stream Power (lb/ft s) | 292.30 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | | Cum volume (acre-ft) | 2.11 | 2.19 |
| 3.58 | | | | |
| C & E Loss (ft) | | Cum SA (acres) | 1.00 | 0.51 |
| 1.08 | | | | |

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CULVERT

RIVER: JonesFalls
 REACH: IntsTrib RS: 6.5

CULVERT OUTPUT Profile #2 Yr Culv Group: GrnsprngVal

| | | | |
|--------------------|-------|--------------------|------|
| Q Culv Group (cfs) | 66.30 | Culv Full Len (ft) | |
| # Barrels | 1 | Culv Vel US (ft/s) | 7.54 |

| EcclestonMod.rep | | | |
|---------------------|--------|------------------------|--------|
| Q Barrel (cfs) | 66.30 | Culv Vel DS (ft/s) | 17.60 |
| E.G. US. (ft) | 388.16 | Culv Inv El Up (ft) | 384.54 |
| W.S. US. (ft) | 387.79 | Culv Inv El Dn (ft) | 378.86 |
| E.G. DS (ft) | 381.08 | Culv Frctn Ls (ft) | 2.81 |
| W.S. DS (ft) | 380.98 | Culv Exit Loss (ft) | 3.83 |
| Delta EG (ft) | 7.08 | Culv Entr Loss (ft) | 0.44 |
| Delta WS (ft) | 6.80 | Q Weir (cfs) | |
| E.G. IC (ft) | 387.71 | Weir Sta Lft (ft) | |
| E.G. OC (ft) | 388.16 | Weir Sta Rgt (ft) | |
| Culvert Control | Outlet | Weir Submerg | |
| Culv WS Inlet (ft) | 386.84 | Weir Max Depth (ft) | |
| Culv WS Outlet (ft) | 380.09 | Weir Avg Depth (ft) | |
| Culv Nml Depth (ft) | 1.15 | Weir Flow Area (sq ft) | |
| Culv Crt Depth (ft) | 2.30 | Min El Weir Flow (ft) | 395.01 |

Warning: During subcritical analysis, the water surface upstream of culvert went to critical depth.

Warning: Since the culvert has supercritical flow, the program should be run in mixed flow in order to check if the cross section

downstream of the culvert has supercritical flow.

Note: The flow in the culvert is entirely supercritical.

CULVERT OUTPUT Profile #10 Yr Culv Group: GrnsprngVal

| | | | |
|---------------------|--------|------------------------|--------|
| Q Culv Group (cfs) | 138.90 | Culv Full Len (ft) | |
| # Barrels | 1 | Culv Vel US (ft/s) | 9.85 |
| Q Barrel (cfs) | 138.90 | Culv Vel DS (ft/s) | 20.21 |
| E.G. US. (ft) | 390.17 | Culv Inv El Up (ft) | 384.54 |
| W.S. US. (ft) | 390.12 | Culv Inv El Dn (ft) | 378.86 |
| E.G. DS (ft) | 381.88 | Culv Frctn Ls (ft) | 2.31 |
| W.S. DS (ft) | 381.69 | Culv Exit Loss (ft) | 5.23 |
| Delta EG (ft) | 8.29 | Culv Entr Loss (ft) | 0.75 |
| Delta WS (ft) | 8.43 | Q Weir (cfs) | |
| E.G. IC (ft) | 389.79 | Weir Sta Lft (ft) | |
| E.G. OC (ft) | 390.17 | Weir Sta Rgt (ft) | |
| Culvert Control | Outlet | Weir Submerg | |
| Culv WS Inlet (ft) | 387.92 | Weir Max Depth (ft) | |
| Culv WS Outlet (ft) | 380.77 | Weir Avg Depth (ft) | |
| Culv Nml Depth (ft) | 1.68 | Weir Flow Area (sq ft) | |
| Culv Crt Depth (ft) | 3.38 | Min El Weir Flow (ft) | 395.01 |

Warning: Since the culvert has supercritical flow, the program should be run in mixed flow in order to check if the cross section

downstream of the culvert has supercritical flow.

Note: The flow in the culvert is entirely supercritical.

CULVERT OUTPUT Profile #100 Yr Culv Group: GrnsprngVal

| | | | |
|--------------------|--------|---------------------|--------|
| Q Culv Group (cfs) | 261.20 | Culv Full Len (ft) | |
| # Barrels | 1 | Culv Vel US (ft/s) | 13.30 |
| Q Barrel (cfs) | 261.20 | Culv Vel DS (ft/s) | 24.10 |
| E.G. US. (ft) | 394.81 | Culv Inv El Up (ft) | 384.54 |
| W.S. US. (ft) | 394.81 | Culv Inv El Dn (ft) | 378.86 |
| E.G. DS (ft) | 382.88 | Culv Frctn Ls (ft) | 2.86 |
| W.S. DS (ft) | 382.54 | Culv Exit Loss (ft) | 7.70 |
| Delta EG (ft) | 11.93 | Culv Entr Loss (ft) | 1.37 |
| Delta WS (ft) | 12.27 | Q Weir (cfs) | |
| E.G. IC (ft) | 394.81 | Weir Sta Lft (ft) | |
| E.G. OC (ft) | 393.63 | Weir Sta Rgt (ft) | |
| Culvert Control | Inlet | Weir Submerg | |
| Culv WS Inlet (ft) | 389.54 | Weir Max Depth (ft) | |

EcclestonMod.rep

| | | | |
|---------------------|--------|------------------------|--------|
| Culv WS Outlet (ft) | 381.56 | Weir Avg Depth (ft) | |
| Culv Nml Depth (ft) | 2.37 | Weir Flow Area (sq ft) | |
| Culv Crt Depth (ft) | 4.49 | Min El Weir Flow (ft) | 395.01 |

Warning: Since the culvert has supercritical flow, the program should be run in mixed flow in order to check if the cross section downstream of the culvert has supercritical flow.
 Note: The flow in the culvert is entirely supercritical.

CROSS SECTION

RIVER: JonesFalls
 REACH: IntsTrib RS: 6

CROSS SECTION OUTPUT Profile #2 Yr

| | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 381.08 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.09 | wt. n-val. | 0.040 | 0.046 |
| 0.040 | | | | |
| W.S. Elev (ft) | 380.98 | Reach Len. (ft) | 117.00 | 118.00 |
| 119.00 | | | | |
| Crit w.s. (ft) | 380.06 | Flow Area (sq ft) | 0.33 | 26.60 |
| 0.05 | | | | |
| E.G. Slope (ft/ft) | 0.003314 | Area (sq ft) | 0.39 | 26.60 |
| 0.05 | | | | |
| Q Total (cfs) | 66.30 | Flow (cfs) | 0.36 | 65.92 |
| 0.02 | | | | |
| Top width (ft) | 18.43 | Top width (ft) | 1.40 | 16.61 |
| 0.42 | | | | |
| Vel Total (ft/s) | 2.46 | Avg. Vel. (ft/s) | 1.10 | 2.48 |
| 0.47 | | | | |
| Max Chl Dpth (ft) | 2.32 | Hydr. Depth (ft) | 0.40 | 1.60 |
| 0.12 | | | | |
| Conv. Total (cfs) | 1151.6 | Conv. (cfs) | 6.2 | 1145.0 |
| 0.4 | | | | |
| Length wtd. (ft) | 118.00 | wetted Per. (ft) | 0.88 | 17.29 |
| 0.48 | | | | |
| Min Ch El (ft) | 378.66 | Shear (lb/sq ft) | 0.08 | 0.32 |
| 0.02 | | | | |
| Alpha | 1.01 | Stream Power (lb/ft s) | 318.42 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 0.74 | Cum Volume (acre-ft) | 0.62 | 0.66 |
| 0.80 | | | | |
| C & E Loss (ft) | 0.04 | Cum SA (acres) | 0.00 | 0.36 |
| 0.03 | | | | |

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.
 This may indicate the need for additional cross sections.
 Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION OUTPUT Profile #10 Yr

| | | | | |
|----------------|--------|---------|---------|---------|
| E.G. Elev (ft) | 381.88 | Element | Left OB | Channel |
|----------------|--------|---------|---------|---------|

EcclestonMod.rep

| | | | | |
|--------------------|----------|------------------------|--------|--------|
| Right OB | | | | |
| Vel Head (ft) | 0.19 | wt. n-val. | 0.040 | 0.046 |
| 0.040 | | | | |
| W.S. Elev (ft) | 381.69 | Reach Len. (ft) | 117.00 | 118.00 |
| 119.00 | | | | |
| Crit w.s. (ft) | 380.68 | Flow Area (sq ft) | 0.91 | 38.43 |
| 0.81 | | | | |
| E.G. Slope (ft/ft) | 0.004116 | Area (sq ft) | 2.02 | 38.43 |
| 0.81 | | | | |
| Q Total (cfs) | 138.90 | Flow (cfs) | 2.21 | 135.62 |
| 1.07 | | | | |
| Top width (ft) | 21.50 | Top width (ft) | 3.17 | 16.61 |
| 1.71 | | | | |
| Vel Total (ft/s) | 3.46 | Avg. Vel. (ft/s) | 2.43 | 3.53 |
| 1.32 | | | | |
| Max Chl Dpth (ft) | 3.03 | Hydr. Depth (ft) | 1.11 | 2.31 |
| 0.47 | | | | |
| Conv. Total (cfs) | 2165.0 | Conv. (cfs) | 34.5 | 2113.8 |
| 16.7 | | | | |
| Length wtd. (ft) | 117.99 | wetted Per. (ft) | 0.88 | 17.29 |
| 1.96 | | | | |
| Min Ch El (ft) | 378.66 | Shear (lb/sq ft) | 0.26 | 0.57 |
| 0.11 | | | | |
| Alpha | 1.02 | Stream Power (lb/ft s) | 318.42 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 0.87 | Cum Volume (acre-ft) | 1.11 | 1.03 |
| 1.58 | | | | |
| C & E Loss (ft) | 0.05 | Cum SA (acres) | 0.07 | 0.42 |
| 0.58 | | | | |

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

This may indicate the need for additional cross sections.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION OUTPUT Profile #100 Yr

| | | | | |
|--------------------|----------|-------------------|---------|---------|
| E.G. Elev (ft) | 382.88 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.34 | wt. n-val. | 0.040 | 0.046 |
| 0.040 | | | | |
| W.S. Elev (ft) | 382.54 | Reach Len. (ft) | 117.00 | 118.00 |
| 119.00 | | | | |
| Crit w.s. (ft) | 381.37 | Flow Area (sq ft) | 1.60 | 52.48 |
| 2.91 | | | | |
| E.G. Slope (ft/ft) | 0.004894 | Area (sq ft) | 5.60 | 52.48 |
| 2.91 | | | | |
| Q Total (cfs) | 261.20 | Flow (cfs) | 6.20 | 248.58 |
| 6.42 | | | | |
| Top width (ft) | 25.14 | Top width (ft) | 5.28 | 16.61 |
| 3.25 | | | | |
| Vel Total (ft/s) | 4.58 | Avg. Vel. (ft/s) | 3.87 | 4.74 |
| 2.21 | | | | |
| Max Chl Dpth (ft) | 3.88 | Hydr. Depth (ft) | 1.96 | 3.16 |
| 0.90 | | | | |
| Conv. Total (cfs) | 3733.9 | Conv. (cfs) | 88.6 | 3553.4 |
| 91.8 | | | | |
| Length wtd. (ft) | 117.99 | wetted Per. (ft) | 0.88 | 17.29 |
| 3.71 | | | | |

| EcclestonMod.rep | | | | |
|------------------|--------|------------------------|--------|------|
| Min Ch El (ft) | 378.66 | Shear (lb/sq ft) | 0.55 | 0.93 |
| 0.24 | | | | |
| Alpha | 1.04 | Stream Power (lb/ft s) | 318.42 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 1.09 | Cum volume (acre-ft) | 2.11 | 1.59 |
| 3.58 | | | | |
| C & E Loss (ft) | 0.10 | Cum SA (acres) | 0.67 | 0.46 |
| 0.94 | | | | |

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

This may indicate the need for additional cross sections.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION

RIVER: JonesFalls
 REACH: IntsTrib RS: 5

CROSS SECTION OUTPUT Profile #2 Yr

| | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 380.30 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.22 | wt. n-val. | | 0.046 |
| W.S. Elev (ft) | 380.08 | Reach Len. (ft) | 363.00 | 358.00 |
| 354.00 | | | | |
| Crit w.s. (ft) | 379.85 | Flow Area (sq ft) | | 17.59 |
| E.G. Slope (ft/ft) | 0.015759 | Area (sq ft) | | 17.59 |
| Q Total (cfs) | 66.30 | Flow (cfs) | | 66.30 |
| Top width (ft) | 19.28 | Top width (ft) | | 19.28 |
| Vel Total (ft/s) | 3.77 | Avg. Vel. (ft/s) | | 3.77 |
| Max Chl Dpth (ft) | 1.66 | Hydr. Depth (ft) | | 0.91 |
| Conv. Total (cfs) | 528.1 | Conv. (cfs) | | 528.1 |
| Length wtd. (ft) | 358.00 | wetted Per. (ft) | | 19.62 |
| Min Ch El (ft) | 378.42 | Shear (lb/sq ft) | | 0.88 |
| Alpha | 1.00 | Stream Power (lb/ft s) | 285.71 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 8.01 | Cum volume (acre-ft) | 0.62 | 0.60 |
| 0.80 | | | | |
| C & E Loss (ft) | 0.02 | Cum SA (acres) | | 0.31 |
| 0.03 | | | | |

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

This may indicate the need for additional cross sections.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, energy was used.

CROSS SECTION OUTPUT Profile #10 Yr

| | | | | |
|---------------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 380.96 | Element | Left OB | Channel |
| Right OB Vel Head (ft) | 0.36 | wt. n-val. | 0.040 | 0.046 |
| W.S. Elev (ft) | 380.60 | Reach Len. (ft) | 363.00 | 358.00 |
| 354.00 Crit w.s. (ft) | 380.36 | Flow Area (sq ft) | 0.28 | 28.59 |
| E.G. slope (ft/ft) | 0.016866 | Area (sq ft) | 0.28 | 28.59 |
| Q Total (cfs) | 138.90 | Flow (cfs) | 0.29 | 138.61 |
| Top width (ft) | 25.38 | Top width (ft) | 2.81 | 22.58 |
| Vel Total (ft/s) | 4.81 | Avg. Vel. (ft/s) | 1.04 | 4.85 |
| Max Chl Dpth (ft) | 2.18 | Hydr. Depth (ft) | 0.10 | 1.27 |
| Conv. Total (cfs) | 1069.5 | Conv. (cfs) | 2.3 | 1067.3 |
| Length wtd. (ft) | 358.01 | wetted Per. (ft) | 2.81 | 23.02 |
| Min Ch El (ft) | 378.42 | Shear (lb/sq ft) | 0.11 | 1.31 |
| Alpha 0.00 | 1.01 | Stream Power (lb/ft s) | 285.71 | 0.00 |
| Frctn Loss (ft) | 8.00 | Cum Volume (acre-ft) | 1.11 | 0.94 |
| 1.58 C & E Loss (ft) | 0.02 | Cum SA (acres) | 0.06 | 0.37 |
| 0.58 | | | | |

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, energy was used.

CROSS SECTION OUTPUT Profile #100 Yr

| | | | | |
|---------------------------|----------|-------------------|---------|---------|
| E.G. Elev (ft) | 381.69 | Element | Left OB | Channel |
| Right OB Vel Head (ft) | 0.68 | wt. n-val. | 0.040 | 0.046 |
| W.S. Elev (ft) | 381.01 | Reach Len. (ft) | 363.00 | 358.00 |
| 354.00 Crit w.s. (ft) | 381.01 | Flow Area (sq ft) | 2.60 | 38.07 |
| E.G. slope (ft/ft) | 0.023771 | Area (sq ft) | 3.92 | 38.07 |

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| | | | | |
|-------------------|--------|------------------------|--------|--------|
| Q Total (cfs) | 261.20 | Flow (cfs) | 6.50 | 254.70 |
| Top width (ft) | 54.47 | Top width (ft) | 30.53 | 23.95 |
| Vel Total (ft/s) | 6.42 | Avg. Vel. (ft/s) | 2.50 | 6.69 |
| Max Chl Dpth (ft) | 2.59 | Hydr. Depth (ft) | 0.29 | 1.59 |
| Conv. Total (cfs) | 1694.1 | Conv. (cfs) | 42.1 | 1652.0 |
| Length wtd. (ft) | 358.15 | wetted Per. (ft) | 9.03 | 24.45 |
| Min Ch El (ft) | 378.42 | Shear (lb/sq ft) | 0.43 | 2.31 |
| Alpha | 1.06 | Stream Power (lb/ft s) | 285.71 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 7.60 | Cum Volume (acre-ft) | 2.10 | 1.47 |
| 3.58 | | | | |
| C & E Loss (ft) | 0.04 | Cum SA (acres) | 0.62 | 0.41 |
| 0.93 | | | | |

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth

for the water surface and continued on with the calculations.

Warning: Divided flow computed for this cross-section.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, energy was used.

CROSS SECTION

RIVER: JonesFalls

REACH: IntsTrib RS: 4

CROSS SECTION OUTPUT Profile #2 Yr

| | | | | |
|--------------------|----------|-------------------|---------|---------|
| E.G. Elev (ft) | 372.27 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.39 | wt. n-val. | | 0.046 |
| w.s. Elev (ft) | 371.88 | Reach Len. (ft) | 188.00 | 207.00 |
| 219.00 | | | | |
| Crit w.s. (ft) | 371.88 | Flow Area (sq ft) | | 13.27 |
| E.G. slope (ft/ft) | 0.034227 | Area (sq ft) | | 13.27 |
| Q Total (cfs) | 66.30 | Flow (cfs) | | 66.30 |
| Top width (ft) | 17.10 | Top width (ft) | | 17.10 |

| | | | |
|-------------------|--------|------------------------|--------|
| Vel Total (ft/s) | 5.00 | Avg. Vel. (ft/s) | 5.00 |
| Max Chl Dpth (ft) | 1.48 | Hydr. Depth (ft) | 0.78 |
| Conv. Total (cfs) | 358.4 | Conv. (cfs) | 358.4 |
| Length wtd. (ft) | 207.00 | wetted Per. (ft) | 17.37 |
| Min Ch El (ft) | 370.40 | Shear (lb/sq ft) | 1.63 |
| Alpha | 1.00 | Stream Power (lb/ft s) | 253.75 |
| 0.00 | | | |
| Frctn Loss (ft) | 2.52 | Cum Volume (acre-ft) | 0.62 |
| 0.80 | | | |
| C & E Loss (ft) | 0.06 | Cum SA (acres) | 0.16 |
| 0.03 | | | |

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, energy was used.

CROSS SECTION OUTPUT Profile #10 Yr

| | | | | |
|--------------------|----------|-------------------|---------|---------|
| E.G. Elev (ft) | 372.94 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.53 | wt. n-Val. | | 0.046 |
| W.S. Elev (ft) | 372.41 | Reach Len. (ft) | 188.00 | 207.00 |
| 219.00 | | | | |
| Crit W.S. (ft) | 372.41 | Flow Area (sq ft) | | 23.67 |
| E.G. Slope (ft/ft) | 0.031022 | Area (sq ft) | | 23.67 |
| Q Total (cfs) | 138.90 | Flow (cfs) | | 138.90 |
| Top Width (ft) | 22.23 | Top Width (ft) | | 22.23 |
| Vel Total (ft/s) | 5.87 | Avg. Vel. (ft/s) | | 5.87 |
| Max Chl Dpth (ft) | 2.01 | Hydr. Depth (ft) | | 1.06 |
| Conv. Total (cfs) | 788.6 | Conv. (cfs) | | 788.6 |
| Length wtd. (ft) | 206.53 | wetted Per. (ft) | | 22.61 |
| Min Ch El (ft) | 370.40 | Shear (lb/sq ft) | | 2.03 |

| EcclestonMod.rep | | | | |
|------------------|------|------------------------|--------|------|
| Alpha | 1.00 | Stream Power (lb/ft s) | 253.75 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 1.77 | Cum Volume (acre-ft) | 1.11 | 0.72 |
| 1.58 | | | | |
| C & E Loss (ft) | 0.11 | Cum SA (acres) | 0.05 | 0.18 |
| 0.58 | | | | |

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, energy was used.

CROSS SECTION OUTPUT Profile #100 Yr

| | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 373.70 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.54 | wt. n-Val. | 0.040 | 0.046 |
| W.S. Elev (ft) | 373.15 | Reach Len. (ft) | 188.00 | 207.00 |
| 219.00 | | | | |
| Crit W.S. (ft) | 373.15 | Flow Area (sq ft) | 4.67 | 42.00 |
| E.G. Slope (ft/ft) | 0.019080 | Area (sq ft) | 4.67 | 42.00 |
| Q Total (cfs) | 261.20 | Flow (cfs) | 8.71 | 252.49 |
| Top width (ft) | 47.64 | Top width (ft) | 21.24 | 26.39 |
| Vel Total (ft/s) | 5.60 | Avg. Vel. (ft/s) | 1.87 | 6.01 |
| Max Chl Dpth (ft) | 2.75 | Hydr. Depth (ft) | 0.22 | 1.59 |
| Conv. Total (cfs) | 1890.9 | Conv. (cfs) | 63.1 | 1827.9 |
| Length Wtd. (ft) | 208.99 | wetted Per. (ft) | 21.27 | 26.86 |
| Min Ch El (ft) | 370.40 | Shear (lb/sq ft) | 0.26 | 1.86 |
| Alpha | 1.12 | Stream Power (lb/ft s) | 253.75 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 0.06 | Cum Volume (acre-ft) | 2.06 | 1.14 |
| 3.58 | | | | |
| C & E Loss (ft) | 0.16 | Cum SA (acres) | 0.41 | 0.20 |
| 0.93 | | | | |

Warning: The energy equation could not be balanced within the specified number of iterations.
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iterations. The program used critical depth for the water surface and continued on with the calculations.
 Warning: The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.
 Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.
 Warning: The energy loss was greater than 1.0 ft (0.3 m) between the current and previous cross section. This may indicate the need for additional cross sections.
 Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.
 Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, energy was used.

CROSS SECTION

RIVER: JonesFalls
 REACH: IntsTrib RS: 3

CROSS SECTION OUTPUT Profile #2 Yr

| | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 367.47 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.19 | wt. n-val. | | 0.046 |
| W.S. Elev (ft) | 367.28 | Reach Len. (ft) | 112.00 | 116.00 |
| 119.00 | | | | |
| Crit w.s. (ft) | 365.59 | Flow Area (sq ft) | | 19.11 |
| E.G. slope (ft/ft) | 0.006169 | Area (sq ft) | | 19.11 |
| Q Total (cfs) | 66.30 | Flow (cfs) | | 66.30 |
| Top width (ft) | 6.16 | Top width (ft) | | 6.16 |
| Vel Total (ft/s) | 3.47 | Avg. vel. (ft/s) | | 3.47 |
| Max Chl Dpth (ft) | 3.42 | Hydr. Depth (ft) | | 3.10 |
| Conv. Total (cfs) | 844.1 | Conv. (cfs) | | 844.1 |
| Length wtd. (ft) | 116.00 | wetted Per. (ft) | | 11.95 |
| Min Ch El (ft) | 363.86 | Shear (lb/sq ft) | | 0.62 |
| Alpha | 1.00 | Stream Power (lb/ft s) | 446.13 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | | Cum volume (acre-ft) | 0.62 | 0.40 |
| 0.80 | | | | |
| C & E Loss (ft) | | Cum SA (acres) | | 0.11 |
| 0.03 | | | | |

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

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CROSS SECTION OUTPUT Profile #10 Yr

| | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 369.49 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.18 | wt. n-val. | 0.046 | 0.046 |
| 0.042 | | | | |
| W.S. Elev (ft) | 369.31 | Reach Len. (ft) | 112.00 | 116.00 |
| 119.00 | | | | |
| Crit w.s. (ft) | 366.65 | Flow Area (sq ft) | 8.25 | 31.99 |
| 4.36 | | | | |
| E.G. slope (ft/ft) | 0.003947 | Area (sq ft) | 8.32 | 31.99 |
| 30.22 | | | | |
| Q Total (cfs) | 138.90 | Flow (cfs) | 13.35 | 115.24 |
| 10.31 | | | | |
| Top width (ft) | 91.80 | Top width (ft) | 12.73 | 6.42 |
| 72.65 | | | | |
| Vel Total (ft/s) | 3.11 | Avg. vel. (ft/s) | 1.62 | 3.60 |
| 2.36 | | | | |
| Max Chl Dpth (ft) | 5.45 | Hydr. Depth (ft) | 0.72 | 4.98 |
| 1.08 | | | | |
| Conv. Total (cfs) | 2210.8 | Conv. (cfs) | 212.6 | 1834.2 |
| 164.0 | | | | |
| Length wtd. (ft) | 116.00 | wetted Per. (ft) | 11.57 | 13.53 |
| 4.03 | | | | |
| Min Ch El (ft) | 363.86 | Shear (lb/sq ft) | 0.18 | 0.58 |
| 0.27 | | | | |
| Alpha | 1.18 | Stream Power (lb/ft s) | 446.13 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | | Cum volume (acre-ft) | 1.09 | 0.59 |
| 1.50 | | | | |
| C & E Loss (ft) | | Cum SA (acres) | 0.02 | 0.11 |
| 0.40 | | | | |

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION OUTPUT Profile #100 Yr

| | | | | |
|--------------------|----------|-------------------|---------|---------|
| E.G. Elev (ft) | 371.99 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.00 | wt. n-val. | 0.043 | 0.046 |
| 0.040 | | | | |
| W.S. Elev (ft) | 371.98 | Reach Len. (ft) | 112.00 | 116.00 |
| 119.00 | | | | |
| Crit w.s. (ft) | 368.80 | Flow Area (sq ft) | 119.72 | 49.16 |
| 334.22 | | | | |
| E.G. slope (ft/ft) | 0.000077 | Area (sq ft) | 119.72 | 49.16 |
| 334.22 | | | | |
| Q Total (cfs) | 261.20 | Flow (cfs) | 49.52 | 32.92 |
| 178.76 | | | | |
| Top width (ft) | 269.29 | Top width (ft) | 104.03 | 6.42 |
| 158.83 | | | | |
| Vel Total (ft/s) | 0.52 | Avg. vel. (ft/s) | 0.41 | 0.67 |
| 0.53 | | | | |
| Max Chl Dpth (ft) | 8.12 | Hydr. Depth (ft) | 1.15 | 7.66 |
| 2.10 | | | | |
| Conv. Total (cfs) | 29777.7 | Conv. (cfs) | 5645.4 | 3753.2 |
| 20379.1 | | | | |

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|------------------|--------|------------------------|--------|-------|
| Length wtd. (ft) | 116.00 | Wetted Per. (ft) | 104.18 | 13.53 |
| 158.91 | | | | |
| Min Ch El (ft) | 363.86 | Shear (lb/sq ft) | 0.01 | 0.02 |
| 0.01 | | | | |
| Alpha | 1.06 | Stream Power (lb/ft s) | 446.13 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | | Cum Volume (acre-ft) | 1.80 | 0.92 |
| 2.74 | | | | |
| C & E Loss (ft) | | Cum SA (acres) | 0.14 | 0.12 |
| 0.54 | | | | |

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CULVERT

RIVER: JonesFalls
 REACH: IntsTrib RS: 2.5

CULVERT OUTPUT Profile #2 Yr Culv Group: ParkHgtsAve

| | | | |
|---------------------|--------|------------------------|--------|
| Q Culv Group (cfs) | 66.30 | Culv Full Len (ft) | |
| # Barrels | 1 | Culv Vel US (ft/s) | 7.54 |
| Q Barrel (cfs) | 66.30 | Culv Vel DS (ft/s) | 8.36 |
| E.G. US. (ft) | 367.48 | Culv Inv El Up (ft) | 363.86 |
| W.S. US. (ft) | 367.28 | Culv Inv El Dn (ft) | 363.47 |
| E.G. DS (ft) | 365.83 | Culv Frctn Ls (ft) | 0.36 |
| W.S. DS (ft) | 365.47 | Culv Exit Loss (ft) | 0.84 |
| Delta EG (ft) | 1.65 | Culv Entr Loss (ft) | 0.44 |
| Delta WS (ft) | 1.82 | Q Weir (cfs) | |
| E.G. IC (ft) | 367.14 | Weir Sta Lft (ft) | |
| E.G. OC (ft) | 367.48 | Weir Sta Rgt (ft) | |
| Culvert Control | Outlet | Weir Submerg | |
| Culv WS Inlet (ft) | 366.16 | Weir Max Depth (ft) | |
| Culv WS Outlet (ft) | 365.59 | Weir Avg Depth (ft) | |
| Culv Nml Depth (ft) | 2.12 | Weir Flow Area (sq ft) | |
| Culv Crt Depth (ft) | 2.30 | Min El Weir Flow (ft) | 371.14 |

Warning: Since the culvert has supercritical flow, the program should be run in mixed flow in order to check if the cross section downstream of the culvert has supercritical flow.

Note: During supercritical analysis, the culvert direct step method went to normal depth. The program then assumed normal depth at the outlet.

Note: The flow in the culvert is entirely supercritical.

CULVERT OUTPUT Profile #10 Yr Culv Group: ParkHgtsAve

| | | | |
|--------------------|--------|---------------------|--------|
| Q Culv Group (cfs) | 138.90 | Culv Full Len (ft) | |
| # Barrels | 1 | Culv Vel US (ft/s) | 9.85 |
| Q Barrel (cfs) | 138.90 | Culv Vel DS (ft/s) | 9.97 |
| E.G. US. (ft) | 369.49 | Culv Inv El Up (ft) | 363.86 |
| W.S. US. (ft) | 369.31 | Culv Inv El Dn (ft) | 363.47 |
| E.G. DS (ft) | 366.43 | Culv Frctn Ls (ft) | 0.39 |
| W.S. DS (ft) | 366.18 | Culv Exit Loss (ft) | 1.92 |
| Delta EG (ft) | 3.06 | Culv Entr Loss (ft) | 0.75 |
| Delta WS (ft) | 3.12 | Q Weir (cfs) | |
| E.G. IC (ft) | 369.22 | Weir Sta Lft (ft) | |

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| | | | |
|---------------------|--------|------------------------|--------|
| E.G. OC (ft) | 369.49 | Weir Sta Rgt (ft) | |
| Culvert Control | Outlet | Weir Submerg | |
| Culv WS Inlet (ft) | 367.24 | Weir Max Depth (ft) | |
| Culv WS Outlet (ft) | 366.81 | Weir Avg Depth (ft) | |
| Culv Nml Depth (ft) | 3.34 | Weir Flow Area (sq ft) | |
| Culv Crt Depth (ft) | 3.38 | Min El Weir Flow (ft) | 371.14 |

Warning: Since the culvert has supercritical flow, the program should be run in mixed flow in order to check if the cross section downstream of the culvert has supercritical flow.

Note: During supercritical analysis, the culvert direct step method went to normal depth. The program then assumed normal depth at the outlet.

Note: The flow in the culvert is entirely supercritical.

CULVERT OUTPUT Profile #100 Yr Culv Group: ParkHgtsAve

| | | | |
|---------------------|--------|------------------------|--------|
| Q Culv Group (cfs) | 215.36 | Culv Full Len (ft) | |
| # Barrels | 1 | Culv Vel US (ft/s) | 10.97 |
| Q Barrel (cfs) | 215.36 | Culv Vel DS (ft/s) | 14.14 |
| E.G. US. (ft) | 371.99 | Culv Inv El Up (ft) | 363.86 |
| W.S. US. (ft) | 371.98 | Culv Inv El Dn (ft) | 363.47 |
| E.G. DS (ft) | 366.80 | Culv Frctn Ls (ft) | 0.86 |
| W.S. DS (ft) | 366.45 | Culv Exit Loss (ft) | 3.40 |
| Delta EG (ft) | 5.19 | Culv Entr Loss (ft) | 0.93 |
| Delta WS (ft) | 5.53 | Q Weir (cfs) | 45.84 |
| E.G. IC (ft) | 371.99 | Weir Sta Lft (ft) | 287.89 |
| E.G. OC (ft) | 371.50 | Weir Sta Rgt (ft) | 358.89 |
| Culvert Control | Inlet | Weir Submerg | 0.00 |
| Culv WS Inlet (ft) | 368.86 | Weir Max Depth (ft) | 0.85 |
| Culv WS Outlet (ft) | 367.09 | Weir Avg Depth (ft) | 0.37 |
| Culv Nml Depth (ft) | 5.00 | Weir Flow Area (sq ft) | 26.51 |
| Culv Crt Depth (ft) | 4.17 | Min El Weir Flow (ft) | 371.14 |

Warning: Since the culvert has supercritical flow, the program should be run in mixed flow in order to check if the cross section downstream of the culvert has supercritical flow.

Note: The normal depth exceeds the height of the culvert. The program assumes that the normal depth is equal to the height of the culvert.

Note: The flow in the culvert is entirely supercritical.

CROSS SECTION

RIVER: JonesFalls
 REACH: IntsTrib RS: 2

CROSS SECTION OUTPUT Profile #2 Yr

| | | | | |
|--------------------|----------|-------------------|---------|---------|
| E.G. Elev (ft) | 365.83 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.37 | wt. n-val. | | 0.046 |
| 0.045 | | | | |
| W.S. Elev (ft) | 365.47 | Reach Len. (ft) | 209.00 | 187.00 |
| 167.00 | | | | |
| Crit W.S. (ft) | 365.18 | Flow Area (sq ft) | | 12.50 |
| 2.37 | | | | |
| E.G. slope (ft/ft) | 0.016488 | Area (sq ft) | | 12.50 |

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| | | | | |
|-------------------|--------|------------------------|--------|-------|
| 2.37 | | | | |
| Q Total (cfs) | 66.30 | Flow (cfs) | | 62.49 |
| 3.81 | | | | |
| Top width (ft) | 17.64 | Top width (ft) | | 7.44 |
| 10.20 | | | | |
| Vel Total (ft/s) | 4.46 | Avg. Vel. (ft/s) | | 5.00 |
| 1.60 | | | | |
| Max Chl Dpth (ft) | 2.00 | Hydr. Depth (ft) | | 1.68 |
| 0.23 | | | | |
| Conv. Total (cfs) | 516.3 | Conv. (cfs) | | 486.7 |
| 29.6 | | | | |
| Length wtd. (ft) | 186.43 | wetted Per. (ft) | | 9.45 |
| 10.21 | | | | |
| Min Ch El (ft) | 363.47 | Shear (lb/sq ft) | | 1.36 |
| 0.24 | | | | |
| Alpha | 1.19 | Stream Power (lb/ft s) | 321.80 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 4.53 | Cum Volume (acre-ft) | 0.62 | 0.38 |
| 0.80 | | | | |
| C & E Loss (ft) | 0.06 | Cum SA (acres) | | 0.09 |
| 0.02 | | | | |

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

This may indicate the need for additional cross sections.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION OUTPUT Profile #10 Yr

| | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 366.43 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.25 | wt. n-val. | 0.045 | 0.046 |
| 0.045 | | | | |
| W.S. Elev (ft) | 366.18 | Reach Len. (ft) | 209.00 | 187.00 |
| 167.00 | | | | |
| Crit w.s. (ft) | 366.18 | Flow Area (sq ft) | 0.05 | 18.10 |
| 27.46 | | | | |
| E.G. Slope (ft/ft) | 0.010415 | Area (sq ft) | 0.05 | 18.10 |
| 38.15 | | | | |
| Q Total (cfs) | 138.90 | Flow (cfs) | 0.03 | 87.32 |
| 51.54 | | | | |
| Top width (ft) | 96.30 | Top width (ft) | 0.52 | 8.00 |
| 87.77 | | | | |
| Vel Total (ft/s) | 3.05 | Avg. Vel. (ft/s) | 0.66 | 4.82 |
| 1.88 | | | | |
| Max Chl Dpth (ft) | 2.71 | Hydr. Depth (ft) | 0.09 | 2.26 |
| 0.42 | | | | |
| Conv. Total (cfs) | 1361.1 | Conv. (cfs) | 0.3 | 855.7 |
| 505.1 | | | | |
| Length wtd. (ft) | 183.21 | wetted Per. (ft) | 0.56 | 10.22 |
| 66.06 | | | | |
| Min Ch El (ft) | 363.47 | Shear (lb/sq ft) | 0.06 | 1.15 |
| 0.27 | | | | |
| Alpha | 1.72 | Stream Power (lb/ft s) | 321.80 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 3.09 | Cum Volume (acre-ft) | 1.09 | 0.55 |

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| | | | | |
|-----------------|------|----------------|------|------|
| 1.50 | | | | |
| C & E Loss (ft) | 0.04 | Cum SA (acres) | 0.00 | 0.09 |
| 0.18 | | | | |

warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.

warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION OUTPUT Profile #100 Yr

| | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 366.80 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.35 | wt. n-Val. | 0.045 | 0.046 |
| 0.045 | | | | |
| W.S. Elev (ft) | 366.45 | Reach Len. (ft) | 209.00 | 187.00 |
| 167.00 | | | | |
| Crit w.s. (ft) | 366.45 | Flow Area (sq ft) | 0.29 | 20.24 |
| 45.08 | | | | |
| E.G. Slope (ft/ft) | 0.014253 | Area (sq ft) | 0.29 | 20.24 |
| 62.06 | | | | |
| Q Total (cfs) | 261.20 | Flow (cfs) | 0.41 | 123.02 |
| 137.77 | | | | |
| Top width (ft) | 100.67 | Top width (ft) | 1.28 | 8.00 |
| 91.38 | | | | |
| Vel Total (ft/s) | 3.98 | Avg. Vel. (ft/s) | 1.40 | 6.08 |
| 3.06 | | | | |
| Max Chl Dpth (ft) | 2.98 | Hydr. Depth (ft) | 0.23 | 2.53 |
| 0.68 | | | | |
| Conv. Total (cfs) | 2187.9 | Conv. (cfs) | 3.4 | 1030.5 |
| 1154.0 | | | | |
| Length wtd. (ft) | 181.36 | wetted Per. (ft) | 1.36 | 10.22 |
| 66.06 | | | | |
| Min Ch El (ft) | 363.47 | Shear (lb/sq ft) | 0.19 | 1.76 |
| 0.61 | | | | |
| Alpha | 1.41 | Stream Power (lb/ft s) | 321.80 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 3.48 | Cum Volume (acre-ft) | 1.80 | 0.77 |
| 2.74 | | | | |
| C & E Loss (ft) | 0.04 | Cum SA (acres) | 0.00 | 0.10 |
| 0.19 | | | | |

warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and

previous cross section. This may indicate the need for additional cross sections.
 Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.
 Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION

RIVER: JonesFalls
 REACH: IntsTrib RS: 1

CROSS SECTION OUTPUT Profile #2 Yr

| | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 361.24 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.25 | wt. n-val. | | 0.046 |
| w.s. Elev (ft) | 360.99 | Reach Len. (ft) | 507.00 | 507.00 |
| 507.00 | | | | |
| Crit w.s. (ft) | 360.99 | Flow Area (sq ft) | | 16.55 |
| E.G. Slope (ft/ft) | 0.039364 | Area (sq ft) | | 16.55 |
| Q Total (cfs) | 66.30 | Flow (cfs) | | 66.30 |
| Top width (ft) | 33.41 | Top width (ft) | | 33.41 |
| Vel Total (ft/s) | 4.01 | Avg. Vel. (ft/s) | | 4.01 |
| Max Chl Dpth (ft) | 0.99 | Hydr. Depth (ft) | | 0.50 |
| Conv. Total (cfs) | 334.2 | Conv. (cfs) | | 334.2 |
| Length wtd. (ft) | 507.00 | wetted Per. (ft) | | 33.49 |
| Min Ch El (ft) | 360.00 | Shear (lb/sq ft) | | 1.21 |
| Alpha | 1.00 | Stream Power (lb/ft s) | 371.98 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 5.44 | Cum Volume (acre-ft) | 0.62 | 0.32 |
| 0.80 | | | | |
| C & E Loss (ft) | 0.04 | Cum SA (acres) | | |

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
 warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
 warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program

defaulted to critical depth.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, energy was used.

CROSS SECTION OUTPUT Profile #10 Yr

| | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 361.69 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.37 | wt. n-Val. | | 0.046 |
| 0.045 | | | | |
| W.S. Elev (ft) | 361.33 | Reach Len. (ft) | 507.00 | 507.00 |
| 507.00 | | | | |
| Crit w.s. (ft) | 361.33 | Flow Area (sq ft) | | 28.22 |
| 0.69 | | | | |
| E.G. slope (ft/ft) | 0.031925 | Area (sq ft) | | 28.22 |
| 0.69 | | | | |
| Q Total (cfs) | 138.90 | Flow (cfs) | | 137.70 |
| 1.20 | | | | |
| Top width (ft) | 40.43 | Top width (ft) | | 36.21 |
| 4.22 | | | | |
| Vel Total (ft/s) | 4.80 | Avg. vel. (ft/s) | | 4.88 |
| 1.75 | | | | |
| Max Chl Dpth (ft) | 1.33 | Hydr. Depth (ft) | | 0.78 |
| 0.16 | | | | |
| Conv. Total (cfs) | 777.4 | Conv. (cfs) | | 770.7 |
| 6.7 | | | | |
| Length wtd. (ft) | 507.00 | wetted Per. (ft) | | 36.32 |
| 4.23 | | | | |
| Min Ch El (ft) | 360.00 | Shear (lb/sq ft) | | 1.55 |
| 0.32 | | | | |
| Alpha | 1.02 | Stream Power (lb/ft s) | 371.98 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 5.26 | Cum volume (acre-ft) | 1.09 | 0.45 |
| 1.43 | | | | |
| C & E Loss (ft) | 0.05 | Cum SA (acres) | | |

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, energy was used.

CROSS SECTION OUTPUT Profile #100 Yr

| | | | | |
|----------------|--------|-----------------|---------|---------|
| E.G. Elev (ft) | 362.23 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.49 | wt. n-Val. | | 0.046 |
| 0.045 | | | | |
| W.S. Elev (ft) | 361.74 | Reach Len. (ft) | 507.00 | 507.00 |
| 507.00 | | | | |

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| | | | | |
|--------------------|----------|------------------------|--------|--------|
| Crit w.s. (ft) | 361.74 | Flow Area (sq ft) | | 43.92 |
| 3.55 | | | | |
| E.G. slope (ft/ft) | 0.027244 | Area (sq ft) | | 43.92 |
| 3.55 | | | | |
| Q Total (cfs) | 261.20 | Flow (cfs) | | 251.23 |
| 9.97 | | | | |
| Top width (ft) | 49.00 | Top width (ft) | | 39.40 |
| 9.60 | | | | |
| Vel Total (ft/s) | 5.50 | Avg. Vel. (ft/s) | | 5.72 |
| 2.80 | | | | |
| Max Chl Dpth (ft) | 1.74 | Hydr. Depth (ft) | | 1.11 |
| 0.37 | | | | |
| Conv. Total (cfs) | 1582.5 | Conv. (cfs) | | 1522.1 |
| 60.4 | | | | |
| Length wtd. (ft) | 507.00 | wetted Per. (ft) | | 39.53 |
| 9.63 | | | | |
| Min Ch El (ft) | 360.00 | Shear (lb/sq ft) | | 1.89 |
| 0.63 | | | | |
| Alpha | 1.05 | Stream Power (lb/ft s) | 371.98 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 4.95 | Cum Volume (acre-ft) | 1.80 | 0.64 |
| 2.61 | | | | |
| C & E Loss (ft) | 0.07 | Cum SA (acres) | | |

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth

for the water surface and continued on with the calculations.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, energy was used.

CROSS SECTION

RIVER: JonesFalls
 REACH: JonesFalls3 RS: 10

CROSS SECTION OUTPUT Profile #2 Yr

| | | | | |
|--------------------|----------|-------------------|---------|---------|
| E.G. Elev (ft) | 367.21 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.38 | wt. n-Val. | 0.110 | 0.049 |
| 0.110 | | | | |
| W.S. Elev (ft) | 366.83 | Reach Len. (ft) | 110.95 | 122.86 |
| 127.14 | | | | |
| Crit w.s. (ft) | 365.98 | Flow Area (sq ft) | 72.54 | 110.27 |
| 9.13 | | | | |
| E.G. slope (ft/ft) | 0.007744 | Area (sq ft) | 72.54 | 110.27 |
| 27.26 | | | | |
| Q Total (cfs) | 655.40 | Flow (cfs) | 70.93 | 578.20 |
| 6.27 | | | | |

| | | | | |
|---------------------------|--------|------------------------|--------|--------|
| Top width (ft) | 176.92 | Top width (ft) | 97.19 | 37.50 |
| 42.23 Vel Total (ft/s) | 3.41 | Avg. Vel. (ft/s) | 0.98 | 5.24 |
| 0.69 Max Chl Dpth (ft) | 4.53 | Hydr. Depth (ft) | 0.75 | 2.94 |
| 0.44 Conv. Total (cfs) | 7447.8 | Conv. (cfs) | 806.1 | 6570.5 |
| 71.2 Length wtd. (ft) | 122.02 | wetted Per. (ft) | 97.22 | 40.03 |
| 20.83 Min Ch El (ft) | 362.30 | Shear (lb/sq ft) | 0.36 | 1.33 |
| 0.21 Alpha | 2.09 | Stream Power (lb/ft s) | 465.75 | 0.00 |
| 0.00 Frctn Loss (ft) | 1.05 | Cum Volume (acre-ft) | 3.37 | 2.98 |
| 4.70 C & E Loss (ft) | 0.02 | Cum SA (acres) | 2.96 | 0.99 |
| 4.71 | | | | |

Warning: Divided flow computed for this cross-section.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, energy was used.

CROSS SECTION OUTPUT Profile #10 Yr

| | | | | |
|------------------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 368.56 | Element | Left OB | Channel |
| Right OB Vel Head (ft) | 0.38 | wt. n-val. | 0.110 | 0.049 |
| 0.110 W.S. Elev (ft) | 368.18 | Reach Len. (ft) | 110.95 | 122.86 |
| 127.14 Crit w.s. (ft) | 367.50 | Flow Area (sq ft) | 224.71 | 160.94 |
| 138.34 E.G. slope (ft/ft) | 0.006274 | Area (sq ft) | 224.71 | 160.94 |
| 138.34 Q Total (cfs) | 1520.50 | Flow (cfs) | 368.66 | 977.41 |
| 174.43 Top width (ft) | 263.19 | Top width (ft) | 118.24 | 37.50 |
| 107.45 Vel Total (ft/s) | 2.90 | Avg. Vel. (ft/s) | 1.64 | 6.07 |
| 1.26 Max Chl Dpth (ft) | 5.88 | Hydr. Depth (ft) | 1.90 | 4.29 |
| 1.29 Conv. Total (cfs) | 19196.7 | Conv. (cfs) | 4654.4 | 12340.1 |
| 2202.3 Length wtd. (ft) | 120.89 | wetted Per. (ft) | 118.35 | 40.03 |
| 108.13 Min Ch El (ft) | 362.30 | Shear (lb/sq ft) | 0.74 | 1.57 |
| 0.50 Alpha | 2.91 | Stream Power (lb/ft s) | 465.75 | 0.00 |
| 0.00 Frctn Loss (ft) | 0.99 | Cum Volume (acre-ft) | 11.95 | 4.42 |
| 17.00 C & E Loss (ft) | 0.04 | Cum SA (acres) | 5.45 | 0.99 |
| 7.60 | | | | |

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Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

CROSS SECTION OUTPUT Profile #100 Yr

| | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 370.06 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.50 | wt. n-val. | 0.110 | 0.049 |
| 0.110 | | | | |
| W.S. Elev (ft) | 369.55 | Reach Len. (ft) | 110.95 | 122.86 |
| 127.14 | | | | |
| Crit w.s. (ft) | 368.59 | Flow Area (sq ft) | 391.79 | 212.46 |
| 300.66 | | | | |
| E.G. slope (ft/ft) | 0.006843 | Area (sq ft) | 391.79 | 212.46 |
| 300.66 | | | | |
| Q Total (cfs) | 3144.30 | Flow (cfs) | 935.16 | 1621.72 |
| 587.42 | | | | |
| Top width (ft) | 293.43 | Top width (ft) | 125.26 | 37.50 |
| 130.68 | | | | |
| Vel Total (ft/s) | 3.47 | Avg. vel. (ft/s) | 2.39 | 7.63 |
| 1.95 | | | | |
| Max Chl Dpth (ft) | 7.25 | Hydr. Depth (ft) | 3.13 | 5.67 |
| 2.30 | | | | |
| Conv. Total (cfs) | 38009.6 | Conv. (cfs) | 11304.6 | 19604.0 |
| 7101.0 | | | | |
| Length wtd. (ft) | 120.54 | wetted Per. (ft) | 125.50 | 40.03 |
| 131.43 | | | | |
| Min Ch El (ft) | 362.30 | shear (lb/sq ft) | 1.33 | 2.27 |
| 0.98 | | | | |
| Alpha | 2.69 | Stream Power (lb/ft s) | 465.75 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 0.97 | Cum Volume (acre-ft) | 24.57 | 7.10 |
| 34.82 | | | | |
| C & E Loss (ft) | 0.02 | Cum SA (acres) | 6.52 | 0.99 |
| 9.24 | | | | |

Warning: Divided flow computed for this cross-section.

CROSS SECTION

RIVER: JonesFalls
 REACH: JonesFalls3 RS: 9

CROSS SECTION OUTPUT Profile #2 Yr

| | | | | |
|--------------------|----------|-------------------|---------|---------|
| E.G. Elev (ft) | 366.14 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.57 | wt. n-val. | 0.110 | 0.049 |
| 0.110 | | | | |
| W.S. Elev (ft) | 365.57 | Reach Len. (ft) | 129.00 | 133.89 |
| 139.77 | | | | |
| Crit w.s. (ft) | 364.46 | Flow Area (sq ft) | 42.94 | 89.01 |
| 37.85 | | | | |
| E.G. slope (ft/ft) | 0.009531 | Area (sq ft) | 42.94 | 89.01 |
| 37.85 | | | | |

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|-------------------|--------|------------------------|--------|--------|
| Q Total (cfs) | 655.40 | Flow (cfs) | 38.76 | 575.41 |
| 41.23 | | | | |
| Top width (ft) | 149.30 | Top width (ft) | 75.30 | 25.35 |
| 48.66 | | | | |
| Vel Total (ft/s) | 3.86 | Avg. Vel. (ft/s) | 0.90 | 6.46 |
| 1.09 | | | | |
| Max Chl Dpth (ft) | 4.49 | Hydr. Depth (ft) | 0.57 | 3.51 |
| 0.78 | | | | |
| Conv. Total (cfs) | 6713.3 | Conv. (cfs) | 397.0 | 5893.9 |
| 422.3 | | | | |
| Length wtd. (ft) | 132.76 | wetted Per. (ft) | 75.84 | 27.59 |
| 50.43 | | | | |
| Min Ch El (ft) | 361.08 | Shear (lb/sq ft) | 0.34 | 1.92 |
| 0.45 | | | | |
| Alpha | 2.47 | Stream Power (lb/ft s) | 486.63 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 0.89 | Cum Volume (acre-ft) | 3.23 | 2.70 |
| 4.60 | | | | |
| C & E Loss (ft) | 0.12 | Cum SA (acres) | 2.74 | 0.90 |
| 4.58 | | | | |

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, energy was used.

CROSS SECTION OUTPUT Profile #10 Yr

| | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 367.53 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.77 | wt. n-Val. | 0.110 | 0.049 |
| 0.108 | | | | |
| W.S. Elev (ft) | 366.76 | Reach Len. (ft) | 129.00 | 133.89 |
| 139.77 | | | | |
| Crit w.s. (ft) | 366.61 | Flow Area (sq ft) | 144.54 | 119.10 |
| 114.92 | | | | |
| E.G. Slope (ft/ft) | 0.011233 | Area (sq ft) | 144.54 | 119.10 |
| 114.92 | | | | |
| Q Total (cfs) | 1520.50 | Flow (cfs) | 277.80 | 1014.87 |
| 227.83 | | | | |
| Top width (ft) | 196.27 | Top width (ft) | 92.34 | 25.35 |
| 78.58 | | | | |
| Vel Total (ft/s) | 4.02 | Avg. Vel. (ft/s) | 1.92 | 8.52 |
| 1.98 | | | | |
| Max Chl Dpth (ft) | 5.68 | Hydr. Depth (ft) | 1.57 | 4.70 |
| 1.46 | | | | |
| Conv. Total (cfs) | 14346.5 | Conv. (cfs) | 2621.1 | 9575.7 |
| 2149.7 | | | | |
| Length wtd. (ft) | 132.73 | wetted Per. (ft) | 92.93 | 27.59 |
| 80.38 | | | | |
| Min Ch El (ft) | 361.08 | Shear (lb/sq ft) | 1.09 | 3.03 |
| 1.00 | | | | |
| Alpha | 3.08 | Stream Power (lb/ft s) | 486.63 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 1.38 | Cum Volume (acre-ft) | 11.48 | 4.02 |
| 16.63 | | | | |
| C & E Loss (ft) | 0.12 | Cum SA (acres) | 5.18 | 0.90 |
| 7.32 | | | | |

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Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

CROSS SECTION OUTPUT Profile #100 Yr

| | | Element | Left OB | Channel |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 369.06 | | | |
| Right OB | | | | |
| Vel Head (ft) | 0.75 | wt. n-Val. | 0.110 | 0.049 |
| 0.092 | | | | |
| W.S. Elev (ft) | 368.31 | Reach Len. (ft) | 129.00 | 133.89 |
| 139.77 | | | | |
| Crit w.s. (ft) | 367.88 | Flow Area (sq ft) | 298.75 | 158.50 |
| 271.68 | | | | |
| E.G. slope (ft/ft) | 0.009655 | Area (sq ft) | 298.75 | 158.50 |
| 271.68 | | | | |
| Q Total (cfs) | 3144.30 | Flow (cfs) | 799.38 | 1515.11 |
| 829.81 | | | | |
| Top width (ft) | 249.33 | Top width (ft) | 103.65 | 25.35 |
| 120.32 | | | | |
| Vel Total (ft/s) | 4.31 | Avg. Vel. (ft/s) | 2.68 | 9.56 |
| 3.05 | | | | |
| Max Chl Dpth (ft) | 7.23 | Hydr. Depth (ft) | 2.88 | 6.25 |
| 2.26 | | | | |
| Conv. Total (cfs) | 31999.9 | Conv. (cfs) | 8135.4 | 15419.5 |
| 8445.0 | | | | |
| Length wtd. (ft) | 132.94 | wetted Per. (ft) | 104.38 | 27.59 |
| 122.15 | | | | |
| Min Ch El (ft) | 361.08 | Shear (lb/sq ft) | 1.73 | 3.46 |
| 1.34 | | | | |
| Alpha | 2.60 | Stream Power (lb/ft s) | 486.63 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 1.91 | Cum Volume (acre-ft) | 23.69 | 6.58 |
| 33.98 | | | | |
| C & E Loss (ft) | 0.03 | Cum SA (acres) | 6.23 | 0.90 |
| 8.87 | | | | |

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

This may indicate the need for additional cross sections.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

CROSS SECTION

RIVER: JonesFalls
 REACH: JonesFalls3 RS: 8

CROSS SECTION OUTPUT Profile #2 Yr

| | | Element | Left OB | Channel |
|----------------|--------|------------|---------|---------|
| E.G. Elev (ft) | 365.13 | | | |
| Right OB | | | | |
| Vel Head (ft) | 0.17 | wt. n-Val. | 0.091 | 0.049 |
| 0.040 | | | | |

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| | | | | |
|--------------------|----------|------------------------|--------|--------|
| W.S. Elev (ft) | 364.96 | Reach Len. (ft) | 491.90 | 504.10 |
| 506.12 | | | | |
| Crit w.s. (ft) | 364.31 | Flow Area (sq ft) | 210.89 | 58.80 |
| 15.09 | | | | |
| E.G. slope (ft/ft) | 0.004963 | Area (sq ft) | 210.89 | 58.80 |
| 15.09 | | | | |
| Q Total (cfs) | 655.40 | Flow (cfs) | 347.72 | 278.92 |
| 28.76 | | | | |
| Top width (ft) | 165.06 | Top width (ft) | 125.05 | 15.73 |
| 24.27 | | | | |
| Vel Total (ft/s) | 2.30 | Avg. vel. (ft/s) | 1.65 | 4.74 |
| 1.91 | | | | |
| Max Chl Dpth (ft) | 5.01 | Hydr. Depth (ft) | 1.69 | 3.74 |
| 0.62 | | | | |
| Conv. Total (cfs) | 9302.8 | Conv. (cfs) | 4935.6 | 3959.1 |
| 408.2 | | | | |
| Length wtd. (ft) | 500.33 | wetted Per. (ft) | 125.86 | 17.77 |
| 24.30 | | | | |
| Min Ch El (ft) | 359.95 | Shear (lb/sq ft) | 0.52 | 1.03 |
| 0.19 | | | | |
| Alpha | 2.11 | Stream Power (lb/ft s) | 514.52 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 4.81 | Cum Volume (acre-ft) | 2.85 | 2.48 |
| 4.52 | | | | |
| C & E Loss (ft) | 0.10 | Cum SA (acres) | 2.45 | 0.84 |
| 4.46 | | | | |

Warning: The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.
 Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.
 This may indicate the need for additional cross sections.
 Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

CROSS SECTION OUTPUT Profile #10 Yr

| | | | | |
|--------------------|----------|-------------------|---------|---------|
| E.G. Elev (ft) | 366.03 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.38 | wt. n-Val. | 0.088 | 0.049 |
| 0.040 | | | | |
| W.S. Elev (ft) | 365.65 | Reach Len. (ft) | 491.90 | 504.10 |
| 506.12 | | | | |
| Crit w.s. (ft) | 365.13 | Flow Area (sq ft) | 299.93 | 69.75 |
| 36.45 | | | | |
| E.G. slope (ft/ft) | 0.009597 | Area (sq ft) | 299.93 | 69.75 |
| 36.45 | | | | |
| Q Total (cfs) | 1520.50 | Flow (cfs) | 873.59 | 515.48 |
| 131.43 | | | | |
| Top width (ft) | 183.18 | Top width (ft) | 130.54 | 15.73 |
| 36.90 | | | | |
| Vel Total (ft/s) | 3.74 | Avg. vel. (ft/s) | 2.91 | 7.39 |
| 3.61 | | | | |
| Max Chl Dpth (ft) | 5.70 | Hydr. Depth (ft) | 2.30 | 4.43 |
| 0.99 | | | | |
| Conv. Total (cfs) | 15520.9 | Conv. (cfs) | 8917.4 | 5261.9 |
| 1341.6 | | | | |
| Length wtd. (ft) | 500.31 | wetted Per. (ft) | 131.39 | 17.77 |
| 36.95 | | | | |

| EcclestonMod.rep | | | | |
|------------------|--------|------------------------|--------|------|
| Min Ch El (ft) | 359.95 | Shear (lb/sq ft) | 1.37 | 2.35 |
| 0.59 | | | | |
| Alpha | 1.75 | Stream Power (lb/ft s) | 514.52 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 5.00 | Cum volume (acre-ft) | 10.82 | 3.73 |
| 16.39 | | | | |
| C & E Loss (ft) | 0.01 | Cum SA (acres) | 4.85 | 0.84 |
| 7.14 | | | | |

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

CROSS SECTION OUTPUT Profile #100 Yr

| Profile #100 Yr | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 367.12 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 1.03 | wt. n-Val. | 0.087 | 0.049 |
| 0.040 | | | | |
| W.S. Elev (ft) | 366.09 | Reach Len. (ft) | 491.90 | 504.10 |
| 506.12 | | | | |
| Crit w.s. (ft) | 366.09 | Flow Area (sq ft) | 358.17 | 76.69 |
| 54.46 | | | | |
| E.G. Slope (ft/ft) | 0.023572 | Area (sq ft) | 358.17 | 76.69 |
| 54.46 | | | | |
| Q Total (cfs) | 3144.30 | Flow (cfs) | 1844.41 | 946.23 |
| 353.66 | | | | |
| Top width (ft) | 193.98 | Top width (ft) | 133.50 | 15.73 |
| 44.76 | | | | |
| Vel Total (ft/s) | 6.43 | Avg. vel. (ft/s) | 5.15 | 12.34 |
| 6.49 | | | | |
| Max Chl Dpth (ft) | 6.14 | Hydr. Depth (ft) | 2.68 | 4.88 |
| 1.22 | | | | |
| Conv. Total (cfs) | 20479.7 | Conv. (cfs) | 12013.1 | 6163.1 |
| 2303.5 | | | | |
| Length wtd. (ft) | 499.63 | wetted Per. (ft) | 134.38 | 17.77 |
| 44.82 | | | | |
| Min Ch El (ft) | 359.95 | Shear (lb/sq ft) | 3.92 | 6.35 |
| 1.79 | | | | |
| Alpha | 1.60 | Stream Power (lb/ft s) | 514.52 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 1.16 | Cum volume (acre-ft) | 22.71 | 6.22 |
| 33.46 | | | | |
| C & E Loss (ft) | 0.28 | Cum SA (acres) | 5.88 | 0.84 |
| 8.60 | | | | |

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

This may indicate the need for additional cross sections.

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set

equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION

RIVER: JonesFalls
 REACH: JonesFalls3 RS: 7

CROSS SECTION OUTPUT Profile #2 Yr

| | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 360.22 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 1.16 | wt. n-Val. | 0.110 | 0.049 |
| 0.110 | | | | |
| W.S. Elev (ft) | 359.06 | Reach Len. (ft) | 469.28 | 475.20 |
| 444.49 | | | | |
| Crit w.s. (ft) | 359.06 | Flow Area (sq ft) | 22.71 | 65.43 |
| 2.14 | | | | |
| E.G. Slope (ft/ft) | 0.026068 | Area (sq ft) | 22.71 | 65.43 |
| 2.14 | | | | |
| Q Total (cfs) | 655.40 | Flow (cfs) | 62.42 | 591.43 |
| 1.55 | | | | |
| Top Width (ft) | 48.71 | Top width (ft) | 14.22 | 23.27 |
| 11.22 | | | | |
| Vel Total (ft/s) | 7.26 | Avg. Vel. (ft/s) | 2.75 | 9.04 |
| 0.72 | | | | |
| Max Chl Dpth (ft) | 4.01 | Hydr. Depth (ft) | 1.60 | 2.81 |
| 0.19 | | | | |
| Conv. Total (cfs) | 4059.3 | Conv. (cfs) | 386.6 | 3663.1 |
| 9.6 | | | | |
| Length wtd. (ft) | 467.10 | wetted Per. (ft) | 16.05 | 26.09 |
| 11.22 | | | | |
| Min Ch El (ft) | 355.05 | Shear (lb/sq ft) | 2.30 | 4.08 |
| 0.31 | | | | |
| Alpha | 1.41 | Stream Power (lb/ft s) | 670.42 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 2.09 | Cum Volume (acre-ft) | 1.53 | 1.76 |
| 4.42 | | | | |
| C & E Loss (ft) | 0.32 | Cum SA (acres) | 1.66 | 0.61 |
| 4.25 | | | | |

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.
 Warning: The velocity head has changed by more than 0.5 ft (0.15 m). This may indicate the need for additional cross sections.
 Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4. This may indicate the need for additional cross sections.
 Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
 Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program

defaulted to critical depth.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, energy was used.

CROSS SECTION OUTPUT Profile #10 Yr

| | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 361.01 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.50 | wt. n-val. | 0.085 | 0.049 |
| 0.049 | | | | |
| W.S. Elev (ft) | 360.51 | Reach Len. (ft) | 469.28 | 475.20 |
| 444.49 | | | | |
| Crit w.s. (ft) | 360.51 | Flow Area (sq ft) | 88.57 | 99.08 |
| 183.70 | | | | |
| E.G. slope (ft/ft) | 0.010430 | Area (sq ft) | 88.57 | 99.08 |
| 183.70 | | | | |
| Q Total (cfs) | 1520.50 | Flow (cfs) | 189.20 | 747.07 |
| 584.23 | | | | |
| Top width (ft) | 284.18 | Top width (ft) | 84.87 | 23.27 |
| 176.05 | | | | |
| Vel Total (ft/s) | 4.09 | Avg. vel. (ft/s) | 2.14 | 7.54 |
| 3.18 | | | | |
| Max Chl Dpth (ft) | 5.46 | Hydr. Depth (ft) | 1.04 | 4.26 |
| 1.04 | | | | |
| Conv. Total (cfs) | 14888.0 | Conv. (cfs) | 1852.6 | 7314.9 |
| 5720.5 | | | | |
| Length wtd. (ft) | 459.84 | wetted Per. (ft) | 86.81 | 26.09 |
| 176.11 | | | | |
| Min Ch El (ft) | 355.05 | Shear (lb/sq ft) | 0.66 | 2.47 |
| 0.68 | | | | |
| Alpha | 1.93 | Stream Power (lb/ft s) | 670.42 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 0.33 | Cum volume (acre-ft) | 8.63 | 2.76 |
| 15.11 | | | | |
| C & E Loss (ft) | 0.15 | Cum SA (acres) | 3.63 | 0.61 |
| 5.90 | | | | |

Warning: The energy equation could not be balanced within the specified number of iterations. The program used critical depth for the water surface and continued on with the calculations.

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

This may indicate the need for additional cross sections.

Warning: During the standard step iterations, when the assumed water surface was set equal to critical depth, the calculated water surface came back below critical depth. This indicates that there is not a valid subcritical answer. The program defaulted to critical depth.

CROSS SECTION OUTPUT Profile #100 Yr

| | | | | |
|----------------|--------|-------------------|---------|---------|
| E.G. Elev (ft) | 363.85 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.08 | wt. n-val. | 0.056 | 0.049 |
| 0.047 | | | | |
| W.S. Elev (ft) | 363.77 | Reach Len. (ft) | 469.28 | 475.20 |
| 444.49 | | | | |
| Crit w.s. (ft) | 361.16 | Flow Area (sq ft) | 462.99 | 174.91 |
| 802.15 | | | | |

| EcclestonMod.rep | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Slope (ft/ft) | 0.000813 | Area (sq ft) | 462.99 | 174.91 |
| 802.15 | | | | |
| Q Total (cfs) | 3144.30 | Flow (cfs) | 813.43 | 537.69 |
| 1793.17 | | | | |
| Top width (ft) | 361.39 | Top width (ft) | 134.79 | 23.27 |
| 203.33 | | | | |
| Vel Total (ft/s) | 2.18 | Avg. Vel. (ft/s) | 1.76 | 3.07 |
| 2.24 | | | | |
| Max Chl Dpth (ft) | 8.72 | Hydr. Depth (ft) | 3.44 | 7.52 |
| 3.94 | | | | |
| Conv. Total (cfs) | 110290.8 | Conv. (cfs) | 28532.3 | 18860.4 |
| 62898.1 | | | | |
| Length wtd. (ft) | 455.79 | wetted Per. (ft) | 136.85 | 26.09 |
| 203.59 | | | | |
| Min Ch El (ft) | 355.05 | Shear (lb/sq ft) | 0.17 | 0.34 |
| 0.20 | | | | |
| Alpha | 1.10 | Stream Power (lb/ft s) | 670.42 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 0.13 | cum volume (acre-ft) | 18.08 | 4.76 |
| 28.48 | | | | |
| C & E Loss (ft) | 0.02 | cum SA (acres) | 4.37 | 0.61 |
| 7.16 | | | | |

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.
This may indicate the need for additional cross sections.

CROSS SECTION

RIVER: JonesFalls
REACH: JonesFalls3 RS: 6

CROSS SECTION OUTPUT Profile #2 Yr

| E.G. Elev (ft) | 356.81 | Element | Left OB | Channel |
|--------------------|----------|-------------------|---------|---------|
| Right OB | | | | |
| Vel Head (ft) | 0.09 | wt. n-val. | 0.110 | 0.049 |
| 0.110 | | | | |
| W.S. Elev (ft) | 356.72 | Reach Len. (ft) | 121.97 | 81.55 |
| 93.44 | | | | |
| Crit w.s. (ft) | 355.74 | Flow Area (sq ft) | 43.67 | 90.44 |
| 404.42 | | | | |
| E.G. Slope (ft/ft) | 0.001777 | Area (sq ft) | 85.98 | 90.44 |
| 519.04 | | | | |
| Q Total (cfs) | 655.40 | Flow (cfs) | 24.65 | 303.16 |
| 327.59 | | | | |
| Top width (ft) | 442.46 | Top width (ft) | 105.60 | 18.63 |
| 318.23 | | | | |
| Vel Total (ft/s) | 1.22 | Avg. Vel. (ft/s) | 0.56 | 3.35 |
| 0.81 | | | | |
| Max Chl Dpth (ft) | 5.20 | Hydr. Depth (ft) | 0.99 | 4.85 |
| 1.70 | | | | |
| Conv. Total (cfs) | 15547.9 | Conv. (cfs) | 584.9 | 7191.8 |
| 7771.3 | | | | |
| Length wtd. (ft) | 86.14 | wetted Per. (ft) | 44.23 | 21.30 |
| 238.36 | | | | |
| Min Ch El (ft) | 351.52 | Shear (lb/sq ft) | 0.11 | 0.47 |
| 0.19 | | | | |

EcclestonMod.rep

| | | | | |
|-----------------|------|------------------------|--------|------|
| Alpha | 3.74 | Stream Power (lb/ft s) | 760.76 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 0.17 | Cum Volume (acre-ft) | 0.95 | 0.91 |
| 1.76 | | | | |
| C & E Loss (ft) | 0.00 | Cum SA (acres) | 1.01 | 0.39 |
| 2.57 | | | | |

Warning: Divided flow computed for this cross-section.
 Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, energy was used.

CROSS SECTION OUTPUT Profile #10 Yr

| | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 360.42 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.01 | wt. n-val. | 0.110 | 0.049 |
| 0.110 | | | | |
| W.S. Elev (ft) | 360.40 | Reach Len. (ft) | 121.97 | 81.55 |
| 93.44 | | | | |
| Crit w.s. (ft) | 356.50 | Flow Area (sq ft) | 835.52 | 159.06 |
| 1281.92 | | | | |
| E.G. slope (ft/ft) | 0.000238 | Area (sq ft) | 835.52 | 159.06 |
| 1763.58 | | | | |
| Q Total (cfs) | 1520.50 | Flow (cfs) | 415.87 | 284.36 |
| 820.27 | | | | |
| Top width (ft) | 598.93 | Top width (ft) | 225.89 | 18.63 |
| 354.40 | | | | |
| Vel Total (ft/s) | 0.67 | Avg. vel. (ft/s) | 0.50 | 1.79 |
| 0.64 | | | | |
| Max Chl Dpth (ft) | 8.88 | Hydr. Depth (ft) | 3.70 | 8.54 |
| 5.38 | | | | |
| Conv. Total (cfs) | 98532.6 | Conv. (cfs) | 26949.8 | 18427.3 |
| 53155.5 | | | | |
| Length wtd. (ft) | 93.69 | wetted Per. (ft) | 226.44 | 21.30 |
| 238.36 | | | | |
| Min Ch El (ft) | 351.52 | Shear (lb/sq ft) | 0.05 | 0.11 |
| 0.08 | | | | |
| Alpha | 1.99 | Stream Power (lb/ft s) | 760.76 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 0.04 | Cum volume (acre-ft) | 3.65 | 1.35 |
| 5.17 | | | | |
| C & E Loss (ft) | 0.01 | Cum SA (acres) | 1.96 | 0.39 |
| 3.19 | | | | |

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

This may indicate the need for additional cross sections.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, energy was used.

CROSS SECTION OUTPUT Profile #100 Yr

| | | | | |
|----------------|--------|-----------------|---------|---------|
| E.G. Elev (ft) | 363.69 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.01 | wt. n-val. | 0.110 | 0.049 |
| 0.110 | | | | |
| W.S. Elev (ft) | 363.68 | Reach Len. (ft) | 121.97 | 81.55 |

EcclestonMod.rep

| | | | | |
|--------------------|----------|------------------------|---------|---------|
| 93.44 | | | | |
| Crit w.s. (ft) | 357.34 | Flow Area (sq ft) | 1634.94 | 220.17 |
| 2995.42 | | | | |
| E.G. slope (ft/ft) | 0.000150 | Area (sq ft) | 1634.94 | 220.17 |
| 2995.42 | | | | |
| Q Total (cfs) | 3144.30 | Flow (cfs) | 907.68 | 387.38 |
| 1849.24 | | | | |
| Top width (ft) | 697.26 | Top width (ft) | 264.57 | 18.63 |
| 414.05 | | | | |
| Vel Total (ft/s) | 0.65 | Avg. vel. (ft/s) | 0.56 | 1.76 |
| 0.62 | | | | |
| Max Chl Dpth (ft) | 12.16 | Hydr. Depth (ft) | 6.18 | 11.82 |
| 7.23 | | | | |
| Conv. Total (cfs) | 257141.2 | Conv. (cfs) | 74230.2 | 31680.3 |
| 151230.7 | | | | |
| Length wtd. (ft) | 98.84 | wetted Per. (ft) | 265.33 | 21.30 |
| 414.56 | | | | |
| Min Ch El (ft) | 351.52 | Shear (lb/sq ft) | 0.06 | 0.10 |
| 0.07 | | | | |
| Alpha | 1.65 | Stream Power (lb/ft s) | 760.76 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 0.01 | Cum volume (acre-ft) | 6.78 | 2.60 |
| 9.11 | | | | |
| C & E Loss (ft) | 0.00 | Cum SA (acres) | 2.22 | 0.39 |
| 4.01 | | | | |

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, energy was used.

CROSS SECTION

RIVER: JonesFalls
 REACH: JonesFalls3 RS: 5

CROSS SECTION OUTPUT Profile #2 Yr

| E.G. Elev (ft) | 356.63 | Element | Left OB | Channel |
|--------------------|----------|-------------------|---------|---------|
| Right OB | | | | |
| Vel Head (ft) | 0.12 | wt. n-Val. | 0.110 | 0.054 |
| 0.110 | | | | |
| w.s. Elev (ft) | 356.51 | Reach Len. (ft) | 131.69 | 149.00 |
| 230.44 | | | | |
| Crit w.s. (ft) | 354.52 | Flow Area (sq ft) | 7.81 | 189.24 |
| 95.78 | | | | |
| E.G. slope (ft/ft) | 0.002172 | Area (sq ft) | 24.71 | 189.24 |
| 415.97 | | | | |
| Q Total (cfs) | 655.40 | Flow (cfs) | 3.09 | 568.47 |
| 83.83 | | | | |
| Top width (ft) | 399.72 | Top width (ft) | 45.21 | 57.39 |
| 297.12 | | | | |
| Vel Total (ft/s) | 2.24 | Avg. vel. (ft/s) | 0.40 | 3.00 |
| 0.88 | | | | |
| Max Chl Dpth (ft) | 5.33 | Hydr. Depth (ft) | 0.50 | 3.30 |
| 1.64 | | | | |
| Conv. Total (cfs) | 14061.8 | Conv. (cfs) | 66.4 | 12196.8 |
| 1798.6 | | | | |
| Length wtd. (ft) | 149.00 | wetted Per. (ft) | 15.67 | 59.99 |
| 58.43 | | | | |

| EcclestonMod.rep | | | | |
|------------------|--------|------------------------|--------|------|
| Min Ch El (ft) | 351.18 | Shear (lb/sq ft) | 0.07 | 0.43 |
| 0.22 | | | | |
| Alpha | 1.58 | Stream Power (lb/ft s) | 953.07 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | | Cum Volume (acre-ft) | 0.79 | 0.64 |
| 0.75 | | | | |
| C & E Loss (ft) | | Cum SA (acres) | 0.80 | 0.32 |
| 1.91 | | | | |

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION OUTPUT Profile #10 Yr

| | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 360.37 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.07 | wt. n-Val. | 0.110 | 0.059 |
| 0.110 | | | | |
| W.S. Elev (ft) | 360.30 | Reach Len. (ft) | 131.69 | 149.00 |
| 230.44 | | | | |
| Crit w.s. (ft) | 356.04 | Flow Area (sq ft) | 156.89 | 407.03 |
| 317.40 | | | | |
| E.G. Slope (ft/ft) | 0.000743 | Area (sq ft) | 727.47 | 407.03 |
| 1645.52 | | | | |
| Q Total (cfs) | 1520.50 | Flow (cfs) | 150.06 | 1009.29 |
| 361.14 | | | | |
| Top width (ft) | 619.46 | Top width (ft) | 214.94 | 57.39 |
| 347.13 | | | | |
| Vel Total (ft/s) | 1.73 | Avg. Vel. (ft/s) | 0.96 | 2.48 |
| 1.14 | | | | |
| Max Chl Dpth (ft) | 9.12 | Hydr. Depth (ft) | 4.35 | 7.09 |
| 5.43 | | | | |
| Conv. Total (cfs) | 55781.9 | Conv. (cfs) | 5505.3 | 37027.5 |
| 13249.1 | | | | |
| Length wtd. (ft) | 149.00 | wetted Per. (ft) | 37.47 | 59.99 |
| 58.43 | | | | |
| Min Ch El (ft) | 351.18 | Shear (lb/sq ft) | 0.19 | 0.31 |
| 0.25 | | | | |
| Alpha | 1.50 | Stream Power (lb/ft s) | 953.07 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | | Cum Volume (acre-ft) | 1.46 | 0.82 |
| 1.52 | | | | |
| C & E Loss (ft) | | Cum SA (acres) | 1.34 | 0.32 |
| 2.44 | | | | |

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION OUTPUT Profile #100 Yr

| | | | | |
|----------------|--------|-------------------|---------|---------|
| E.G. Elev (ft) | 363.68 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.01 | wt. n-Val. | 0.110 | 0.061 |
| 0.110 | | | | |
| W.S. Elev (ft) | 363.67 | Reach Len. (ft) | 131.69 | 149.00 |
| 230.44 | | | | |
| Crit w.s. (ft) | 357.39 | Flow Area (sq ft) | 1471.00 | 600.18 |

EcclestonMod.rep

| | | | | |
|--------------------|----------|------------------------|---------|---------|
| 2944.61 | | | | |
| E.G. slope (ft/ft) | 0.000123 | Area (sq ft) | 1471.00 | 600.18 |
| 2944.61 | | | | |
| Q Total (cfs) | 3144.30 | Flow (cfs) | 757.08 | 751.20 |
| 1636.01 | | | | |
| Top width (ft) | 756.66 | Top width (ft) | 239.07 | 57.39 |
| 460.20 | | | | |
| Vel Total (ft/s) | 0.63 | Avg. Vel. (ft/s) | 0.51 | 1.25 |
| 0.56 | | | | |
| Max Chl Dpth (ft) | 12.49 | Hydr. Depth (ft) | 6.15 | 10.46 |
| 6.40 | | | | |
| Conv. Total (cfs) | 283597.0 | Conv. (cfs) | 68284.3 | 67754.1 |
| 147558.6 | | | | |
| Length wtd. (ft) | 149.00 | wetted Per. (ft) | 241.60 | 59.99 |
| 460.55 | | | | |
| Min Ch El (ft) | 351.18 | Shear (lb/sq ft) | 0.05 | 0.08 |
| 0.05 | | | | |
| Alpha | 1.52 | Stream Power (lb/ft s) | 953.07 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | | Cum Volume (acre-ft) | 2.43 | 1.84 |
| 2.74 | | | | |
| C & E Loss (ft) | | Cum SA (acres) | 1.51 | 0.32 |
| 3.08 | | | | |

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CULVERT

RIVER: JonesFalls
 REACH: JonesFalls3 RS: 4.5

CULVERT OUTPUT Profile #2 Yr Culv Group: Culvert #4

| | | | |
|---------------------|--------|------------------------|--------|
| Q Culv Group (cfs) | 16.16 | Culv Full Len (ft) | 8.37 |
| # Barrels | 1 | Culv Vel US (ft/s) | 6.63 |
| Q Barrel (cfs) | 16.16 | Culv Vel DS (ft/s) | 5.14 |
| E.G. US. (ft) | 356.64 | Culv Inv El Up (ft) | 354.16 |
| W.S. US. (ft) | 356.51 | Culv Inv El Dn (ft) | 353.23 |
| E.G. DS (ft) | 355.37 | Culv Frctn Ls (ft) | 0.62 |
| W.S. DS (ft) | 355.26 | Culv Exit Loss (ft) | 0.30 |
| Delta EG (ft) | 1.26 | Culv Entr Loss (ft) | 0.34 |
| Delta WS (ft) | 1.25 | Q Weir (cfs) | |
| E.G. IC (ft) | 356.54 | Weir Sta Lft (ft) | |
| E.G. OC (ft) | 356.63 | Weir Sta Rgt (ft) | |
| Culvert Control | Outlet | Weir Submerg | |
| Culv WS Inlet (ft) | 355.61 | Weir Max Depth (ft) | |
| Culv WS Outlet (ft) | 355.23 | Weir Avg Depth (ft) | |
| Culv Nml Depth (ft) | 1.30 | Weir Flow Area (sq ft) | |
| Culv Crt Depth (ft) | 1.45 | Min El Weir Flow (ft) | 363.01 |

Note: During supercritical analysis, the culvert direct step method went to normal depth. The program then assumed normal depth at the outlet.

Note: During the supercritical calculations a hydraulic jump occurred inside of the culvert.

CULVERT OUTPUT Profile #10 Yr Culv Group: Culvert #4

EcclestonMod.rep

| | | | |
|---------------------|--------|------------------------|--------|
| Q Culv Group (cfs) | 31.68 | Culv Full Len (ft) | 103.71 |
| # Barrels | 1 | Culv Vel US (ft/s) | 10.08 |
| Q Barrel (cfs) | 31.68 | Culv Vel DS (ft/s) | 10.08 |
| E.G. US. (ft) | 360.37 | Culv Inv El Up (ft) | 354.16 |
| W.S. US. (ft) | 360.30 | Culv Inv El Dn (ft) | 353.23 |
| E.G. DS (ft) | 356.22 | Culv Frctn Ls (ft) | 2.03 |
| W.S. DS (ft) | 355.97 | Culv Exit Loss (ft) | 1.33 |
| Delta EG (ft) | 4.16 | Culv Entr Loss (ft) | 0.79 |
| Delta WS (ft) | 4.33 | Q Weir (cfs) | |
| E.G. IC (ft) | 359.54 | Weir Sta Lft (ft) | |
| E.G. OC (ft) | 360.37 | Weir Sta Rgt (ft) | |
| Culvert Control | Outlet | Weir Submerg | |
| Culv WS Inlet (ft) | 356.16 | Weir Max Depth (ft) | |
| Culv WS Outlet (ft) | 355.23 | Weir Avg Depth (ft) | |
| Culv Nml Depth (ft) | 2.00 | Weir Flow Area (sq ft) | |
| Culv Crt Depth (ft) | 2.00 | Min El Weir Flow (ft) | 363.01 |

Note: The normal depth exceeds the height of the culvert. The program assumes that the normal depth is equal to the height of the culvert.

Note: Culvert critical depth exceeds the height of the culvert.

CULVERT OUTPUT Profile #100 Yr Culv Group: Culvert #4

| | | | |
|---------------------|--------|------------------------|--------|
| Q Culv Group (cfs) | 39.63 | Culv Full Len (ft) | 103.71 |
| # Barrels | 1 | Culv Vel US (ft/s) | 12.62 |
| Q Barrel (cfs) | 39.63 | Culv Vel DS (ft/s) | 12.62 |
| E.G. US. (ft) | 363.68 | Culv Inv El Up (ft) | 354.16 |
| W.S. US. (ft) | 363.67 | Culv Inv El Dn (ft) | 353.23 |
| E.G. DS (ft) | 357.31 | Culv Frctn Ls (ft) | 3.19 |
| W.S. DS (ft) | 356.78 | Culv Exit Loss (ft) | 1.95 |
| Delta EG (ft) | 6.37 | Culv Entr Loss (ft) | 1.24 |
| Delta WS (ft) | 6.89 | Q Weir (cfs) | 699.30 |
| E.G. IC (ft) | 361.83 | Weir Sta Lft (ft) | 323.17 |
| E.G. OC (ft) | 363.68 | Weir Sta Rgt (ft) | 850.70 |
| Culvert Control | Outlet | Weir Submerg | 0.00 |
| Culv WS Inlet (ft) | 356.16 | Weir Max Depth (ft) | 0.68 |
| Culv WS Outlet (ft) | 355.23 | Weir Avg Depth (ft) | 0.63 |
| Culv Nml Depth (ft) | 2.00 | Weir Flow Area (sq ft) | 333.53 |
| Culv Crt Depth (ft) | 2.00 | Min El Weir Flow (ft) | 363.01 |

Note: The normal depth exceeds the height of the culvert. The program assumes that the normal depth is equal to the height of the culvert.

Note: Culvert critical depth exceeds the height of the culvert.

CULVERT OUTPUT Profile #2 Yr Culv Group: PHAVE 24 N

| | | | |
|--------------------|--------|---------------------|--------|
| Q Culv Group (cfs) | 622.36 | Culv Full Len (ft) | |
| # Barrels | 1 | Culv Vel US (ft/s) | 9.62 |
| Q Barrel (cfs) | 622.36 | Culv Vel DS (ft/s) | 6.84 |
| E.G. US. (ft) | 356.64 | Culv Inv El Up (ft) | 351.75 |
| W.S. US. (ft) | 356.51 | Culv Inv El Dn (ft) | 351.22 |
| E.G. DS (ft) | 355.37 | Culv Frctn Ls (ft) | 0.07 |
| W.S. DS (ft) | 355.26 | Culv Exit Loss (ft) | 0.62 |
| Delta EG (ft) | 1.26 | Culv Entr Loss (ft) | 0.57 |
| Delta WS (ft) | 1.25 | Q Weir (cfs) | |
| E.G. IC (ft) | 356.25 | Weir Sta Lft (ft) | |
| E.G. OC (ft) | 356.64 | Weir Sta Rgt (ft) | |
| Culvert Control | Outlet | Weir Submerg | |

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| | | | |
|---------------------|--------|------------------------|--------|
| Culv WS Inlet (ft) | 354.62 | Weir Max Depth (ft) | |
| Culv WS Outlet (ft) | 355.26 | Weir Avg Depth (ft) | |
| Culv Nml Depth (ft) | 1.80 | Weir Flow Area (sq ft) | |
| Culv Crt Depth (ft) | 2.87 | Min El Weir Flow (ft) | 363.01 |

Note: During the supercritical calculations a hydraulic jump occurred inside of the culvert.

CULVERT OUTPUT Profile #10 Yr Culv Group: PHAVE 24 N

| | | | |
|---------------------|---------|------------------------|--------|
| Q Culv Group (cfs) | 1458.74 | Culv Full Len (ft) | |
| # Barrels | 1 | Culv Vel US (ft/s) | 12.78 |
| Q Barrel (cfs) | 1458.74 | Culv Vel DS (ft/s) | 15.66 |
| E.G. US. (ft) | 360.37 | Culv Inv El Up (ft) | 351.75 |
| W.S. US. (ft) | 360.30 | Culv Inv El Dn (ft) | 351.22 |
| E.G. DS (ft) | 356.22 | Culv Frctn Ls (ft) | 0.19 |
| W.S. DS (ft) | 355.97 | Culv Exit Loss (ft) | 2.95 |
| Delta EG (ft) | 4.16 | Culv Entr Loss (ft) | 1.01 |
| Delta WS (ft) | 4.33 | Q Weir (cfs) | |
| E.G. IC (ft) | 359.87 | Weir Sta Lft (ft) | |
| E.G. OC (ft) | 360.37 | Weir Sta Rgt (ft) | |
| Culvert Control | Outlet | Weir Submerg | |
| Culv WS Inlet (ft) | 356.82 | Weir Max Depth (ft) | |
| Culv WS Outlet (ft) | 355.36 | Weir Avg Depth (ft) | |
| Culv Nml Depth (ft) | 3.12 | Weir Flow Area (sq ft) | |
| Culv Crt Depth (ft) | 5.07 | Min El Weir Flow (ft) | 363.01 |

Warning: Since the culvert has supercritical flow, the program should be run in mixed flow in order to check if the cross section downstream of the culvert has supercritical flow.

Note: The flow in the culvert is entirely supercritical.

CULVERT OUTPUT Profile #100 Yr Culv Group: PHAVE 24 N

| | | | |
|---------------------|---------|------------------------|--------|
| Q Culv Group (cfs) | 2367.72 | Culv Full Len (ft) | |
| # Barrels | 1 | Culv Vel US (ft/s) | 15.02 |
| Q Barrel (cfs) | 2367.72 | Culv Vel DS (ft/s) | 17.90 |
| E.G. US. (ft) | 363.68 | Culv Inv El Up (ft) | 351.75 |
| W.S. US. (ft) | 363.67 | Culv Inv El Dn (ft) | 351.22 |
| E.G. DS (ft) | 357.31 | Culv Frctn Ls (ft) | 0.18 |
| W.S. DS (ft) | 356.78 | Culv Exit Loss (ft) | 4.77 |
| Delta EG (ft) | 6.37 | Culv Entr Loss (ft) | 1.42 |
| Delta WS (ft) | 6.89 | Q Weir (cfs) | 699.30 |
| E.G. IC (ft) | 363.68 | Weir Sta Lft (ft) | 323.17 |
| E.G. OC (ft) | 363.66 | Weir Sta Rgt (ft) | 850.70 |
| Culvert Control | Inlet | Weir Submerg | 0.00 |
| Culv WS Inlet (ft) | 358.76 | Weir Max Depth (ft) | 0.68 |
| Culv WS Outlet (ft) | 357.10 | Weir Avg Depth (ft) | 0.63 |
| Culv Nml Depth (ft) | 4.31 | Weir Flow Area (sq ft) | 333.53 |
| Culv Crt Depth (ft) | 7.01 | Min El Weir Flow (ft) | 363.01 |

Warning: Since the culvert has supercritical flow, the program should be run in mixed flow in order to check if the cross section downstream of the culvert has supercritical flow.

Note: The flow in the culvert is entirely supercritical.

CULVERT OUTPUT Profile #2 Yr Culv Group: PHAVE 24 S

| | | | |
|--------------------|-------|--------------------|--------|
| Q Culv Group (cfs) | 16.88 | Culv Full Len (ft) | 128.15 |
| # Barrels | 1 | Culv Vel US (ft/s) | 5.37 |

| | | | |
|---------------------|--------|------------------------|--------|
| EcclestonMod.rep | | | |
| Q Barrel (cfs) | 16.88 | Culv Vel DS (ft/s) | 5.37 |
| E.G. US. (ft) | 356.64 | Culv Inv El Up (ft) | 352.71 |
| W.S. US. (ft) | 356.51 | Culv Inv El Dn (ft) | 352.35 |
| E.G. DS (ft) | 355.37 | Culv Frctn Ls (ft) | 0.70 |
| W.S. DS (ft) | 355.26 | Culv Exit Loss (ft) | 0.34 |
| Delta EG (ft) | 1.26 | Culv Entr Loss (ft) | 0.22 |
| Delta WS (ft) | 1.25 | Q Weir (cfs) | |
| E.G. IC (ft) | 355.19 | Weir Sta Lft (ft) | |
| E.G. OC (ft) | 356.65 | Weir Sta Rgt (ft) | |
| Culvert Control | Outlet | Weir Submerg | |
| Culv WS Inlet (ft) | 354.71 | Weir Max Depth (ft) | |
| Culv WS Outlet (ft) | 354.35 | Weir Avg Depth (ft) | |
| Culv Nml Depth (ft) | | Weir Flow Area (sq ft) | |
| Culv Crt Depth (ft) | 1.48 | Min El Weir Flow (ft) | 363.01 |

CULVERT OUTPUT Profile #10 Yr Culv Group: PHAve 24 S

| | | | |
|---------------------|--------|------------------------|--------|
| Q Culv Group (cfs) | 30.08 | Culv Full Len (ft) | 128.15 |
| # Barrels | 1 | Culv Vel US (ft/s) | 9.58 |
| Q Barrel (cfs) | 30.08 | Culv Vel DS (ft/s) | 9.58 |
| E.G. US. (ft) | 360.37 | Culv Inv El Up (ft) | 352.71 |
| W.S. US. (ft) | 360.30 | Culv Inv El Dn (ft) | 352.35 |
| E.G. DS (ft) | 356.22 | Culv Frctn Ls (ft) | 2.27 |
| W.S. DS (ft) | 355.97 | Culv Exit Loss (ft) | 1.18 |
| Delta EG (ft) | 4.16 | Culv Entr Loss (ft) | 0.71 |
| Delta WS (ft) | 4.33 | Q Weir (cfs) | |
| E.G. IC (ft) | 357.70 | Weir Sta Lft (ft) | |
| E.G. OC (ft) | 360.37 | Weir Sta Rgt (ft) | |
| Culvert Control | Outlet | Weir Submerg | |
| Culv WS Inlet (ft) | 354.71 | Weir Max Depth (ft) | |
| Culv WS Outlet (ft) | 354.35 | Weir Avg Depth (ft) | |
| Culv Nml Depth (ft) | | Weir Flow Area (sq ft) | |
| Culv Crt Depth (ft) | 1.86 | Min El Weir Flow (ft) | 363.01 |

CULVERT OUTPUT Profile #100 Yr Culv Group: PHAve 24 S

| | | | |
|---------------------|--------|------------------------|--------|
| Q Culv Group (cfs) | 37.65 | Culv Full Len (ft) | 128.15 |
| # Barrels | 1 | Culv Vel US (ft/s) | 11.98 |
| Q Barrel (cfs) | 37.65 | Culv Vel DS (ft/s) | 11.98 |
| E.G. US. (ft) | 363.68 | Culv Inv El Up (ft) | 352.71 |
| W.S. US. (ft) | 363.67 | Culv Inv El Dn (ft) | 352.35 |
| E.G. DS (ft) | 357.31 | Culv Frctn Ls (ft) | 3.55 |
| W.S. DS (ft) | 356.78 | Culv Exit Loss (ft) | 1.70 |
| Delta EG (ft) | 6.37 | Culv Entr Loss (ft) | 1.12 |
| Delta WS (ft) | 6.89 | Q Weir (cfs) | 699.30 |
| E.G. IC (ft) | 359.76 | Weir Sta Lft (ft) | 323.17 |
| E.G. OC (ft) | 363.68 | Weir Sta Rgt (ft) | 850.70 |
| Culvert Control | Outlet | Weir Submerg | 0.00 |
| Culv WS Inlet (ft) | 354.71 | Weir Max Depth (ft) | 0.68 |
| Culv WS Outlet (ft) | 354.35 | Weir Avg Depth (ft) | 0.63 |
| Culv Nml Depth (ft) | 2.00 | Weir Flow Area (sq ft) | 333.53 |
| Culv Crt Depth (ft) | 2.00 | Min El Weir Flow (ft) | 363.01 |

Note: The normal depth exceeds the height of the culvert. The program assumes that the normal depth is equal to the height of the culvert.

Note: Culvert critical depth exceeds the height of the culvert.

CROSS SECTION

EcclestonMod.rep

RIVER: JonesFalls
 REACH: JonesFalls3

RS: 4

CROSS SECTION OUTPUT Profile #2 Yr

| | | Element | Left OB | Channel |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 355.37 | | | |
| Right OB | | | | |
| Vel Head (ft) | 0.11 | wt. n-val. | 0.045 | 0.045 |
| 0.049 | | | | |
| W.S. Elev (ft) | 355.26 | Reach Len. (ft) | 31.99 | 41.27 |
| 41.76 | | | | |
| Crit w.s. (ft) | 354.43 | Flow Area (sq ft) | 39.33 | 114.91 |
| 127.18 | | | | |
| E.G. slope (ft/ft) | 0.002391 | Area (sq ft) | 53.55 | 114.91 |
| 201.86 | | | | |
| Q Total (cfs) | 655.40 | Flow (cfs) | 46.74 | 366.17 |
| 242.49 | | | | |
| Top width (ft) | 380.61 | Top width (ft) | 129.10 | 41.00 |
| 210.51 | | | | |
| Vel Total (ft/s) | 2.33 | Avg. vel. (ft/s) | 1.19 | 3.19 |
| 1.91 | | | | |
| Max Chl Dpth (ft) | 3.26 | Hydr. Depth (ft) | 0.64 | 2.80 |
| 1.47 | | | | |
| Conv. Total (cfs) | 13402.4 | Conv. (cfs) | 955.8 | 7487.9 |
| 4958.6 | | | | |
| Length wtd. (ft) | 39.57 | wetted Per. (ft) | 62.28 | 41.45 |
| 87.24 | | | | |
| Min Ch El (ft) | 352.00 | shear (lb/sq ft) | 0.09 | 0.41 |
| 0.22 | | | | |
| Alpha | 1.31 | Stream Power (lb/ft s) | 1040.91 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 0.09 | Cum Volume (acre-ft) | 0.79 | 0.53 |
| 0.75 | | | | |
| C & E Loss (ft) | 0.02 | Cum SA (acres) | 0.54 | 0.15 |
| 0.57 | | | | |

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION OUTPUT Profile #10 Yr

| | | Element | Left OB | Channel |
|--------------------|----------|-------------------|---------|---------|
| E.G. Elev (ft) | 356.22 | | | |
| Right OB | | | | |
| Vel Head (ft) | 0.25 | wt. n-val. | 0.045 | 0.045 |
| 0.049 | | | | |
| W.S. Elev (ft) | 355.97 | Reach Len. (ft) | 31.99 | 41.27 |
| 41.76 | | | | |
| Crit w.s. (ft) | 355.00 | Flow Area (sq ft) | 82.89 | 143.92 |
| 188.62 | | | | |
| E.G. slope (ft/ft) | 0.004092 | Area (sq ft) | 172.28 | 143.92 |
| 376.68 | | | | |
| Q Total (cfs) | 1520.50 | Flow (cfs) | 211.54 | 697.15 |
| 611.81 | | | | |
| Top width (ft) | 538.37 | Top width (ft) | 213.87 | 41.00 |
| 283.50 | | | | |
| Vel Total (ft/s) | 3.66 | Avg. vel. (ft/s) | 2.55 | 4.84 |
| 3.24 | | | | |

| EcclestonMod.rep | | | | |
|-------------------|---------|------------------------|---------|---------|
| Max Chl Dpth (ft) | 3.97 | Hydr. Depth (ft) | 1.35 | 3.51 |
| 2.17 | | | | |
| Conv. Total (cfs) | 23768.9 | Conv. (cfs) | 3306.8 | 10898.0 |
| 9564.0 | | | | |
| Length wtd. (ft) | 39.05 | wetted Per. (ft) | 62.41 | 41.45 |
| 87.24 | | | | |
| Min Ch El (ft) | 352.00 | Shear (lb/sq ft) | 0.34 | 0.89 |
| 0.55 | | | | |
| Alpha | 1.19 | Stream Power (lb/ft s) | 1040.91 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 0.14 | Cum Volume (acre-ft) | 1.46 | 0.68 |
| 1.52 | | | | |
| C & E Loss (ft) | 0.05 | Cum SA (acres) | 0.69 | 0.15 |
| 0.77 | | | | |

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION OUTPUT Profile #100 Yr

| Profile #100 Yr | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 357.31 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.53 | wt. n-Val. | 0.045 | 0.045 |
| 0.049 | | | | |
| W.S. Elev (ft) | 356.78 | Reach Len. (ft) | 31.99 | 41.27 |
| 41.76 | | | | |
| Crit w.s. (ft) | 356.02 | Flow Area (sq ft) | 132.97 | 177.29 |
| 259.26 | | | | |
| E.G. slope (ft/ft) | 0.006518 | Area (sq ft) | 355.68 | 177.29 |
| 629.96 | | | | |
| Q Total (cfs) | 3144.30 | Flow (cfs) | 586.92 | 1245.39 |
| 1311.99 | | | | |
| Top width (ft) | 612.62 | Top width (ft) | 233.69 | 41.00 |
| 337.93 | | | | |
| Vel Total (ft/s) | 5.52 | Avg. Vel. (ft/s) | 4.41 | 7.02 |
| 5.06 | | | | |
| Max Chl Dpth (ft) | 4.78 | Hydr. Depth (ft) | 2.16 | 4.32 |
| 2.99 | | | | |
| Conv. Total (cfs) | 38946.9 | Conv. (cfs) | 7269.9 | 15426.0 |
| 16251.0 | | | | |
| Length wtd. (ft) | 38.72 | wetted Per. (ft) | 62.41 | 41.45 |
| 87.24 | | | | |
| Min Ch El (ft) | 352.00 | Shear (lb/sq ft) | 0.87 | 1.74 |
| 1.21 | | | | |
| Alpha | 1.11 | Stream Power (lb/ft s) | 1040.91 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 0.20 | Cum Volume (acre-ft) | 2.43 | 0.86 |
| 2.74 | | | | |
| C & E Loss (ft) | 0.12 | Cum SA (acres) | 0.80 | 0.15 |
| 0.96 | | | | |

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, water surface was used.

CROSS SECTION

RIVER: JonesFalls

REACH: JonesFalls3

RS: 3.5

CROSS SECTION OUTPUT Profile #2 Yr

| | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 355.26 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.07 | wt. n-val. | 0.045 | 0.049 |
| 0.045 | | | | |
| W.S. Elev (ft) | 355.19 | Reach Len. (ft) | 129.00 | 124.00 |
| 114.00 | | | | |
| Crit w.s. (ft) | 354.61 | Flow Area (sq ft) | 130.94 | 95.87 |
| 112.97 | | | | |
| E.G. slope (ft/ft) | 0.002228 | Area (sq ft) | 150.11 | 95.87 |
| 135.08 | | | | |
| Q Total (cfs) | 655.40 | Flow (cfs) | 216.18 | 257.10 |
| 182.12 | | | | |
| Top width (ft) | 371.32 | Top width (ft) | 159.17 | 37.04 |
| 175.11 | | | | |
| Vel Total (ft/s) | 1.93 | Avg. Vel. (ft/s) | 1.65 | 2.68 |
| 1.61 | | | | |
| Max Chl Dpth (ft) | 3.19 | Hydr. Depth (ft) | 1.09 | 2.59 |
| 1.05 | | | | |
| Conv. Total (cfs) | 13883.6 | Conv. (cfs) | 4579.4 | 5446.2 |
| 3858.0 | | | | |
| Length wtd. (ft) | 123.62 | wetted Per. (ft) | 120.13 | 37.40 |
| 107.41 | | | | |
| Min Ch El (ft) | 352.00 | Shear (lb/sq ft) | 0.15 | 0.36 |
| 0.15 | | | | |
| Alpha | 1.19 | Stream Power (lb/ft s) | 879.65 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 0.56 | Cum Volume (acre-ft) | 0.72 | 0.43 |
| 0.59 | | | | |
| C & E Loss (ft) | 0.02 | Cum SA (acres) | 0.43 | 0.11 |
| 0.38 | | | | |

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

This may indicate the need for additional cross sections.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, energy was used.

CROSS SECTION OUTPUT Profile #10 Yr

| | | | | |
|--------------------|----------|-------------------|---------|---------|
| E.G. Elev (ft) | 356.03 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.14 | wt. n-val. | 0.045 | 0.049 |
| 0.045 | | | | |
| W.S. Elev (ft) | 355.89 | Reach Len. (ft) | 129.00 | 124.00 |
| 114.00 | | | | |
| Crit w.s. (ft) | 355.06 | Flow Area (sq ft) | 214.32 | 121.59 |
| 187.53 | | | | |
| E.G. slope (ft/ft) | 0.003061 | Area (sq ft) | 274.04 | 121.59 |
| 281.61 | | | | |
| Q Total (cfs) | 1520.50 | Flow (cfs) | 576.00 | 447.73 |
| 496.77 | | | | |
| Top width (ft) | 481.97 | Top width (ft) | 197.86 | 37.04 |
| 247.06 | | | | |
| Vel Total (ft/s) | 2.90 | Avg. Vel. (ft/s) | 2.69 | 3.68 |

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| | | | | |
|-------------------|---------|------------------------|---------|--------|
| 2.65 | | | | |
| Max Chl Dpth (ft) | 3.89 | Hydr. Depth (ft) | 1.78 | 3.28 |
| 1.75 | | | | |
| Conv. Total (cfs) | 27481.5 | Conv. (cfs) | 10410.7 | 8092.2 |
| 8978.6 | | | | |
| Length wtd. (ft) | 123.09 | wetted Per. (ft) | 120.13 | 37.40 |
| 107.41 | | | | |
| Min Ch El (ft) | 352.00 | Shear (lb/sq ft) | 0.34 | 0.62 |
| 0.33 | | | | |
| Alpha | 1.07 | Stream Power (lb/ft s) | 879.65 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 0.73 | Cum Volume (acre-ft) | 1.30 | 0.55 |
| 1.20 | | | | |
| C & E Loss (ft) | 0.02 | Cum SA (acres) | 0.54 | 0.11 |
| 0.52 | | | | |

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

This may indicate the need for additional cross sections.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, energy was used.

CROSS SECTION OUTPUT Profile #100 Yr

| | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 356.99 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.29 | wt. n-val. | 0.045 | 0.049 |
| 0.045 | | | | |
| w.s. Elev (ft) | 356.70 | Reach Len. (ft) | 129.00 | 124.00 |
| 114.00 | | | | |
| Crit w.s. (ft) | 355.65 | Flow Area (sq ft) | 312.18 | 151.76 |
| 275.03 | | | | |
| E.G. Slope (ft/ft) | 0.004257 | Area (sq ft) | 449.75 | 151.76 |
| 508.59 | | | | |
| Q Total (cfs) | 3144.30 | Flow (cfs) | 1271.31 | 763.97 |
| 1109.02 | | | | |
| Top width (ft) | 575.75 | Top width (ft) | 231.95 | 37.04 |
| 306.76 | | | | |
| Vel Total (ft/s) | 4.26 | Avg. Vel. (ft/s) | 4.07 | 5.03 |
| 4.03 | | | | |
| Max Chl Dpth (ft) | 4.70 | Hydr. Depth (ft) | 2.60 | 4.10 |
| 2.56 | | | | |
| Conv. Total (cfs) | 48190.7 | Conv. (cfs) | 19484.5 | 11708.9 |
| 16997.3 | | | | |
| Length wtd. (ft) | 122.83 | wetted Per. (ft) | 120.13 | 37.40 |
| 107.41 | | | | |
| Min Ch El (ft) | 352.00 | Shear (lb/sq ft) | 0.69 | 1.08 |
| 0.68 | | | | |
| Alpha | 1.03 | Stream Power (lb/ft s) | 879.65 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 0.96 | Cum Volume (acre-ft) | 2.13 | 0.70 |
| 2.19 | | | | |
| C & E Loss (ft) | 0.03 | Cum SA (acres) | 0.63 | 0.11 |
| 0.66 | | | | |

Warning: The conveyance ratio (upstream conveyance divided by downstream conveyance) is less than 0.7 or greater than 1.4.

This may indicate the need for additional cross sections.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, energy was used.

CROSS SECTION

RIVER: JonesFalls
 REACH: JonesFalls3 RS: 3

CROSS SECTION OUTPUT Profile #2 Yr

| | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 354.68 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.24 | wt. n-val. | 0.045 | 0.049 |
| 0.045 | | | | |
| W.S. Elev (ft) | 354.44 | Reach Len. (ft) | 170.00 | 170.00 |
| 170.00 | | | | |
| Crit w.s. (ft) | 353.99 | Flow Area (sq ft) | 83.08 | 65.24 |
| 45.69 | | | | |
| E.G. slope (ft/ft) | 0.014080 | Area (sq ft) | 83.08 | 65.24 |
| 45.69 | | | | |
| Q Total (cfs) | 655.40 | Flow (cfs) | 237.68 | 323.21 |
| 94.50 | | | | |
| Top width (ft) | 292.32 | Top width (ft) | 133.10 | 40.11 |
| 119.11 | | | | |
| Vel Total (ft/s) | 3.38 | Avg. vel. (ft/s) | 2.86 | 4.95 |
| 2.07 | | | | |
| Max Chl Dpth (ft) | 2.44 | Hydr. Depth (ft) | 0.62 | 1.63 |
| 0.38 | | | | |
| Conv. Total (cfs) | 5523.4 | Conv. (cfs) | 2003.1 | 2723.9 |
| 796.4 | | | | |
| Length wtd. (ft) | 170.00 | wetted Per. (ft) | 133.17 | 40.38 |
| 119.11 | | | | |
| Min Ch El (ft) | 352.00 | Shear (lb/sq ft) | 0.55 | 1.42 |
| 0.34 | | | | |
| Alpha | 1.37 | Stream Power (lb/ft s) | 882.29 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 1.97 | Cum volume (acre-ft) | 0.37 | 0.20 |
| 0.36 | | | | |
| C & E Loss (ft) | 0.04 | Cum SA (acres) | | |

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, energy was used.

CROSS SECTION OUTPUT Profile #10 Yr

| | | | | |
|----------------|--------|-------------------|---------|---------|
| E.G. Elev (ft) | 355.27 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.36 | wt. n-val. | 0.045 | 0.049 |
| 0.045 | | | | |
| W.S. Elev (ft) | 354.91 | Reach Len. (ft) | 170.00 | 170.00 |
| 170.00 | | | | |
| Crit w.s. (ft) | 354.84 | Flow Area (sq ft) | 154.53 | 84.21 |
| 109.42 | | | | |

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| | | | | |
|----------------------------|----------|------------------------|--------|--------|
| E.G. Slope (ft/ft) | 0.016323 | Area (sq ft) | 154.53 | 84.21 |
| 109.42 Q Total (cfs) | 1520.50 | Flow (cfs) | 614.26 | 532.63 |
| 373.61 Top width (ft) | 359.27 | Top width (ft) | 168.89 | 40.11 |
| 150.28 Vel Total (ft/s) | 4.37 | Avg. Vel. (ft/s) | 3.98 | 6.32 |
| 3.41 Max Chl Dpth (ft) | 2.91 | Hydr. Depth (ft) | 0.91 | 2.10 |
| 0.73 Conv. Total (cfs) | 11901.0 | Conv. (cfs) | 4807.8 | 4169.0 |
| 2924.3 Length wtd. (ft) | 170.00 | wetted Per. (ft) | 168.96 | 40.38 |
| 150.28 Min Ch El (ft) | 352.00 | Shear (lb/sq ft) | 0.93 | 2.13 |
| 0.74 Alpha | 1.22 | Stream Power (lb/ft s) | 882.29 | 0.00 |
| 0.00 Frctn Loss (ft) | 2.08 | Cum volume (acre-ft) | 0.67 | 0.26 |
| 0.69 C & E Loss (ft) | 0.05 | Cum SA (acres) | | |

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, energy was used.

CROSS SECTION OUTPUT Profile #100 Yr

| | | | | |
|------------------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 356.00 | Element | Left OB | Channel |
| Right OB Vel Head (ft) | 0.56 | wt. n-val. | 0.045 | 0.049 |
| 0.045 W.S. Elev (ft) | 355.45 | Reach Len. (ft) | 170.00 | 170.00 |
| 170.00 Crit w.s. (ft) | 355.39 | Flow Area (sq ft) | 251.66 | 105.71 |
| 199.39 E.G. slope (ft/ft) | 0.018691 | Area (sq ft) | 251.66 | 105.71 |
| 201.25 Q Total (cfs) | 3144.30 | Flow (cfs) | 1367.58 | 832.45 |
| 944.27 Top width (ft) | 424.49 | Top width (ft) | 190.46 | 40.11 |
| 193.92 Vel Total (ft/s) | 5.65 | Avg. Vel. (ft/s) | 5.43 | 7.88 |
| 4.74 Max Chl Dpth (ft) | 3.45 | Hydr. Depth (ft) | 1.32 | 2.64 |
| 1.07 Conv. Total (cfs) | 22999.0 | Conv. (cfs) | 10003.2 | 6089.0 |
| 6906.9 Length wtd. (ft) | 170.00 | wetted Per. (ft) | 190.54 | 40.38 |
| 185.58 Min Ch El (ft) | 352.00 | Shear (lb/sq ft) | 1.54 | 3.05 |
| 1.25 Alpha | 1.13 | Stream Power (lb/ft s) | 882.29 | 0.00 |
| 0.00 Frctn Loss (ft) | 2.13 | Cum volume (acre-ft) | 1.09 | 0.33 |
| 1.26 C & E Loss (ft) | 0.09 | Cum SA (acres) | | |

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Warning: Divided flow computed for this cross-section.
 Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.
 Note: Multiple critical depths were found at this location. The critical depth with the lowest, valid, energy was used.

CROSS SECTION

RIVER: JonesFalls
 REACH: JonesFalls4 RS: 2

CROSS SECTION OUTPUT Profile #2 Yr

| | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 352.67 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.11 | wt. n-val. | 0.041 | 0.049 |
| 0.042 | | | | |
| W.S. Elev (ft) | 352.56 | Reach Len. (ft) | 261.00 | 248.00 |
| 241.00 | | | | |
| Crit w.s. (ft) | 352.42 | Flow Area (sq ft) | 106.72 | 38.29 |
| 136.94 | | | | |
| E.G. Slope (ft/ft) | 0.009853 | Area (sq ft) | 106.72 | 38.29 |
| 136.94 | | | | |
| Q Total (cfs) | 721.70 | Flow (cfs) | 257.43 | 139.97 |
| 324.30 | | | | |
| Top width (ft) | 479.35 | Top width (ft) | 195.90 | 28.32 |
| 255.12 | | | | |
| Vel Total (ft/s) | 2.56 | Avg. Vel. (ft/s) | 2.41 | 3.66 |
| 2.37 | | | | |
| Max Chl Dpth (ft) | 2.33 | Hydr. Depth (ft) | 0.54 | 1.35 |
| 0.54 | | | | |
| Conv. Total (cfs) | 7270.5 | Conv. (cfs) | 2593.4 | 1410.1 |
| 3267.0 | | | | |
| Length wtd. (ft) | 247.24 | wetted Per. (ft) | 195.92 | 28.62 |
| 255.19 | | | | |
| Min Ch El (ft) | 350.23 | Shear (lb/sq ft) | 0.34 | 0.82 |
| 0.33 | | | | |
| Alpha | 1.10 | Stream Power (lb/ft s) | 857.88 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 1.89 | Cum Volume (acre-ft) | 0.52 | 0.19 |
| 1.06 | | | | |
| C & E Loss (ft) | 0.01 | Cum SA (acres) | 0.94 | 0.15 |
| 1.76 | | | | |

Warning: Divided flow computed for this cross-section.
 Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

CROSS SECTION OUTPUT Profile #10 Yr

| | | | | |
|----------------|--------|---------|---------|---------|
| E.G. Elev (ft) | 353.15 | Element | Left OB | Channel |
|----------------|--------|---------|---------|---------|

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| | | | | |
|--------------------|----------|------------------------|--------|--------|
| Right OB | | | | |
| Vel Head (ft) | 0.19 | Wt. n-val. | 0.041 | 0.049 |
| 0.042 | | | | |
| W.S. Elev (ft) | 352.96 | Reach Len. (ft) | 261.00 | 248.00 |
| 241.00 | | | | |
| Crit w.s. (ft) | | Flow Area (sq ft) | 186.99 | 49.75 |
| 244.75 | | | | |
| E.G. slope (ft/ft) | 0.009669 | Area (sq ft) | 186.99 | 49.75 |
| 244.75 | | | | |
| Q Total (cfs) | 1659.40 | Flow (cfs) | 637.71 | 214.46 |
| 807.23 | | | | |
| Top width (ft) | 517.87 | Top width (ft) | 201.35 | 28.32 |
| 288.20 | | | | |
| Vel Total (ft/s) | 3.45 | Avg. vel. (ft/s) | 3.41 | 4.31 |
| 3.30 | | | | |
| Max Chl Dpth (ft) | 2.73 | Hydr. Depth (ft) | 0.93 | 1.76 |
| 0.85 | | | | |
| Conv. Total (cfs) | 16875.6 | Conv. (cfs) | 6485.3 | 2181.0 |
| 8209.3 | | | | |
| Length wtd. (ft) | 247.34 | wetted Per. (ft) | 201.38 | 28.62 |
| 288.31 | | | | |
| Min Ch El (ft) | 350.23 | Shear (lb/sq ft) | 0.56 | 1.05 |
| 0.51 | | | | |
| Alpha | 1.02 | Stream Power (lb/ft s) | 857.88 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 1.88 | Cum Volume (acre-ft) | 0.93 | 0.25 |
| 1.84 | | | | |
| C & E Loss (ft) | 0.02 | Cum SA (acres) | 1.03 | 0.15 |
| 1.90 | | | | |

Warning: Divided flow computed for this cross-section.
 Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

CROSS SECTION OUTPUT Profile #100 Yr

| | | | | |
|--------------------|----------|-------------------|---------|---------|
| E.G. Elev (ft) | 353.79 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.27 | Wt. n-val. | 0.041 | 0.049 |
| 0.041 | | | | |
| W.S. Elev (ft) | 353.51 | Reach Len. (ft) | 261.00 | 248.00 |
| 241.00 | | | | |
| Crit w.s. (ft) | | Flow Area (sq ft) | 308.50 | 65.45 |
| 445.05 | | | | |
| E.G. slope (ft/ft) | 0.009184 | Area (sq ft) | 308.50 | 65.45 |
| 445.05 | | | | |
| Q Total (cfs) | 3405.50 | Flow (cfs) | 1332.89 | 330.16 |
| 1742.45 | | | | |
| Top width (ft) | 624.06 | Top width (ft) | 224.43 | 28.32 |
| 371.31 | | | | |
| Vel Total (ft/s) | 4.16 | Avg. vel. (ft/s) | 4.32 | 5.04 |
| 3.92 | | | | |
| Max Chl Dpth (ft) | 3.28 | Hydr. Depth (ft) | 1.37 | 2.31 |
| 1.20 | | | | |
| Conv. Total (cfs) | 35535.0 | Conv. (cfs) | 13908.2 | 3445.1 |
| 18181.7 | | | | |
| Length wtd. (ft) | 247.41 | wetted Per. (ft) | 224.48 | 28.62 |
| 371.43 | | | | |
| Min Ch El (ft) | 350.23 | Shear (lb/sq ft) | 0.79 | 1.31 |

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| | | | | |
|-----------------|------|------------------------|--------|------|
| 0.69 | | | | |
| Alpha | 1.02 | Stream Power (lb/ft s) | 857.88 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | 1.84 | Cum Volume (acre-ft) | 1.57 | 0.34 |
| 3.05 | | | | |
| C & E Loss (ft) | 0.02 | Cum SA (acres) | 1.18 | 0.15 |
| 2.19 | | | | |

Warning: The energy loss was greater than 1.0 ft (0.3 m). between the current and previous cross section. This may indicate the need for additional cross sections.

CROSS SECTION

RIVER: JonesFalls
 REACH: JonesFalls4 RS: 1

CROSS SECTION OUTPUT Profile #2 Yr

| | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 350.76 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.07 | wt. n-val. | 0.045 | 0.049 |
| 0.041 | | | | |
| w.s. Elev (ft) | 350.69 | Reach Len. (ft) | | |
| | | | | |
| Crit w.s. (ft) | 350.42 | Flow Area (sq ft) | 66.92 | 28.51 |
| 247.55 | | | | |
| E.G. Slope (ft/ft) | 0.006131 | Area (sq ft) | 66.92 | 28.51 |
| 247.55 | | | | |
| Q Total (cfs) | 721.70 | Flow (cfs) | 118.22 | 74.43 |
| 529.05 | | | | |
| Top width (ft) | 523.08 | Top width (ft) | 118.50 | 24.61 |
| 379.97 | | | | |
| Vel Total (ft/s) | 2.10 | Avg. vel. (ft/s) | 1.77 | 2.61 |
| 2.14 | | | | |
| Max Chl Dpth (ft) | 1.81 | Hydr. Depth (ft) | 0.56 | 1.16 |
| 0.65 | | | | |
| Conv. Total (cfs) | 9217.1 | Conv. (cfs) | 1509.8 | 950.6 |
| 6756.7 | | | | |
| Length wtd. (ft) | | wetted Per. (ft) | 118.51 | 24.73 |
| 379.99 | | | | |
| Min Ch El (ft) | 348.88 | Shear (lb/sq ft) | 0.22 | 0.44 |
| 0.25 | | | | |
| Alpha | 1.03 | Stream Power (lb/ft s) | 821.31 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | | Cum Volume (acre-ft) | | |
| | | | | |
| C & E Loss (ft) | | Cum SA (acres) | | |

CROSS SECTION OUTPUT Profile #10 Yr

| | | | | |
|----------------|--------|------------|---------|---------|
| E.G. Elev (ft) | 351.26 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.13 | wt. n-val. | 0.045 | 0.049 |

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| | | | | |
|--------------------|----------|------------------------|--------|--------|
| 0.041 | | | | |
| W.S. Elev (ft) | 351.13 | Reach Len. (ft) | | |
| Crit w.s. (ft) | 350.72 | Flow Area (sq ft) | 125.08 | 39.38 |
| 419.04 | | | | |
| E.G. Slope (ft/ft) | 0.006135 | Area (sq ft) | 125.08 | 39.38 |
| 419.04 | | | | |
| Q Total (cfs) | 1659.40 | Flow (cfs) | 295.10 | 127.52 |
| 1236.78 | | | | |
| Top Width (ft) | 565.06 | Top width (ft) | 143.56 | 24.61 |
| 396.89 | | | | |
| Vel Total (ft/s) | 2.84 | Avg. Vel. (ft/s) | 2.36 | 3.24 |
| 2.95 | | | | |
| Max Chl Dpth (ft) | 2.25 | Hydr. Depth (ft) | 0.87 | 1.60 |
| 1.06 | | | | |
| Conv. Total (cfs) | 21186.1 | Conv. (cfs) | 3767.6 | 1628.1 |
| 15790.4 | | | | |
| Length wtd. (ft) | | wetted Per. (ft) | 143.57 | 24.73 |
| 396.92 | | | | |
| Min Ch El (ft) | 348.88 | Shear (lb/sq ft) | 0.33 | 0.61 |
| 0.40 | | | | |
| Alpha | 1.02 | Stream Power (lb/ft s) | 821.31 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | | Cum Volume (acre-ft) | | |
| C & E Loss (ft) | | Cum SA (acres) | | |

CROSS SECTION OUTPUT Profile #100 Yr

| | | | | |
|--------------------|----------|------------------------|---------|---------|
| E.G. Elev (ft) | 351.93 | Element | Left OB | Channel |
| Right OB | | | | |
| Vel Head (ft) | 0.21 | wt. n-Val. | 0.045 | 0.049 |
| 0.041 | | | | |
| W.S. Elev (ft) | 351.71 | Reach Len. (ft) | | |
| Crit w.s. (ft) | 351.13 | Flow Area (sq ft) | 217.08 | 53.80 |
| 658.20 | | | | |
| E.G. Slope (ft/ft) | 0.006131 | Area (sq ft) | 217.08 | 53.80 |
| 658.20 | | | | |
| Q Total (cfs) | 3405.50 | Flow (cfs) | 659.43 | 214.45 |
| 2531.62 | | | | |
| Top Width (ft) | 614.41 | Top Width (ft) | 170.44 | 24.61 |
| 419.35 | | | | |
| Vel Total (ft/s) | 3.67 | Avg. Vel. (ft/s) | 3.04 | 3.99 |
| 3.85 | | | | |
| Max Chl Dpth (ft) | 2.83 | Hydr. Depth (ft) | 1.27 | 2.19 |
| 1.57 | | | | |
| Conv. Total (cfs) | 43493.2 | Conv. (cfs) | 8421.9 | 2738.8 |
| 32332.4 | | | | |
| Length wtd. (ft) | | wetted Per. (ft) | 170.46 | 24.73 |
| 419.39 | | | | |
| Min Ch El (ft) | 348.88 | Shear (lb/sq ft) | 0.49 | 0.83 |
| 0.60 | | | | |
| Alpha | 1.03 | Stream Power (lb/ft s) | 821.31 | 0.00 |
| 0.00 | | | | |
| Frctn Loss (ft) | | Cum Volume (acre-ft) | | |
| C & E Loss (ft) | | Cum SA (acres) | | |

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SUMMARY OF MANNING'S N VALUES

River:JonesFalls

| Reach n6 | n7 | River Sta. | n1 | n2 | n3 | n4 | n5 | |
|--------------------|-----|------------|---------|------|------|------|------|--|
| JonesFalls | | 15 | .11 | .049 | .11 | .04 | | |
| JonesFalls | | 14 | .11 | .049 | .11 | .04 | | |
| JonesFalls | | 13 | .04 | .11 | .049 | .04 | | |
| NorthTrib | | 2 | .04 | .061 | .04 | | | |
| NorthTrib | | 1 | .04 | .061 | .04 | | | |
| JonesFalls2 .11 | .04 | 12 | .04 | .11 | .04 | .11 | .049 | |
| JonesFalls2 .11 | .04 | 11 | .04 | .11 | .04 | .11 | .049 | |
| SouthTrib | | 8 | .045 | .057 | .045 | | | |
| SouthTrib | | 7 | .045 | .057 | .045 | | | |
| SouthTrib | | 6.5 | Bridge | | | | | |
| SouthTrib | | 6 | .045 | .057 | .045 | | | |
| SouthTrib | | 5 | .04 | .045 | .057 | .045 | .04 | |
| SouthTrib | | 4 | .04 | .057 | .04 | .045 | | |
| SouthTrib | | 3 | .04 | .057 | .04 | .057 | .04 | |
| SouthTrib | | 2 | .04 | .057 | .04 | .057 | .04 | |
| SouthTrib | | 1 | .04 | .057 | .04 | .057 | .04 | |
| IntsTrib .045 | | 8 | .013 | .045 | .046 | .045 | .013 | |
| IntsTrib | | 7 | .013 | .045 | .046 | .045 | | |
| IntsTrib | | 6.5 | Culvert | | | | | |
| IntsTrib | | 6 | .013 | .04 | .046 | .04 | | |
| IntsTrib | | 5 | .013 | .04 | .046 | .04 | | |
| IntsTrib | | 4 | .013 | .04 | .046 | .04 | | |
| IntsTrib | | 3 | .04 | .046 | .04 | | | |
| IntsTrib | | 2.5 | Culvert | | | | | |
| IntsTrib | | 2 | .045 | .046 | .045 | .013 | | |

EcclestonMod.rep

| | | | | | | |
|-------------|-----|---------|------|------|------|------|
| IntsTrib | 1 | .04 | .046 | .045 | | |
| JonesFalls3 | 10 | .04 | .11 | .049 | .11 | .04 |
| JonesFalls3 | 9 | .04 | .11 | .049 | .11 | .04 |
| JonesFalls3 | 8 | .04 | .11 | .049 | .04 | |
| JonesFalls3 | 7 | .04 | .11 | .049 | .11 | .04 |
| JonesFalls3 | 6 | .04 | .11 | .049 | .11 | |
| JonesFalls3 | 5 | .04 | .11 | .049 | .11 | .045 |
| JonesFalls3 | 4.5 | Culvert | | | | |
| JonesFalls3 | 4 | .045 | .045 | .049 | .045 | |
| JonesFalls3 | 3.5 | .045 | .049 | .045 | | |
| JonesFalls3 | 3 | .045 | .049 | .045 | | |
| JonesFalls4 | 2 | .04 | .045 | .049 | .045 | .04 |
| JonesFalls4 | 1 | .045 | .049 | .045 | .04 | |

SUMMARY OF REACH LENGTHS

River: JonesFalls

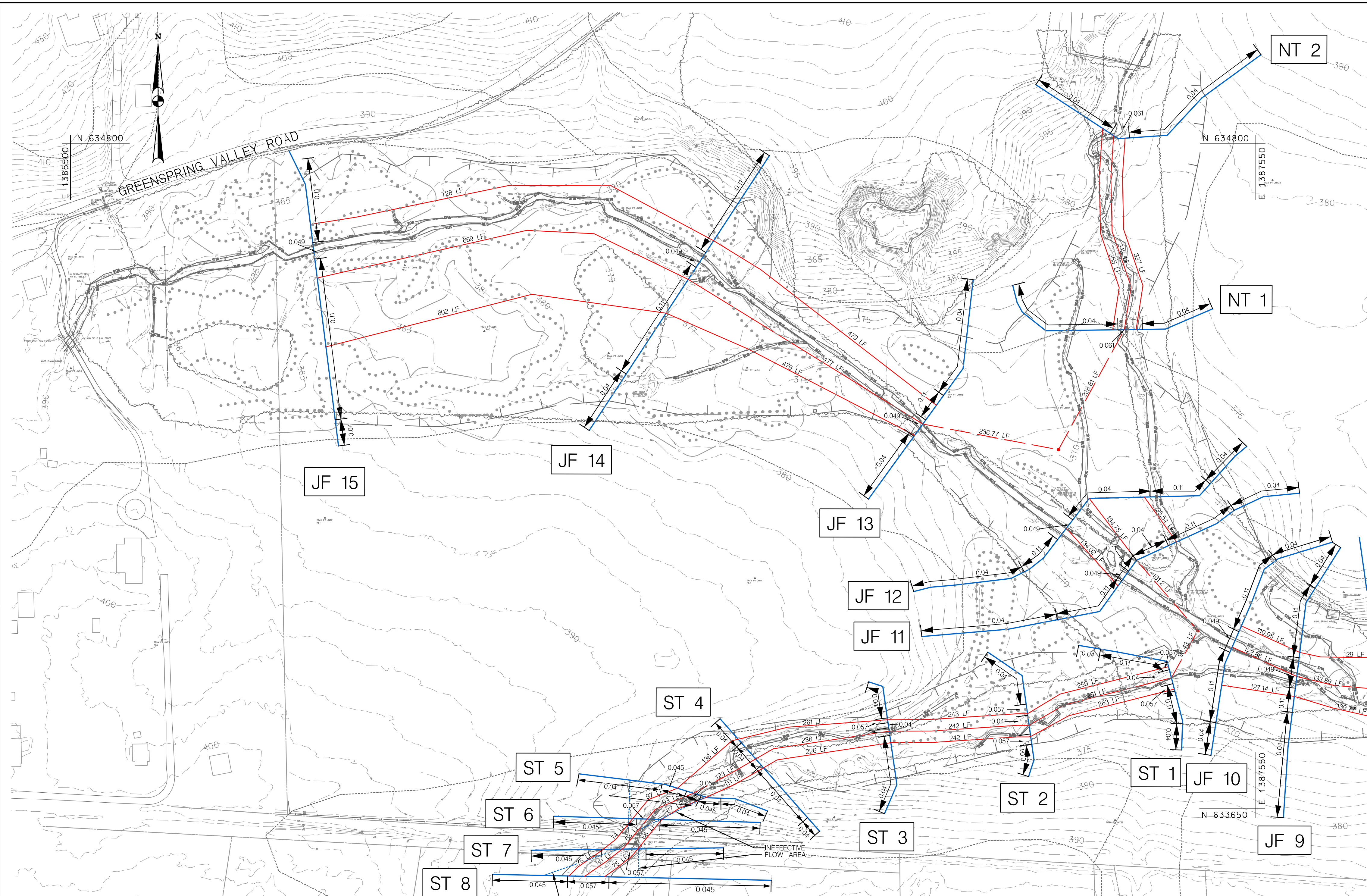
| Reach | River Sta. | Left | Channel | Right |
|-------------|------------|---------|---------|--------|
| JonesFalls | 15 | 728 | 669 | 602 |
| JonesFalls | 14 | 479 | 477 | 479 |
| JonesFalls | 13 | 306 | 307 | 306 |
| NorthTrib | 2 | 337.47 | 342.24 | 354.84 |
| NorthTrib | 1 | | | |
| JonesFalls2 | 12 | 95.54 | 134.75 | 134.02 |
| JonesFalls2 | 11 | | | |
| SouthTrib | 8 | 75 | 80 | 75 |
| SouthTrib | 7 | 74.34 | 67.83 | 65.615 |
| SouthTrib | 6.5 | Bridge | | |
| SouthTrib | 6 | 96.56 | 93.29 | 86.62 |
| SouthTrib | 5 | 136.21 | 123.08 | 111.2 |
| SouthTrib | 4 | 261.13 | 237.95 | 226.16 |
| SouthTrib | 3 | 243 | 242 | 242 |
| SouthTrib | 2 | 259 | 261 | 263 |
| SouthTrib | 1 | | | |
| IntsTrib | 8 | 135 | 134 | 134 |
| IntsTrib | 7 | 151 | 152 | 154 |
| IntsTrib | 6.5 | Culvert | | |
| IntsTrib | 6 | 117 | 118 | 119 |
| IntsTrib | 5 | 363 | 358 | 354 |
| IntsTrib | 4 | 188 | 207 | 219 |
| IntsTrib | 3 | 112 | 116 | 119 |
| IntsTrib | 2.5 | Culvert | | |
| IntsTrib | 2 | 209 | 187 | 167 |

EcclestonMod.rep

| | | | | |
|-------------|-----|---------|--------|--------|
| IntsTrib | 1 | | | |
| JonesFalls3 | 10 | 110.95 | 122.86 | 127.14 |
| JonesFalls3 | 9 | 129 | 133.89 | 139.77 |
| JonesFalls3 | 8 | 491.9 | 504.1 | 506.12 |
| JonesFalls3 | 7 | 469.28 | 475.2 | 444.49 |
| JonesFalls3 | 6 | 121.97 | 81.55 | 93.44 |
| JonesFalls3 | 5 | 131.69 | 149 | 230.44 |
| JonesFalls3 | 4.5 | Culvert | | |
| JonesFalls3 | 4 | 31.99 | 41.27 | 41.76 |
| JonesFalls3 | 3.5 | 129 | 124 | 114 |
| JonesFalls3 | 3 | | | |
| JonesFalls4 | 2 | 261 | 248 | 241 |
| JonesFalls4 | 1 | | | |

SUMMARY OF CONTRACTION AND EXPANSION COEFFICIENTS
River: JonesFalls

| Reach | River Sta. | Contr. | Expan. |
|-------------|------------|---------|--------|
| JonesFalls | 15 | .1 | .3 |
| JonesFalls | 14 | .1 | .3 |
| JonesFalls | 13 | .1 | .3 |
| NorthTrib | 2 | .1 | .3 |
| NorthTrib | 1 | .1 | .3 |
| JonesFalls2 | 12 | .1 | .3 |
| JonesFalls2 | 11 | .1 | .3 |
| SouthTrib | 8 | .1 | .3 |
| SouthTrib | 7 | .3 | .5 |
| SouthTrib | 6.5 | Bridge | |
| SouthTrib | 6 | .3 | .5 |
| SouthTrib | 5 | .1 | .3 |
| SouthTrib | 4 | .1 | .3 |
| SouthTrib | 3 | .1 | .3 |
| SouthTrib | 2 | .1 | .3 |
| SouthTrib | 1 | .1 | .3 |
| IntsTrib | 8 | .1 | .3 |
| IntsTrib | 7 | .3 | .5 |
| IntsTrib | 6.5 | Culvert | |
| IntsTrib | 6 | .3 | .5 |
| IntsTrib | 5 | .1 | .3 |
| IntsTrib | 4 | .1 | .3 |
| IntsTrib | 3 | .3 | .5 |
| IntsTrib | 2.5 | Culvert | |
| IntsTrib | 2 | .3 | .5 |
| IntsTrib | 1 | .1 | .3 |
| JonesFalls3 | 10 | .1 | .3 |
| JonesFalls3 | 9 | .1 | .3 |
| JonesFalls3 | 8 | .1 | .3 |
| JonesFalls3 | 7 | .1 | .3 |
| JonesFalls3 | 6 | .1 | .3 |
| JonesFalls3 | 5 | .3 | .5 |
| JonesFalls3 | 4.5 | Culvert | |
| JonesFalls3 | 4 | .3 | .5 |
| JonesFalls3 | 3.5 | .1 | .3 |
| JonesFalls3 | 3 | .1 | .3 |
| JonesFalls4 | 2 | .1 | .3 |
| JonesFalls4 | 1 | .1 | .3 |

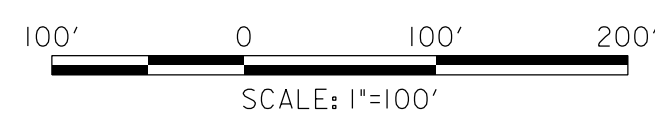


MATCHLINE (SEE EX FP-2)

LEGEND

- REACH LENGTHS —
- EXISTING HEC-RAS CROSS SECTIONS —
- EXISTING FLOODPLAIN
- INEFFECTIVE FLOW AREA

PLAN
SCALE: 1"=100'



ECCLESTON MITIGATION BANK

REVISIONS

FLOODPLAIN MAP – EXISTING CONDITIONS

| | | |
|----------------------------|-------------------------|--------------------------|
| SCALE AS SHOWN | DATE OCTOBER, 2018 | PROJECT NO. 17-10977-001 |
| DESIGNED BY PVC | COUNTY BALTIMORE COUNTY | |
| DRAWN BY PVC | LOGMILE | |
| CHECKED BY MRG | HORIZONTAL SCALE N/A | |
| F.A.P. NO. SEE TITLE SHEET | VERTICAL SCALE N/A | |

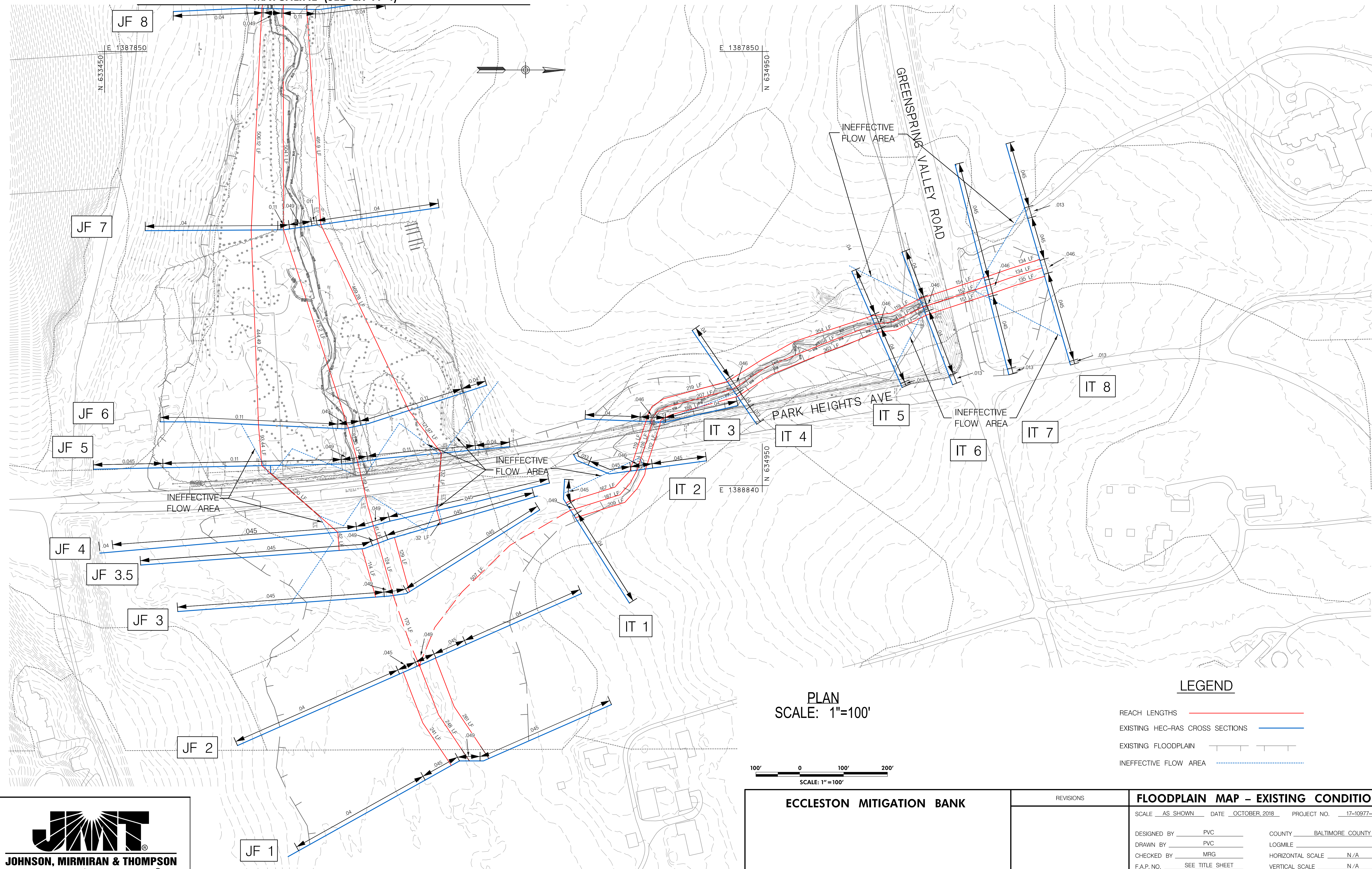
| | |
|---|--------------------|
| DRAWING NO. EX. FP - 1 OF 2 | SHEET NO. xx OF xx |
|---|--------------------|

BY: PCrawford

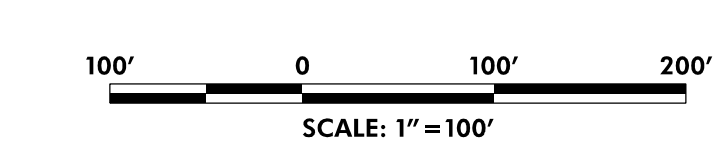


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Monday, November 05, 2018 12:27 PM

MATCHLINE (SEE EX FP-1)



PLAN
SCALE: 1"=100'



LEGEND

- REACH LENGTHS —
- EXISTING HEC-RAS CROSS SECTIONS —
- EXISTING FLOODPLAIN
- INEFFECTIVE FLOW AREA

ECCLESTON MITIGATION BANK

REVISIONS

FLOODPLAIN MAP - EXISTING CONDITIONS

| | | | | | |
|-------------|-----------------|------------------|------------------|-------------|--------------|
| SCALE | AS SHOWN | DATE | OCTOBER, 2018 | PROJECT NO. | 17-10977-001 |
| DESIGNED BY | PVC | COUNTY | BALTIMORE COUNTY | | |
| DRAWN BY | PVC | LOGMILE | | | |
| CHECKED BY | MRG | HORIZONTAL SCALE | N/A | | |
| F.A.P. NO. | SEE TITLE SHEET | VERTICAL SCALE | N/A | | |

| | | | | | | | |
|-------------|-------------------|----|----------|-----------|----|----|----|
| DRAWING NO. | EX. FP - 2 | OF | 2 | SHEET NO. | xx | OF | xx |
|-------------|-------------------|----|----------|-----------|----|----|----|



BY: PCrawford

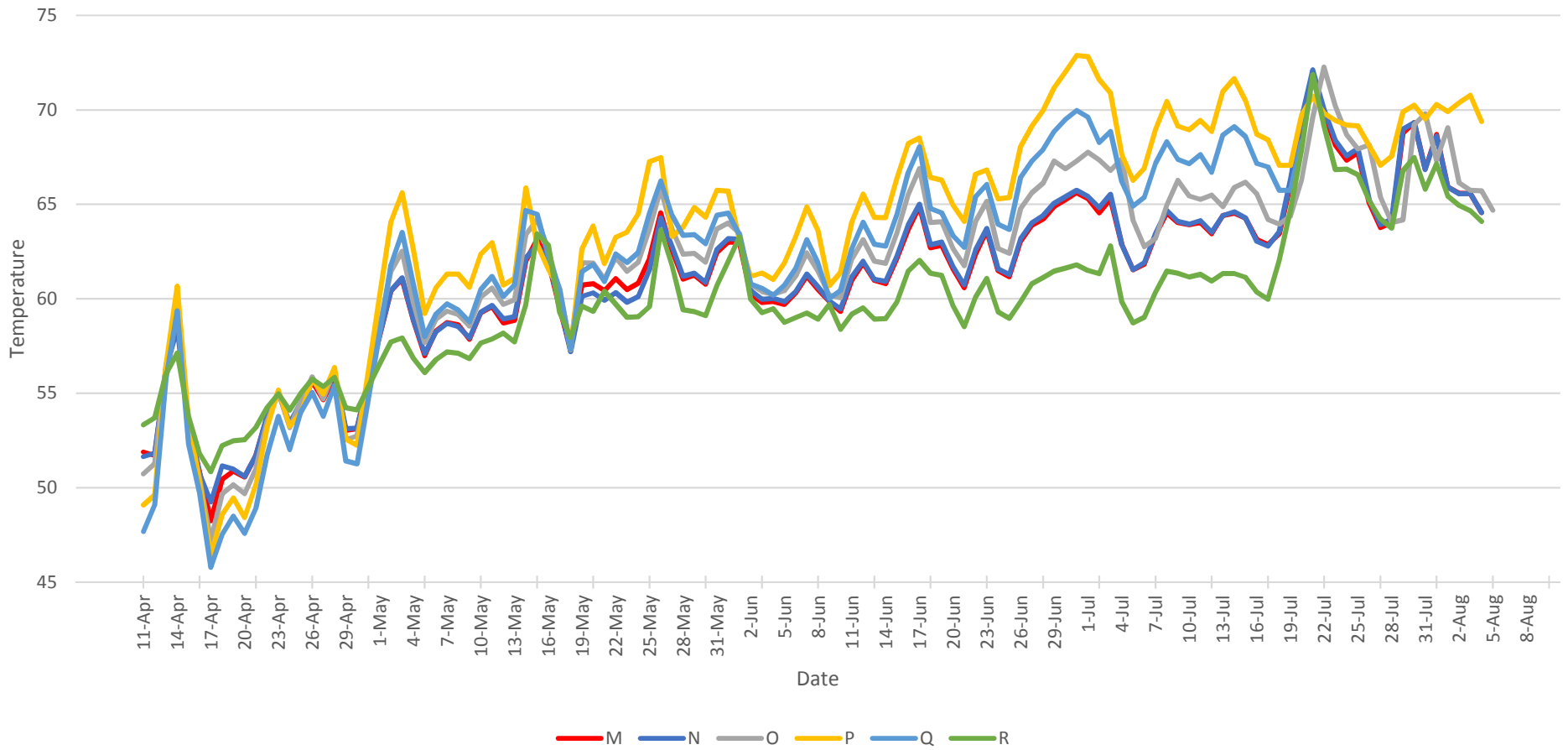
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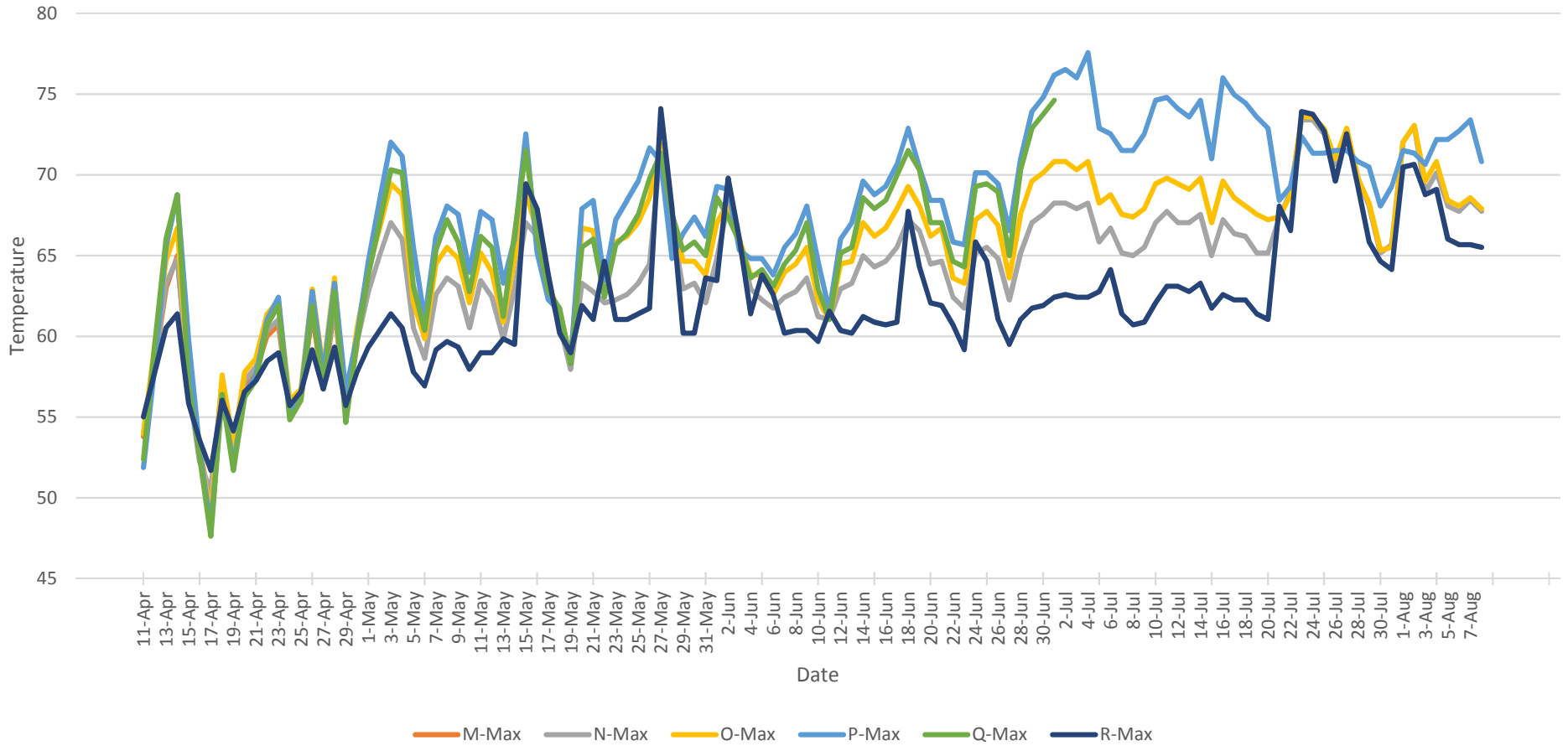
APPENDIX I

Temperature Gauge Locations Map and Data

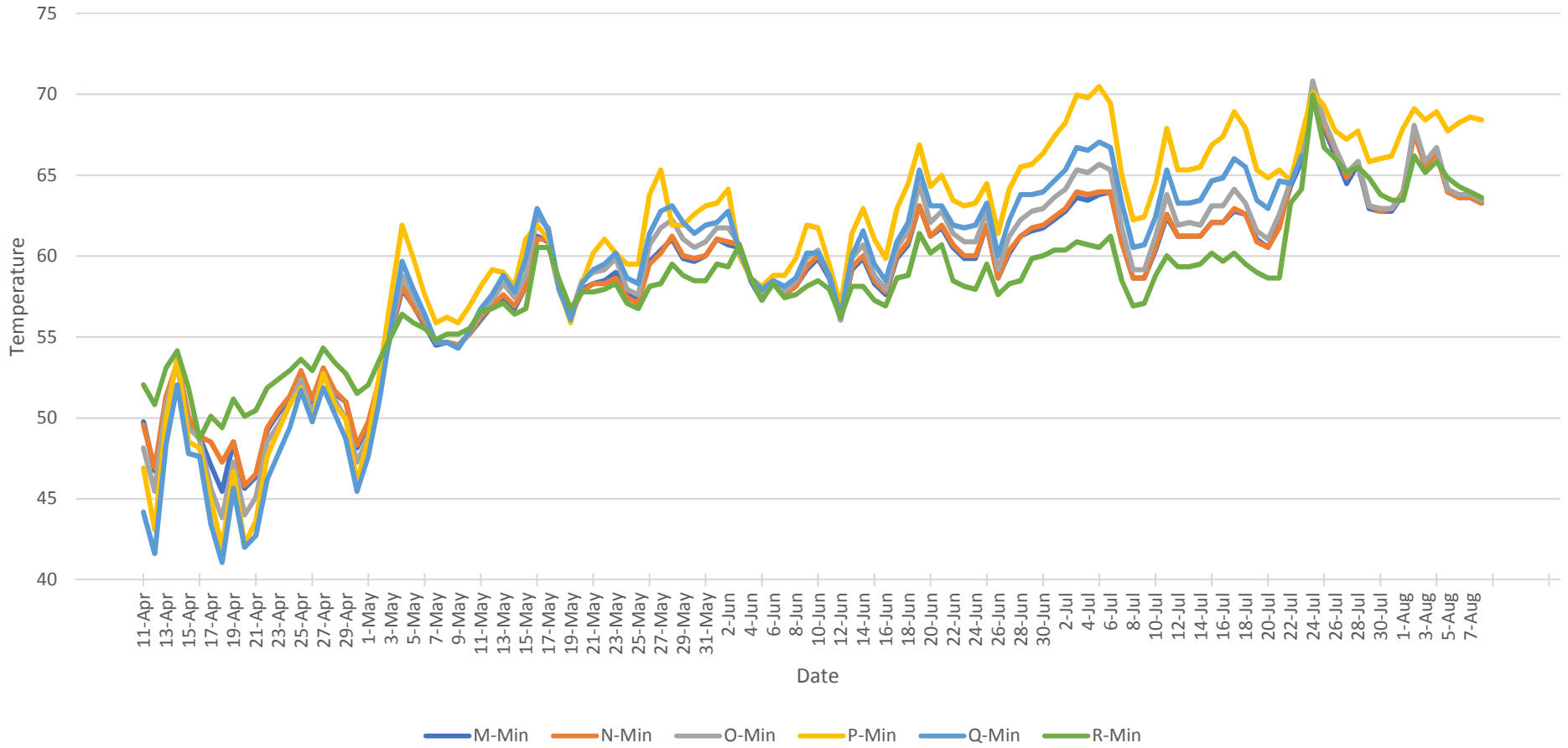
Eccleston - Jones Falls Daily-Average Temperature Data



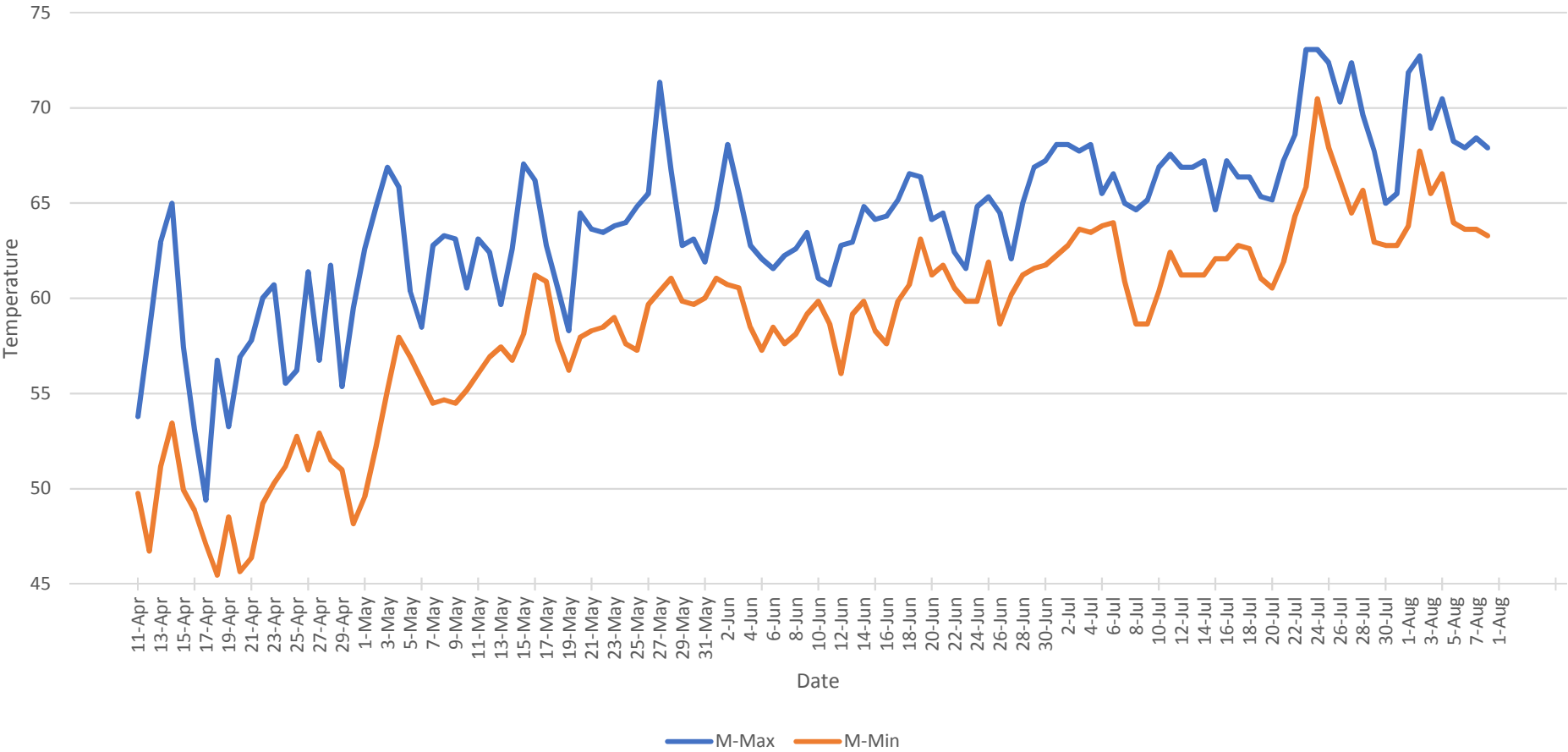
Eccleston - Jones Falls Daily-Max Temperature Data



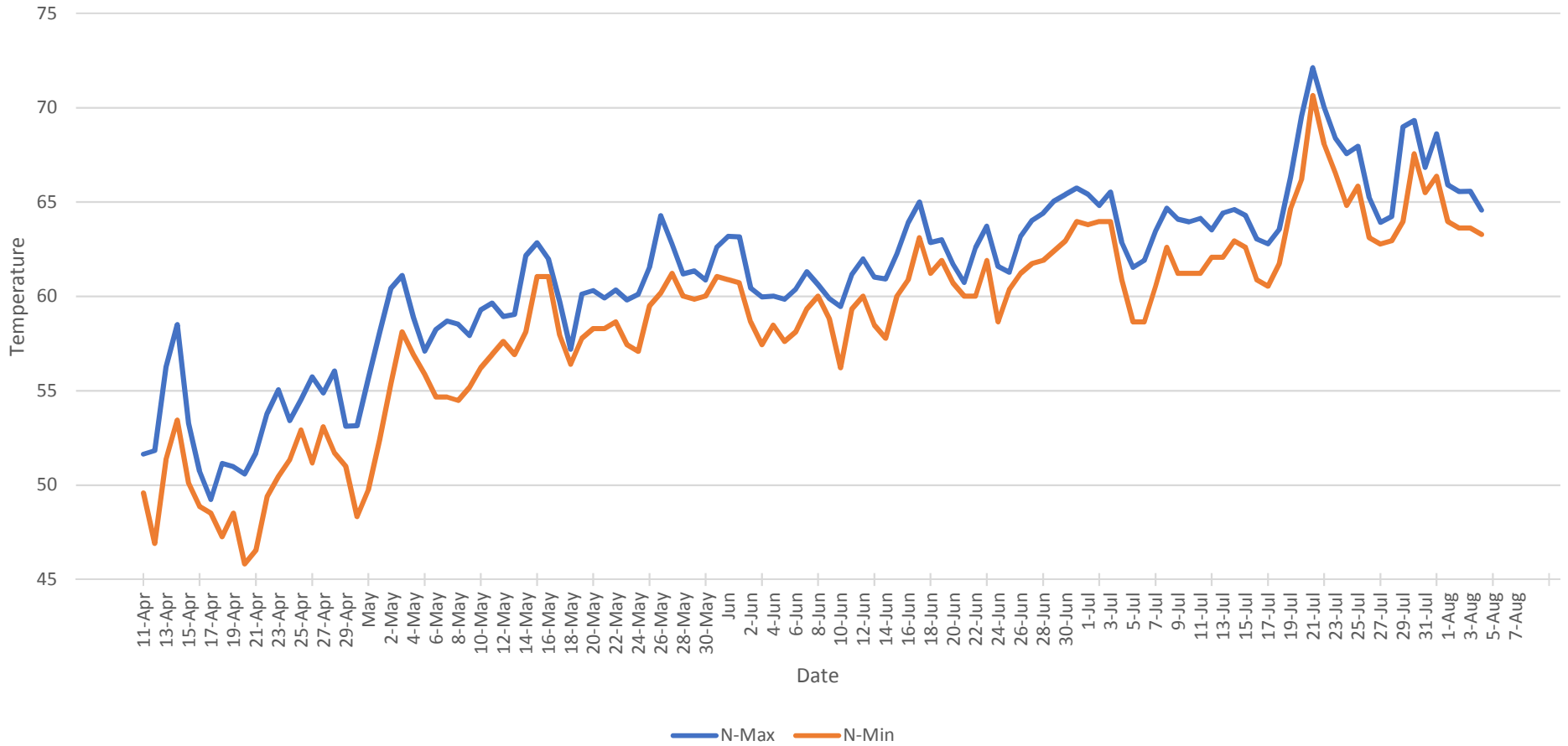
Eccleston - Jones Falls Daily-Min Temperature Data



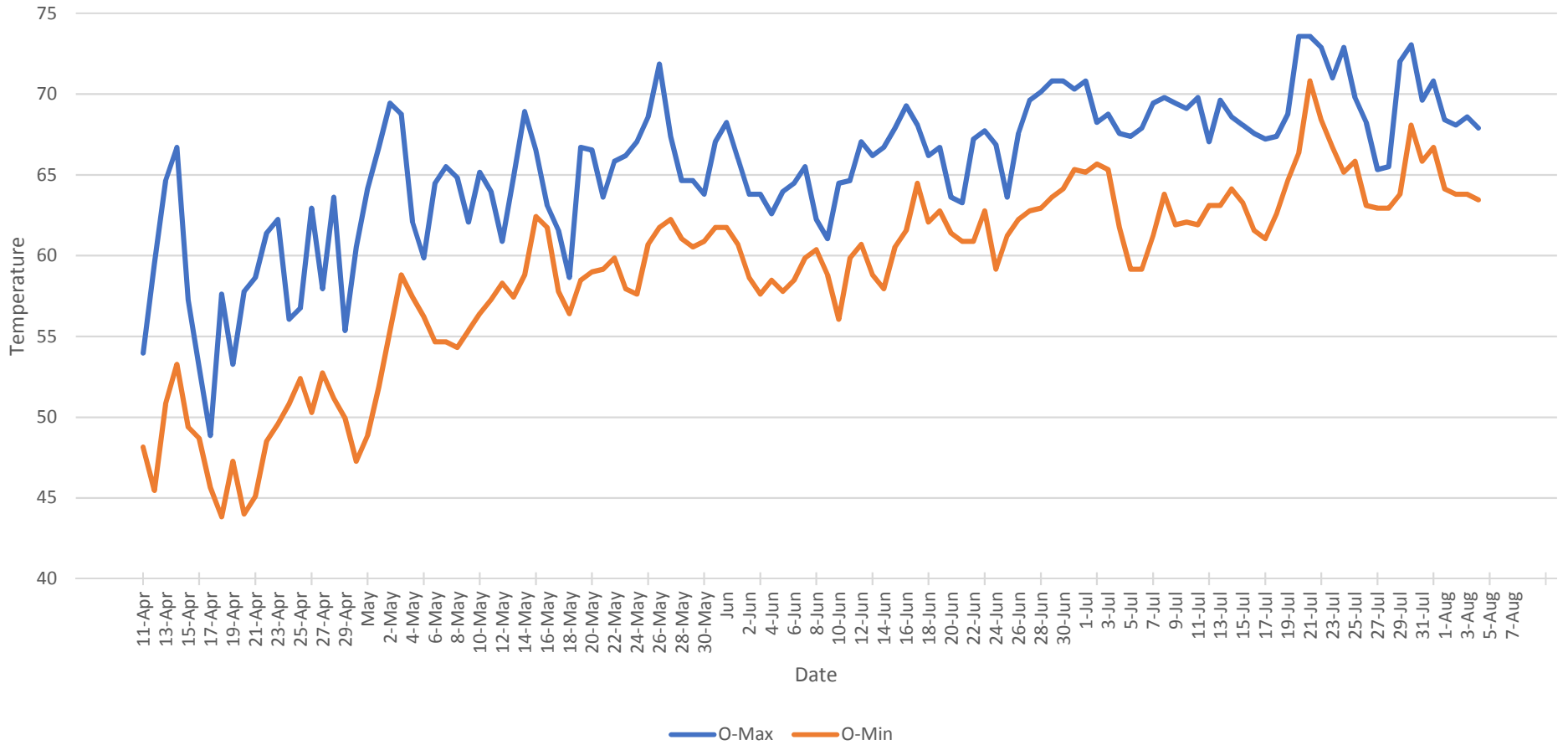
Eccleston - Jones Falls Daily Min-Max Temperature Data (M)



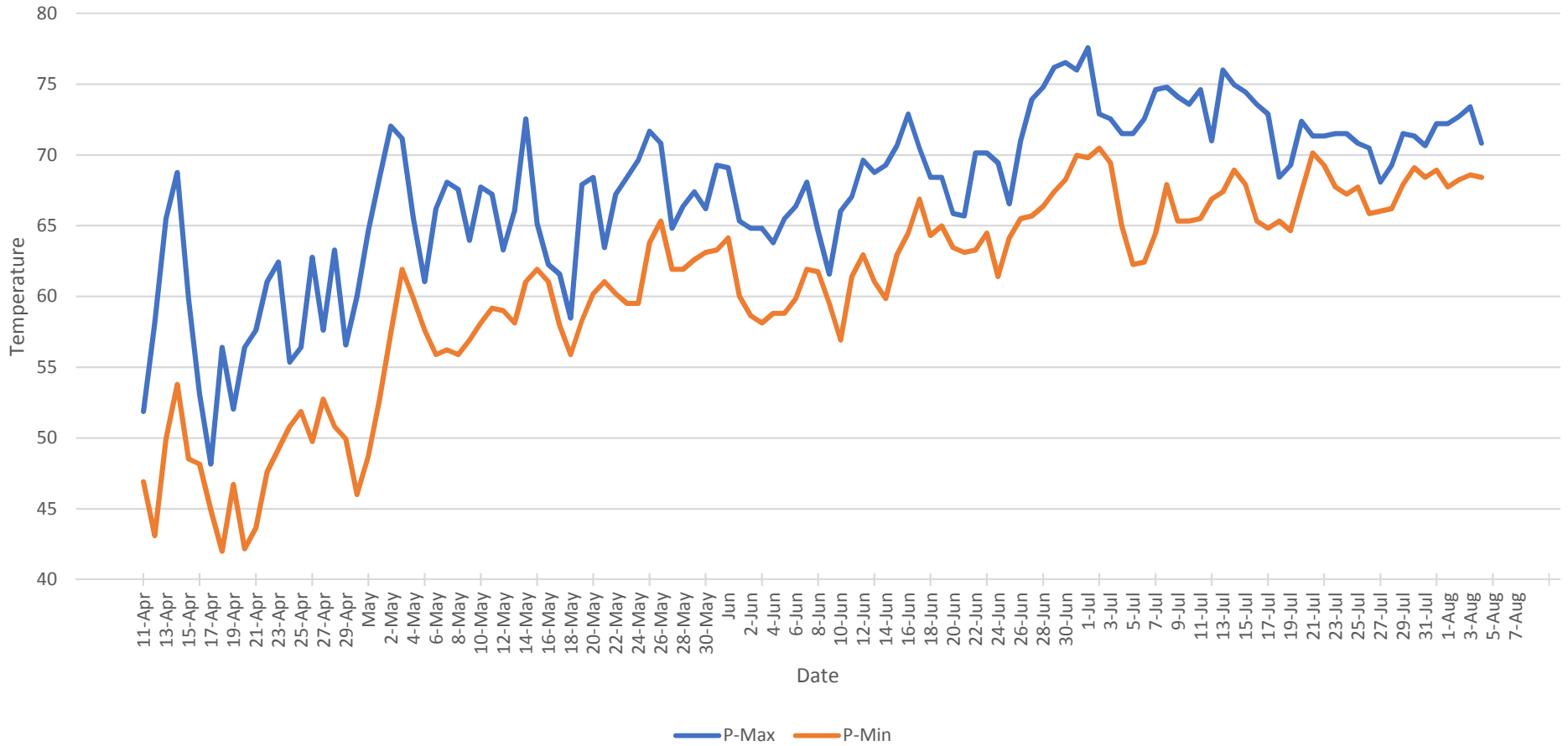
Eccleston - Jones Falls Daily Min-Max Temperature Data (N)



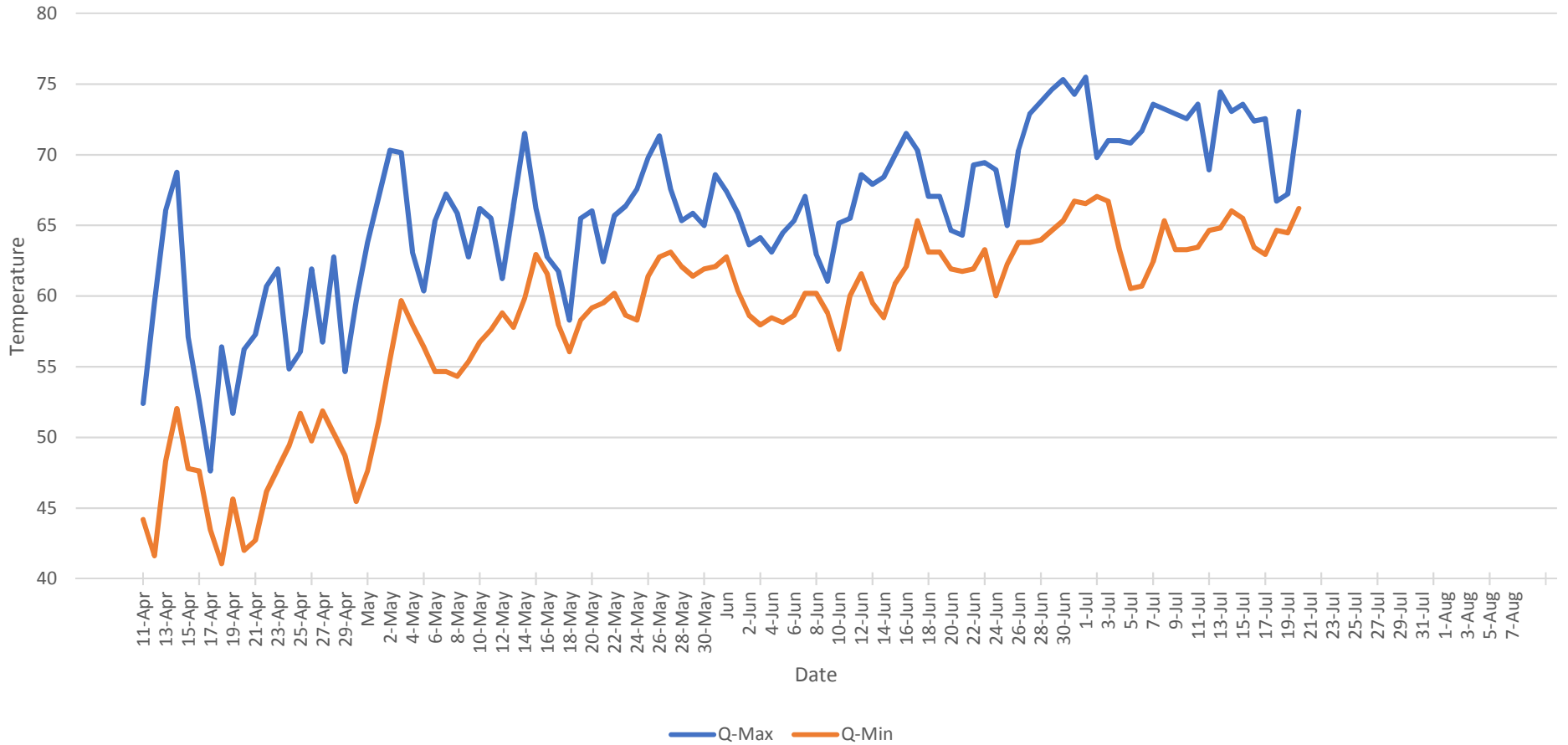
Eccleston - Jones Falls Daily Min-Max Temperature Data (O)



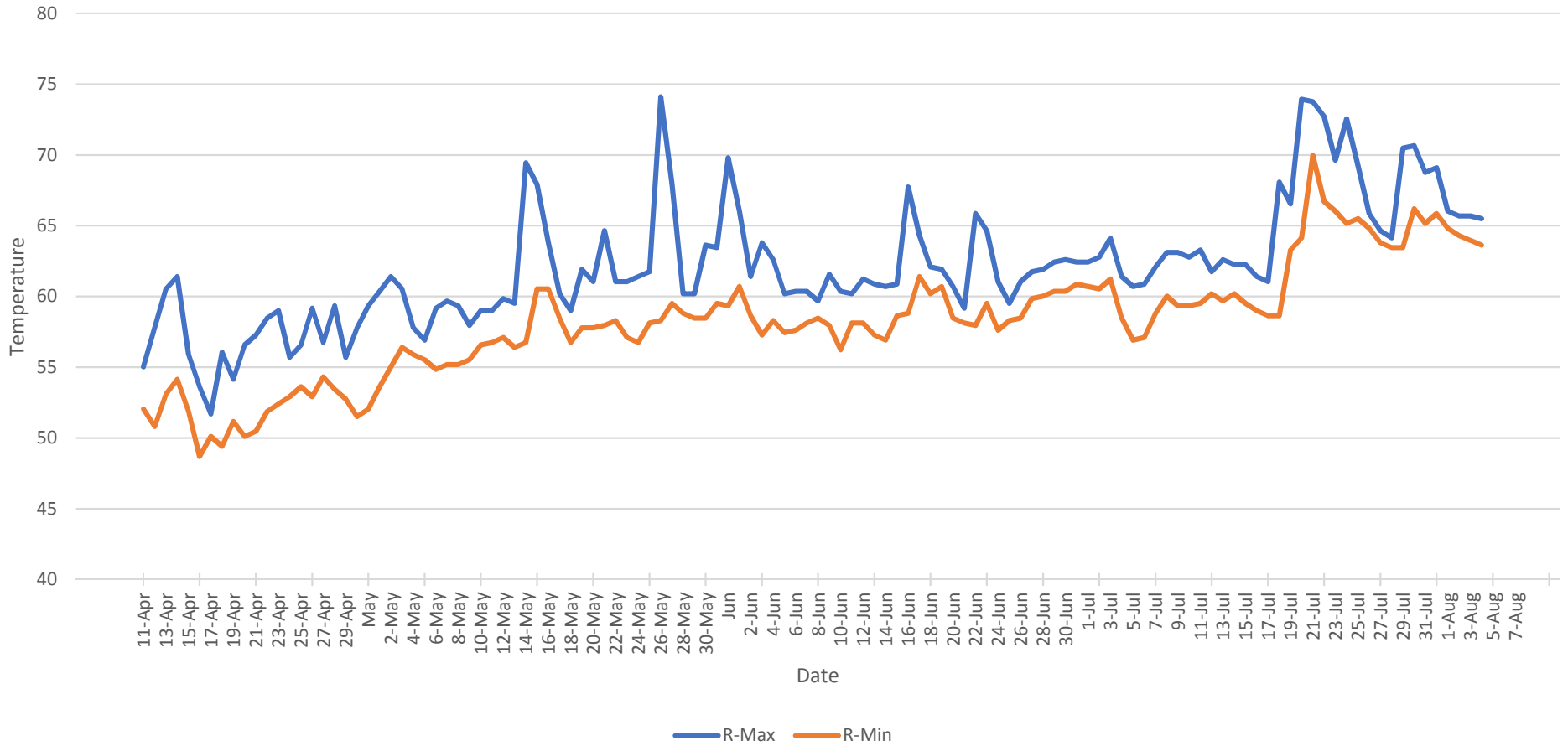
Eccleston - Jones Falls Daily Min-Max Temperature Data (P)



Eccleston - Jones Falls Daily Min-Max Temperature Data (Q)



Eccleston - Jones Falls Daily Min-Max Temperature Data (R)



Eccleston Temperature Gauge Locations





APPENDIX J
Preliminary Design Plans
(under separate cover)